

## CSD87352Q5D Synchronous Buck NexFET™ Power Block

### 1 Features

- Half-Bridge Power Block
- 91% System Efficiency at 15 A
- Up to 25-A Operation
- High-Frequency Operation (up to 1.5 MHz)
- High-Density SON 5-mm × 6-mm Footprint
- Optimized for 5-V Gate Drive
- Low-Switching Losses
- Ultra-Low-Inductance Package
- RoHS Compliant
- Halogen Free
- Lead-Free Terminal Plating

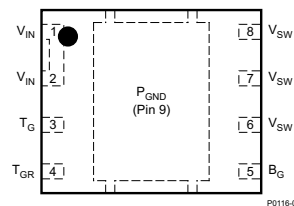
### 2 Applications

- Synchronous Buck Converters
  - High-Frequency Applications
  - High-Current, Low-Duty Cycle Applications
- Multiphase Synchronous Buck Converters
- POL DC-DC Converters
- IMVP, VRM, and VRD Applications

### 3 Description

The CSD87352Q5D NexFET™ power block is an optimized design for synchronous buck applications offering high-current, high-efficiency, and high-frequency capability in a small 5-mm × 6-mm outline. Optimized for 5-V gate drive applications, this product offers a flexible solution capable of offering a high-density power supply when paired with any 5-V gate drive from an external controller/driver.

#### Top View

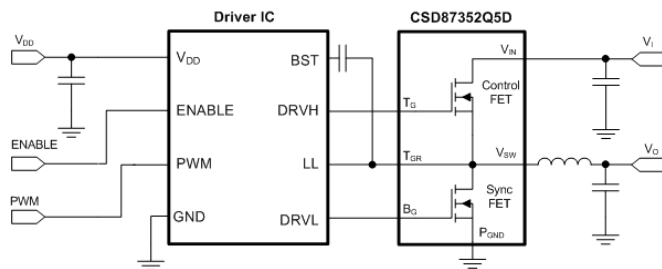


#### Device Information(1)

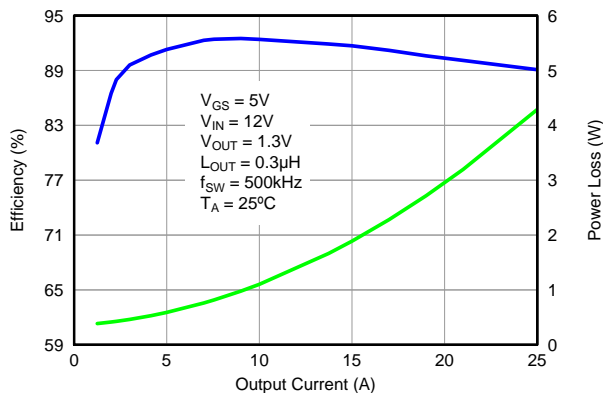
DEVICE	MEDIA	QTY	PACKAGE	SHIP
CSD87352Q5D	13-Inch Reel	2500	SON 5.00-mm × 6.00-mm Plastic Package	Tape and Reel

(1) For all available packages, see the orderable addendum at the end of the data sheet.

#### Typical Circuit



#### Typical Power Block Efficiency and Power Loss



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## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision C (January 2012) to Revision D</b>	<b>Page</b>
• Added note 2 to the <i>Absolute Maximum Ratings</i> table .....	3
• Changed <i>Recommended PCB Design Overview</i> section to <i>Layout</i> section .....	15
• Added the <i>Device and Documentation Support</i> section .....	17
• Changed <i>Mechanical Data</i> section to <i>Mechanical, Packaging, and Orderable Information</i> section .....	18

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<b>Changes from Revision B (October 2011) to Revision C</b>	<b>Page</b>
• Changed Features bullet From: Up to 35 A Operation To: Up to 25 A Operation .....	1

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<b>Changes from Revision A (September 2011) to Revision B</b>	<b>Page</b>
• Changed <a href="#">Figure 5</a> .....	5
• Changed "DIM a" Millimeter Max value From: 1.55 To: 1.5 and Inches Max value From: 0.061 To: 0.059 .....	18

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<b>Changes from Original (June 2011) to Revision A</b>	<b>Page</b>
• Remove $Z_{DS(on)}$ Max .....	4
• Remove $Z_{DS(on)}$ Max .....	12
• Add Electrical Performance bullet .....	15

## 5 Specifications

### 5.1 Absolute Maximum Ratings

 $T_A = 25^\circ\text{C}$  (unless otherwise noted) <sup>(1)</sup>

PARAMETER	CONDITIONS	MIN	MAX	UNIT
Voltage	$V_{IN}$ to $P_{GND}$	30		V
	$V_{SW}$ to $P_{GND}$	30		
	$V_{SW}$ to $P_{GND}$ (10 ns)	32		
	$T_G$ to $T_{GR}$	-8	10	
	$B_G$ to $P_{GND}$	-8	10	
Pulsed current rating, $I_{DM}$ <sup>(2)</sup>		60		A
Power dissipation, $P_D$		8.5		W
Avalanche energy, $E_{AS}$	Sync FET, $I_D = 65$ A, $L = 0.1$ mH	211		mJ
	Control FET, $I_D = 37$ A, $L = 0.1$ mH	68		
Operating junction, $T_J$		-55	150	$^\circ\text{C}$
Storage temperature, $T_{STG}$		-55	150	$^\circ\text{C}$

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Pulse duration  $\leq 50$   $\mu\text{s}$ . Duty cycle  $\leq 0.01\%$ .

### 5.2 Recommended Operating Conditions

 $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER	CONDITIONS	MIN	MAX	UNIT
Gate drive voltage, $V_{GS}$		4.5	8	V
Input supply voltage, $V_{IN}$			27	V
Switching frequency, $f_{SW}$	$C_{BST} = 0.1$ $\mu\text{F}$ (min)		1500	kHz
Operating current			25	A
Operating temperature, $T_J$			125	$^\circ\text{C}$

### 5.3 Power Block Performance

 $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
Power loss, $P_{LOSS}$ <sup>(1)</sup>	$V_{IN} = 12$ V, $V_{GS} = 5$ V, $V_{OUT} = 1.3$ V, $I_{OUT} = 15$ A, $f_{SW} = 500$ kHz, $L_{OUT} = 0.3$ $\mu\text{H}$ , $T_J = 25^\circ\text{C}$		1.8		W
$V_{IN}$ quiescent current, $I_{QVIN}$	$T_G$ to $T_{GR} = 0$ V $B_G$ to $P_{GND} = 0$ V		10		$\mu\text{A}$

- (1) Measurement made with six 10- $\mu\text{F}$  (TDK C3216X5R1C106KT or equivalent) ceramic capacitors placed across  $V_{IN}$  to  $P_{GND}$  pins and using a high-current 5-V driver IC.

### 5.4 Thermal Information

 $T_A = 25^\circ\text{C}$  (unless otherwise stated)

THERMAL METRIC		MIN	TYP	MAX	UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance (min Cu) <sup>(1)(2)</sup>			150	$^\circ\text{C/W}$
	Junction-to-ambient thermal resistance (max Cu) <sup>(1)(2)</sup>			82	
$R_{\theta JC}$	Junction-to-case thermal resistance (top of package) <sup>(2)</sup>			33	$^\circ\text{C/W}$
	Junction-to-case thermal resistance ( $P_{GND}$ pin) <sup>(2)</sup>			2.8	

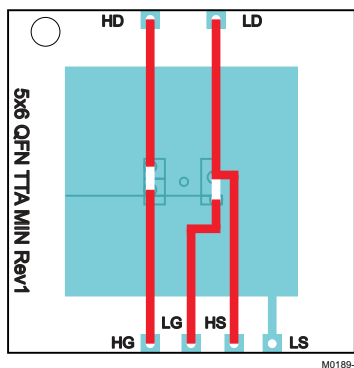
- (1) Device mounted on FR4 material with 1-in<sup>2</sup> (6.45-cm<sup>2</sup>) Cu.
- (2)  $R_{\theta JC}$  is determined with the device mounted on a 1-in<sup>2</sup> (6.45-cm<sup>2</sup>), 2-oz (0.071-mm) thick Cu pad on a 1.5-in  $\times$  1.5-in (3.81-cm  $\times$  3.81-cm), 0.06-in (1.52-mm) thick FR4 board.  $R_{\theta JC}$  is specified by design while  $R_{\theta JA}$  is determined by the user's board design.

## 5.5 Electrical Characteristics

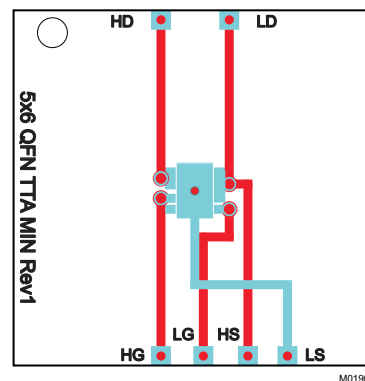
 $T_A = 25^\circ\text{C}$  (unless otherwise stated)

PARAMETER		TEST CONDITIONS	Q1 Control FET			Q2 Sync FET			UNIT	
			MIN	TYP	MAX	MIN	TYP	MAX		
<b>STATIC CHARACTERISTICS</b>										
$BV_{DSS}$	Drain-to-source voltage	$V_{GS} = 0\text{ V}, I_{DS} = 250\ \mu\text{A}$	30			30			V	
$I_{DSS}$	Drain-to-source leakage current	$V_{GS} = 0\text{ V}, V_{DS} = 24\text{ V}$			1			1	$\mu\text{A}$	
$I_{GSS}$	Gate-to-source leakage current	$V_{DS} = 0\text{ V}, V_{GS} = +10 / -8\text{ V}$			100			100	nA	
$V_{GS(th)}$	Gate-to-source threshold voltage	$V_{DS} = V_{GS}, I_{DS} = 250\ \mu\text{A}$	1		2.1	0.75		1.15	V	
$Z_{DS(on)}^{(1)}$	Effective AC on-impedance	$V_{IN} = 12\text{ V}, V_{GS} = 5\text{ V}, V_{OUT} = 1.3\text{ V}, I_{OUT} = 15\text{ A}, f_{SW} = 500\text{ kHz}, L_{OUT} = 0.3\ \mu\text{H}, T_J = 25^\circ\text{C}$			9			2.8	$\text{m}\Omega$	
$g_{fs}$	Transconductance	$V_{DS} = 15\text{ V}, I_{DS} = 15\text{ A}$			51			87	S	
<b>DYNAMIC CHARACTERISTICS</b>										
$C_{ISS}$	Input capacitance	$V_{GS} = 0\text{ V}, V_{DS} = 15\text{ V}, f = 1\text{ MHz}$			740	890		1500	1800	pF
$C_{OSS}$	Output capacitance				315	380		645	775	pF
$C_{RSS}$	Reverse transfer capacitance				12	14		38	46	pF
$R_G$	Series gate resistance			1.2	2.4		0.6	1.2	$\Omega$	
$Q_g$	Gate charge total (4.5 V)	$V_{DS} = 15\text{ V}, I_{DS} = 15\text{ A}$			4.6	5.5		10.4	12.5	nC
$Q_{gd}$	Gate charge gate-to-drain				0.9			1.9		nC
$Q_{gs}$	Gate charge gate-to-source				1.5			2.2		nC
$Q_{g(th)}$	Gate charge at $V_{th}$				0.9			1.2		nC
$Q_{OSS}$	Output charge	$V_{DS} = 9.8\text{ V}, V_{GS} = 0\text{ V}$			6.6			13		nC
$t_{d(on)}$	Turnon delay time	$V_{DS} = 15\text{ V}, V_{GS} = 4.5\text{ V}, I_{DS} = 15\text{ A}, R_G = 2\ \Omega$			5.4			6.1		ns
$t_r$	Rise time				11			7		ns
$t_{d(off)}$	Turnoff delay time				9.5			16		ns
$t_f$	Fall time				2			2.7		ns
<b>DIODE CHARACTERISTICS</b>										
$V_{SD}$	Diode forward voltage	$I_{DS} = 15\text{ A}, V_{GS} = 0\text{ V}$			0.8			0.8		V
$Q_{rr}$	Reverse recovery charge	$V_{dd} = 9.8\text{ V}, I_F = 15\text{ A}, di/dt = 300\text{ A}/\mu\text{s}$			11.3			16.3		nC
$t_{rr}$	Reverse recovery time				16			20		ns

(1) Equivalent system performance based on application testing. See [Application and Implementation](#) for details.



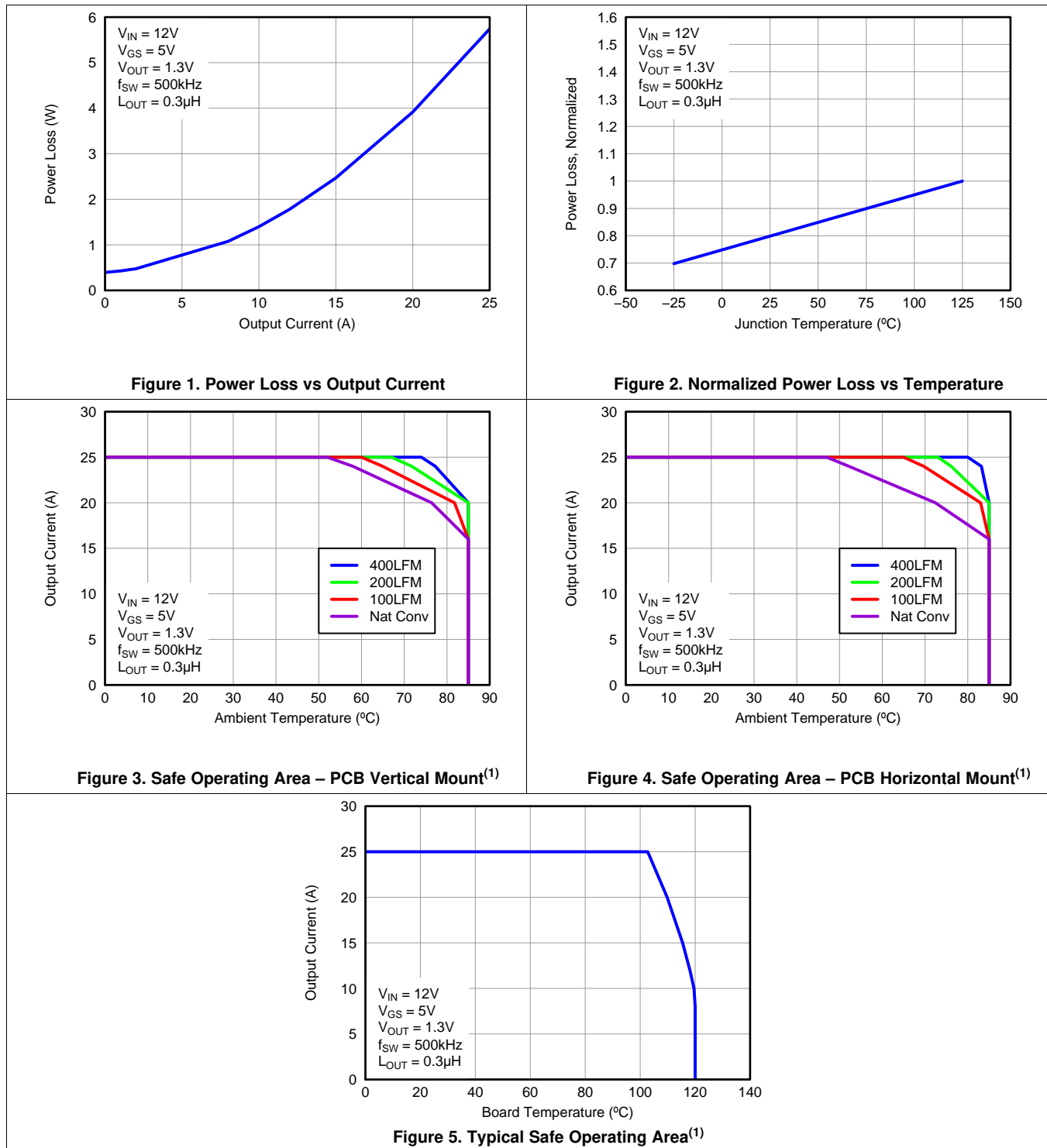
Max  $R_{\theta JA} = 82^\circ\text{C}/\text{W}$   
when mounted on  
1 in<sup>2</sup> (6.45 cm<sup>2</sup>) of 2-  
oz (0.071-mm) thick  
Cu.



Max  $R_{\theta JA} = 150^\circ\text{C}/\text{W}$   
when mounted on  
minimum pad area of  
2-oz (0.071-mm) thick  
Cu.

## 5.6 Typical Power Block Device Characteristics

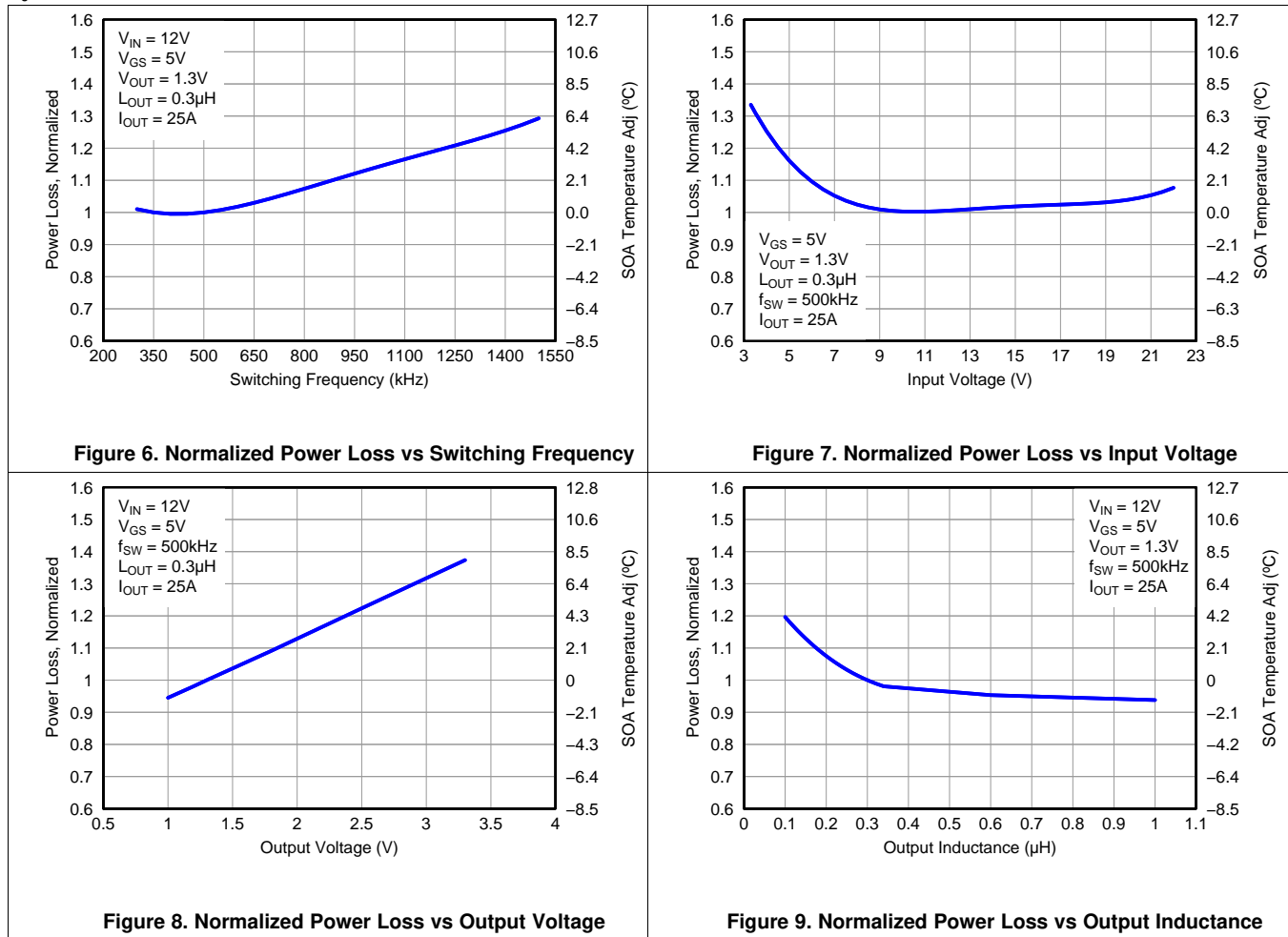
$T_j = 125^\circ\text{C}$ , unless stated otherwise.



(1) The typical power block system characteristic curves are based on measurements made on a PCB design with dimensions of 4 in (W)  $\times$  3.5 in (L)  $\times$  0.062 in (H) and 6 copper layers of 1-oz copper thickness. See [Application and Implementation](#) section for detailed explanation.

### Typical Power Block Device Characteristics (continued)

$T_J = 125^\circ\text{C}$ , unless stated otherwise.



### 5.7 Typical Power Block MOSFET Characteristics

$T_A = 25^\circ\text{C}$ , unless stated otherwise.

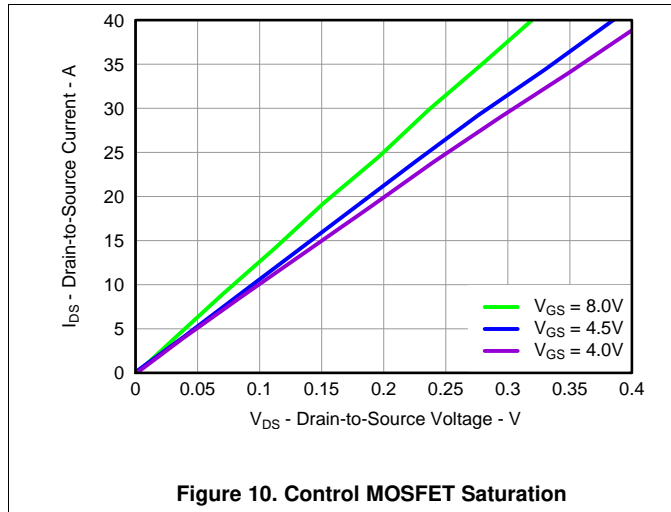


Figure 10. Control MOSFET Saturation

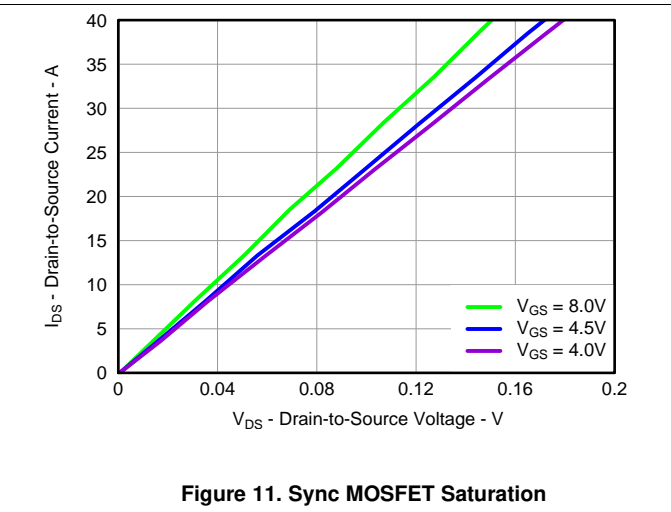


Figure 11. Sync MOSFET Saturation

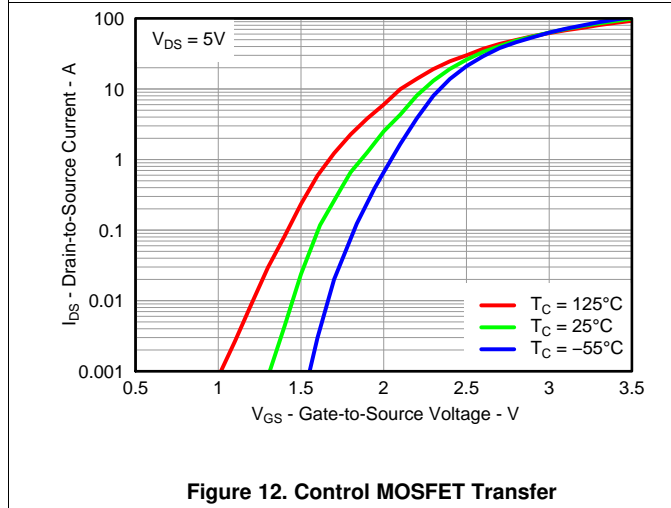


Figure 12. Control MOSFET Transfer

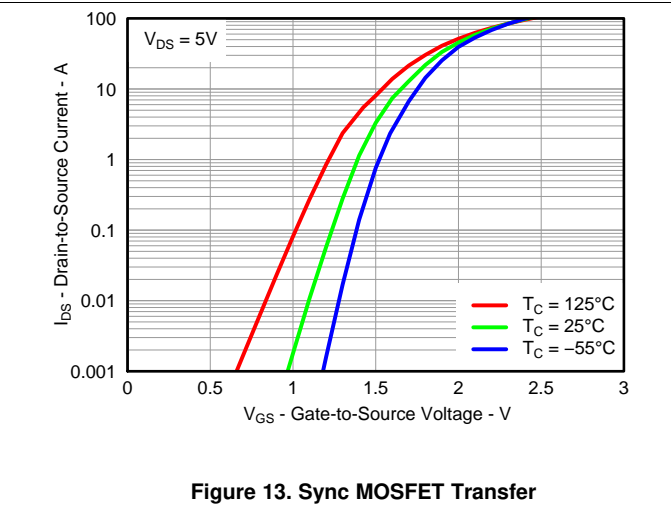


Figure 13. Sync MOSFET Transfer

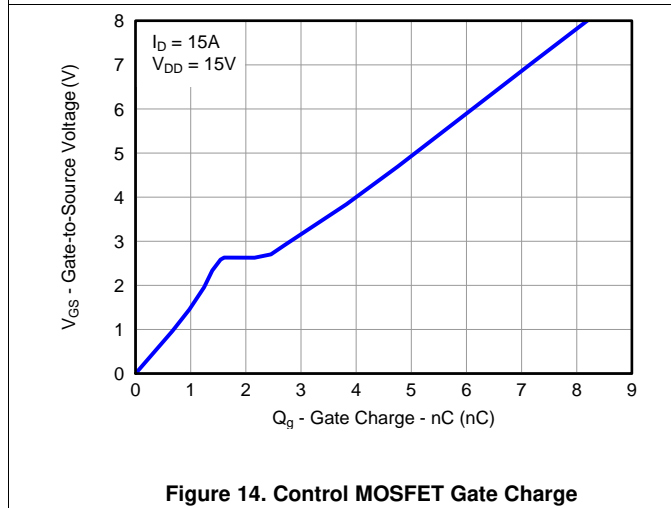


Figure 14. Control MOSFET Gate Charge

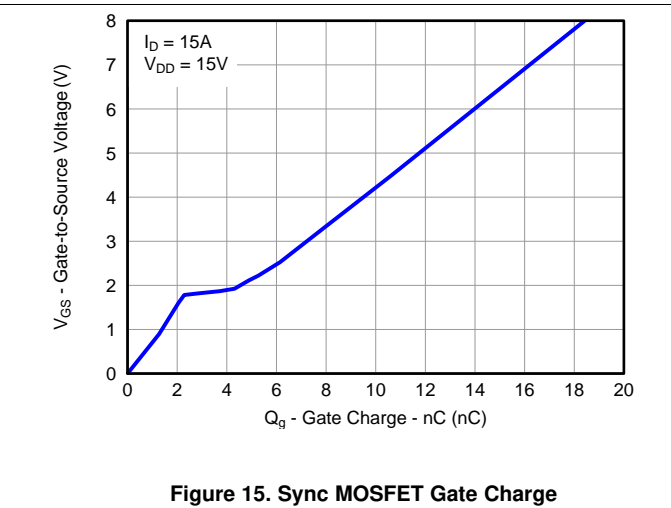


Figure 15. Sync MOSFET Gate Charge

Typical Power Block MOSFET Characteristics (continued)

T<sub>A</sub> = 25°C, unless stated otherwise.

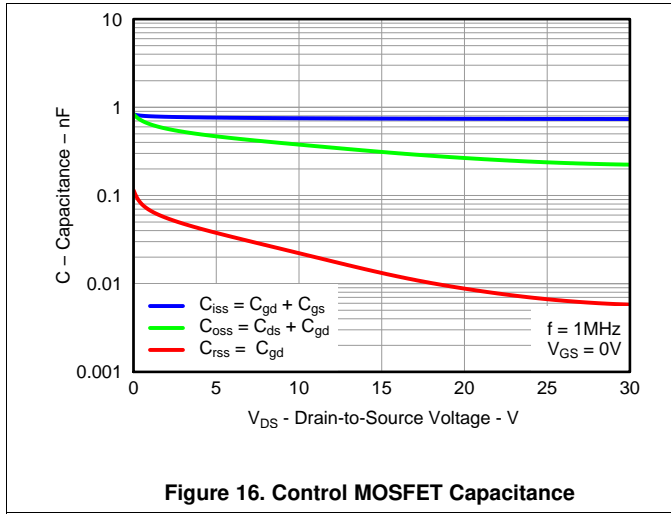


Figure 16. Control MOSFET Capacitance

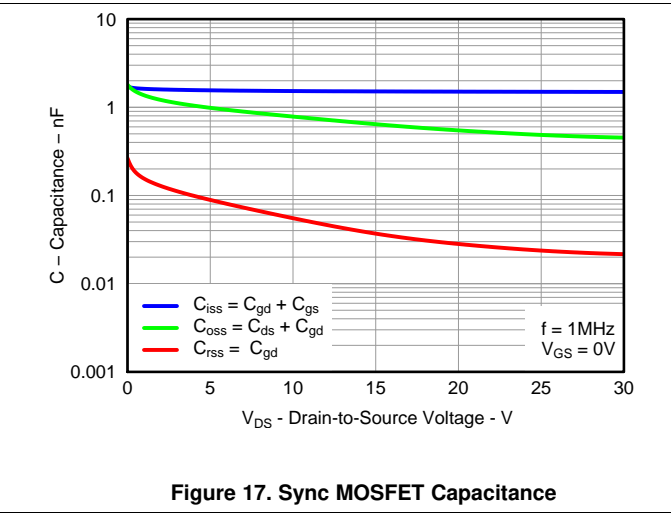


Figure 17. Sync MOSFET Capacitance

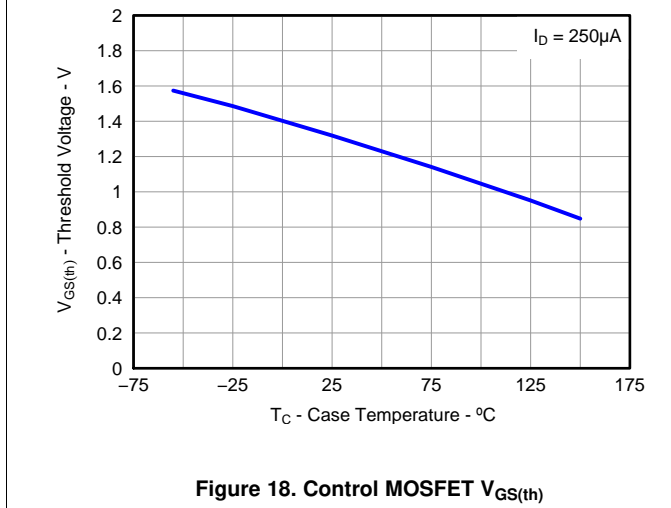


Figure 18. Control MOSFET V<sub>GS(th)</sub>

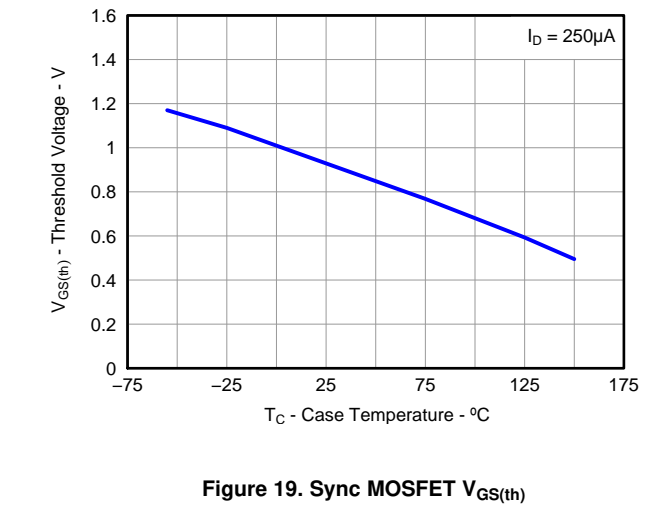


Figure 19. Sync MOSFET V<sub>GS(th)</sub>

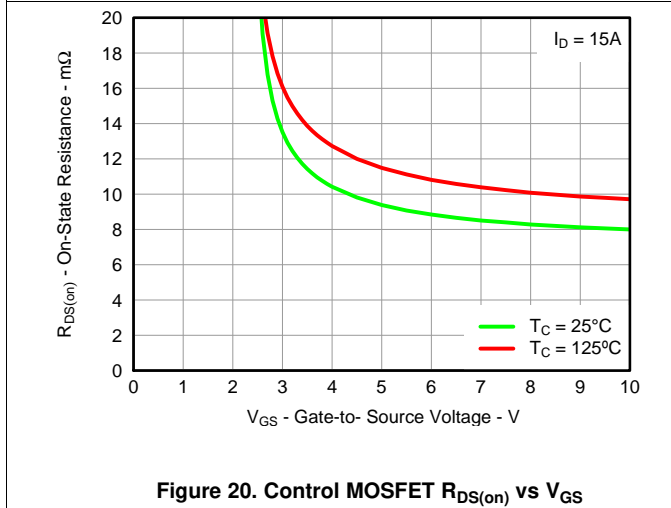


Figure 20. Control MOSFET R<sub>DS(on)</sub> vs V<sub>GS</sub>

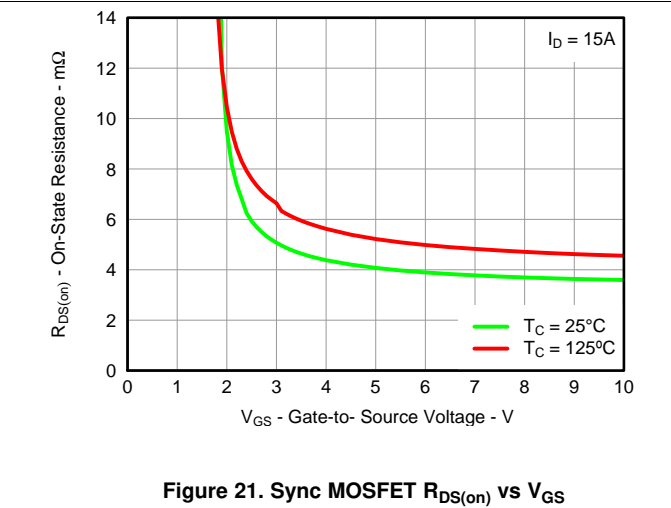


Figure 21. Sync MOSFET R<sub>DS(on)</sub> vs V<sub>GS</sub>



Typical Power Block MOSFET Characteristics (continued)

$T_A = 25^\circ\text{C}$ , unless stated otherwise.

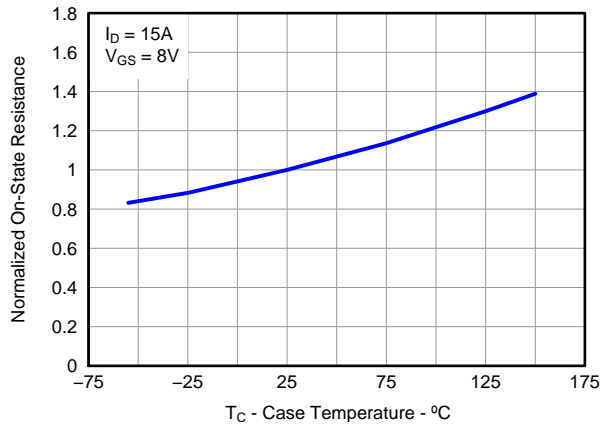


Figure 22. Control MOSFET Normalized  $R_{DS(on)}$

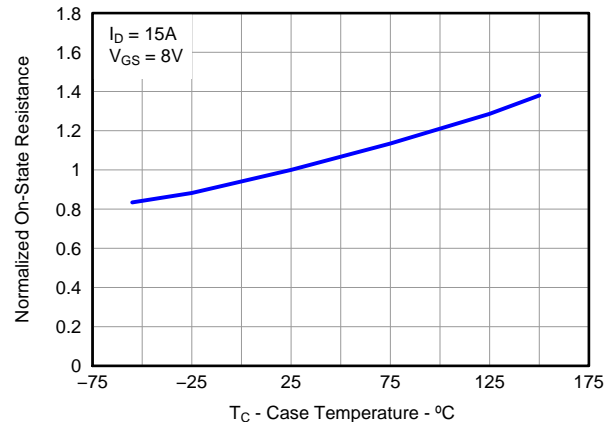


Figure 23. Sync MOSFET Normalized  $R_{DS(on)}$

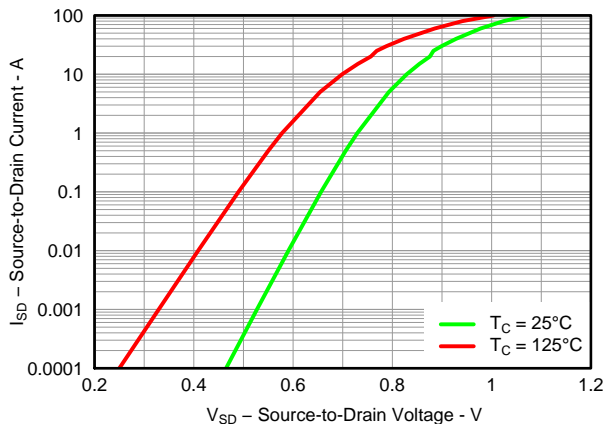


Figure 24. Control MOSFET Body Diode

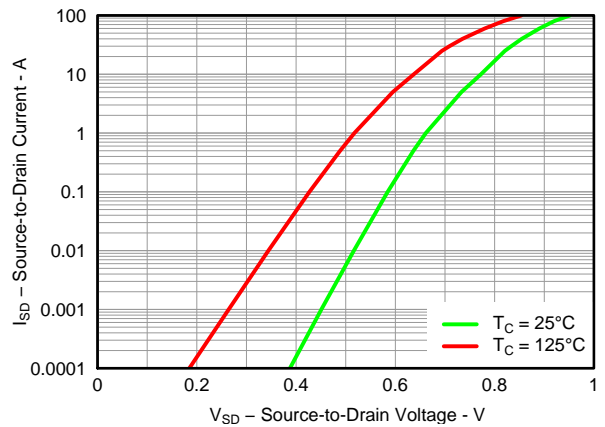


Figure 25. Sync MOSFET Body Diode

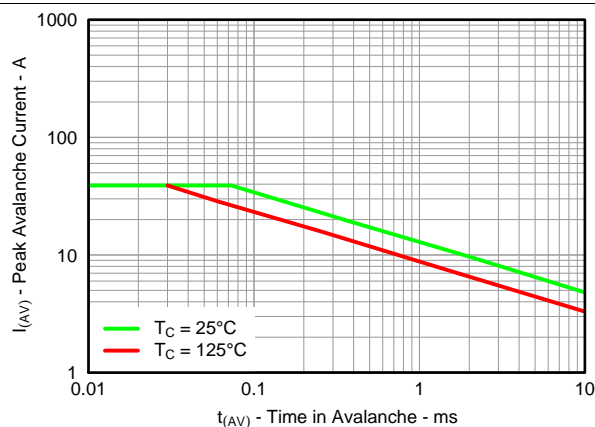


Figure 26. Control MOSFET Unclamped Inductive Switching

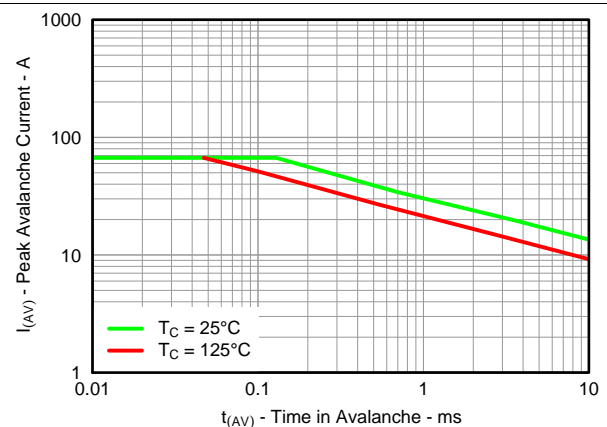


Figure 27. Sync MOSFET Unclamped Inductive Switching

## 6 Application and Implementation

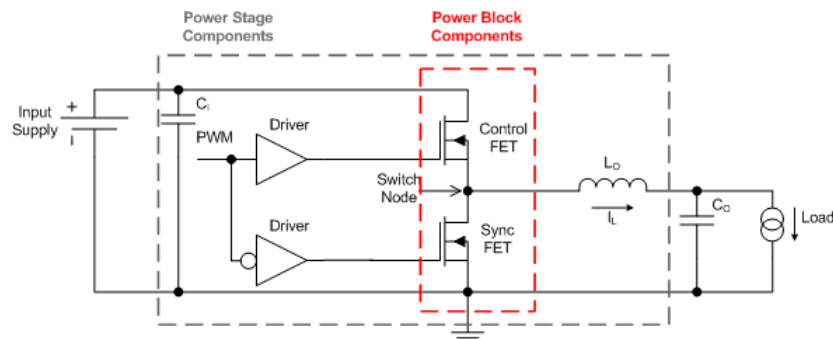
### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 6.1 Application Information

#### 6.1.1 Equivalent System Performance

Many of today's high-performance computing systems require low power consumption in an effort to reduce system operating temperatures and improve overall system efficiency. This has created a major emphasis on improving the conversion efficiency of today's synchronous buck topology. In particular, there has been an emphasis in improving the performance of the critical power semiconductor in the power stage of this application (see [Figure 28](#)). As such, optimization of the power semiconductors in these applications, needs to go beyond simply reducing  $R_{DS(ON)}$ .



**Figure 28. Equivalent System Schematic**

The CSD87352Q5D is part of TI's power block product family which is a highly optimized product for use in a synchronous buck topology requiring high current, high efficiency, and high frequency. It incorporates TI's latest generation silicon which has been optimized for switching performance, as well as minimizing losses associated with  $Q_{GD}$ ,  $Q_{GS}$ , and  $Q_{RR}$ . Furthermore, TI's patented packaging technology has minimized losses by nearly eliminating parasitic elements between the control FET and sync FET connections (see [Figure 29](#)). A key challenge solved by TI's patented packaging technology is the system level impact of Common Source Inductance (CSI). CSI greatly impedes the switching characteristics of any MOSFET which in turn increases switching losses and reduces system efficiency. As a result, the effects of CSI need to be considered during the MOSFET selection process. In addition, standard MOSFET switching loss equations used to predict system efficiency need to be modified in order to account for the effects of CSI. Further details behind the effects of CSI and modification of switching loss equations are outlined in [Power Loss Calculation With Common Source Inductance Consideration for Synchronous Buck Converters](#) (SLPA009).

Application Information (continued)

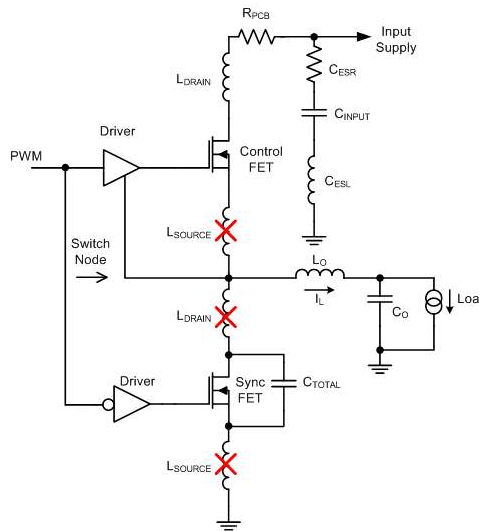


Figure 29. Elimination of Parasitic Inductances

The combination of TI's latest generation silicon and optimized packaging technology has created a benchmarking solution that outperforms industry standard MOSFET chipsets of similar  $R_{DS(ON)}$  and MOSFET chipsets with lower  $R_{DS(ON)}$ . Figure 30 and Figure 31 compare the efficiency and power loss performance of the CSD87352Q5D versus industry standard MOSFET chipsets commonly used in this type of application. This comparison purely focuses on the efficiency and generated loss of the power semiconductors only. The performance of CSD87352Q5D clearly highlights the importance of considering AC on-impedance ( $Z_{DS(ON)}$ ) during the MOSFET selection process of any new design. Simply normalizing to traditional MOSFET  $R_{DS(ON)}$  specifications is not an indicator of the actual in-circuit performance when using TI's power block technology.

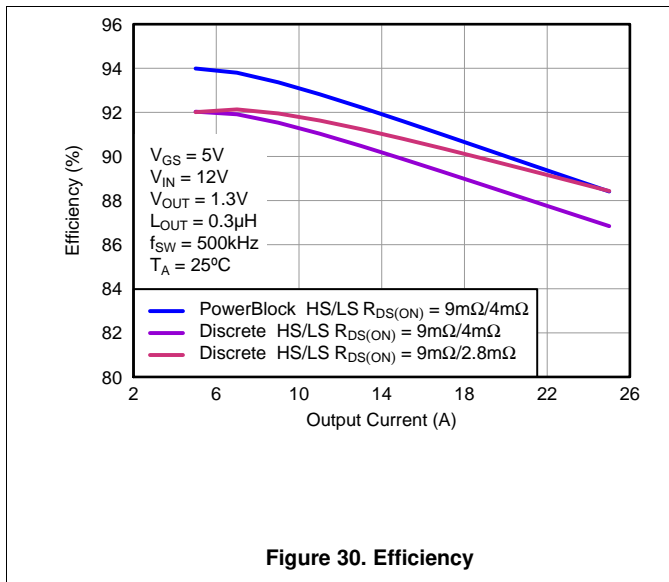


Figure 30. Efficiency

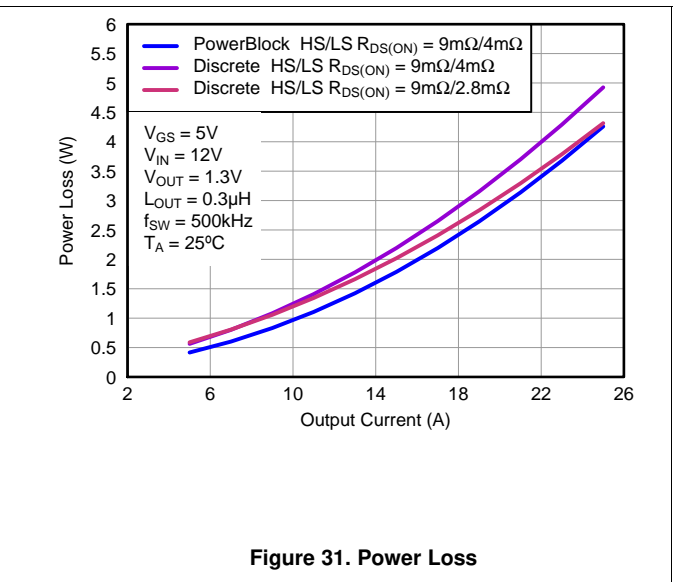


Figure 31. Power Loss

## Application Information (continued)

The chart below compares the traditional DC measured  $R_{DS(ON)}$  of CSD87352Q5D versus its  $Z_{DS(ON)}$ . This comparison takes into account the improved efficiency associated with TI's patented packaging technology. As such, when comparing TI's power block products to individually packaged discrete MOSFETs or dual MOSFETs in a standard package, the in-circuit switching performance of the solution must be considered. In this example, individually packaged discrete MOSFETs or dual MOSFETs in a standard package would need to have DC measured  $R_{DS(ON)}$  values that are equivalent to CSD87352Q5D's  $Z_{DS(ON)}$  value in order to have the same efficiency performance at full load. Mid to light-load efficiency will still be lower with individually packaged discrete MOSFETs or dual MOSFETs in a standard package.

**Table 1. Comparison of  $R_{DS(ON)}$  vs  $Z_{DS(ON)}$**

PARAMETER	HS		LS	
	TYP	MAX	TYP	MAX
Effective AC on-impedance $Z_{DS(ON)}$ ( $V_{GS} = 5\text{ V}$ )	9	—	2.8	—
DC measured $R_{DS(ON)}$ ( $V_{GS} = 4.5\text{ V}$ )	9	10.8	4	4.8

The CSD87352Q5D NexFET™ power block is an optimized design for synchronous buck applications using 5-V gate drive. The control FET and sync FET silicon are parametrically tuned to yield the lowest power loss and highest system efficiency. As a result, a new rating method is needed which is tailored towards a more systems-centric environment. System-level performance curves such as power loss, Safe Operating Area (SOA), and normalized graphs allow engineers to predict the product performance in the actual application.

### 6.1.2 Power Loss Curves

MOSFET centric parameters such as  $R_{DS(ON)}$  and  $Q_{gd}$  are needed to estimate the loss generated by the devices. In an effort to simplify the design process for engineers, Texas Instruments has provided measured power loss performance curves. [Figure 1](#) plots the power loss of the CSD87352Q5D as a function of load current. This curve is measured by configuring and running the CSD87352Q5D as it would be in the final application (see [Figure 32](#)). The measured power loss is the CSD87352Q5D loss and consists of both input conversion loss and gate drive loss. [Equation 1](#) is used to generate the power loss curve.

$$\text{Power loss} = (V_{IN} \times I_{IN}) + (V_{DD} \times I_{DD}) - (V_{SW\_AVG} \times I_{OUT}) \quad (1)$$

The power loss curve in [Figure 1](#) is measured at the maximum recommended junction temperatures of 125°C under isothermal test conditions.

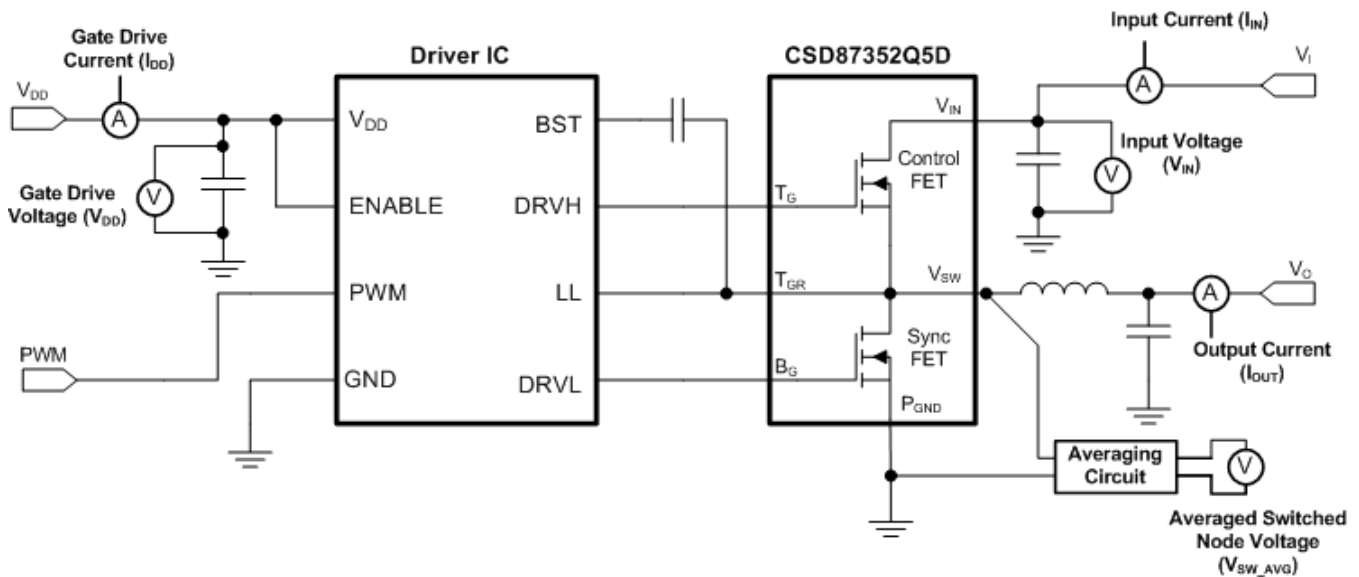
### 6.1.3 Safe Operating Area (SOA) Curves

The SOA curves in the CSD87352Q5D data sheet provides guidance on the temperature boundaries within an operating system by incorporating the thermal resistance and system power loss. [Figure 3](#) to [Figure 5](#) outline the temperature and airflow conditions required for a given load current. The area under the curve dictates the safe operating area. All the curves are based on measurements made on a PCB design with dimensions of 4 in (W) x 3.5 in (L) x 0.062 in (T) and 6 copper layers of 1-oz copper thickness.

### 6.1.4 Normalized Curves

The normalized curves in the CSD87352Q5D data sheet provides guidance on the power loss and SOA adjustments based on their application specific needs. These curves show how the power loss and SOA boundaries will adjust for a given set of systems conditions. The primary Y-axis is the normalized change in power loss and the secondary Y-axis is the change in system temperature required in order to comply with the SOA curve. The change in power loss is a multiplier for the power loss curve and the change in temperature is subtracted from the SOA curve.

## 6.2 Typical Application



**Figure 32. Typical Application**

### 6.2.1 Calculating Power Loss and SOA

The user can estimate product loss and SOA boundaries by arithmetic means (see [Design Example](#)). Though the power loss and SOA curves in this data sheet are taken for a specific set of test conditions, the following procedure will outline the steps the user should take to predict product performance for any set of system conditions.

#### 6.2.1.1 Design Example

Operating conditions:

- Output current = 15 A
- Input voltage = 7 V
- Output voltage = 1 V
- Switching frequency = 800 kHz
- Inductor = 0.2  $\mu$ H

#### 6.2.1.2 Calculating Power Loss

- Power loss at 15 A = 2.5 W ([Figure 1](#))
- Normalized power loss for input voltage  $\approx$  1.05 ([Figure 7](#))
- Normalized power loss for output voltage  $\approx$  0.95 ([Figure 8](#))
- Normalized power loss for switching frequency  $\approx$  1.08 ([Figure 6](#))
- Normalized power loss for output inductor  $\approx$  1.07 ([Figure 9](#))
- **Final calculated Power Loss = 2.5 W  $\times$  1.05  $\times$  0.95  $\times$  1.08  $\times$  1.07  $\approx$  2.88 W**

#### 6.2.1.3 Calculating SOA Adjustments

- SOA adjustment for input voltage  $\approx$  1.05°C ([Figure 7](#))
- SOA adjustment for output voltage  $\approx$  -1.05°C ([Figure 8](#))
- SOA adjustment for switching frequency  $\approx$  1.8°C ([Figure 6](#))
- SOA adjustment for output inductor  $\approx$  1.7°C ([Figure 9](#))
- **Final calculated SOA adjustment = 1.05 + (-1.05) + 1.8 + 1.7  $\approx$  3.5°C**

### Typical Application (continued)

In the design example above, the estimated power loss of the CSD87352Q5D would increase to 2.88 W. In addition, the maximum allowable board and/or ambient temperature would have to decrease by 3.5°C. Figure 33 graphically shows how the SOA curve would be adjusted accordingly.

1. Start by drawing a horizontal line from the application current to the SOA curve.
2. Draw a vertical line from the SOA curve intercept down to the board/ambient temperature.
3. Adjust the SOA board/ambient temperature by subtracting the temperature adjustment value.

In the design example, the SOA temperature adjustment yields a reduction in allowable board/ambient temperature of 3.5°C. In the event the adjustment value is a negative number, subtracting the negative number would yield an increase in allowable board/ambient temperature.

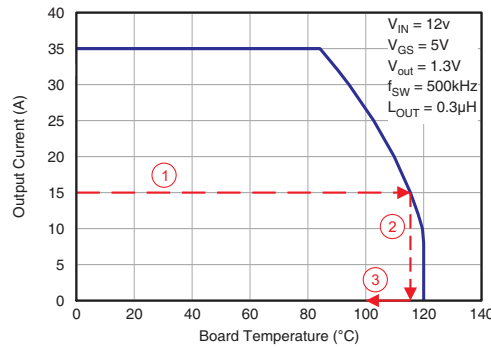


Figure 33. Power Block SOA

## 7 Layout

### 7.1 Layout Guidelines

There are two key system-level parameters that can be addressed with a proper PCB design: electrical and thermal performance. Properly optimizing the PCB layout will yield maximum performance in both areas. A brief description on how to address each parameter is provided.

#### 7.1.1 Electrical Performance

The power block has the ability to switch voltages at rates greater than 10 kV/μs. Special care must be then taken with the PCB layout design and placement of the input capacitors, Driver IC, and output inductor.

- The placement of the input capacitors relative to the power block's VIN and PGND pins should have the highest priority during the component placement routine. It is critical to minimize these node lengths. As such, ceramic input capacitors need to be placed as close as possible to the VIN and PGND pins (see [Figure 34](#)). The example in [Figure 34](#) uses 6 × 10-μF ceramic capacitors (TDK C3216X5R1C106KT or equivalent). Notice there are ceramic capacitors on both sides of the board with an appropriate amount of vias interconnecting both layers. In terms of priority of placement next to the power block, C5, C7, C19, and C8 should follow in order.
- The driver IC should be placed relatively close to the power block gate pins. T<sub>G</sub> and B<sub>G</sub> should connect to the outputs of the driver IC. The T<sub>GR</sub> pin serves as the return path of the high-side gate drive circuitry and should be connected to the phase pin of the IC (sometimes called LX, LL, SW, PH, etc.). The bootstrap capacitor for the driver IC will also connect to this pin.
- The switching node of the output inductor should be placed relatively close to the power block VSW pins. Minimizing the node length between these two components will reduce the PCB conduction losses and actually reduce the switching noise level.
- The switching node of the output inductor should be placed relatively close to the power block VSW pins. Minimizing the node length between these two components will reduce the PCB conduction losses and actually reduce the switching noise level. In the event the switch node waveform exhibits ringing that reaches undesirable levels, the use of a boost resistor or RC snubber can be an effective way to reduce the peak ring level. The recommended boost resistor value will range between 1 Ω to 4.7 Ω depending on the output characteristics of driver IC used in conjunction with the power block. The RC snubber values can range from 0.5 Ω to 2.2 Ω for the R and 330 pF to 2200 pF for the C. Refer to [Snubber Circuits: Theory, Design and Application](#) (SLUP100) for more details on how to properly tune the RC snubber values. The RC snubber should be placed as close as possible to the Vsw node and PGND see [Figure 34](#) <sup>(1)</sup>

#### 7.1.2 Thermal Performance

The power block has the ability to utilize the GND planes as the primary thermal path. As such, the use of thermal vias is an effective way to pull away heat from the device and into the system board. Concerns of solder voids and manufacturability problems can be addressed by the use of three basic tactics to minimize the amount of solder attach that will wick down the via barrel:

- Intentionally space out the vias from each other to avoid a cluster of holes in a given area.
- Use the smallest drill size allowed in your design. The example in [Figure 34](#) uses vias with a 10-mil drill hole and a 16-mil capture pad.
- Tent the opposite side of the via with solder-mask.

In the end, the number and drill size of the thermal vias should align with the end user's PCB design rules and manufacturing capabilities.

(1) Keong W. Kam, David Pommerenke, "EMI Analysis Methods for Synchronous Buck Converter EMI Root Cause Analysis", University of Missouri – Rolla

## 7.2 Layout Example

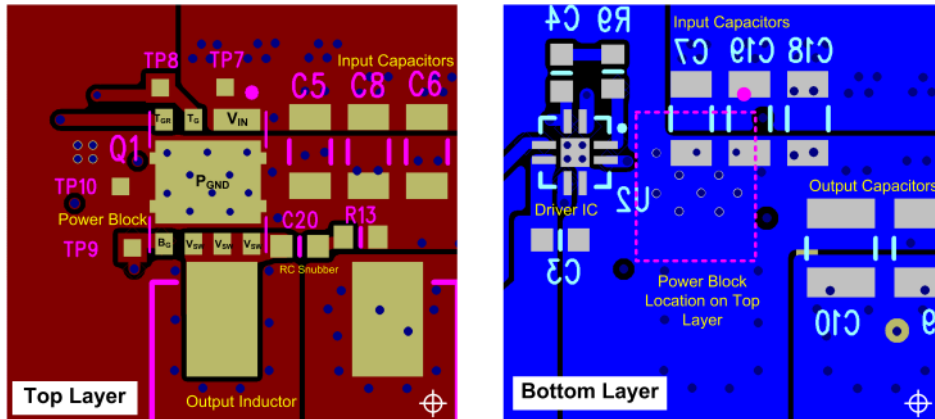


Figure 34. Recommended PCB Layout (Top Down View)



## 8 Device and Documentation Support

### 8.1 Documentation Support

#### 8.1.1 Related Documentation

For related documentation see the following:

- [Power Loss Calculation With Common Source Inductance Consideration for Synchronous Buck Converters \(SLPA009\)](#)
- [Snubber Circuits: Theory, Design and Application \(SLUP100\)](#)

### 8.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 8.3 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 8.4 Trademarks

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All other trademarks are the property of their respective owners.

### 8.5 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

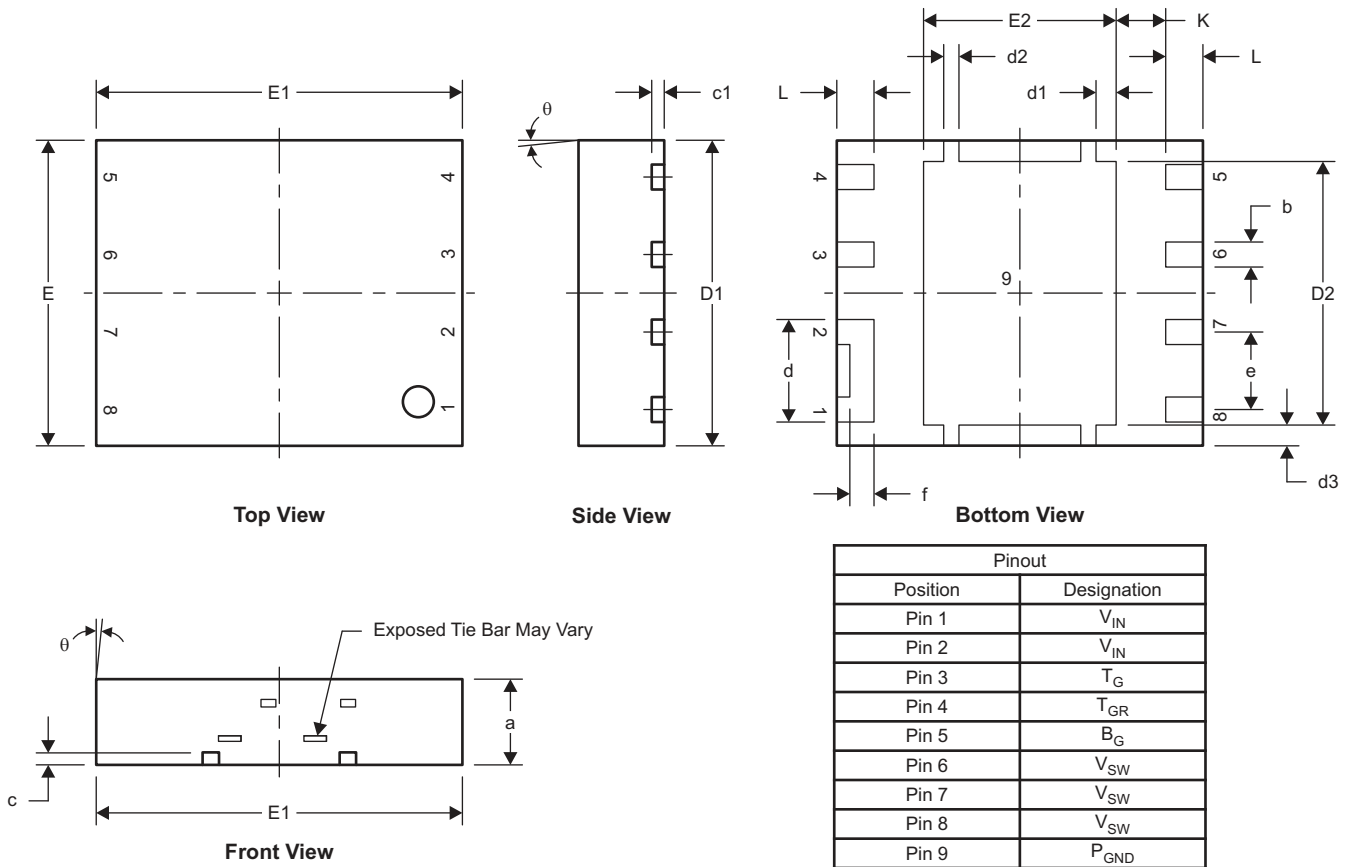
### 8.6 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 9 Mechanical, Packaging, and Orderable Information

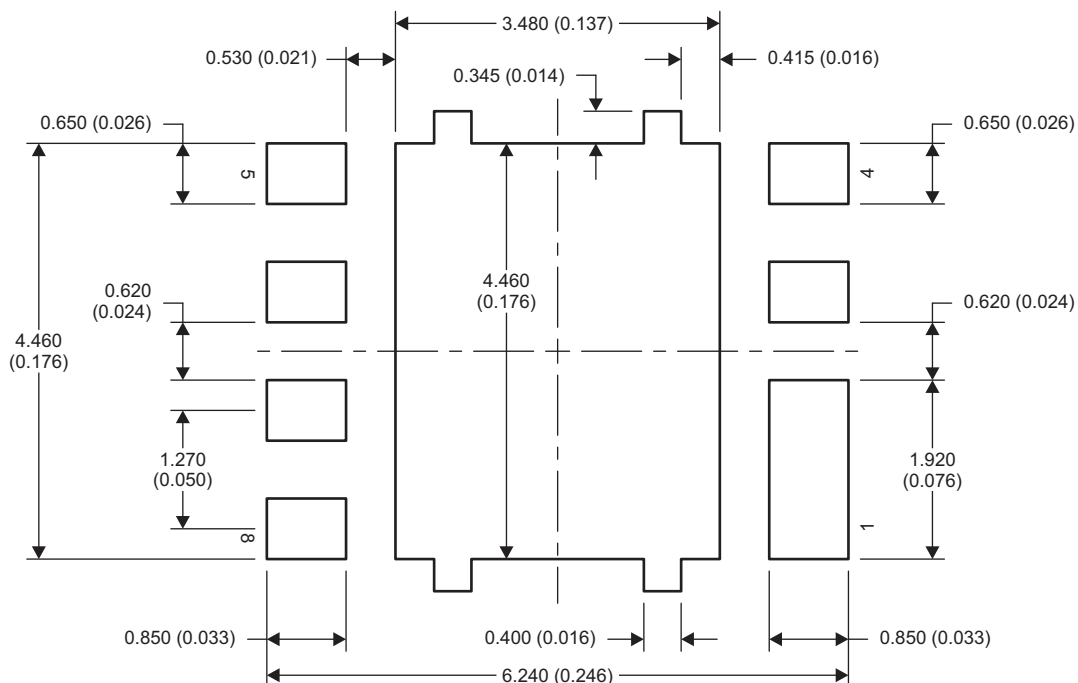
### 9.1 Q5D Package Dimensions



M0187-01

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
a	1.400	1.500	0.055	0.059
b	0.360	0.460	0.014	0.018
c	0.150	0.250	0.006	0.010
c1	0.150	0.250	0.006	0.010
d	1.630	1.730	0.064	0.068
d1	0.280	0.380	0.011	0.015
d2	0.200	0.300	0.008	0.012
d3	0.291	0.391	0.012	0.015
D1	4.900	5.100	0.193	0.201
D2	4.269	4.369	0.168	0.172
E	4.900	5.100	0.193	0.201
E1	5.900	6.100	0.232	0.240
E2	3.106	3.206	0.122	0.126
e	1.270 TYP		0.050	
f	0.396	0.496	0.016	0.020
L	0.510	0.710	0.020	0.028
theta	0.000	—	—	—
K	0.812		0.032	

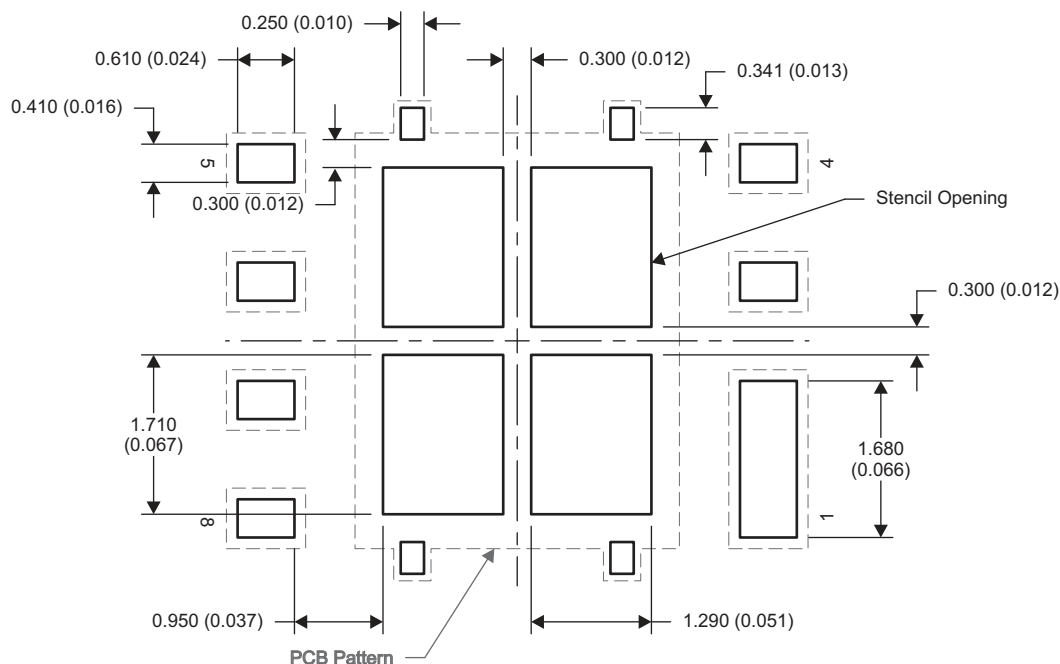
## 9.2 Land Pattern Recommendation



M0188-01

NOTE: Dimensions are in mm (in).

## 9.3 Stencil Recommendation

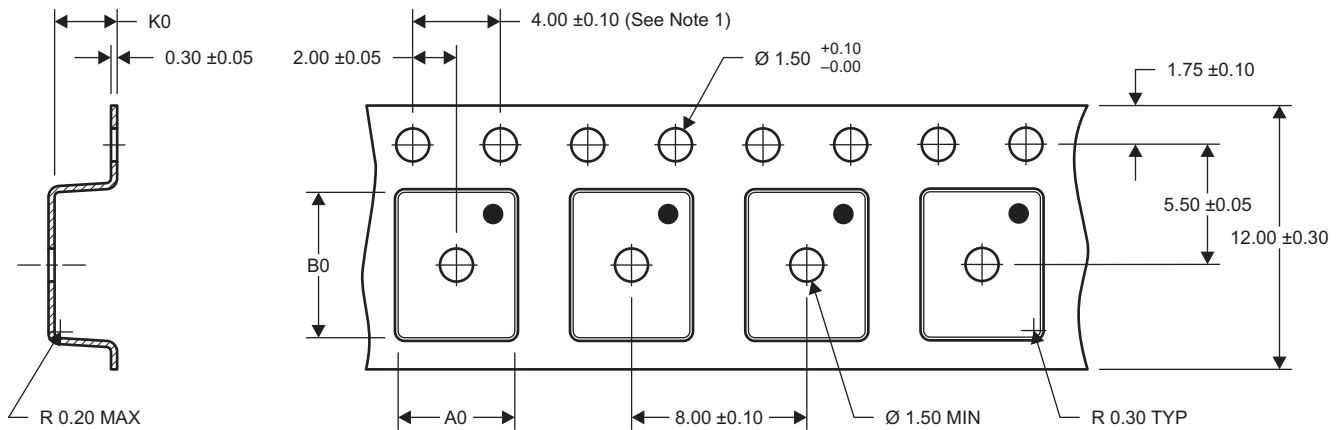


M0208-01

NOTE: Dimensions are in mm (in).

For recommended circuit layout for PCB designs, see [Reducing Ringing Through PCB Layout Techniques \(SLPA005\)](#).

## 9.4 Q5D Tape and Reel Information




$A0 = 5.30 \pm 0.10$   
 $B0 = 6.50 \pm 0.10$   
 $K0 = 1.90 \pm 0.10$

M0191-01

- NOTES:
1. 10-sprocket hole-pitch cumulative tolerance  $\pm 0.2$ .
  2. Camber not to exceed 1 mm in 100 mm, noncumulative over 250 mm.
  3. Material: black static-dissipative polystyrene.
  4. All dimensions are in mm, unless otherwise specified.
  5. Thickness:  $0.3 \pm 0.05$  mm.
  6. MSL1 260°C (IR and convection) PbF reflow compatible.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
CSD87352Q5D	ACTIVE	LSON-CLIP	DQY	8	2500	RoHS-Exempt & Green	NIPDAU   SN	Level-1-260C-UNLIM	-55 to 150	87352D	

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBsolete:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=100ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

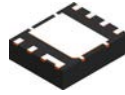
(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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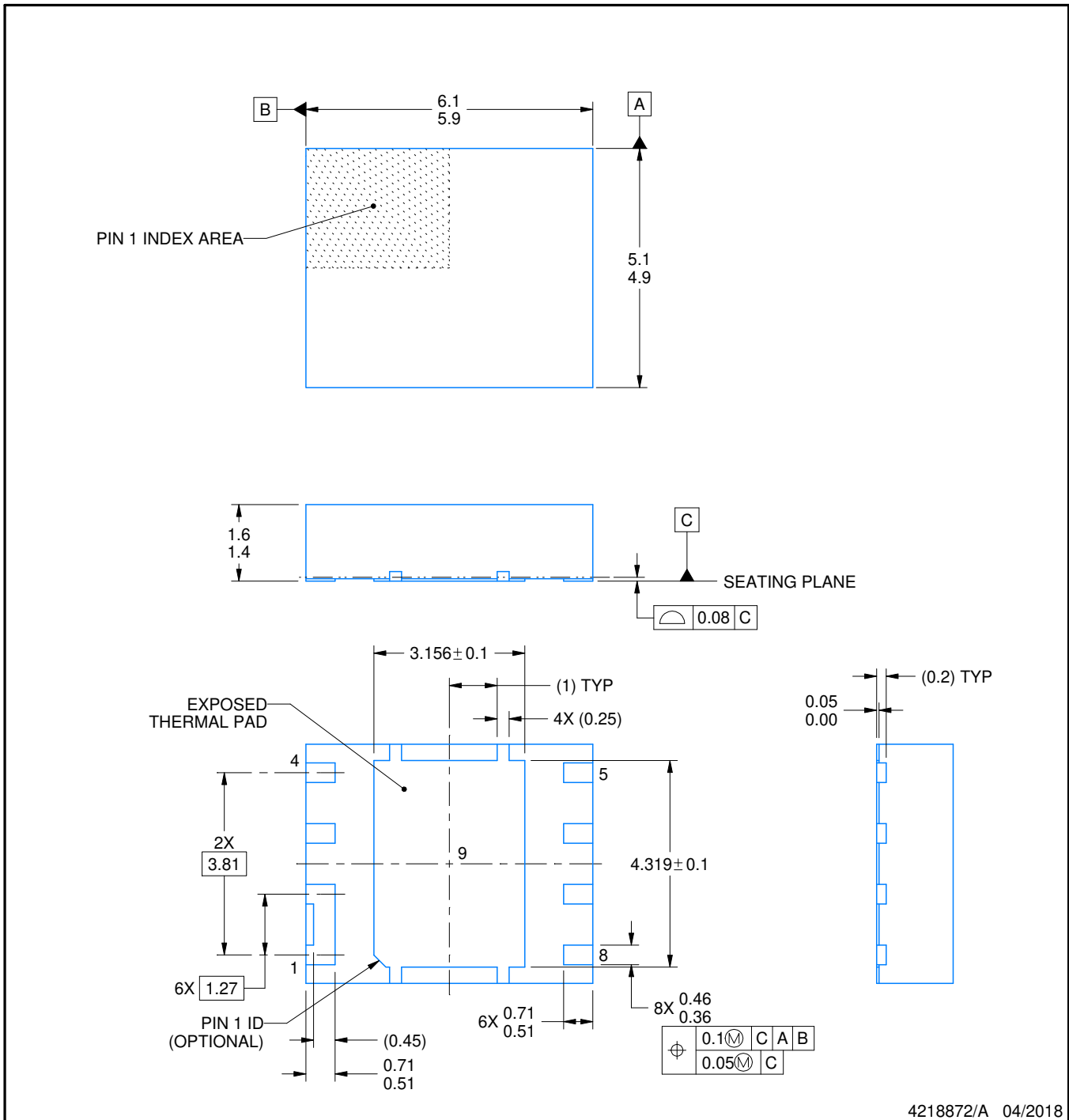
DQY0008A



# PACKAGE OUTLINE

## LSON-CLIP - 1.6 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



**NOTES:**

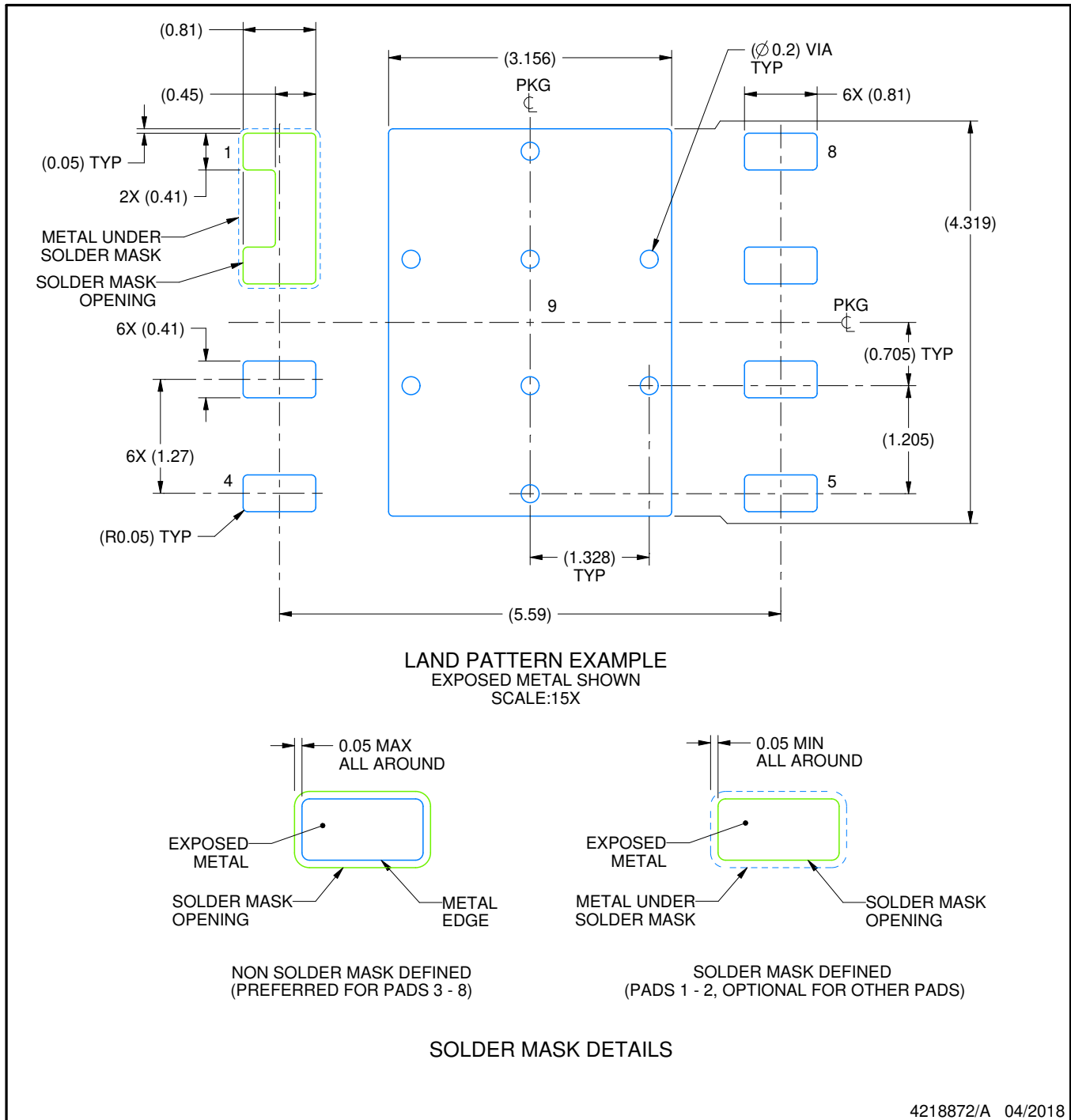
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

# EXAMPLE BOARD LAYOUT

DQY0008A

LSON-CLIP - 1.6 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



NOTES: (continued)

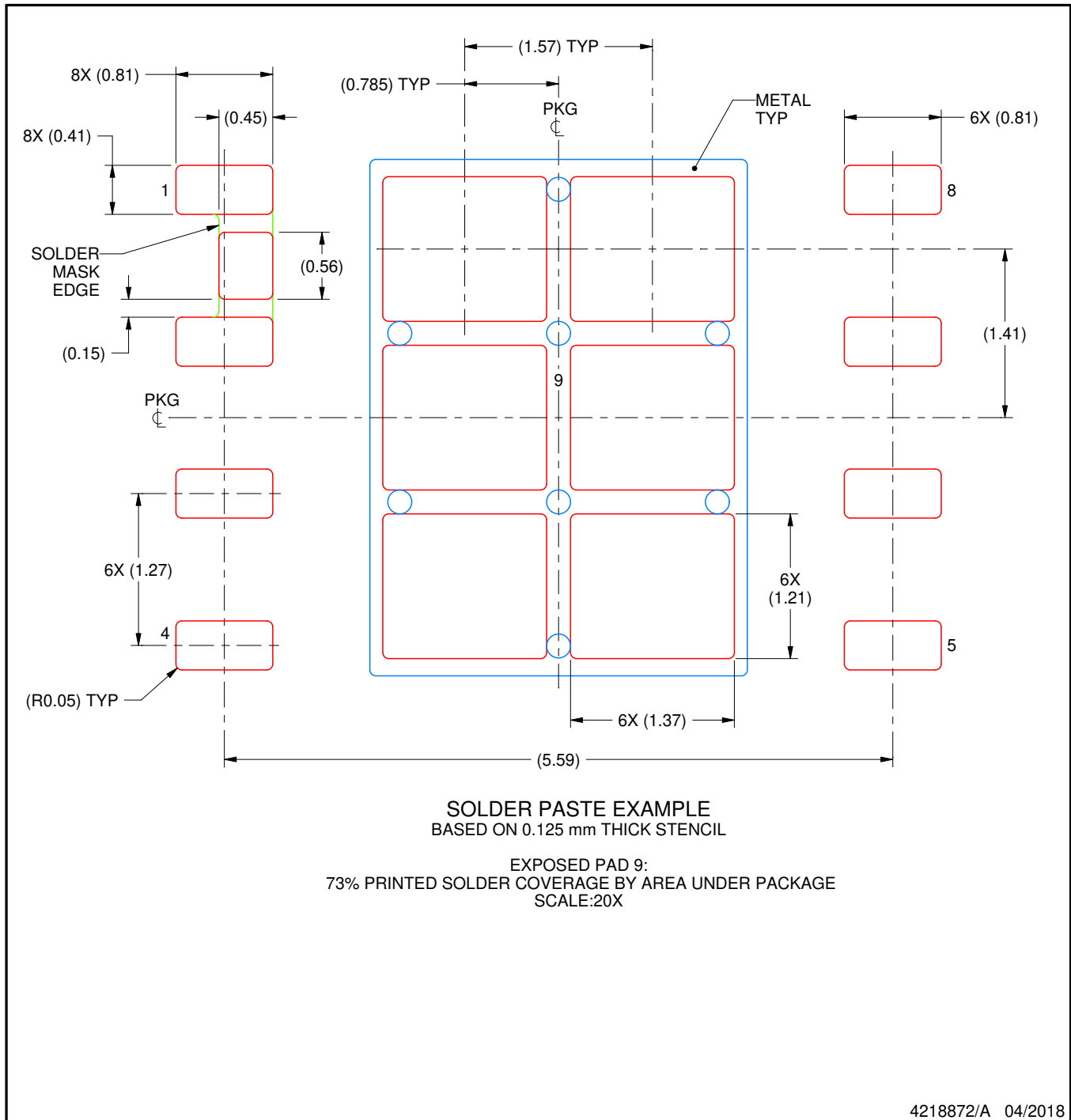
- This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/slue271](http://www.ti.com/lit/slue271)).
- Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.

# EXAMPLE STENCIL DESIGN

DQY0008A

LSON-CLIP - 1.6 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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