

### Ultra Low-Power Single/Dual-Supply Comparators with Reference

### **FEATURES**

- ♦ Alternate source for MAX931-MAX934
- ◆ Ultra-Low Quiescent Current Over Temperature TSM931 Single+Reference: 4µA (max) TSM932/TSM933 Dual+Reference: 6µA (max) TSM934 Quad+Reference: 8.5µA (max)
- ♦ Single or Dual Power Supplies: Single: +2.5V to +11V Dual: ±1.25V to ±5.5V
- Input Voltage Range Includes Negative Supply
- ♦ 12µs Propagation Delay at 10mV Overdrive
- Push-pull TTL/CMOS-Compatible Outputs
- ♦ Crowbar-Current-Free Switching
- Continuous Source Current Capability: 40mA
- Internal 1.182V ±2% Reference: TSM931/TSM932/TSM933
- ♦ Adjustable Hysteresis: TSM931/TSM932/TSM933

## **APPLICATIONS**

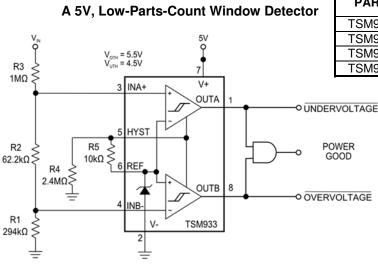
Threshold Detectors Window Comparator Level Translators Oscillator Circuits Battery-Powered Systems

### DESCRIPTION

The TSM931–TSM934 family of single/dual/quad, low-voltage, micropower analog comparators is electrically and form-factor identical to the MAX931-MAX934 family of analog comparators. Ideal for 3V or 5V single-supply applications, the TSM931–TSM934 family can operate from single +2.5V to +11V supplies or from  $\pm 1.25V$  to  $\pm 5.5V$  dual supplies. The single TSM931 draws less than 4µA (max) supply current over temperature. The dual TSM932/933 and the quad TSM934 each draw less than 3µA per comparator over temperature.

All comparators in this family exhibit an input voltage range from the negative supply rail to within 1.3V of the positive supply. In addition, the comparators' push-pull output stages are TTL/CMOS compatible and capable of sinking and sourcing current. The TSM931/TSM932/TSM933 each incorporates an internal 1.182V ±2% voltage reference. Without complicated feedback configurations and only requiring two additional resistors, adding external hysteresis via a separate pin is available on the TSM931, the TSM932, and the TSM933.

# TYPICAL APPLICATION CIRCUIT



PART	INTERNAL REFERENCE	COMPARATORS PER PACKAGE	
TSM931	Yes	1	Yes
TSM932	Yes	2	Yes
TSM933	Yes	2	Yes
TSM934	Yes	4	No

PART	TEMPERATURE RANGE	PACKAGE
TSM931C	0ºC to 70ºC	8-Pin MSOP/SOIC
TSM931E	-40ºC to 85ºC	0-PIII MISOP/SOIC
TSM932C	0ºC to 70ºC	8-Pin MSOP/SOIC
TSM932E	-40ºC to 85ºC	0-FIII WISOF/SOIC
TSM933C	0ºC to 70ºC	8-Pin MSOP/SOIC
TSM933E	-40ºC to 85ºC	
TSM934C	0ºC to 70ºC	16-Pin SOIC
TSM934E	-40ºC to 85ºC	10-FIII 3010



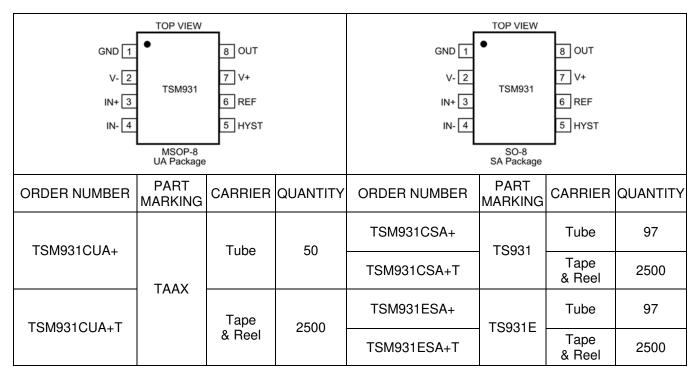
### **ABSOLUTE MAXIMUM RATINGS**

Supply Voltage (V+ to V-, V+ to GND, GND to V-).....-0.3V, +12V

$\begin{array}{l} \mbox{Continuous Power Dissipation} (T_A = +70^\circ C) \\ \mbox{8-Pin MSOP} (derate 4.1mW/^\circ C \mbox{ above } +70^\circ C) \\ \mbox{8-Pin SOIC} (derate 5.88mW/^\circ C \mbox{ above } +70^\circ C) \end{array}$	471mW
16-Pin SOIC (8.7mW/°C above +70°C)	696mW
Operating Temperature Range	
TSM93xC	0°C to +70°C
TSM93xE	40°C to +85°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Electrical and thermal stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to any absolute maximum rating conditions for extended periods may affect device reliability and lifetime.

## **PACKAGE/ORDERING INFORMATION**



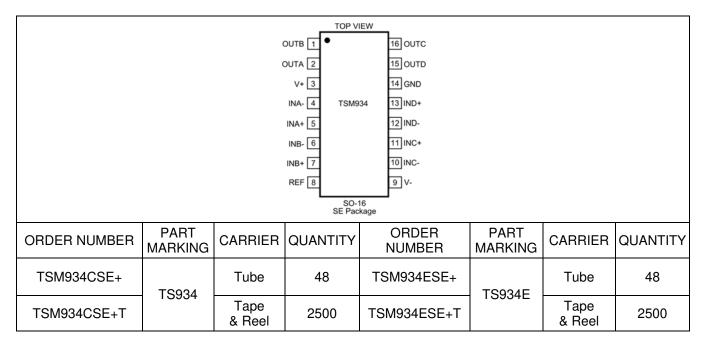


## **PACKAGE/ORDERING INFORMATION**

	TOP VIEW	_		TOP VIEW				
OUTA 1	<b>_</b> ]●	8 OUTB		OUTA 1	•	8 OUTB		
V- 2	тѕм932	7 V+		V- 2		7 V+		
INA+ 3		6 REF		TSM932 INA+ 3		6 REF		
INB+ 4		5 HYST		INB+ 4		5 HYST		
	MSOP-8 UA Package	] ;		SO-8 SA Package				
ORDER NUMBER	PART MARKING	CARRIER	QUANTITY	ORDER NUMBER	PART MARKING	CARRIER	QUANTITY	
TSM932CUA+		Tube	50	TSM932CSA+	TS932	Tube	97	
1000020044	TABD	Tube	50	TSM932CSA+T	10002	Tape & Reel	2500	
TSM932CUA+T	TABD	Таре	TSM932ESA+ 2500 TSM932ESA+T	TS932E	Tube	97		
1311932004+1		& Reel		TSM932ESA+T	- 13932E	Tape & Reel	2500	
	TOP VIEW	_		TOP VIEW				
OUTA 1	<b> </b> •	8 OUTB		OUTA 1	•	8 OUTB		
V- 2		7 V+		V- 2		7 V+		
INA+ 3	TSM933	6 REF		INA+ 3	TSM933	6 REF		
INB- 4		5 HYST		INB- 4		5 HYST		
	MSOP-8 UA Package	<b>]</b>			SO-8 SA Package			
ORDER NUMBER	PART MARKING	CARRIER	QUANTITY	ORDER NUMBER	PART MARKING	CARRIER	QUANTITY	
TSM933CUA+		Tube	50	TSM933CSA+	TS933	Tube	97	
	TABB	1000		TSM933CSA+T	10000	Tape & Reel	2500	
TSM933CUA+T	1,100	Tape	2500	TSM933ESA+	- TS933E	Tube	97	
		& Reel	2000	TSM933ESA+T		Tape & Reel	2500	



## PACKAGE/ORDERING INFORMATION



Lead-free Program: Silicon Labs supplies only lead-free packaging.

Consult Silicon Labs for products specified with wider operating temperature ranges.



### **ELECTRICAL CHARACTERISTICS – 5V OPERATION**

 $V_{+} = 5V$ ,  $V_{-} = GND = 0V$ ;  $T_{A} = -40^{\circ}C$  to  $+85^{\circ}C$ , unless otherwise noted. Typical values are at  $T_{A} = +25^{\circ}C$ . See Note 1.

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS		
POWER REQUIREMENTS								
Supply Voltage Range	See Note 2	See Note 2			2.5		11	V
		TSM	931;	$T_A = +25^{\circ}C$		2.5	3.2	
		HYS	T = REF	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			4	
		TSM	932	$T_A = +25^{\circ}C$		3.1	4.5	
Supply Current	IN+ = IN- + 100mV	HYS	T = REF	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			6	μA
Supply Current	110+=110-+1001110	TSM	933	$T_A = +25^{\circ}C$		3.1	4.5	μΑ
		HYS	T = REF	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			6	
		TSM	004	$T_A = +25^{\circ}C$		5.5	6.5	
		1 21/1	934	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			8.5	
COMPARATOR								
Input Offset Voltage	$V_{CM} = 2.5V$						±10	mV
Input Leakage Current (IN-, IN+)	IN+ = IN- = 2.5V		$T_{A} = -40$	°C to +85°C		±0.01	±5	nA
Input Leakage Current (HYST)	TSM931, TSM932, T	SM933	}			±0.02		nA
Input Common-Mode Voltage Range					V-		V+-1.3V	V
Common-Mode Rejection Ratio	V- to (V+ - 1.3V)					0.1	1	mV/V
Power-Supply Rejection Ratio	V+ = 2.5V to 11V					0.1	1	mV/V
Voltage Noise	100Hz to 100kHz	100Hz to 100kHz				20		$\mu V_{RMS}$
Hysteresis Input Voltage Range	TSM931, TSM932, T	SM933	}		REF- 0.05V		REF	V
Response Time	$T_A = +25^{\circ}C; 100pF load$		Overdrive = 10mV			12		110
nesponse mine			Overdrive = 100mV			4		μs
Output High Voltage	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$ :	I <sub>OUT</sub> =	17mA		V+-0.4			V
Output Low Voltage	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$ :	TSM	932, TSN	1933			V- + 0.4	V
Output Low Voltage	I <sub>OUT</sub> = 1.8mA	I <sub>OUT</sub> = 1.8mA TSM931, TSM934					GND + 0.4	V
REFERENCE								
Reference Voltage	$T_A = 0^{\circ}C$ to $+70^{\circ}C$				1.158	1.182	1.206	V
neierence vollage	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$				1.147		1.217	V
Source Current			$T_A = +$	25°C	15	25		μA
Source Current			$T_{A} = -4$	40°C to +85°C	6			μΑ
Sink Current			$T_A = +$		8	15		
			$T_{A} = -4$	40°C to +85°C	4			μA
Voltage Noise	100Hz to 100kHz					100		$\mu V_{RMS}$



### **ELECTRICAL CHARACTERISTICS – 3V OPERATION**

 $V_{+} = 3V$ ,  $V_{-} = GND = 0V$ ;  $T_{A} = -40^{\circ}C$  to  $+85^{\circ}C$ , unless otherwise noted. Typical values are at  $T_{A} = +25^{\circ}C$ . See Note 1.

PARAMETER	CONDITIONS			MIN	TYP	MAX	UNITS	
POWER REQUIREMENTS								
	IN+ = IN- + 100mV	TSMS	931;	$T_A = +25^{\circ}C$		2.4	3	
		HYST	Γ = REF	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			3.8	
		TSMS		T <sub>A</sub> = +25°C		3.4	4.3	
Supply Current		HYST	Γ = REF	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			5.8	μA
Supply Cultern	110+=110++1001110	TSMS		T <sub>A</sub> = +25°C		3.4	4.3	μΑ
		HYST	Γ = REF	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			5.8	
		TSMS	224	T <sub>A</sub> = +25°C		5.2	6.2	
		T SIVIS	934	$T_A = -40^{\circ}C$ to $+85^{\circ}C$			8	
COMPARATOR								-
Input Offset Voltage	$V_{CM} = 1.5V$						±10	mV
Input Leakage Current (IN-, IN+)	IN+ = IN- = 1.5V		1.	°C to +85°C		±0.01	±1	nA
Input Leakage Current (HYST)	TSM931, TSM932, T	SM933			V-	±0.02		nA
Input Common-Mode Voltage Range							V+-1.3V	V
Common-Mode Rejection Ratio	V- to (V+ - 1.3V)					0.2	1	mV/V
Power-Supply Rejection Ratio	V+ = 2.5V to 11V	V+ = 2.5V to 11V				0.1	1	mV/V
Voltage Noise	100Hz to 100kHz					20		$\mu V_{RMS}$
Hysteresis Input Voltage Range	TSM931, TSM932, T	SM933			REF- 0.05V		REF	V
Response Time	T <sub>A</sub> = +25°C; 100pF lc	ad	Overdrive = 10mV			14		μs
Response nine			Overdrive = 100mV			5		•
Output High Voltage	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$ :	I <sub>OUT</sub> = 1	10mA		V+-0.4			V
Output Low Voltage	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$ :						V- + 0.4	V
Oulput Low Voltage	$I_{OUT} = 0.8 \text{mA}$	TSMS	931, TSN	1934			GND + 0.4	V
REFERENCE								
Reference Voltage	$T_A = 0^{\circ}C$ to $+70^{\circ}C$				1.158	1.182	1.206	V
noioronoe voltage	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$				1.147		1.217	
Source Current			$T_A = +25^{\circ}C$		15	25		μA
			$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$		6			μΑ
Sink Current			$T_A = +$		8	15		μA
	$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$				4			
Voltage Noise	100Hz to 100kHz					100		$\mu V_{RMS}$

Note 1: All specifications are 100% tested at T<sub>A</sub> = +25°C. Specification limits over temperature (T<sub>A</sub> = T<sub>MIN</sub> to T<sub>MAX</sub>) are guaranteed by device characterization, not production tested.

Note 2: The TSM934 comparator operates below 2.5V. Refer to the "Low-Voltage Operation: V+ = 1.5V (TSM934 Only)" section.



Output Voltage Low vs Load Current

V + = 3V

8 12

V+ = 3V or 5V

V + = 5V

16

LOAD CURRENT - mA

**Reference Output Voltage vs** 

**Output Load Current** 

20

24 28

SINK

SOURCE

20

25

30

2.5

2

1.5

1

0.5

0

1.190

1.185

1.180
1.180
1.175
1.175
1.170
1.165
1.165
1.160

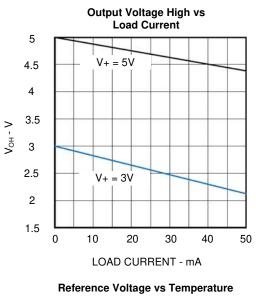
1.155

0

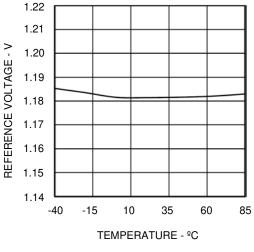
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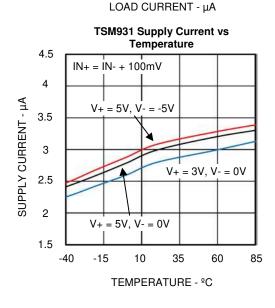
0 4

V - V



**TSM931-TSM934** 

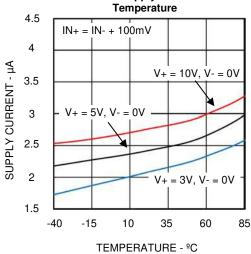




10

15

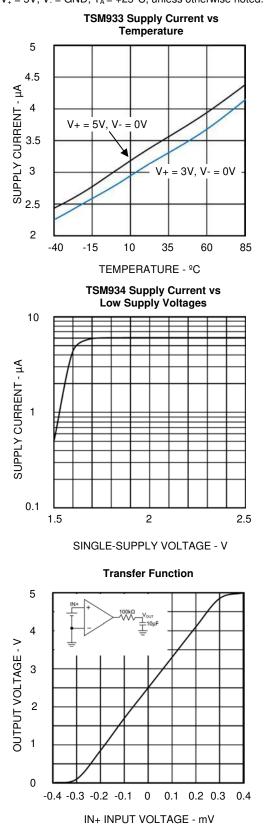
TSM932 Supply Current vs

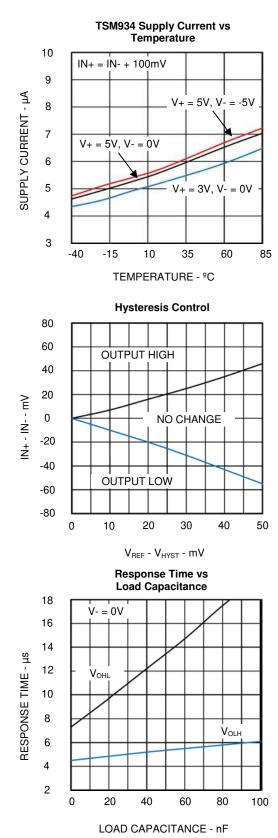




### **TYPICAL PERFORMANCE CHARACTERISTICS**

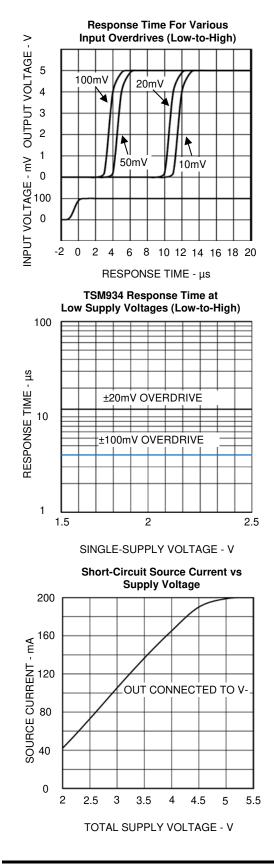
 $V_{*}$  = 5V;  $V_{\cdot}$  = GND;  $T_{A}$  = +25°C, unless otherwise noted.

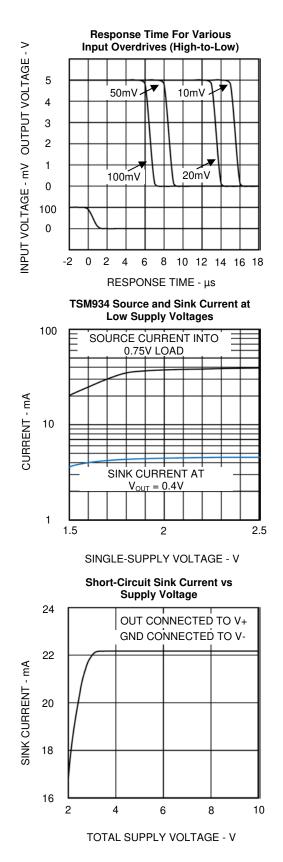






 $V_{+} = 5V$ ;  $V_{-} = GND$ ;  $T_{A} = +25^{\circ}C$ , unless otherwise noted.







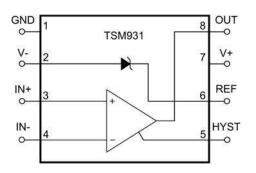
## **PIN FUNCTIONS**

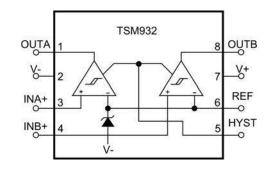
	PIN				NAME	FUNCTION
TSM931	TSM932	TSM933	NAME	FUNCTION		
1	_		GND	Ground. Connect to V- for single-supply operation. Output swings from V+ to GND.		
—	1	1	OUTA	Comparator A Output. Sinks and sources current. Swings from V+ to V		
2	2	2	V-	Negative Supply. Connect to ground for single-supply operation.		
3	_		IN+	Comparator Noninverting Input		
	3	3	INA+	Comparator A Noninverting Input		
4			IN-	Comparator Inverting Input		
—	4	_	INB+	Comparator B Noninverting Input		
—	—	4	INB-	Comparator B Inverting Input		
5	5	5	HYST	Hysteresis Input. Connect to REF if not used. Input voltage range is from $V_{REF}$ to ( $V_{REF}$ - 50mV).		
6	6	6	REF	1.182V Reference Output with respect to V		
7	7	7	V+	Positive Supply Voltage		
8	_		OUT Comparator Output. Sinks and sources current. Swings fr to GND.			
_	8	8	OUTB Comparator B Output. Sinks and sources current. Swings V+ to V			

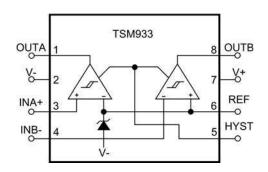
PIN	NAME	FUNCTION		
<b>TSM934</b>		FUNCTION		
1	OUTB	Comparator B Output. Sinks and sources current. Swings from V+ to GND.		
2	OUTA	OUTA Comparator A Output. Sinks and sources current. Swings from V+ to GND.		
3	V+	Positive Supply Voltage		
4	INA-	Comparator A Inverting Input		
5	INA+	Comparator A Noninverting Input		
6	INB-	Comparator B Inverting Input		
7	INB+	Comparator B Noninverting Input		
8	REF	1.182V Reference Output with respect to V		
9	V-	Negative Supply Voltage. Connect to ground for single- supply operation.		
10	INC-	Comparator C Inverting Input		
11	INC+	Comparator C Noninverting Input		
12	IND-	Comparator D Inverting Input		
13	IND+	Comparator D Noninverting Input		
14	GND	Ground. Connect to V- for single-supply operation.		
15	OUTD	Comparator D Output, Sinks and sources current, Swings		
16	OUTC	Comparator C Output. Sinks and sources current. Swings JTC from V+ to GND.		

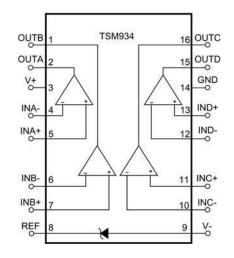


## **BLOCK DIAGRAMS**











### THEORY OF OPERATION

The TSM931-TSM934 family of single/dual/quad, low-voltage. micropower analog comparators provide excellent flexibility and performance while sourcing continuously up to 40mA of current. The TSM931-TSM934 provide an on-board 1.182V ±2% reference voltage. To minimize glitches that can occur with parasitic feedback or a less than optimal board layout, the design of the TSM931-TSM934 output stage is optimized to eliminate crowbar glitches as the output switches. To minimize current consumption while providing flexibility, the TSM931-TSM933 have an on-board HYST pin in order to add additional hysteresis.

#### Power-Supply and Input Signal Ranges

The TSM931-TSM934 can operate from a single supply voltage range of +2.5V to +11V, provide a wide common mode input voltage range of V- to V+-1.3V, and accept input signals ranging from V- to V+ - 1V. The inputs can accept an input as much as 300mV above the below the power supply rails without damage to the part. While the TSM931 and the TSM934 are able to operate from a single supply voltage range, a GND pin is available that allows for a dual supply operation with a range of ±1.25V to ±5.5V. If a single supply operation is desired, the GND pin needs to be tied to V-. In a dual supply mode, the TSM931 and the TSM934 are compatible with TTL/CMOS with a ±5V voltage and the TSM932 and the TSM933 are compatible with TTL with a single +5V supply.

### Low-Voltage Operation: V+ = 1.5V (TSM934 Only)

Due to a decrease in propagation delay and a reduction in output drive, the TSM931-TSM933 cannot be used with a supply voltage much lower than 2.5V. However, the TSM934 can operate down to a supply voltage of 2V; however, as the supply voltage reduces, the TSM934 supply current drops and the performance is degraded. When the supply voltage drops to 2.2V, the reference voltage will no longer function; however, the comparators will function down to a 1.5V supply voltage. Furthermore, the input voltage range is extended to just below 1V the positive supply rail. For applications with a sub-2.5V power supply, it is

recommended to evaluate the circuit over the entire power supply range and temperature.

#### Comparator Output

The TSM931 and the TSM934 have a GND pin that allows the output to swing from V+ to GND while the V- pin can be set to a voltage below GND as long as the voltage difference between V+ and V- is within 11V. Having a different voltage on V- will not affect the output swing. For TTL applications, V+ can be set to +5V±10% and V- can be set anywhere between 0V and -5V±10%. On the other hand, the TSM932 and the TSM933 do not have a GND pin; hence, for TTL applications, V+ needs to be set to a +5V power supply and V- to 0V. Furthermore, the output design of the TSM931-TSM934 can source and sink more than 40mA and 5mA, respectively, while simultaneously maintaining a quiescent current in the microampere range. If the power dissipation of the package is maintained within the max limit, the output can source pulses of 100mA of current with V+ set to +5V. In an effort to minimize external component count needed to address power supply feedback, the TSM931-TSM934 output does not produce crowbar switching current as the output switches. With a 100mV input overdrive, the propagation delay of the TSM931-TSM934 is 4µs.

### Voltage Reference

The TSM931-TSM934 have an on-board 1.182V reference voltage with an accuracy of  $\pm 2\%$  across a temperature range of 0°C to +70°C. The REF pin is able to source and sink 15µA and 8µA of current, respectively. The REF pin is referenced to V- and it should not be bypassed.

#### Noise Considerations

Noise can play a role in the overall performance of the TSM931-TSM934. Despite having a large gain, if the input voltage is near or equal to the input offset voltage, the output will randomly switch HIGH and LOW. As a result, the TSM931-TSM934 produces a peak-to-peak noise of about 0.3mV<sub>PP</sub> while the reference voltage produces a peak-to-peak noise of about 1mV<sub>PP</sub>. Furthermore, it is important to design a layout that minimizes capacitive coupling from a given output to the reference pin as crosstalk can add noise and as a result, degrade performance.



### **APPLICATIONS INFORMATION**

#### **Hysteresis**

As a result of circuit noise or unintended parasitic feedback, many analog comparators often break into oscillation within their linear region of operation especially when the applied differential input voltage approaches 0V (zero volt). Externally-introduced hysteresis is a well-established technique to stabilizing analog comparator behavior and requires external components. As shown in Figure 1, adding comparator hysteresis creates two trip points: V<sub>THR</sub> (for the rising input voltage) and  $V_{THF}$  (for the falling input voltage). The hysteresis band (V<sub>HB</sub>) is defined as the voltage difference between the two trip points. When a comparator's input voltages are equal, hysteresis effectively forces one comparator input to move quickly past the other input, moving the input out of the region where oscillation occurs. Figure 1 illustrates the case in which an IN- input is a fixed voltage and an IN+ is varied. If the input signals were reversed, the figure would be the same with an inverted output.

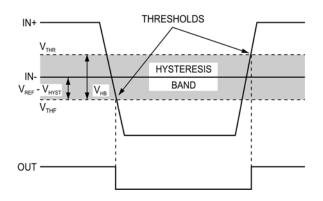


Figure 1. Threshold Hysteresis Band

#### Hysteresis (TSM931-TSM933)

Hysteresis can be generated with two external resistors using positive feedback as shown in Figure 2. Resistor R1 is connected between REF and HYST and R2 is connected between HYST and V-. This will increase the trip point for the rising input voltage,  $V_{THR}$ , and decrease the trip point for the falling input voltage,  $V_{THF}$ , by the same amount. If no hysteresis is required, connect HYST to REF. The hysteresis band,  $V_{HB}$ , is voltage across the REF and HYST pin multiplied by a factor of 2. The HYST pin

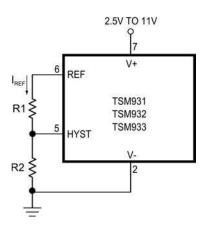


Figure 2. Programming the HYST Pin

can accept a voltage between REF and REF-50mV, where a voltage of REF-50mV generates the maximum voltage across R1 and thus, the maximum hysteresis and hysteresis band of 50mV and 100mV, respectively. To design the circuit for a desired hysteresis band, consider the equations below to acquire the values for resistors R1 and R2:

$$R1 = \frac{V_{HB}}{(2 \times I_{REF})}$$

$$R2 = \frac{1.182 - \frac{V_{HB}}{2}}{I_{REF}}$$

where I<sub>REF</sub> is the primary source of current out of the reference pin and should be maintained within the maximum current the reference can source. This is typically in the range of 0.1µA and 4µA. It is also important to ensure that the current from reference is much larger than the HYST pin input current. Given R2 = 2.4M $\Omega$ , the current sourced by the reference is 0.5µA. This allows the hysteresis band and R1 to be approximated as follows:

 $R1(k\Omega) = V_{HB}(mv)$ 

For the TSM932-TSM933, the hysteresis is the same for both comparators.

#### Hysteresis (TSM934)

Relative to adding hysteresis with the HYST pin as was done for the TSM931-TSM933, the circuit in Figure 3 uses positive feedback along with two external resistors to set the desired hysteresis. The circuit consumes more current and it slows down the hysteresis effect due to the high impedance on the



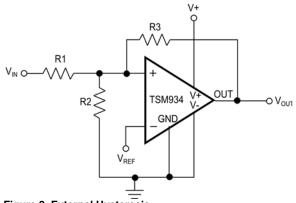


Figure 3. External Hysteresis

feedback. The following procedure explains the steps to design the circuit for a desired hysteresis:

- 1. Choosing R3. As the leakage current at the IN+ pin is less than 1nA, the current through R3 should be at least 100nA to minimize offset voltage errors caused by the input leakage current. For R3 = 11.8M $\Omega$ , the current through R3 is V<sub>REF</sub>/R3 at the trip point. In this case, a 10M $\Omega$  resistor is a good standard value for R3.
- 2. Next, the desired hysteresis band (  $V_{HB}$ ) is set. In this example,  $V_{HB}$  is set to 50mV.
- 3. Calculating R1.

$$R1 = R3 \times \frac{V_{HB}}{V_{+}}$$
$$= 10M\Omega \times \frac{50m^{1}}{5V}$$

= 100kΩ

In this example, a  $100k\Omega$ , 1% standard value resistor is selected for R1.

- 4. Choose the trip point for V<sub>IN</sub> rising (V<sub>THR</sub>), which is the threshold voltage at which the comparator switches its output from low to high as V<sub>IN</sub> rises above the trip point. In this example, choose V<sub>THR</sub> = 3V.
- 5. Calculating R2.

$$R2 = \frac{1}{\left[\left(\frac{V_{\text{THR}}}{V_{\text{REF}} \times R1}\right) - \frac{1}{R1} - \frac{1}{R3}\right]}$$
$$= \frac{1}{\left[\left(\frac{3}{1.182V \times 100k\Omega}\right) - \frac{1}{100k\Omega} - \frac{1}{10M\Omega}\right]}$$

= 65.44kΩ

In this example, a  $64.9k\Omega$ , 1% standard value resistor is selected for R2.

6. The last step is to verify the trip voltages and hysteresis band using the standard resistance values:

$$V_{THR} = V_{REF} x R1 x \left(\frac{1}{R1} + \frac{1}{R2} + \frac{1}{R3}\right)$$
$$V_{THF} = V_{THR} - \frac{(R1 \times V_{+})}{R3}$$

### **Board Layout and Bypassing**

While power-supply bypass capacitors are not typically required, it is good engineering practice to use  $0.1\mu$ F bypass capacitors close to the device's power supply pins when the power supply impedance is high, the power supply leads are long, or there is excessive noise on the power supply traces. To reduce stray capacitance, it is also good engineering practice to make signal trace lengths as short as possible. Also recommended are a ground plane and surface mount resistors and capacitors.

### **TYPICAL APPLICATION CIRCUITS**

### Auto-Off Power Source

A timed auto power-off circuit can be designed as shown in Figure 4 where the output of the TSM931 is the switched power-supply output. With an internal reference, hysteresis, high current output, and a 2.5  $\mu$ A supply current, the TSM931 provides a wealth of features that make it perfect for this application. While consuming only 3.5 $\mu$ A of quiescent current with a 10mA load, the TSM931 is able to generate a voltage of VBATT – 0.12V. As shown in the figure, three resistors are used to generate a hysteresis band of 100mV and sets the IN+ trip point to 50mV when IN+ is going low. The maximum power-on period of the OUT pin before power-down occurs



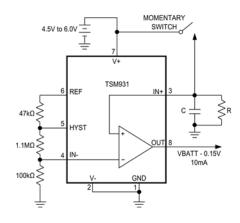


Figure 4. Auto-Off Power Switch Operates on 2.5µA quiescent current.

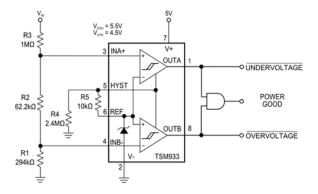
can be determined by the RC time constant as follows:

#### R x C X 4.6 s

The period value will change depending on the leakage current and the voltage applied to the circuit. For instance:  $2M\Omega \times 10\mu F \times 4.6 \text{ s} = 92 \text{ s}.$ 

#### Window Detector

The schematic shown in Figure 5 is for a 4.5V undervoltage threshold detector and a 5.5V overvoltage threshold detector using the TSM933. Resistor components R1, R2, and R3 can be



#### Figure 5. Window Detector

selected based on the threshold voltage desired while resistors R4 and R5 can be selected based on the hysteresis desired. Adding hysteresis to the circuit will minimize chattering on the output when the input voltage is close to the trip point. OUTA and OUTB generate the active low undervoltage indication and active-low overvoltage indication, respectively. If both OUTA and OUTB signals are ANDed together, the resulting output of the AND gate is an active-high, power-good signal. To design the circuit, the following procedure needs to be performed:

- As described in the section "Hysteresis (TSM931-TSM933)", determine the desired hysteresis and select resistors R4 and R5 accordingly. This circuit has ±5mV of hysteresis at the input where the input voltage V<sub>IN</sub> will appear larger due to the input resistor divider.
- 2. Selecting R1. As the leakage current at the INB- pin is less than 1nA, the current through R1 should be at least 100nA to minimize offset voltage errors caused by the input leakage current. Values within 100k $\Omega$  and 1M $\Omega$  are recommended. In this example, a 294k $\Omega$ , 1% standard value resistor is selected for R1.
- Calculating R2 + R3. As the input voltage V<sub>IN</sub> rises, the overvoltage threshold should be 5.5V. Choose R2 + R3 as follows:

R2 + R3 = R1 x 
$$\left(\frac{V_{OTH}}{V_{REF}+V_{HYS}}-1\right)$$
  
= 294k $\Omega$  x  $\left(\frac{5.5V}{1.182V+5mV}-1\right)$ 

4. Calculating R2. As the input voltage VIN falls, the undervoltage threshold should be 4.5V. Choose R2 as follows:

R2 = (R1 + R2+ R3) x 
$$\frac{(V_{REF}-V_{HYS})}{V_{UTH}}$$
- 294k

$$= (294k\Omega + 1.068M\Omega) \times \frac{(1.182V-5mV)}{4.5} - 294k$$

 $= 62.2 k\Omega$ 

In this example, a  $61.9k\Omega$ , 1% standard value resistor is selected for R2.

5. Calculating R3.

$$R3 = (R2 + R3) - R2$$



- = 1.068MΩ 61.9kΩ
- = 1.006MΩ

In this example, a  $1M\Omega$ , 1% standard value resistor is selected for R3.

6. Using the equations below, verify all resistor values selected:

$$V_{OTH} = (V_{REF} + V_{HYS}) \times \frac{(R1 + R2 + R3)}{R1}$$

$$V_{OTH} = (V_{REF} - V_{HYS}) \times \frac{(R1 + R2 + R3)}{(R1 + R2)}$$
  
= 4.484V

Where the hysteresis voltage is given by:

$$V_{HYS} = V_{REF} \times \frac{R5}{R4}$$

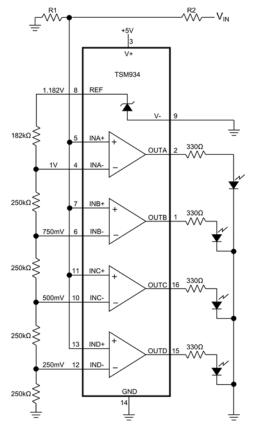


Figure 6. Bar-Graph Level Gauge

A simple four-stage level detector is shown in Figure 6 using the TSM934. Due to its high output source capability, the TSM921 is perfect for driving LEDs. When all of the LEDs are on, the threshold voltage is given as  $V_{IN} = (R1 + R2)/R1$  volts. All other threshold voltages are scaled down accordingly by  $^{34}$ ,  $^{12}$ , and  $^{14}$  the threshold voltage. The current through the LEDs is limited by the output resistors.

### Level Shifter

Figure 7 provides a simple way to shift from bipolar  $\pm 5V$  inputs to TTL signals by using the TSM934. To protect the comparator inputs,  $10k\Omega$  resistors are placed in series and do not have an effect on the performance of the circuit.

#### Two-Stage Low-Voltage Detector

A two step, input voltage monitoring circuit can be designed using the TSM932 as shown in Figure 8. In this circuit, when  $V_{IN}$  is above the LOW and FAIL thresholds, the outputs will be HIGH. The design procedure used to design the window detector can be used to design this circuit.

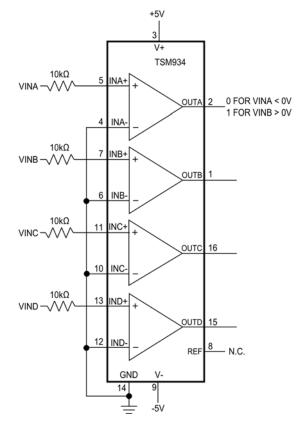


Figure 7. Level Shifter: ±5V Input into CMOS output



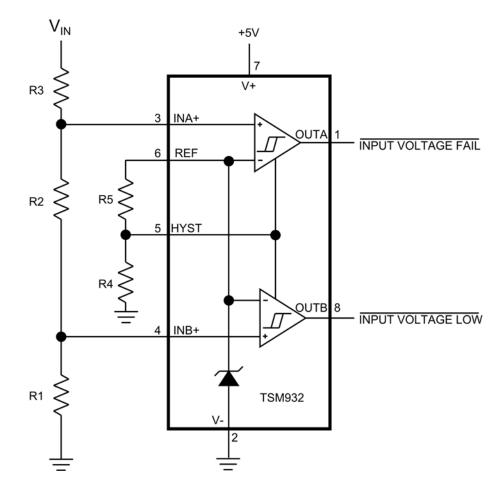
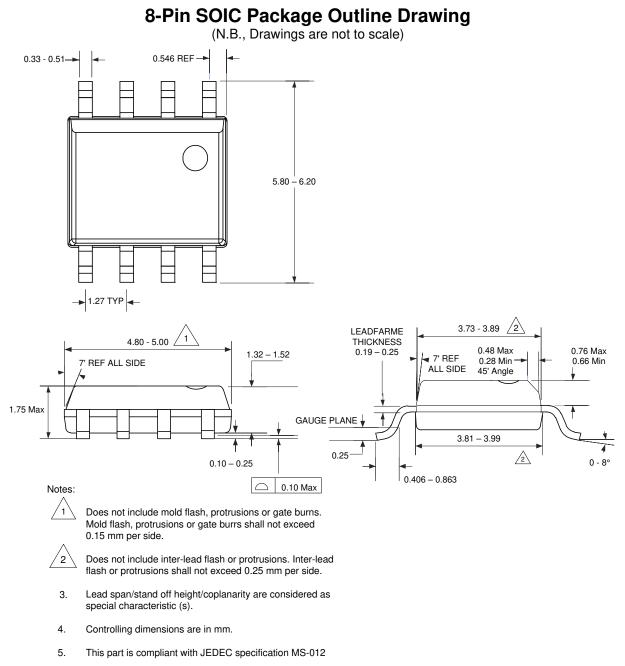


Figure 8. Two-Stage Low-Voltage Detector



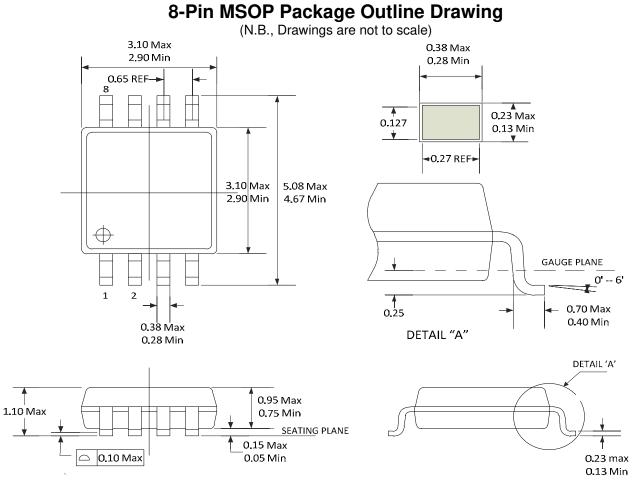
### PACKAGE OUTLINE DRAWING



6. Lead span/stand off height/coplanarity are considered as Special characteristic.



PACKAGE OUTLINE DRAWING

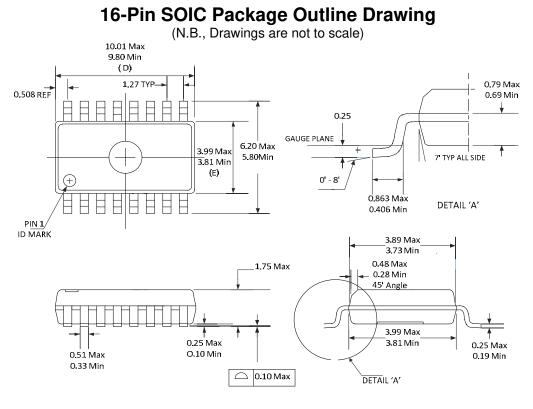


NOTE:

- 1. PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
- 2. PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTUSIONS.
- 3. CONTROLLING DIMENSION IN MILIMETERS.
- 4. THIS PART IS COMPLIANT WITH JEDEC MO-187 VARIATIONS AA
- 5. LEAD SPAN/STAND OFF HEIGHT/COPLANARITY ARE CONSIDERED AS SPECIAL CHARACTERISTIC.



### PACKAGE OUTLINE DRAWING



#### NOTE:

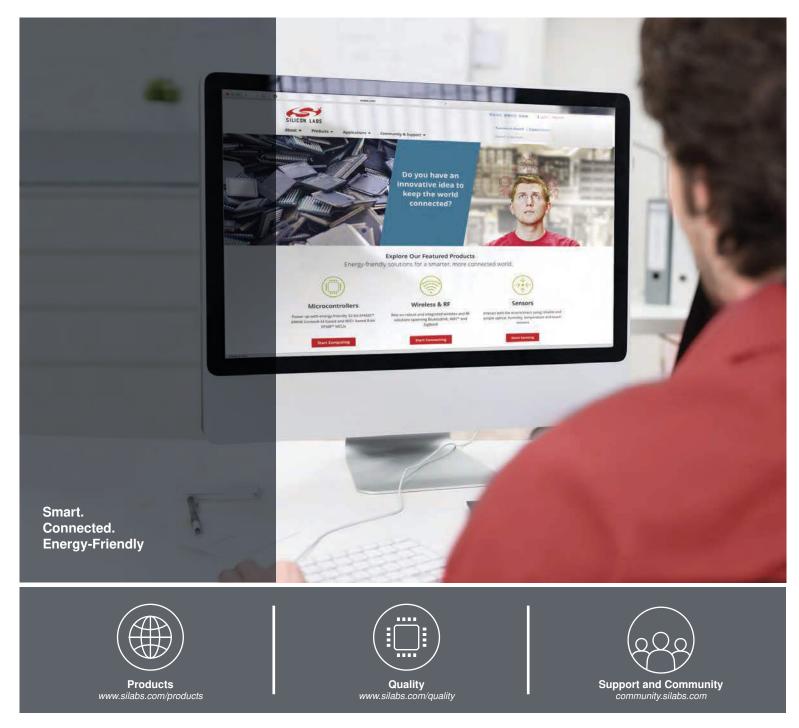
- "D" DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.15 mm PER SIDE.
- 2. "E" DOES NOT INCLUDE INTER-LEAD FLASH OR PROTRUSIONS. INTER-LEAD FLASH AND PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.25 mm PER SIDE.
- 3. CONTROLLING DIMENSIONS IN MILIMETERS AND ANGLES IN DEGREES.
- 4. THIS PART IS COMPLIANT WITH JEDEC SPECIFICATION MS-012 AB
- 5. LEAD SPAN/STAND OFF HEIGHT/COPLANARITY ARE CONSIDERED AS SPECIAL CHARACTERISTIC.

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