General Description

The 844N255I is a 6-output clock synthesizer designed for wireless infrastructure clock applications. The device uses IDT's fourth generation FemtoClock® NG technology for an optimum of high clock frequency and low phase noise performance, combined with a low power consumption and high power supply noise rejection. The reference frequency is selectable and the following frequency is supported: 25MHz. The synthesizer generates selectable 156.25MHz, 125MHz, 100MHz, 50MHz and 25MHz clock signals. The device is optimized for very low phase noise and cycle to cycle jitter. The synthesized clock frequency and the phase-noise performance are optimized for driving SRIO 1.3 and 2.0 SerDes reference, DSP and host-processor clocks. The device supports a 2.5V voltage supply and is packaged in a small, lead-free (RoHS 6) 48-lead VFQFN package. The extended temperature range supports wireless infrastructure, telecommunication and networking end equipment requirements.

Features

- **•** 4 TH generation FemtoClock® NG technology
- **•** Selectable 156.25MHz, 125MHz, 100MHz, 50MHz and 25MHz output clock signals synthesized from a 25MHz reference frequency
- **•** Six differential LVDS clock outputs
- **•** Crystal interface designed for a 25MHz crystal
- **•** RMS phase jitter @ 156.25MHz, using a 25MHz crystal (1MHz - 20MHz): 0.27ps (typical)
- **•** Internal regulator for optimum noise rejection
- **•** LVCMOS interface levels for the frequency select and output enable inputs
- **•** Full 2.5V supply voltage
- **•** Lead-free (RoHS 6) 48-lead VFQFN package
- **•** -40°C to 85°C ambient operating temperature

Block Diagram

Pin Assignment

Table 1. Pin Descriptions

NOTE: Pulldown and Pullup refer to an internal input resistors. See Table 2, Pin Characteristics, for typical values.

Table 2. Pin Characteristics

Function Tables

Table 3A. Input Reference Frequency and PLL Feedback Multiplier

Table 3B. PLL Reference Clock Select Function Table

NOTE: REF_SEL is an asynchronous control.

Table 3C. Output QB[1:0] Frequency Select Function Table

NOTE: FSELB is an asynchronous control.

Table 3D. Output QC Frequency Select Function Table

NOTE: FSELC is an asynchronous control.

Table 3E. Output QD Frequency Select Function Table

NOTE: FSELD is an asynchronous control.

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Table 3F. Output QE Frequency Select Function Table

NOTE 1: FSELE is an asynchronous control.

Table 3G. nOEA Output Enable Function Table

NOTE: nOEA is an asynchronous control.

Table 3H. nOEB Output Enable Function Table

NOTE: nOEB is an asynchronous control.

Table 3I. nOEC Output Enable Function Table

NOTE: nOEC is an asynchronous control.

Table 3J. nOED Output Enable Function Table

NOTE: nOED is an asynchronous control.

Table 3K. nOEE Output Enable Function Table

NOTE 1: nOEE is an asynchronous control.

Absolute Maximum Ratings

NOTE: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These ratings are stress specifications only. Functional operation of product at these conditions or any conditions beyond those listed in the DC Characteristics or AC Characteristics is not implied. Exposure to absolute maximum rating conditions for extended periods may affect product reliability.

NOTE 1: According to JEDEC/JESD 22-A114/22-C101.

DC Electrical Characteristics

Table 4A. Power Supply DC Characteristics, $V_{DD} = V_{DDOX} = 2.5V \pm 5\%$, $T_A = -40^{\circ}C$ to 85°C

NOTE: V_{DDOX} denotes V_{DDOA,} V_{DDOB,} V_{DDOC,} V_{DDOD}, and V_{DDOE.}

NOTE: I_{DDOX} denotes I_{DDOA,} I_{DDOB,} I_{DDOC,} I_{DDOD}, and I_{DDOE.}

Table 4B. LVCMOS/LVTTL Input DC Characteristics, $V_{DD} = V_{DDOX} = 2.5V \pm 5\%$, $T_A = -40^{\circ}C$ to 85°C

NOTE: V_{DDOX} denotes V_{DDOA,} V_{DDOB,} V_{DDOC,} V_{DDOD}, and V_{DDOE.}

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Table 4C. LVDS DC Characteristics, $V_{DD} = V_{DDOX} = 2.5V \pm 5\%, T_A = -40^{\circ}C$ to 85°C

NOTE: V_{DDOX} denotes V_{DDOA} , V_{DDOB} , V_{DDOC} , V_{DDOD} , and V_{DDOE} .

Table 5. Crystal Characteristics

AC Electrical Characteristics

Table 6. AC Characteristics, $V_{DD} = V_{DDOX} = 2.5V \pm 5\%$, $T_A = -40^{\circ}C$ to 85°C

NOTE: Electrical parameters are guaranteed over the specified ambient operating temperature range, which is established when the device is mounted in a test socket with maintained transverse airflow greater than 500 lfpm. The device will meet specifications after thermal equilibrium has been reached under these conditions.

NOTE: Characterized with 25MHz crystal, unless otherwise noted.

NOTE: V_{DDOX} denotes V_{DDOA,} V_{DDOB,} V_{DDOC,} V_{DDOD,} and V_{DDOE.}

NOTE 1: Please refer to the phase noise plots.

NOTE 2: This parameter is defined in accordance with JEDEC Standard 65.

NOTE 3: Defined as skew within a bank of outputs at the same voltage and with equal load conditions.

Noise Power dBc

Noise Power

 $rac{6}{9}$

Typical Phase Noise at 156.25MHz

Offset Frequency (Hz)

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Parameter Measurement Information

LVDS Output Load AC Test Circuit

Cycle-to-Cycle Jitter

Output Duty Cycle/Pulse Width/Period

RMS Phase Jitter

Bank Skew

Output Rise/Fall Time

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Parameter Measurement Information, continued

Offset Voltage Setup

Differential Output Voltage Setup

Applications Information

Interface to IDT SRIO Switches

The 844N255I is designed for driving the differential reference clock input (REF_CLK) of IDT's SRIO 1.3 and 2.0 switch devices. The LVDS outputs of the ICS844N255I have the low-jitter, differential voltage and impedance characteristics required to provide a high-quality 156.25MHz clock signal for both SRIO 1.3 and 2.0 switch devices. Please refer to *Figure 1* for a suggested interfaces. In Figure 1, the AC-coupling capacitors are mandatory by the IDT SRIO switch devices. The differential REF_CLK input is internally re-biased and AC-terminated. The interface circuit is optimized for 50Ω transmission lines and generates the voltage swing required to reliably drive the clock reference input of a IDT SRIO switch. Please refer to IDT's SRIO device datasheet for more details.

Figure 1 shows the recommended interface circuit for driving the 156.25MHz reference clock of an IDT SRIO 2.0 switch by a LVDS output of the ICS844N255I. The LVDS-to-differential interface as shown in Figure 1 does not require any external termination resistors: the ICS844N255I driver contains an internal source termination at QA0 and QA1. The differential REF_CLK input contains an internal AC-termination (R_L) and re-bias $(\mathsf{V_{BIAS}}).$

Figure 1. LVDS-to-SRIO 2.0 Reference Clock Interface

Recommendations for Unused Input and Output Pins

Inputs:

LVCMOS Control Pins

All control pins have internal pullups and pulldowns; additional resistance is not required but can be added for additional protection. A 1k Ω resistor can be used.

Crystal Inputs

For applications not requiring the use of the crystal oscillator input, both XTAL_IN and XTAL_OUT can be left floating. Though not required, but for additional protection, a 1k Ω resistor can be tied from XTAL IN to ground.

REF_CLK Input

For applications not requiring the use of the reference clock, it can be left floating. Though not required, but for additional protection, a $1k\Omega$ resistor can be tied from the REF CLK to ground.

Outputs:

LVDS Outputs

All unused LVDS output pairs can be either left floating or terminated with 100 Ω across. If they are left floating, there should be no trace attached.

Overdriving the XTAL Interface

The XTAL_IN input can be overdriven by an LVCMOS driver or by one side of a differential driver through an AC coupling capacitor. The XTAL_OUT pin can be left floating. The amplitude of the input signal should be between 500mV and 1.8V and the slew rate should not be less than 0.2V/nS. For 3.3V LVCMOS inputs, the amplitude must be reduced from full swing to at least half the swing in order to prevent signal interference with the power rail and to reduce internal noise. Figure 2A shows an example of the interface diagram for a high speed 3.3V LVCMOS driver. This configuration requires that the sum of the output impedance of the driver (Ro) and the series resistance (Rs) equals the transmission line impedance. In addition, matched termination at the crystal input will attenuate the signal in half. This

can be done in one of two ways. First, R1 and R2 in parallel should equal the transmission line impedance. For most 50Ω applications, R1 and R2 can be 100 Ω . This can also be accomplished by removing R1 and changing R2 to 50 Ω . The values of the resistors can be increased to reduce the loading for a slower and weaker LVCMOS driver. Figure 2B shows an example of the interface diagram for an LVPECL driver. This is a standard LVPECL termination with one side of the driver feeding the XTAL_IN input. It is recommended that all components in the schematics be placed in the layout. Though some components might not be used, they can be utilized for debugging purposes. The datasheet specifications are characterized and guaranteed by using a quartz crystal as the input.

Figure 2A. General Diagram for LVCMOS Driver to XTAL Input Interface

Figure 2B. General Diagram for LVPECL Driver to XTAL Input Interface

LVDS Driver Termination

For a general LVDS interface, the recommended value for the termination impedance (Z_T) is between 90 Ω and 132 Ω . The actual value should be selected to match the differential impedance (Z₀) of your transmission line. A typical point-to-point LVDS design uses a 100 Ω parallel resistor at the receiver and a 100 Ω differential transmission-line environment. In order to avoid any transmission-line reflection issues, the components should be surface mounted and must be placed as close to the receiver as possible. IDT offers a full line of LVDS compliant devices with two types of output structures: current source and voltage source. The

standard termination schematic as shown in *Figure 3A* can be used with either type of output structure. *Figure 3B*, which can also be used with both output types, is an optional termination with center tap capacitance to help filter common mode noise. The capacitor value should be approximately 50pF. If using a non-standard termination, it is recommended to contact IDT and confirm if the output structure is current source or voltage source type. In addition, since these outputs are LVDS compatible, the input receiver's amplitude and common-mode input range should be verified for compatibility with the output.

LVDS Termination

VFQFN EPAD Thermal Release Path

In order to maximize both the removal of heat from the package and the electrical performance, a land pattern must be incorporated on the Printed Circuit Board (PCB) within the footprint of the package corresponding to the exposed metal pad or exposed heat slug on the package, as shown in *Figure 4.* The solderable area on the PCB, as defined by the solder mask, should be at least the same size/shape as the exposed pad/slug area on the package to maximize the thermal/electrical performance. Sufficient clearance should be designed on the PCB between the outer edges of the land pattern and the inner edges of pad pattern for the leads to avoid any shorts.

While the land pattern on the PCB provides a means of heat transfer and electrical grounding from the package to the board through a solder joint, thermal vias are necessary to effectively conduct from the surface of the PCB to the ground plane(s). The land pattern must be connected to ground through these vias. The vias act as "heat pipes". The number of vias (i.e. "heat pipes") are application specific and dependent upon the package power dissipation as well as electrical conductivity requirements. Thus, thermal and electrical analysis and/or testing are recommended to determine the minimum number needed. Maximum thermal and electrical performance is achieved when an array of vias is incorporated in the land pattern. It is recommended to use as many vias connected to ground as possible. It is also recommended that the via diameter should be 12 to 13mils (0.30 to 0.33mm) with 1oz copper via barrel plating. This is desirable to avoid any solder wicking inside the via during the soldering process which may result in voids in solder between the exposed pad/slug and the thermal land. Precautions should be taken to eliminate any solder voids between the exposed heat slug and the land pattern. Note: These recommendations are to be used as a guideline only. For further information, please refer to the Application Note on the Surface Mount Assembly of Amkor's Thermally/ Electrically Enhance Leadframe Base Package, Amkor Technology.

Figure 4. P.C. Assembly for Exposed Pad Thermal Release Path – Side View (drawing not to scale)

Schematic Layout

Figure 5 shows an example of 844N255I application schematic. In this example, the device is operated at $V_{DD} = V_{DDOA} = V_{DDOB} =$ $V_{DDOC} = V_{DDOD} = V_{DDOE} = 2.5V$. The 16pF parallel resonant 25MHz crystal is used. The load capacitance $C1 = 15pF$ and $C2 = 15pF$ are recommended for frequency accuracy. Depending on the parasitics of the printed circuit board layout, these values might require a slight adjustment to optimize the frequency accuracy. Crystals with other load capacitance specifications can be used. For this device, the crystal load capacitors are required for proper operation.

As with any high speed analog circuitry, the power supply pins are vulnerable to noise. To achieve optimum jitter performance, power supply isolation is required. The 844N255I provides separate power supplies to isolate from coupling into the internal PLL.

In order to achieve the best possible filtering, it is recommended that the placement of the filter components be on the device side of the PCB as close to the power pins as possible. If space is limited, the 0.1uF capacitor in each power pin filter should be placed on the device side of the PCB and the other components can be placed on the opposite side.

Figure 5. 844N255I Application Schematic

Power supply filter recommendations are a general guideline to be used for reducing external noise from coupling into the devices. The filter performance is designed for wide range of noise frequencies. This low-pass filter starts to attenuate noise at approximately 10kHz. If a specific frequency noise component is known, such as switching power supply frequencies, it is recommended that component values be adjusted and if required, additional filtering be added. Additionally, good general design practices for power plane voltage stability suggests adding bulk capacitances in the local area of all devices.

The schematic example focuses on functional connections and is not configuration specific. Refer to the pin description and functional tables in the datasheet to ensure the logic control inputs are properly set.

Power Considerations

This section provides information on power dissipation and junction temperature for the 844N255I. Equations and example calculations are also provided.

1. Power Dissipation.

The total power dissipation for the 844N255I is the sum of the core power plus the analog power plus the power dissipation in the load(s). The following is the power dissipation for $V_{DD} = 2.5V + 5\% = 2.625V$, which gives worst case results.

NOTE: Please refer to Section 3 for details on calculating power dissipation in the load.

- Power (core)_{MAX} = V_{DD_MAX} * (I_{DD_MAX} + I_{DD_MAX}) = 2.625V * (140mA + 24mA) = 430.5mW
- $Power (outputs)_{MAX} = V_{DDO_MAX} * I_{DDO_MAX} = 2.625V * 111mA = 291.375mW$

Total Power_MAX = 430.5mW + 291.375mW = **721.875mW**

2. Junction Temperature.

Junction temperature, Tj, is the temperature at the junction of the bond wire and bond pad, and directly affects the reliability of the device. The maximum recommended junction temperature is 125°C. Limiting the internal transistor junction temperature, Tj, to 125°C ensures that the bond wire and bond pad temperature remains below 125°C.

The equation for Tj is as follows: Tj = θ_{JA} * Pd_total + T_A

 Tj = Junction Temperature

 θ_{JA} = Junction-to-Ambient Thermal Resistance

Pd_total = Total Device Power Dissipation (example calculation is in section 1 above)

 T_A = Ambient Temperature

In order to calculate junction temperature, the appropriate junction-to-ambient thermal resistance θ_{JA} must be used. Assuming no air flow of and a multi-layer board, the appropriate value is 29°C/W per Table 7 below.

Therefore, Tj for an ambient temperature of 85 \degree C with all outputs switching is:

 85° C + 0.722W $*$ 29 $^{\circ}$ C/W = 105.9 $^{\circ}$ C. This is below the limit of 125 $^{\circ}$ C.

This calculation is only an example. Tj will obviously vary depending on the number of loaded outputs, supply voltage, air flow and the type of board (multi-layer).

Table 7. Thermal Resistance θ_{JA} for 48 Lead VFQFN, Forced Convection

Reliability Information

Table 8. JA vs. Air Flow Table for a 48-lead VFQFN

Transistor Count

The transistor count for 844N255I is: 21,109

Package Outline and Package Dimensions

Package Outputline -K Suffix for 48 Lead VFQFN

FOR REFERENCE ONLY

CHAMFER 1 \mathfrak{D}

Bottom View w/Type A ID

 $N-N-1$

 $\overline{4}$

There are 2 methods of indicating pin 1 corner at the back of the VFQFN package:

1. Type A: Chamfer on the paddle (near pin 1)

2. Type C: Mouse bite on the paddle (near pin 1)

Table 9. PackageDimensions for 48 Lead VFQFN

Reference Document: IDT Drawing #PSC-4203

Ordering Information

Table 10. Ordering Information Table

Revision History

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Corporate Headquarters

TOYOSU FORESIA, 3-2-24 Toyosu,

Koto-ku, Tokyo 135-0061, Japan

Koto-ku, Tokyo 135-0061, Japan www.renesas.com office, please visit:

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