

December 2013

FAN3268 2 A Low-Voltage PMOS-NMOS Bridge Driver

Features

- 4.5 V to 18 V Operating Range
- Drives High-Side PMOS and Low-Side NMOS in Motor Control or Buck Step-Down Applications
- Inverting Channel B Biases High-Side PMOS Device Off (with internal 100 kΩ Resistor) when V_{DD} is below UVLO Threshold
- TTL Input Thresholds
- 2.4 A Sink / 1.6 A Source at $V_{\text{OUT}}=6$ V
- Internal Resistors Turn Driver Off If No Inputs
- MillerDrive™ Technology
- 8-Lead SOIC Package
- Rated from –40°C to +125°C Ambient
- Automotive Qualified to AEC-Q100 (F085 Version)

Applications

- Motor Control with PMOS / NMOS Half-Bridge **Configuration**
- Buck Converters with High-Side PMOS Device; 100% Duty Cycle Operation Possible
- Logic-Controlled Load Circuits with High-Side PMOS Switch
- Automotive-Qualified Systems (F085 version)

Description

The FAN3268 dual 2 A gate driver is optimized to drive a high-side P-channel MOSFET and a low-side Nchannel MOSFET in motor control applications operating from a voltage rail up to 18 V. The driver has TTL input thresholds and provides buffer and level translation functions from logic inputs. Internal circuitry provides an under-voltage lockout function that prevents the output switching devices from operating if the V_{DD} supply voltage is below the operating level. Internal 100 kΩ resistors bias the non-inverting output low and the inverting output to V_{DD} to keep the external MOSFETs off during startup intervals when logic control signals may not be present.

The FAN3268 driver incorporates MillerDrive™ architecture for the final output stage. This bipolar-MOSFET combination provides high current during the Miller plateau stage of the MOSFET turn-on / turn-off process to minimize switching loss, while providing railto-rail voltage swing and reverse current capability.

The FAN3268 has two independent enable pins that default to on if not connected. If the enable pin for noninverting channel A is pulled low, OUTA is forced low; if the enable pin for inverting channel B is pulled low, OUTB is forced high. If an input is left unconnected, internal resistors bias the inputs such that the external MOSFETs are off.

Related Resources

[AN-6069 — Application Review and Comparative](http://www.fairchildsemi.com/an/AN/AN-6069.pdf) [Evaluation of Low-Side Gate Drivers](http://www.fairchildsemi.com/an/AN/AN-6069.pdf)

Ordering Information

1. Qualified to AEC-Q100

Package Outline

Figure 2. Pin Configuration (Top View)

Thermal Characteristics(2)

Notes:

- 2. Estimates derived from thermal simulation; actual values depend on the application.
- 3. Theta_JL (ΘJL): Thermal resistance between the semiconductor junction and the bottom surface of all the leads (including any thermal pad) that are typically soldered to a PCB.
- 4. Theta_JT (Θ_{JT}): Thermal resistance between the semiconductor junction and the top surface of the package, assuming it is held at a uniform temperature by a top-side heatsink.
- 5. Theta_JA (ΘJA): Thermal resistance between junction and ambient, dependent on the PCB design, heat sinking, and airflow. The value given is for natural convection with no heatsink using a 2S2P board, as specified in JEDEC standards JESD51-2, JESD51-5, and JESD51-7, as appropriate.
- 6. Psi_JB (ΨJB): Thermal characterization parameter providing correlation between semiconductor junction temperature and an application circuit board reference point for the thermal environment defined in Not[e 5.](#page-1-3) For the SOIC-8 package, the board reference is defined as the PCB copper adjacent to pin 6.
- 7. Psi_JT (Ψ_{JT}): Thermal characterization parameter providing correlation between the semiconductor junction temperature and the center of the top of the package for the thermal environment defined in Note [5.](#page-1-3)

Output Logic

Note:

8. Default input signal if no external connection is made.

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Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Electrical Characteristics

Unless otherwise noted, $V_{DD}=12$ V and $T_{J}=40^{\circ}$ C to +125°C. Currents are defined as positive into the device and negative out of the device.

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Electrical Characteristics (Continued)

Unless otherwise noted, $V_{DD}=12$ V and $T_{J}=40^{\circ}$ C to +125°C. Currents are defined as positive into the device and negative out of the device.

Notes:

9. EN inputs have TTL thresholds; refer to the ENABLE section.

10. Not tested in production.

11. *See the Timing Diagrams of [Figure 4](#page-6-3) and [Figure 5](#page-6-4)*.

12. Apply only to Automotive Version(FAN3268TMX_F085)

Timing Diagrams

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Typical Performance Characteristics

Typical characteristics are provided at $T_A = 25^{\circ}$ C and $V_{DD} = 12$ V unless otherwise noted.

Figure 22. Quasi-Static Source Current with V_{DD}=12 V Figure 23. Quasi-Static Sink Current with V_{DD}=12 V

Figure 24. Quasi-Static Source Current with V_{DD}=8 V Figure 25. Quasi-Static Sink Current with V_{DD}=8 V

Note:

13. For any inverting inputs pulled low, non-inverting inputs pulled high, or outputs driven high, static I_{DD} increases by the current flowing through the corresponding pull-up/down resistor shown in the block diagram in [Figure 3.](#page-3-0)

Test Circuit

Applications Information

Input Thresholds

The FAN3268 driver has TTL input thresholds and provides buffer and level translation functions from logic inputs. The input thresholds meet industry-standard TTL-logic thresholds, independent of the V_{DD} voltage, and there is a hysteresis voltage of approximately 0.4 V. These levels permit the inputs to be driven from a range of input logic signal levels for which a voltage over 2 V is considered logic high. The driving signal for the TTL inputs should have fast rising and falling edges with a slew rate of 6 V/us or faster, so a rise time from 0 to 3.3 V should be 550 ns or less. With reduced slew rate, circuit noise could cause the driver input voltage to exceed the hysteresis voltage and retrigger the driver input, causing erratic operation.

Static Supply Current

In the I_{DD} (static) typical performance characteristics *(see [Figure 6\)](#page-7-0)*, the curve is produced with all inputs / enables floating (OUT is low) and indicates the lowest static I_{DD} current for the tested configuration. For other states, additional current flows through the 100 kΩ resistors on the inputs and outputs shown in the block diagram *(*see *[Figure 3\)](#page-3-0)*. In these cases, the actual static I_{DD} current is the value obtained from the curves plus this additional current.

MillerDrive™ Gate Drive Technology

FAN3268 gate drivers incorporate the MillerDrive™ architecture shown in [Figure 1.](#page-0-0) For the output stage, a combination of bipolar and MOS devices provide large currents over a wide range of supply voltage and temperature variations. The bipolar devices carry the bulk of the current as OUT swings between one and two thirds V_{DD} and the MOS devices pull the output to the high or low rail.

The purpose of the MillerDrive™ architecture is to speed up switching by providing high current during the Miller plateau region when the gate-drain capacitance of the MOSFET is being charged or discharged as part of the turn-on / turn-off process.

For applications with zero voltage switching during the MOSFET turn-on or turn-off interval, the driver supplies high peak current for fast switching even though the Miller plateau is not present. This situation often occurs in synchronous rectifier applications because the body diode is generally conducting before the MOSFET is switched on.

The output pin slew rate is determined by V_{DD} voltage and the load on the output. It is not user adjustable, but a series resistor can be added if a slower rise or fall time at the MOSFET gate is needed.

Figure 27. MillerDrive™ Output Architecture

Under-Voltage Lockout

Internal circuitry provides an under-voltage lockout function that prevents the output switching devices from operating if the V_{DD} supply voltage is below the operating level. When V_{DD} is rising, but below the 3.9 V operational level, internal 100 kΩ resistors bias the noninverting output low and the inverting output to V_{DD} to keep the external MOSFETs off during startup intervals when logic control signals may not be present. After the part is active, the supply voltage must drop 0.2 V before the part shuts down. This hysteresis helps prevent chatter when low V_{DD} supply voltages have noise from the power switching.

V_{DD} Bypass Capacitor Guidelines

To enable this IC to turn a device on quickly, a local highfrequency bypass capacitor C_{BYP} with low ESR and ESL should be connected between the VDD and GND pins with minimal trace length. This capacitor is in addition to bulk electrolytic capacitance of 10 µF to 47 µF commonly found on driver and controller bias circuits.

A typical criterion for choosing the value of C_{BYP} is to keep the ripple voltage on the V_{DD} supply to $\leq 5\%$. This is often achieved with a value \geq 20 times the equivalent load capacitance C_{EQV} , defined here as Q_{GATE}/V_{DD} . Ceramic capacitors of 0.1μ F to 1μ F or larger are common choices, as are dielectrics, such as X5R and X7R, with good temperature characteristics and high pulse current capability.

If circuit noise affects normal operation, the value of $C_{\rm BYP}$ may be increased to 50-100 times the $C_{\rm EOV}$ or C_{BYP} may be split into two capacitors. One should be a larger value, based on equivalent load capacitance, and the other a smaller value, such as 1-10 nF mounted closest to the VDD and GND pins to carry the higher frequency components of the current pulses. The bypass capacitor must provide the pulsed current from both of the driver channels and, if the drivers are switching simultaneously, the combined peak current sourced from the C_{BYP} would be twice as large as when a single channel is switching.

Layout and Connection Guidelines

The FAN3268 gate driver incorporates fast-reacting input circuits, short propagation delays, and powerful output stages capable of delivering current peaks over 2 A to facilitate voltage transition times from under 10ns to over 150 ns. The following layout and connection guidelines are strongly recommended:

- Keep high-current output and power ground paths separate from **l**ogic and enable input signals and signal ground paths. This is especially critical when dealing with TTL-level logic thresholds at driver inputs and enable pins.
- Keep the driver as close to the load as possible to minimize the length of high-current traces. This reduces the series inductance to improve highspeed switching, while reducing the loop area that can radiate EMI to the driver inputs and surrounding circuitry.
- If the inputs to a channel are not externally connected, the internal 100 kΩ resistors indicated on block diagrams command a low output (channel A) or a high output (channel B). In noisy environments, it may be necessary to tie inputs or enables of an unused channel to VDD or GND using short traces to prevent noise from causing spurious output switching.
- Many high-speed power circuits can be susceptible to noise injected from their own output or other external sources, possibly causing output retriggering. These effects can be obvious if the circuit is tested in breadboard or non-optimal circuit layouts with long input, enable, or output leads. For best results, make connections to all pins as short and direct as possible.
- The turn-on and turn-off current paths should be minimized.

Operational Waveforms

[Figure 28](#page-12-0) shows startup waveforms for non-inverting channel A. At power-up, the driver output for channel A remains low until the V_{DD} voltage reaches the UVLO turnon threshold, then OUTA operates in-phase with INA.

Figure 28. Non-Inverting Startup Waveforms

[Figure 29](#page-12-1) illustrates startup waveforms for inverting channel B. At power-up, the driver output for channel B is tied to V_{DD} through an internal 100 kΩ resistor until the V_{DD} voltage reaches the UVLO turn-on threshold, then OUTB operates out of phase with INB.

Figure 29. Inverting Startup Waveforms

Thermal Guidelines

Gate drivers used to switch MOSFETs and IGBTs at high frequencies can dissipate significant amounts of power. It is important to determine the driver power dissipation and the resulting junction temperature in the application to ensure that the part is operating within acceptable temperature limits.

The total power dissipation in a gate driver is the sum of two components, P_{GATE} and P_{DYNAMIC}:

$$
P_{\text{TOTAL}} = P_{\text{GATE}} + P_{\text{DYNAMIC}} \tag{1}
$$

Gate Driving Loss: The most significant power loss results from supplying gate current (charge per unit time) to switch the load MOSFET on and off at the switching frequency. The power dissipation that results from driving a MOSFET at a specified gatesource voltage, V_{GS} , with gate charge, Q_G , at switching frequency, f_{SW} , is determined by:

$$
P_{GATE} = Q_G \cdot V_{GS} \cdot f_{SW} \cdot n \tag{2}
$$

where n is the number of driver channels in use (1 or 2).

Dynamic Pre-drive / Shoot-through Current: A power loss resulting from internal current consumption under dynamic operating conditions, including pin pull-up / pull-down resistors, can be obtained using the "I_{DD} (No-Load) vs. Frequency" graphs in Typical Performance Characteristics to determine the current $I_{DYNAMIC}$ drawn from V_{DD} under actual operating conditions:

$$
P_{DYNAMIC} = I_{DYNAMIC} \cdot V_{DD} \cdot n \tag{3}
$$

Once the power dissipated in the driver is determined, the driver junction rise with respect to circuit board can be evaluated using the following thermal equation, assuming ψ_{JB} was determined for a similar thermal design (heat sinking and air flow):

$$
T_J = P_{\text{TOTAL}} \cdot \Psi_{JB} + T_B \tag{4}
$$

where:

 T_J =driver junction temperature

- $\Psi_{JB} = (psi)$ thermal characterization parameter relating temperature rise to total power dissipation
- T_B =board temperature in location defined in Note 2 under Thermal Resistance table.

As an example of a power dissipation calculation, consider an application driving two MOSFETs with a gate charge of 60 nC with $V_{GS}=V_{DD}=7$ V. At a switching frequency of 500 kHz, the total power dissipation is:

 $P_{GATE} = 60nC \cdot 7V \cdot 500kHz \cdot 2 = 0.42W$ (5)

 $P_{DYNAMIC} = 3mA \cdot 7V \cdot 2 = 0.042W$ (6)

$$
P_{\text{TOTAL}} = 0.46W \tag{7}
$$

The SOIC-8 has a junction-to-board thermal characterization parameter of $\Psi_{\text{LB}}=43^{\circ}\text{C/W}$. In a system application, the localized temperature around the device is a function of the layout and construction of the PCB along with airflow across the surfaces. To ensure reliable operation, the maximum junction temperature of the device must be prevented from exceeding the maximum rating of 150° C; with 80% derating, T_J would be limited to 120°C. Rearranging Equation 4 determines the board temperature required to maintain the junction temperature below 120°C:

$$
T_B = 120^{\circ}C - 0.46W \cdot 43^{\circ}C/W = 100^{\circ}C
$$
 (9)

Table 1. Related Products

Notes:

14. Typical currents with OUT at 6 V and $V_{DD}=12$ V.

15. Thresholds proportional to an externally supplied reference voltage.

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