

Low-Power Triple-Output TFT LCD DC-DC Converter

General Description

The MAX1779 triple-output DC-DC converter provides highly efficient regulated voltages required by small active matrix, thin-film transistor (TFT) liquid-crystal displays (LCDs). One high-power DC-DC converter and two low-power charge pumps convert the +2.7V to +5.5V input supply voltage into three independent output voltages.

The primary high-power DC-DC converter generates a boosted output voltage (VMAIN) up to 13V that is regulated within ±1%. The low-power BiCMOS control circuitry and the low on-resistance (1 Ω) of the integrated power MOSFET allows efficiency up to 91%. The 250kHz current-mode pulse-width modulation (PWM) architecture provides fast transient response and allows the use of ultra-small inductors and ceramic capacitors.

The dual charge pumps independently regulate one positive output (VPOS) and one negative output (VNEG). These low-power outputs use external diode and capacitor stages (as many stages as required) to regulate output voltages up to +40V and down to -40V. A proprietary regulation algorithm minimizes output ripple, as well as capacitor sizes for both charge pumps.

The MAX1779 is available in the ultra-thin TSSOP package (1.1mm max height).

Applications

TFT Active-Matrix LCD Displays Passive-Matrix LCD Displays **PDAs** Digital-Still Cameras Camcorders

Typical Operating Circuit appears at end of data sheet.

Features

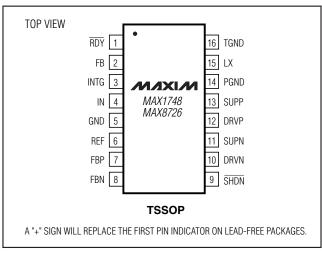
- ♦ Three Integrated DC-DC Converters
- ♦ 250kHz Current-Mode PWM Boost Regulator Up to +13V Main High-Power Output ±1% Accuracy High Efficiency (91%)
- **♦ Dual Charge-Pump Outputs** Up to +40V Positive Charge-Pump Output **Down to -40V Negative Charge-Pump Output**
- ♦ Internal Supply Sequencing
- **♦ Internal Power MOSFETs**
- ♦ +2.7V to +5.5V Input Supply
- ♦ 0.1µA Shutdown Current
- ♦ 0.5mA Quiescent Current
- ♦ Internal Soft-Start
- **♦** Power-Ready Output
- **♦ Ultra-Small External Components**
- **♦** Thin TSSOP Package (1.1mm max)

Ordering Information

PART	TEMP RANGE	PIN-PACKAGE
MAX1779EUE	-40°C to +85°C	16 TSSOP
MAX1779EUE+	-40°C to +85°C	16 TSSOP

+ Denotes lead-free package.

Pin Configuration



ABSOLUTE MAXIMUM RATINGS

IN, SHDN, TGND to GND	0.3V to +6V
DRVN to GND	0.3V to (V _{SUPN} + 0.3V)
DRVP to GND	0.3V to (VSUPP + 0.3V)
PGND to GND	±0.3V
RDY to GND	0.3V to +14V
LX, SUPP, SUPN to PGND	0.3V to +14V
INTG, REF, FB, FBN, FBP to GND	0.3V to $(V_{IN} + 0.3V)$

Continuous Power Dissipation ($T_A = +70$	O°C)
16-Pin TSSOP (derate 9.4mW/°C abov	re +70°C)755mW
Operating Temperature Range	
MAX1779EUE	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = +10V, TGND = PGND = GND, C_{REF} = 0.22\mu F, C_{INTG} = 2200pF, T_A = 0°C to +85°C, unless otherwise noted. Typical values are at T_A = +25°C.)$

	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Input Supply Range	VIN		2.7		5.5	V
Input Undervoltage Threshold	VUVLO	V _{IN} rising, 40mV hysteresis (typ)	2.2	2.4	2.6	V
IN Quiescent Supply Current	I _{IN}	V _{FB} = V _{FBP} = +1.5V, V _{FBN} = -0.2V		0.5	1	mA
SUPP Quiescent Current	ISUPP	$V_{FBP} = +1.5V$		0.25	0.55	mA
SUPN Quiescent Current	I _{SUPN}	$V_{FBN} = -0.1V$		0.25	0.55	mA
IN Shutdown Current		$V_{\overline{SHDN}} = 0$, $V_{IN} = +5V$		0.1	10	μΑ
SUPP Shutdown Current		V SHDN = 0, V _{SUPP} = +13V		0.1	10	μА
SUPN Shutdown Current		$V\overline{SHDN} = 0$, $VSUPN = +13V$		0.1	10	μΑ
MAIN BOOST CONVERTER						
Output Voltage Range	VMAIN		VIN		13	V
FB Regulation Voltage	V _{FB}		1.235	1.248	1.261	V
FB Input Bias Current	I _{FB}	V _{FB} = +1.25V, INTG = GND	-50		50	nA
Operating Frequency	fosc		212	250	288	kHz
Oscillator Maximum Duty Cycle			79	85	92	%
Load Regulation		$I_{MAIN} = 0$ to 50mA, $V_{MAIN} = +5V$		0.1		%
Line Regulation				0.1		%/V
Integrator Gm				320		μs
LX Switch On-Resistance	R _{LX} (ON)	$I_{LX} = 100mA$		1.0	2.0	Ω
LX Leakage Current	ILX	$V_{LX} = +13V$		0.01	20	μА
LX Current Limit	I _{LIM}		350	450	650	mA
Maximum RMS LX Current				250		mA
FB Fault Trip Level		Falling edge	1.07	1.1	1.14	V
POSITIVE CHARGE PUMP	_		1			
V _{SUPP} Input Supply Range	VSUPP		2.7		13	V

ELECTRICAL CHARACTERISTICS (continued)

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = +10V, TGND = PGND = GND, C_{REF} = 0.22 \mu F, C_{INTG} = 2200 pF, T_A = 0^{\circ}C$ to +85°C, unless otherwise noted. Typical values are at TA = +25°C.)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Operating Frequency				0.5 ×		Hz
Operating Frequency				fosc		112
FBP Regulation Voltage	V _{FBP}		1.20	1.25	1.30	V
FBP Input Bias Current	IFBP	$V_{FBP} = +1.5V$	-50		50	nA
DRVP PCH On-Resistance				3	10	Ω
DRVP NCH On-Resistance		$V_{FBP} = +1.200V$		1.5	5	Ω
DRVP NCH OII-Resistance		$V_{FBP} = +1.300V$	20			kΩ
FBP Power-Ready Trip Level		Rising edge	1.09	1.13	1.16	V
FBP Fault Trip Level		Falling edge		1.11		V
Maximum RMS DRVP Current				0.1		А
NEGATIVE CHARGE PUMP	•		•			
V _{SUPN} Input Supply Range	Vsupn		2.7		13	V
O				0.5 ×		1.1-
Operating Frequency				fosc		Hz
FBN Regulation Voltage	V _{FBN}		-50	0	50	mV
FBN Input Bias Current	I _{FBN}	$V_{FBN} = -0.05V$	-50		50	nA
DRVN PCH On-Resistance				3	10	Ω
DRVN NCH On-Resistance		$V_{FBN} = +0.050V$		1.5	5	Ω
DRVIN INCH OH-NESISIANCE		$V_{FBN} = -0.050V$	20			kΩ
FBN Power-Ready Trip Level		Falling edge	80	120	165	mV
FBN Fault Trip Level		Rising edge		140		mV
Maximum RMS DRVN Current				0.1		А
REFERENCE			·			
Reference Voltage	V _{REF}	-2μA < I _{REF} < 50μA	1.231	1.25	1.269	V
Reference Undervoltage		V _{REF} rising	0.9	1.05	1.2	V
Threshold		VREF IISING	0.9	1.00	1.2	V
LOGIC SIGNALS	1					1
SHDN Input Low Voltage		0.25V hysteresis (typ)			0.9	V
SHDN Input High Voltage			2.1			V
SHDN Input Current	ISHDN			0.01	1	μΑ
RDY Output Low Voltage		I _{SINK} = 2mA		0.25	0.5	V
RDY Output High Voltage		V _{RDY} = +13V		0.01	1	μΑ

ELECTRICAL CHARACTERISTICS

 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = +10V, TGND = PGND = GND, C_{REF} = 0.22\mu F, C_{INTG} = 2200pF, T_A = -40^{\circ}C to +85^{\circ}C, unless otherwise noted.) (Note 1)$

PARAMETER	SYMBOL	CONDITIONS	MIN	MAX	UNITS
Input Supply Range	VIN		2.7	5.5	V
Input Undervoltage Threshold	Vuvlo	V _{IN} rising, 40mV hysteresis (typ)	2.2	2.6	V
IN Quiescent Supply Current	I _{IN}	V _{FB} = V _{FBP} = +1.5V, V _{FBN} = -0.2V		1	mA
SUPP Quiescent Current	ISUPP	V _{FBP} = +1.5V		0.55	mA
SUPN Quiescent Current	ISUPN	V _{FBN} = -0.1V		0.55	mA
IN Shutdown Current		$V_{\overline{SHDN}} = 0$, $V_{\overline{IN}} = +5V$		10	μΑ
SUPP Shutdown Current		V <u>SHDN</u> = 0, V _{SUPP} = +13V		10	μΑ
SUPN Shutdown Current		$V_{\overline{SHDN}} = 0$, $V_{SUPN} = +13V$		10	μΑ
MAIN BOOST CONVERTER					
Output Voltage Range	V _{MAIN}		VIN	13	V
FB Regulation Voltage	V _{FB}		1.225	1.271	V
FB Input Bias Current	I _{FB}	V _{FB} = +1.25V, INTG = GND	-50	50	nA
Operating Frequency	fosc		195	305	kHz
Oscillator Maximum Duty Cycle			79	92	%
LX Switch On-Resistance	R _L X(ON)	I _L X = 100mA		2.0	Ω
LX Leakage Current	ILX	$V_{LX} = +13V$		20	μΑ
LX Current Limit	I _{LIM}		350	700	mA
FB Fault Trip Level		Falling edge	1.07	1.14	V
POSITIVE CHARGE PUMP			<u>.</u>		•
SUPP Input Supply Range	VSUPP		2.7	13	V
FBP Regulation Voltage	V _{FBP}		1.20	1.30	V
FBP Input Bias Current	I _{FBP}	V _{FBP} = +1.5V	-50	50	nA
DRVP PCH On-Resistance				10	Ω
DDVD NOLLOG Desisters		V _{FBP} = +1.200V		5	Ω
DRVP NCH On-Resistance		V _{FBP} = +1.300V	20		kΩ
FBP Power-Ready Trip Level		Rising edge	1.09	1.16	V
NEGATIVE CHARGE PUMP					
SUPN Input Supply Range	V _{SUPN}		2.7	13	V
FBN Regulation Voltage	V _{FBN}		-50	50	mV
FBN Input Bias Current	I _{FBN}	V _{FBN} = -0.05V	-50	50	nA
DRVN PCH On-Resistance				10	Ω
DDVN NOLLOW Desistence		V _{FBN} = +0.050V		5	Ω
DRVN NCH On-Resistance		V _{FBN} = -0.050V	20		kΩ
FBN Power-Ready Trip Level		Falling edge	80	165	mV
REFERENCE					
Reference Voltage	V _{REF}	-2μA < I _{REF} < 50μA	1.223	1.269	V
Reference Undervoltage		V _{REF} rising	0.9	1.2	V
	•		•		•

MIXIM

ELECTRICAL CHARACTERISTICS (continued)

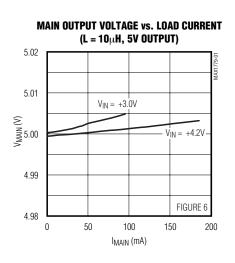
 $(V_{IN} = +3.0V, \overline{SHDN} = IN, V_{SUPP} = V_{SUPN} = +10V, TGND = PGND = GND, C_{REF} = 0.22\mu F, C_{INTG} = 2200 pF, T_A = -40^{\circ}C to +85^{\circ}C, unless otherwise noted.)$ (Note 1)

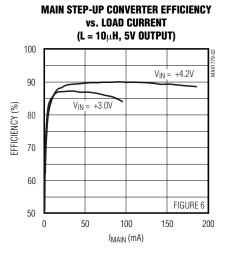
PARAMETER	SYMBOL	CONDITIONS	MIN	MAX	UNITS
LOGIC SIGNALS					
SHDN Input Low Voltage		0.25V hysteresis (typ)		0.9	V
SHDN Input High Voltage			2.1		V
SHDN Input Current	ISHDN			1	μΑ
RDY Output Low Voltage		I _{SINK} = 2mA		0.5	V
RDY Output High Leakage		V RDY = +13V		1	μΑ

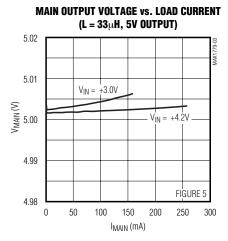
Note 1: Specifications to -40°C are guaranteed by design, not production tested.

Typical Operating Characteristics

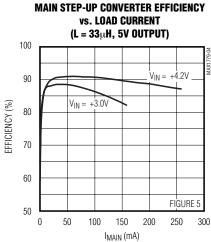
(Circuit of Figure 5, V_{IN} = +3.3V, T_A = +25°C, unless otherwise noted.)

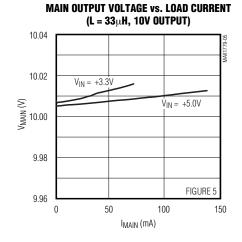


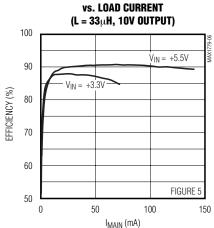




MAIN STEP-UP CONVERTER EFFICIENCY

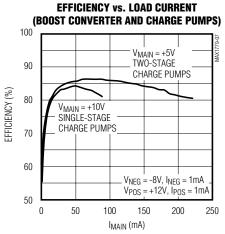


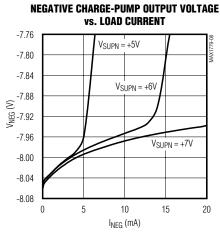


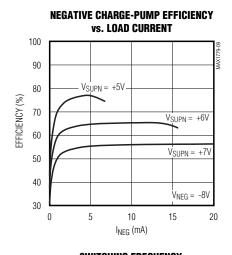


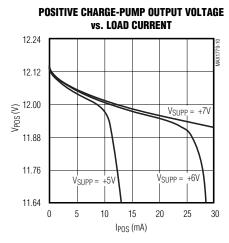
Typical Operating Characteristics (continued)

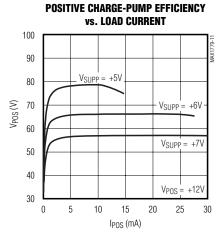
(Circuit of Figure 5, $V_{IN} = +3.3V$, $T_A = +25$ °C, unless otherwise noted.)

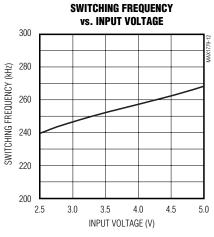


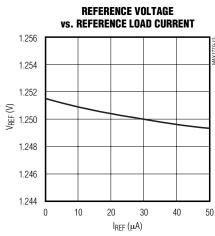


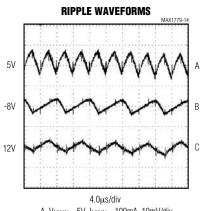


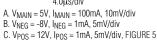


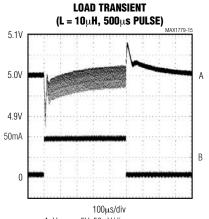








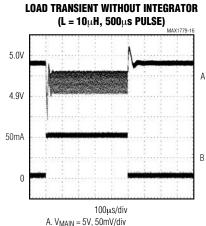




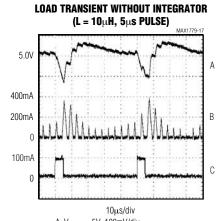
A. V_{MAIN} = 5V, 50mV/div B. V_{MAIN} = 5mA to 50mA, 25mA/div FIGURE 6

Typical Operating Characteristics (continued)

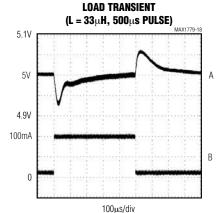
(Circuit of Figure 5, $V_{IN} = +3.3V$, $T_A = +25$ °C, unless otherwise noted.)



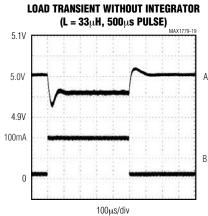
A. $V_{MAIN} = 5V$, 50mV/divB. $V_{MAIN} = 5mA$ to 50mA, 25mA/divINTG = REF, FIGURE 6



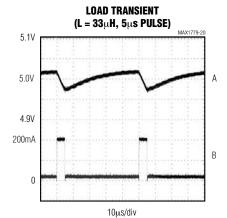
A. V_{MAIN} = 5V, 100mV/div B. I_L, 200mA/div C. I_{MAIN} = 10mA to 100mA, 100mA/div INTG = REF, FIGURE 6



A. V_{MAIN} = 5V, 50mV/div B. I_{MAIN} = 10mA to 100mA, 50mA/div FIGURE 5

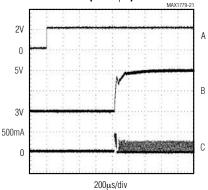


A. V_{MAIN} = 5V, 50mV/div B. I_{MAIN} = 10mA to 100mA, 50mA/div INTG = REF, FIGURE 5



A. V_{MAIN} = 5V, 50mV/div B. I_{MAIN} = 20mA to 200mA, 100mA/div FIGURE 5

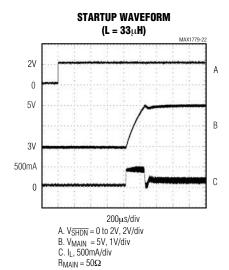
STARTUP WAVEFORM (L = 10μH)

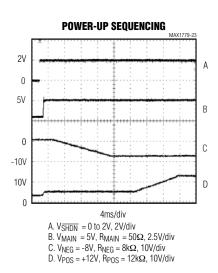


A. $V_{\overline{SHDN}} = 0$ to 2V, 2V/div B. $V_{MAIN} = 5V$, 1V/div C. I_L, 500 mA/div FIGURE 6, $R_{MAIN} = 100\Omega$

Typical Operating Characteristics (continued)

(Circuit of Figure 5, $V_{IN} = +3.3V$, $T_A = +25$ °C, unless otherwise noted.)





Pin Description

PIN	NAME	FUNCTION	
1	RDY	Active-Low Open-Drain Output. Indicates all outputs are ready. The on-resistance is 125 Ω (typ).	
2	FB	Main Boost Regulator Feedback Input. Regulates to 1.25V nominal. Connect feedback resistive divider to analog ground (GND).	
3	INTG	Main Boost Integrator Output. If used, connect 2200pF to analog ground (GND). To disable integrator, connect to REF.	
4 IN Supply Input. +2.7V to +5.5V input range. Bypass with a 0.1μF capacitor between IN and close to the pins as possible.		Supply Input. +2.7V to +5.5V input range. Bypass with a 0.1μF capacitor between IN and GND, as close to the pins as possible.	
5 GND Analog Ground. Connect to power ground (PGN		Analog Ground. Connect to power ground (PGND) underneath the IC.	
6 REF Internal Reference Bypass Terminal. Connect a 0.22μF capacitor from (GND). External load capability to 50μA.		Internal Reference Bypass Terminal. Connect a 0.22μF capacitor from this terminal to analog ground (GND). External load capability to 50μA.	
7 FBP Positive Charge-Pump Regulator Feedback Input. Regulates to 1.25V resistive divider to analog ground (GND).		Positive Charge-Pump Regulator Feedback Input. Regulates to 1.25V nominal. Connect feedback resistive divider to analog ground (GND).	
8 FBN Negative Charge-Pump Regulator Feedback Input. Regulates to 0V nominal.		Negative Charge-Pump Regulator Feedback Input. Regulates to 0V nominal.	
9 SHDN Active-Low Logic-Level Shutdown Input. Connect SHDN to IN for normal operation.		Active-Low Logic-Level Shutdown Input. Connect SHDN to IN for normal operation.	

Pin Description (continued)

PIN	NAME	FUNCTION
10	DRVN Negative Charge-Pump Driver Output. Output high level is V _{SUPN} , and low level is PGN	
11	11 SUPN Negative Charge-Pump Driver Supply Voltage. Bypass to PGND with a 0.1μF capacitor.	
12	DRVP Positive Charge-Pump Driver Output. Output high level is V _{SUPP} , and low level is PGND.	
13	SUPP	Positive Charge-Pump Driver Supply Voltage. Bypass to PGND with a 0.1μF capacitor.
14 PGND Power Ground. Connect to GND underneath the IC.		Power Ground. Connect to GND underneath the IC.
15	Main Boost Regulator Power MOSFET N-Channel Drain. Connect output diode and output das close to PGND as possible.	
16 TGND Must be connected to ground.		Must be connected to ground.

Detailed Description

The MAX1779 is a highly efficient triple-output power supply for TFT LCD applications. The device contains one high-power step-up converter and two low-power charge pumps. The primary boost converter uses an internal N-channel MOSFET to provide maximum efficiency and to minimize the number of external components. The output voltage of the main boost converter (VMAIN) can be set from VIN to 13V with external resistors.

The dual charge pumps independently regulate a positive output (VPOS) and a negative output (VNEG). These low-power outputs use external diode and capacitor stages (as many stages as required) to regulate output voltages up to +40V and down to -40V. A proprietary regulation algorithm minimizes output ripple as well as capacitor sizes for both charge pumps.

Also included in the MAX1779 are a precision 1.25V reference that sources up to $50\mu\text{A}$, logic shutdown, soft-start, power-up sequencing, fault detection, and an active-low open-drain ready output.

Main Boost Converter

The MAX1779 main step-up converter switches at a constant 250kHz internal oscillator frequency to allow the use of small inductors and output capacitors. The MOSFET switch pulse width is modulated to control the power transferred on each switching cycle and to regulate the output voltage.

During PWM operation, the internal clock's rising edge sets a flip-flop, which turns on the N-channel MOSFET (Figure 1). The switch turns off when the voltage-error, slope-compensation, and current-feedback signals trip the comparators and reset the flip-flop. The switch remains off for the rest of the clock cycle. Changes in

the output voltage error signal shift the switch current trip level, consequently modulating the MOSFET duty cycle.

Dual Charge-Pump Regulator

The MAX1779 contains two individual low-power charge pumps. One charge pump inverts the supply voltage (SUPN) and provides a regulated negative output voltage. The second charge pump doubles the supply voltage (SUPP) and provides a regulated positive output voltage. The MAX1779 contains internal P-channel and N-channel MOSFETs to control the power transfer. The internal MOSFETs switch at a constant 125kHz (0.5 × fosc).

Negative Charge Pump

During the first half-cycle, the P-channel MOSFET turns on and the flying capacitor C5 charges to VSUPN minus a diode drop (Figure 2). During the second half-cycle, the P-channel MOSFET turns off, and the N-channel MOSFET turns on, level shifting C5. This connects C5 in parallel with the reservoir capacitor C6. If the voltage across C6 minus a diode drop is lower than the voltage across C5, charge flows from C5 to C6 until the diode (D5) turns off. The amount of charge transferred to the output is controlled by the variable N-channel on-resistance.

Positive Charge Pump

During the first half-cycle, the N-channel MOSFET turns on and charges the flying capacitor C3 (Figure 3). This initial charge is controlled by the variable N-channel on-resistance. During the second half-cycle, the N-channel MOSFET turns off and the P-channel MOSFET turns on, level shifting C3 by VSUPP volts. This connects C3 in parallel with the reservoir capacitor C4. If the voltage across C4 plus a diode drop (VPOS + VDIODE) is smaller than the level-shifted flying capacitor voltage

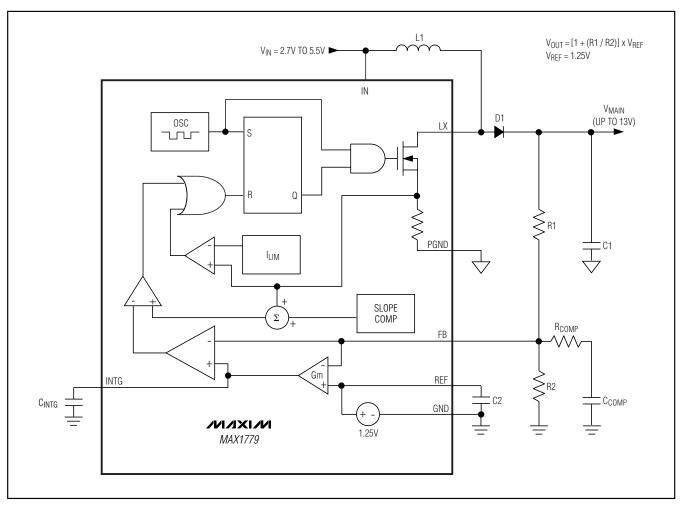


Figure 1. PWM Boost Converter Block Diagram

(VC3 + VSUPP), charge flows from C3 to C4 until the diode (D3) turns off.

Soft-Start

The main boost regulator does not have soft-start.

For the charge pumps, soft-start is achieved by controlling the rise rate of the output voltage. The output voltage regulates within 16ms, regardless of output capacitance and load, limited only by the regulator's output impedance (see the Startup Waveforms in the *Typical Operating Characteristics*).

Shutdown

A logic-low level on SHDN disables all three MAX1779 converters and the reference. When shut down, the supply current drops to 0.1µA to maximize battery life and the reference is pulled to ground. The output

capacitance and load current determine the rate at which each output voltage will decay. A logic-level high on SHDN activates the MAX1779 (see *Power-Up Sequencing*). Do not leave SHDN floating. If unused, connect SHDN to IN.

Power-Up Sequencing

Upon power-up or exiting shutdown, the MAX1779 starts a power-up sequence. First, the reference powers up. Then the main DC-DC step-up converter powers up. Once the main boost converter reaches regulation, the negative charge pump turns on. When the negative output voltage reaches approximately 90% of its nominal value (VFBN < 120mV), the positive charge pump starts up. Finally, when the positive output voltage reaches 90% of its nominal value (VFBP >

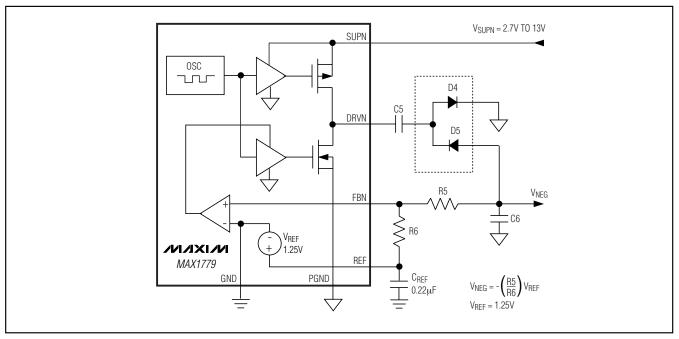


Figure 2. Negative Charge-Pump Block Diagram

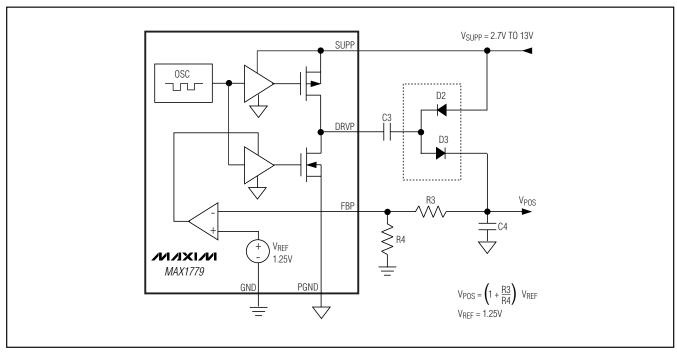


Figure 3. Positive Charge-Pump Block Diagram

1.125V), the active-low ready signal (RDY) is pulled low (see *Power Ready* section).

Power Ready

Power ready is an open-drain output. When the power-up sequence is properly completed, the MOSFET turns on and pulls \overline{RDY} low with a typical 125Ω on-resistance. If a fault is detected, the internal open-drain MOSFET appears as a high impedance. Connect a $100k\Omega$ pullup resistor between \overline{RDY} and IN for a logic-level output.

Fault Detection

Once \overline{RDY} is low, if any output falls below its fault-detection threshold, then \overline{RDY} becomes high impedance.

For the reference, the fault threshold is 1.05V. For the main boost converter, the fault threshold is 88% of its nominal value ($V_{FB} < 1.1V$). For the negative charge pump, the fault threshold is approximately 88% of its nominal value ($V_{FBN} < 140 \text{mV}$). For the positive charge pump, the fault threshold is 88% of its nominal value ($V_{FBP} < 1.11V$).

Once an output faults, all outputs later in the power sequence shut down until the faulted output rises above its power-up threshold. For example, if the negative charge-pump output voltage falls below the fault detection threshold, the main boost converter remains active while the positive charge pump stops switching and its output voltage decays, depending on output capacitance and load. The positive charge-pump output will not power up until the negative charge-pump output voltage rises above its power-up threshold (see the *Power-Up Sequencing* section).

Voltage Reference

The voltage at REF is nominally 1.25V. The reference can source up to 50µA with good load regulation (see *Typical Operating Characteristics*). Connect a 0.22µF bypass capacitor between REF and GND.

Design Procedure

Main Boost Converter

Inductor Selection

Inductor selection depends upon the minimum required inductance value, saturation rating, series resistance, and size. These factors influence the converter's efficiency, maximum output load capability, transient response time, and output voltage ripple. For most applications, values between 10µH and 33µH work best with the controller's switching frequency.

The inductor value depends on the maximum output load the application must support, input voltage, and

output voltage. With high inductor values, the MAX1779 sources higher output currents, has less output ripple, and enters continuous-conduction operation with lighter loads; however, the circuit's transient response time is slower. On the other hand, low-value inductors respond faster to transients, remain in discontinuous-conduction operation, and typically offer smaller physical size. The maximum output current an inductor value will support may be calculated by the following equations:

A. Continuous-conduction: if

$$I_{MAIN(MAX)} \ge \frac{1}{2} \left(\frac{V_{IN(MIN)}}{V_{MAIN}} \right) I_{LIM(MIN)}$$

then

$$L \ge \frac{1}{2} \left(\frac{1}{f} \right) \left(\frac{\mathsf{V}_{\mathsf{IN}(\mathsf{MIN})}}{\mathsf{V}_{\mathsf{MAIN}}} \right)^2 \left[\frac{\mathsf{V}_{\mathsf{MAIN}} \cdot \mathsf{V}_{\mathsf{N}(\mathsf{MIN})}}{\left(\left(\frac{\mathsf{V}_{\mathsf{IN}(\mathsf{MIN})}}{\mathsf{V}_{\mathsf{MAIN}}} \right) \mathsf{I}_{\mathsf{LIM}(\mathsf{MIN})} \right) \cdot \mathsf{I}_{\mathsf{MAIN}(\mathsf{MAX})} \right]$$

B. Discontinuous-conduction: if

$$I_{MAIN(MAX)} < \frac{1}{2} \left(\frac{V_{IN(MIN)}}{V_{MAIN}} \right) I_{LIM(MIN)}$$

then

$$\mathsf{L} \geq 2 \left(\frac{1}{f}\right) \left\lceil \frac{\mathsf{I}_{\mathsf{MAIN}(\mathsf{MAX})} \left(\mathsf{V}_{\mathsf{MAIN}} - \mathsf{V}_{\mathsf{IN}(\mathsf{MIN})}\right)}{\mathsf{I}_{\mathsf{LIM}(\mathsf{MIN})^2}} \right\rceil$$

where $I_{LIM(MIN)} = 350 \text{mA}$ and f = 250 kHz (see the *Electrical Characteristics*).

The inductor's saturation current rating should exceed peak inductor current throughout the normal operating range. Under fault conditions, the inductor current may reach up to 600mA (ILIM(MAX), see the *Electrical Characteristics*). However, the MAX1779's fast current-limit circuitry allows the use of soft-saturation inductors while still protecting the IC.

The inductor's DC resistance significantly affects efficiency due to the power loss in the inductor. The power loss due to the inductor's series resistance (PLR) may be approximated by the following equation:

$$P_{LR} \cong \left(\frac{I_{MAIN} \times V_{MAIN}}{V_{IN}}\right)^2 \times R_L$$

where R_L is the inductor's series resistance. For best performance, select inductors with resistance less than the internal N-channel MOSFET on-resistance (1 Ω typ).

Output Capacitor

The output capacitor selection depends on circuit stability and output voltage ripple. In order to deliver the maximum output current capability of the MAX1779, the inductor must run in continuous-conduction mode (see *Inductor Selection*). The minimum recommended output capacitance is:

$$C_{OUT} > \frac{60 \times L \times I_{MAIN(MAX)}}{V_{MAIN} \times V_{IN(MIN)}}$$

For configurations that need less output current, the MAX1779 allows lower output capacitance when operating in discontinuous-conduction mode throughout the load range. Under these conditions, at least $10\mu F$ is recommended, as shown in Figure 6. In both discontinuous and continuous operation, additional feedback compensation is required (see the Feedback Compensation section) to increase the margin for stability by reducing the bandwidth further. In cases where the output capacitance is sufficiently large, additional feedback compensation will not be necessary. However, in certain applications that require benign load transients and constantly operate in discontinuous-conduction mode, output capacitance less than $10\mu F$ may be used.

Output voltage ripple has two components: variations in the charge stored in the output capacitor with each LX pulse, and the voltage drop across the capacitor's equivalent series resistance (ESR) caused by the current into and out of the capacitor:

VRIPPLE = VRIPPLE(C) + VRIPPLE(ESR)

For low-value ceramic capacitors, the output voltage ripple is dominated by VRIPPLE(C).

Integrator Capacitor

The MAX1779 contains an internal current integrator that improves the DC load regulation but increases the peak-to-peak transient voltage (see the Load Transient Waveforms in the *Typical Operating Characteristics*). For highly accurate DC load regulation, enable the integrator by connecting a capacitor to INTG. The minimum capacitor value should be $C_{OUT}/10k$ or 1nF, whichever is greater. Alternatively, to minimize the peak-to-peak transient voltage at the expense of DC load regulation, disable the integrator by connecting INTG to REF and adding a $100k\Omega$ resistor to GND.

Feedback Compensation

Compensation on the feedback node is required to have enough margin for stability. Add a pole-zero pair from FB to GND in the form of a compensation resistor (R_{COMP} in Figures 5 and 6) in series with a compensation capacitor (C_{COMP} in Figures 5 and 6). For continuous conduction operation, select R_{COMP} to be 1/2 the value of R2, the low-side feedback resistor. For discontinuous-conduction operation, select R_{COMP} to be 1/5th the value of R2.

Start with a compensation capacitor value of (220pF × RCOMP)/10k Ω . Increase this value to improve the DC stability as necessary. Larger compensation values slow down the converter's response time. Check the startup waveform for excessive overshoot each time the compensation capacitor value is increased.

Charge Pump

Efficiency Considerations

The efficiency characteristics of the MAX1779 regulated charge pumps are similar to a linear regulator. They are dominated by quiescent current at low output currents and by the input voltage at higher output currents (see *Typical Operating Characteristics*). So the maximum efficiency may be approximated by:

Efficiency \cong |VNEG| / [VIN \times N]; for the negative charge pump

Efficiency \cong VPOS / [VIN × (N + 1)]; for the positive charge pump

where N is the number of charge-pump stages.

Output Voltage Selection

Adjust the positive output voltage by connecting a voltage-divider from the output (VPOS) to FBP to GND (see *Typical Operating Circuit*). Adjust the negative output voltage by connecting a voltage-divider from the output (VNEG) to FBN to REF. Select R4 and R6 in the $50\text{k}\Omega$ to $100\text{k}\Omega$ range. Higher resistor values improve efficiency at low output current but increase output voltage error due to the feedback input bias current. Calculate the remaining resistors with the following equations:

R3 = R4 [(VPOS / VREF) - 1]

 $R5 = R6 (V_{NEG} / V_{REF})$

where $V_{REF} = 1.25V$. V_{POS} may range from V_{SUPP} to +40V, and V_{NEG} may range from 0 to -40V.

Flying Capacitor

Increasing the flying capacitor's value increases the output current capability. Above a certain point, increasing the capacitance has a negligible effect because the output current capability becomes domi-

nated by the internal switch resistance and the diode impedance. Start with 0.1µF ceramic capacitors. Smaller values may be used for low-current applications.

Charge-Pump Output Capacitor

Increasing the output capacitance or decreasing the ESR reduces the output ripple voltage and the peak-to-peak transient voltage. Use the following equation to approximate the required capacitor value:

CPUMP ≥ [IPUMP / (125kHz × VRIPPLE)]

Charge-Pump Input Capacitor

Use a bypass capacitor with a value equal to or greater than the flying capacitor. Place the capacitor as close to the IC as possible. Connect directly to PGND.

Rectifier Diode

Use Schottky diodes with a current rating equal to or greater than 4 times the average output current, and a voltage rating at least 1.5 times V_{SUPP} for the positive charge pump and V_{SUPN} for the negative charge pump.

PC Board Layout and Grounding

Carefully printed circuit layout is extremely important to minimize ground bounce and noise. First, place the main boost converter output diode and output capacitor less than 0.2in (5mm) from the LX and PGND pins with wide traces and no vias. Then place 0.1µF ceramic bypass capacitors near the charge-pump input pins (SUPP and SUPN) to the PGND pin. Keep the chargepump circuitry as close to the IC as possible, using wide traces and avoiding vias when possible. Locate all feedback resistive dividers as close to their respective feedback pins as possible. The PC board should feature separate GND and PGND areas connected at only one point under the IC. To maximize output power and efficiency and to minimize output power ripple voltage, use extra wide power ground traces and solder the IC's power ground pin directly to it. Avoid having sensitive traces near the switching nodes and high-current lines.

Refer to the MAX1779 evaluation kit for an example of proper board layout.

Applications Information

LX Charge Pump

Some applications require multiple charge-pump stages due to low supply voltages. In order to reduce the circuit's size and component count, an unregulated charge pump may be added onto the LX switching node. The configuration shown in Figure 4 works well for most applications. The maximum output current of the low-power charge pumps depends on the maximum

mum load current that the LX charge pump can provide and is limited by the following formula:

 $I_{LXPUMP} = ((N + 1) \times I_{POS}) + (M + I_{NEG}) \le 5mA$

where N is the number of stages in the positive low-power charge pump, and M is the number of stages in the negative charge pump. Applications requiring more output current should not use the LX charge pump, so they will require extra stages on both low-power charge pumps. The output capacitor of this unregulated charge pump needs to be stacked on top of the main output in order to keep the main regulator stable. Increasing the integrator capacitor may also be required to compensate for the additional charge-pump capacitance on the main regulator loop.

The output capacitor of this unregulated charge pump needs to be stacked on top of the main output in order to keep the main regulator stable. Increasing the integrator capacitor may also be required to compensate for the additional charge-pump capacitance on the main regulator loop.

Table 1. Component Suppliers

SUPPLIER	PHONE	FAX
INDUCTORS		
Coilcraft	847-639-6400	847-639-1469
Coiltronics	561-241-7876	561-241-9339
Sumida USA	847-956-0666	847-956-0702
Toko	847-297-0070	847-699-1194
CAPACITORS		
AVX	803-946-0690	803-626-3123
Kemet	408-986-0424	408-986-1442
Sanyo	619-661-6835	619-661-1055
Taiyo Yuden	408-573-4150	408-573-4159
DIODES		
Central Semiconductor	516-435-1110	516-435-1824
International Rectifier	310-322-3331	310-322-3332
Motorola	602-303-5454	602-994-6430
Nihon	847-843-7500	847-843-2798
Zetex	516-543-7100	516-864-7630

_Chip Information

TRANSISTOR COUNT: 2846

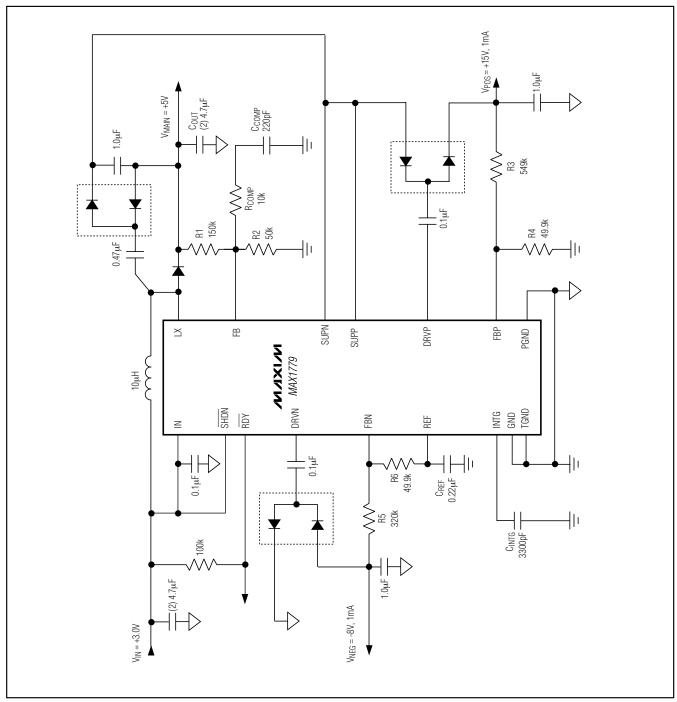


Figure 4. Minimizing the Number of Charge-Pump Stages

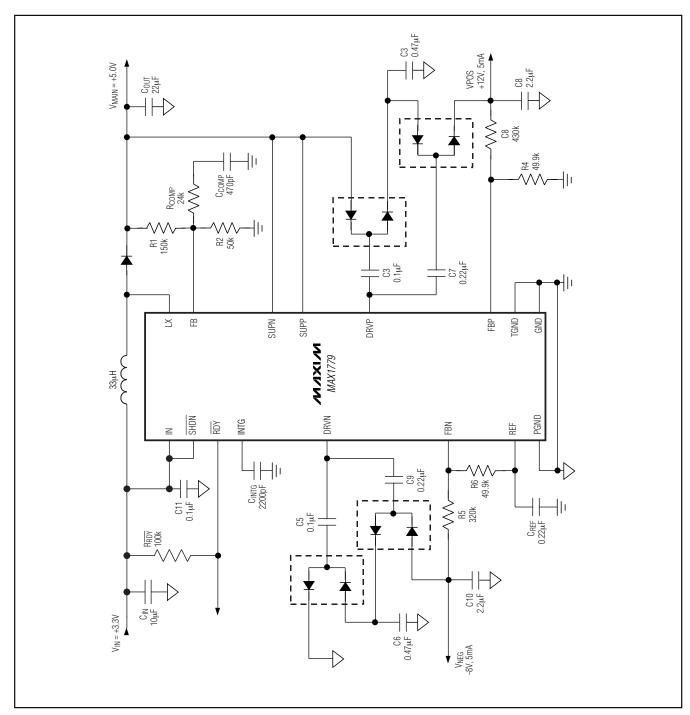


Figure 5. Typical Operating Circuit ($L = 33\mu H$)

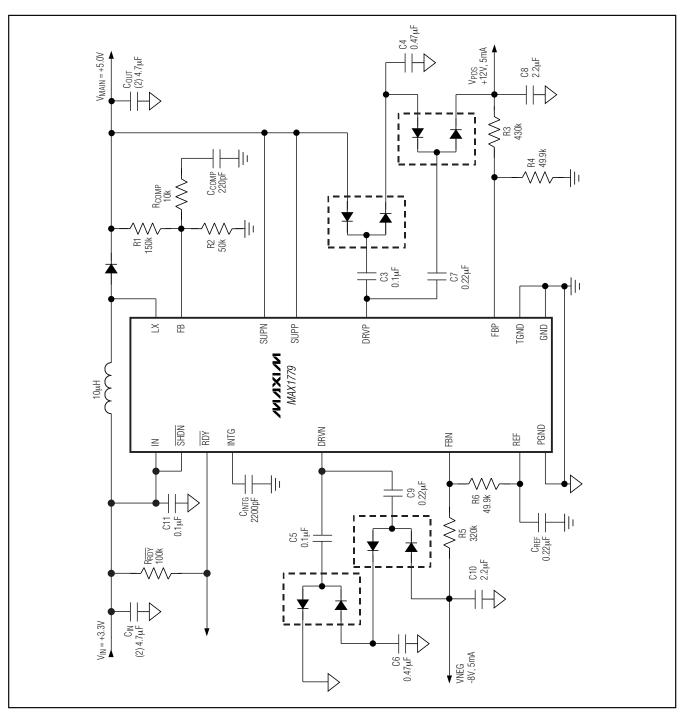
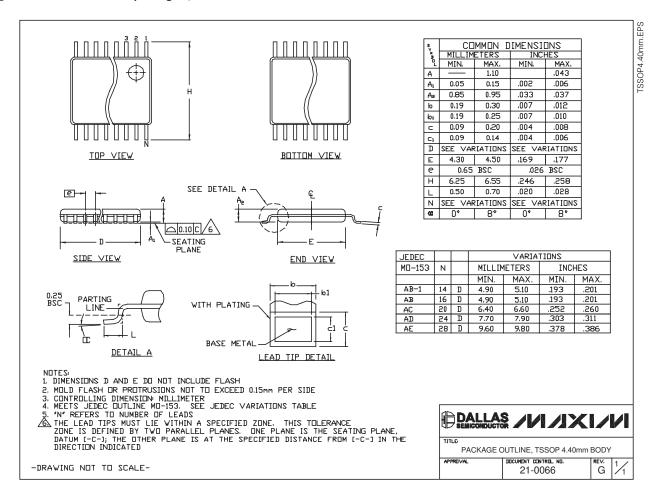


Figure 6. Typical Operating Circuit (L = 10µH)

Package Information

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information go to www.maxim-ic.com/packages.)



Note: The MAX1779 16-pin TSSOP package does not have an exposed pad.

Maxim cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Maxim product. No circuit patent licenses are implied. Maxim reserves the right to change the circuitry and specifications without notice at any time.