

September 2011

FAN302HL mWSaver™ PWM Controller for Low Standby Power Battery-Charger Applications

Features

- mWSaver[™] Technology Provides Industry's Bestin-Class Standby Power
	- Achieve Under 10mW; Far Below Energy Star's 5-Star Level (<30mW)
	- Proprietary 500V High-Voltage JFET Startup Reduces Startup Resistor Loss
	- Low Operation Current in Burst Mode: Maximum 350µA
- Constant-Current (CC) Control without Secondary-Feedback Circuitry
- Fixed PWM Frequency at 85kHz with Frequency Hopping to Solve EMI Problem
- Low Operating Current: 3.5mA
- Peak-Current-Mode Control in CV Regulation
- Cycle-by-Cycle Current Limiting
- V_{DD} Over-Voltage Protection (Auto-Restart)
- V_S Over-Voltage Protection (Latch Mode)
- V_{DD} Under-Voltage Lockout (UVLO)
- Gate Output Maximum Voltage Clamped at 15V
- Fixed Over-Temperature Protection (Latch Mode)
- Available in an 8-Lead SOIC Package

Applications

Battery chargers for cellular phones, cordless phones, PDA, digital cameras, and power tools. Replaces linear transformers and RCC SMPS.

Description

This highly integrated PWM controller, FAN302HL, provides several features to enhance the performance of general flyback converters. The constant-currentcontrol, proprietary topology enables simplified circuit designs without secondary feedback circuitry for batterycharger applications.

A proprietary Burst-Mode function with low operation current minimizes standby power consumption.

The FAN302HL controller also provides several protections. Cycle-by-cycle current limiting ensures the fixed peak current limit level, even if a short circuit occurs. The gate output is clamped at 15V to protect the power MOS from high gate-source voltage conditions. If either V_S OVP or internal OTP is triggered, the circuit enters Latch Mode until AC power is removed.

Using FAN302HL, a charger can be implemented with few external components and minimized cost, compared to a conventional design or a linear transformer. A typical output CV/CC characteristic is shown in Figure 1.

Figure 1. Typical Output V-I Characteristic

Ordering Information

Pin Definitions

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Notes:

1. All voltage values, except differential voltages, are given with respect to GND pin.
2. Stresses beyond those listed under Absolute Maximum Ratings may cause perma

2. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.
3. ESD ratings including HV pin: HBM=400V. CDM=750V.

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 V_{DD} =15V and T_A =25°C unless noted.

FAN302HL - mWSaverTM PWM Controller for Low Standby Power Battery-Charger Applications **FAN302HL — mWSaver™ PWM Controller for Low Standby Power Battery-Charger Applications**

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Electrical Characteristics (Continued)

 V_{DD} =15V and T_A =25°C unless noted.

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Operation Description

Constant-Voltage Regulation Operation

FAN302HL is the high-frequency and ultra-low standby power IC with Constant Voltage (CV) / Constant Current (CC) regulation.

When FAN302HL operates in CV regulation, the feedback voltage (V_{FB}) works as output load and modulates the PWM duty, as shown in Figure 24, causing fixed switching frequency (85kHz). Once the V_{FB} decreases below V_{FB-G} , frequency hopping is disabled and operation current decreases.

Figure 24. f_{OSC} vs. V_{FB} in CV Regulation

Constant-Current Regulation Operation

During CC operation, the proprietary Primary-Side Regulation (PSR) topology simplifies circuit design without secondary feedback circuitry for battery-charger applications. The CC regulation achieved through PSR technique uses a mixed-signal algorithm to detect the primary-side current and to sample the voltage through primary-side auxiliary winding and calculate the average current on secondary side.

Figure 25 shows the basic circuit diagram of a flyback converter, with typical waveforms shown in Figure 26. Generally, Discontinuous Conduction Mode (DCM) operation is preferred for constant-current control since it allows better output regulation. The operation principles of DCM flyback converter are:

During the MOSFET on time (t_{ON}) , input voltage (V_{DL}) is applied across the primary-side inductor (L_m) . Then, MOSFET current (I_{ds}) increases linearly from zero to the peak value (I_{pk}) . During this time, the energy is drawn from the input and stored in the inductor.

When the MOSFET is turned off, the energy stored in the inductor forces the rectifier diode (D) to be turned on. While the diode is conducting, the output voltage (V_O), together with diode forward voltage drop (V_F), are applied across the secondary-side inductor $(L_m \times N_s^2)$ N_p^2) and the diode current (I_D) decreases linearly from the peak value (I_p k $\times N_p/N_s$) to zero. At the end of inductor current discharge time (t_{DIS}) , all the energy stored in the inductor has been delivered to the output.

When the diode current reaches zero, V_S voltage drops quickly: if it is greater than the $V_{VS-OFFSET}$ drop voltage, the IC gets the t_{DIS} for CC regulation.

During the inductor current discharge time, the sum of output voltage and diode forward-voltage drop is reflected to the auxiliary winding side as $(V_0+V_F) \times$ N_a/N_s. This voltage signal is proportional to the secondary winding. In constant-current output operation, this voltage signal is detected and examined by the precise constant-current regulation controller. The on time of the MOSFET is determined to control input power and provide constant-current output property. With feedback voltage V_{CS} across the current-sense resistor, the controller can obtain the input power of power supply. Therefore, the region of constant-current output operation can be adjusted by the current-sense resistor, as shown in Equation (1).

$$
I_{O} = \frac{1}{2} \cdot i_{PK} \cdot \frac{N_{P}}{N_{S}} \cdot \frac{t_{DIS}}{t_{s}} = \frac{1}{2} \cdot \frac{N_{P}}{N_{S}} \cdot \frac{V_{CS}}{R_{CS}} \cdot \frac{t_{DIS}}{t_{s}}
$$
(1)

During CC regulation, the V_S voltage decreases as output voltage decreases. The switching frequency reduces linearly from fosc to fosc-ccm as Vs voltage changes from V_{SN-CC} to V_{SG-CC} . Figure 27 shows the relationship between frequency and V_S voltage. Figure 28 shows the output V-I curve and V_S voltage.

Figure 26. Waveforms of DCM Flyback Converter

High-Voltage Startup

Figure 29 shows the high-voltage (HV) startup circuit for FAN302HL applications. The HV pin is connected to the line input or bulk capacitor through a resistor. During startup, the internal startup circuit is enabled and the line input supplies the current, I_{HV} , to charge the hold-up capacitor, C_{VDD}, through R_{START}. When the V_{DD} voltage reaches V_{DD-ON} , the internal HV startup circuit is disabled, blocking I_{HV} from flowing into the HV pin. Once the IC turns on, C_{VDD} is the only energy source to supply the IC consumption current before the PWM starts to switch. Therefore, C_{VDD} must be large enough to prevent V_{DD} from dropping to V_{DD-OFF} before the power can be delivered from the auxiliary winding.

Frequency Hopping

EMI reduction is accomplished by frequency hopping, which spreads the energy over a wider frequency range than the bandwidth measured by the EMI test equipment. The FAN302HL internal frequency-hopping circuit changes the switching frequency between 82kHz and 88kHz with a period, as shown in Figure 30.

Burst-Mode Operation

The power supply enters "Burst-Mode" at no-load conditions. As shown in Figure 31, when V_{FB} drops below V_{FBL} , the PWM output shuts off and the output voltage drops at a rate dependent on load current. This causes the feedback voltage to rise. Once V_{FB} exceeds V_{FBH} , the internal circuit starts to provide switching pulse. The feedback voltage then falls and the process repeats. Burst Mode operation alternately enables and disables switching of the MOSFET, reducing the switching losses in Standby Mode.

Figure 31. Burst-Mode Operation

Operating Current

The typical operating current is 3.5mA. This low operating current results in higher efficiency and reduces the V_{DD} hold-up capacitance requirement. Once FAN302HL enters Burst Mode, the operating current is reduced to 200μA, allowing the power supply to meet power conservation requirements.

Gate Output

The FAN302HL BiCMOS output stage is a fast totempole gate driver. Cross conduction has been avoided to minimize heat dissipation, increase efficiency, and enhance reliability. The output driver is clamped by an internal Zener diode to protect the power MOSFET transistors against over-voltage gate signals.

Slope Compensation

The sensed voltage across the current-sense resistor is used for Current-Mode control and pulse-by-pulse current limiting. Built-in slope compensation, a synchronized positively-sloped ramp built-in at each switching cycle, improves stability and prevents subharmonic oscillations due to Peak-Current Mode control.

Constant Power Mode Control

When V_S is lower than $V_{S\text{-CM-MIN}}$, FAN302HL enters Constant-Power-Mode control, the primary-side current limit voltage (V_{CS}) changes from V_{STH} to V_{STH-VA} to avoid mis-sampling V_s through the Zero Current Detection (ZCD). Once V_S is higher than $V_{S\text{-}CM\text{-}MAX}$, the V_{CS} returns to V_{STH} .

Protections

The FAN302HL self-protection functions include V_{DD} Over-Voltage Protection (V_{DD} OVP), internal Over-Temperature Protection (OTP), V_S Over-Voltage Protection (V_S OVP), brownout protection, and pulse-bypulse current limit.

The V_{DD} OVP protection is implemented as Auto-Restart Mode. Once an abnormal condition occurs, switching is terminated and the MOSFET remains off, causing V_{DD} to drop. When V_{DD} drops to the V_{DD} turn-off voltage of 5V, the internal startup circuit is enabled, and the supply current drawn from HV pin charges the hold-up capacitor. When V_{DD} reaches the turn-on voltage of 16V, FAN302HL resumes normal operation. In this manner, the auto-restart alternately enables and disables the switching of the MOSFET until the abnormal condition is eliminated (*see Figure 32*).

Figure 32. Auto-Restart Mode Operation

The V_S OVP and internal OTP protections are implemented as Latch Mode. If abnormal conditions occur, PWM switching is terminated and the MOSFET remains off. In this scenario, V_{DD} drops, but keeps working as auto-restart (V_{DD} auto-restart behavior doesn't trigger PWM pulses). FAN302HL enters Latch Mode, disables PWM switching of the MOSFET until V_{DD} is lower than $V_{\text{DD-LH}}$ (AC power is removed), powers on again, then resumes normal operation (*see Figure 33*).

Figure 33. Latch-Mode Operation

VS Over-Voltage Protection (OVP)

V_S over-voltage protection prevents damage due to output over-voltage conditions. Figure 34 shows the V_S OVP protection method. When abnormal system conditions occur that cause V_S to exceed 2.8V, after a period of debounce time; PWM pulses are disabled and FAN302HL enters Latch Mode until V_{DD} drops to under V_{DD-LH} . By that time, PWM pulses revive. V_S over-voltage conditions are usually caused by open feedback loops or abnormal behavior by the VS pin divider resistor.

Figure 34. VS OVP Protection

V_{DD} Over-Voltage Clamping

 V_{DD} over-voltage protection prevents damage due to over-voltage conditions. When the V_{DD} voltage exceeds 26.5V due to abnormal conditions, PWM pulses are disabled until the V_{DD} voltage drops below the UVLO. then starts again. Over-voltage conditions are usually caused by open feedback loops.

Over-Temperature Protection (OTP)

The FAN302HL temperature-sensing circuit shuts down PWM output if the junction temperature exceeds 140°C (T_{OTP}). The PWM pulses are disabled until V_{DD} voltage drops below the V_{DD-LH} .

Leading-Edge Blanking (LEB)

Each time the power MOSFET is switched on, a turn-on spike occurs at the sense resistor. To avoid premature termination of the switching pulse, a 350ns leading-edge blanking time is built in. Conventional RC filtering can therefore be omitted. During this blanking period, the current-limit comparator is disabled and it cannot switch off the gate driver.

Under Voltage Lockout (UVLO)

The turn-on and turn-off thresholds are fixed internally at 16V and 5V, respectively. During startup, the hold-up capacitor must be charged to 16V through the startup resistor to enable the FAN302HL. The hold-up capacitor continues to supply V_{DD} until power can be delivered from the auxiliary winding of the main transformer. V_{DD} must not drop below 5V during this startup process. This UVLO hysteresis window ensures that the hold-up capacitor is adequate to supply V_{DD} during startup.

Noise Immunity

Noise from the current sense or the control signal can cause significant pulse-width jitter, particularly in Continuous-Conduction Mode. While slope compensation helps alleviate these problems, further precautions should still be taken. Good placement and layout practices should be followed. Avoiding long PCB traces and component leads, locating compensation and filter components near the FAN302HL, and increasing the power MOS gate resistance are advised.

Typical Application Circuit (Flyback Charger)

Features

- High Efficiency (Avg. >71%), Meeting Energy Star V2.0 Standard (Avg. 68.17%)
- Ultra-Low Standby Power: Under 10mW at 230 V_{AC} (Pin=6.3mW for 115 V_{AC} and Pin=7.3mW for 230 V_{AC})
- Output Regulation (CV: ±5%, CC: ±15%)

Typical Application Circuit (Continued)

Transformer Specification

- Core: EI12.5
- Bobbin: EI12.5

Figure 37.Transformer

- W1 is four winds; for each wind of turns, refer to Table 1. Add one insulating tape layer between the first and second layers.
- W2 is wound two layers and uses triple-insulated wire: end of positive fly line is 3.5cm, layer end of negative fly line is 2.5cm.
- W3 is spares winding in one layer.
- W4 is wound in the core of the outermost layer and sparse winding.

Table 1. Transformer Turns Specifications

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