# National Semiconductor is now part of Texas Instruments.

Search <a href="http://www.ti.com/">http://www.ti.com/</a> for the latest technical information and details on our current products and services.



## LMC6035/LMC6036 Low Power 2.7V Single Supply CMOS Operational Amplifiers

### **General Description**

The LMC6035/6 is an economical, low voltage op amp capable of rail-to-rail output swing into loads of  $600\Omega$ . LMC6035 is available in a chip sized package (8-Bump micro SMD) using National's micro SMD package technology. Both allow for single supply operation and are guaranteed for 2.7V, 3V, 5V and 15V supply voltage. The 2.7 supply voltage corresponds to the End-of-Life voltage (0.9V/cell) for three NiCd or NiMH batteries in series, making the LMC6035/6 well suited for portable and rechargeable systems. It also features a well behaved decrease in its specifications at supply voltages below its guaranteed 2.7V operation. This provides a "comfort zone" for adequate operation at voltages significantly below 2.7V. Its ultra low input currents (I<sub>IN</sub>) makes it well suited for low power active filter application, because it allows the use of higher resistor values and lower capacitor values. In addition, the drive capability of the LMC6035/6 gives these op amps a broad range of applications for low voltage systems.

#### **Features**

(Typical Unless Otherwise Noted)

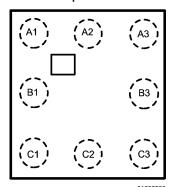
- LMC6035 in micro SMD Package
- Guaranteed 2.7V, 3V, 5V and 15V Performance
- Specified for 2 kΩ and 600Ω Loads
- Wide Operating Range: 2.0V to 15.5V
- Ultra Low Input Current: 20fA
- Rail-to-Rail Output Swing
  - @ 600 $\Omega$ : 200mV from either rail at 2.7V @ 100k $\Omega$ : 5mV from either rail at 2.7V
- High Voltage Gain: 126dB
- Wide Input Common-Mode Voltage Range -0.1V to 2.3V at V<sub>S</sub> = 2.7V
- Low Distortion: 0.01% at 10kHz
- LMC6035 Dual LMC6036 Quad
- See AN-1112 for micro SMD considerations

## **Applications**

- Filters
- High Impedance Buffer or Preamplifier
- Battery Powered Electronics
- Medical Instrumentation

## **Connection Diagram**

#### 8-Bump microSMD



Top View (Bump Side Down)

### microSMD Connection Table

Bump Number	LM6035IBP	LMC6035ITL
	LMC6035IBPX	LMC6035ITLX
A1	OUTPUT A	OUTPUT B
B1	IN A <sup>-</sup>	V <sup>+</sup>
C1	IN A <sup>+</sup>	OUTPUT A
C2	V-	IN A <sup>-</sup>
C3	IN B <sup>+</sup>	IN A <sup>+</sup>
B3	IN B-	V-
A3	OUTPUT B	IN B <sup>+</sup>
A2	V <sup>+</sup>	IN B-

## **Absolute Maximum Ratings** (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

ESD Tolerance (Note 2)

Human Body Model 3000V Machine Model 300V

Differential Input Voltage  $\pm$  Supply Voltage Supply Voltage (V<sup>+</sup> – V<sup>-</sup>) 16V Output Short Circuit to V <sup>+</sup> (Note 8)

Lead Temperature (soldering, 10

Output Short Circuit to V -

 sec.)
 260°C

 Current at Output Pin
 ±18mA

 Current at Input Pin
 ±5mA

 Current at Power Supply Pin
 35mA

Storage Temperature Range -65°C to +150°C

Junction Temperature (Note 4)

150°C

## **Operating Ratings** (Note 1)

Supply Voltage 2.0V to 15.5V

Temperature Range

LMC6035I and LMC6036I  $-40^{\circ}\text{C} \le \text{T}_{\text{J}} \le +85^{\circ}\text{C}$ 

Thermal Resistance ( $\theta_{JA}$ )

 8-pin MSOP
 230°C/W

 8-pin SOIC
 175°C/W

 14-pin SOIC
 127°C/W

 14-pin TSSOP
 137°C/W

 8-Bump (6 mil) micro SMD
 220°C/W

 8-Bump (12 mil) Thin micro
 220°C/W

SMD

### **DC Electrical Characteristics**

Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 2.7V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.0V$ ,  $V_O = 1.35V$  and  $R_L > 1M\Omega$ . **Boldface** limits apply at the temperature extremes.

(Note 3)

			LMC	LMC6035I/LMC6036I		
Symbol	Parameter	Conditions	Min	Тур	Max	Units
			(Note 6)	(Note 5)	(Note 6)	
$V_{OS}$	Input Offset Voltage			0.5	5	mV
					6	
TCV <sub>OS</sub>	Input Offset Voltage			2.3		μV/°C
	Average Drift			2.0		μν, σ
I <sub>IN</sub>	Input Current	(Note 11)		0.02	90	pA
l <sub>os</sub>	Input Offset Current	(Note 11)		0.01	45	PA
$R_{IN}$	Input Resistance			> 10		Tera 🖸
CMRR	Common Mode Rejection	$0.7V \le V_{CM} \le 12.7V$ ,	63	96		dB
	Ratio	$V^{+} = 15V$	60			
+PSRR	Positive Power Supply	$5V \leq V^+ \leq 15V$ ,	63	93		dB
	Rejection Ratio	$V_{O} = 2.5V$	60			
-PSRR	Negative Power Supply	$0V \leq V^- \leq -10V$ ,	74	97		dB
	Rejection Ratio	$V_{O} = 2.5V, V^{+} = 5V$	70			
V <sub>CM</sub>	Input Common-Mode	V <sup>+</sup> = 2.7V		-0.1	0.3	
	Voltage Range	For CMRR ≥ 40dB			0.5	V
			2.0	2.3		ľ
			1.7			
		V+ = 3V		-0.3	0.1	
		For CMRR ≥ 40dB			0.3	V
			2.3	2.6		ď
			2.0			
		$V^{+} = 5V$		-0.5	-0.2	
		For CMRR ≥ 50dB			0.0	V
			4.2	4.5		ď
		3.9				
		V <sup>+</sup> = 15V		-0.5	-0.2	
		For CMRR ≥ 50dB			0.0	V
			14.0	14.4		· •
			13.7			

## DC Electrical Characteristics (Continued)

Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 2.7V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.0V$ ,  $V_O = 1.35V$  and  $R_L > 1M\Omega$ . **Boldface** limits apply at the temperature extremes.

				LMC6035I/LMC6036I				
Symbol	Parameter	Conditions		Min (Note 6)	Typ (Note 5)	Max (Note 6)	Units	
A <sub>V</sub>	Large Signal Voltage Gain (Note 7)	$R_L = 600\Omega$	Sourcing	100 <b>75</b>	1000		V/mV	
			Sinking	25 <b>20</b>	250		V/mV	
		$R_L = 2k\Omega$	Sourcing		2000		V/mV	
			Sinking		500		V/mV	
V <sub>O</sub>	Output Swing	$V^{+} = 2.7V$ $R_{L} = 600\Omega$ to 1.35V		2.0 <b>1.8</b>	2.5			
					0.2	0.5 <b>0.7</b>	V	
		$V^{+} = 2.7V$ $R_{L} = 2k\Omega$ to 1.35V		2.4 <b>2.2</b>	2.62		.,	
				0.07	0.2 <b>0.4</b>	V		
		$V^{+} = 15V$ $R_{L} = 600\Omega$ to 7.5V		13.5 <b>13.0</b>	14.5		V	
					0.36	1.25 <b>1.50</b>	V	
		$V^{+} = 15V$ , $R_{L} = 2 \text{ k}\Omega \text{ to } 7.5V$		14.2 <b>13.5</b>	14.8		V	
					0.12	0.4 <b>0.5</b>	V	
Io	Output Current	V <sub>O</sub> = 0V	Sourcing	4 3	8			
		V <sub>O</sub> = 2.7V	Sinking	3 <b>2</b>	5		mA	
Is	Supply Current	LMC6035 for Both Amplifiers V <sub>O</sub> = 1.35V			0.65	1.6 <b>1.9</b>		
		LMC6036 for All Fou V <sub>O</sub> = 1.35V	r Amplifiers		1.3	2.7 <b>3.0</b>	l	

## **AC Electrical Characteristics**

Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 2.7V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.0V$ ,  $V_O = 1.35V$  and  $R_L > 1$  M $\Omega$ . **Boldface** limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Тур	Units
			(Note 5)	
SR	Slew Rate	(Note 9)	1.5	V/µs
GBW	Gain Bandwidth Product	V <sup>+</sup> = 15V	1.4	MHz
θ <sub>m</sub>	Phase Margin		48	۰
G <sub>m</sub>	Gain Margin		17	dB
	Amp-to-Amp Isolation	(Note 10)	130	dB
e <sub>n</sub>	Input-Referred Voltage Noise	f = 1kHz	27	nV/√Hz
		V <sub>CM</sub> = 1V		
i <sub>n</sub>	Input Referred Current Noise	f = 1kHz	0.2	fA/√Hz
THD	Total Harmonic Distortion	$f = 10kHz, A_V = -10$		
		$R_L = 2k\Omega$ , $V_O = 8 V_{PP}$	0.01	%

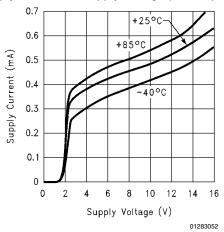
## **AC Electrical Characteristics** (Continued)

Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 2.7V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.0V$ ,  $V_O = 1.35V$  and  $R_L > 1$  M $\Omega$ . **Boldface** limits apply at the temperature extremes.

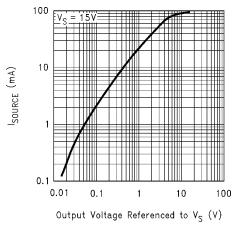
Symbol	Parameter	Conditions	Тур	Units
			(Note 5)	
		V <sup>+</sup> = 10V		

- Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics.
- Note 2: Human body model,  $1.5k\Omega$  in series with 100pF.
- Note 3: Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of 30mA over long term may adversely affect reliability.
- Note 4: The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC board with no air flow.
- Note 5: Typical Values represent the most likely parametric norm or one sigma value.
- Note 6: All limits are guaranteed by testing or statistical analysis.
- Note 7:  $V^+ = 15V$ ,  $V_{CM} = 7.5V$  and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5V \le V_O \le 11.5V$ . For Sinking tests,  $3.5V \le V_O \le 7.5V$ .
- Note 8: Do not short circuit output to  $V^+$  when  $V^+$  is greater than 13V or reliability will be adversely affected.
- Note 9: V<sup>+</sup> = 15V. Connected as voltage follower with 10V step input. Number specified is the slower of the positive and negative slew rates.
- Note 10: Input referred, V  $^+$  = 15V and R<sub>L</sub> = 100k $\Omega$  connected to 7.5V. Each amp excited in turn with 1kHz to produce V<sub>O</sub> = 12 V<sub>PP</sub>.
- Note 11: Guaranteed by design.

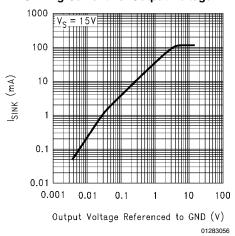
#### Supply Current vs. Supply Voltage (Per Amplifier)



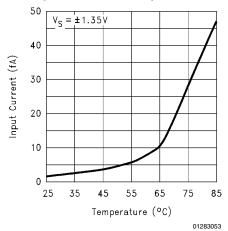
#### Sourcing Current vs. Output Voltage



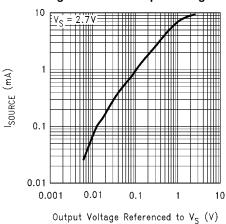
#### Sinking Current vs. Output Voltage



#### Input Current vs. Temperature

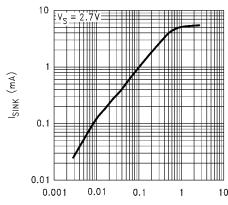


#### Sourcing Current vs. Output Voltage



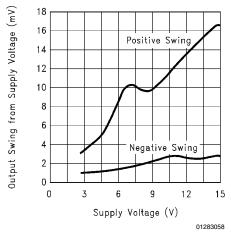
Output Voltage Referenced to V<sub>S</sub> (V)
01283059

#### Sinking Current vs. Output Voltage

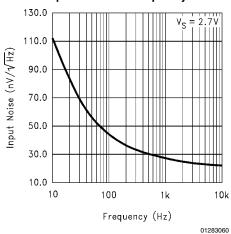


Output Voltage Referenced to GND (V)
01283057

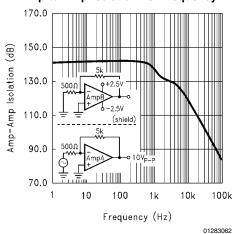
#### **Output Voltage Swing vs. Supply Voltage**



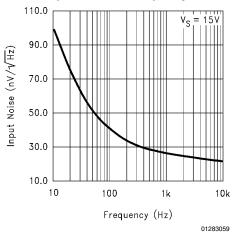
#### Input Noise vs. Frequency



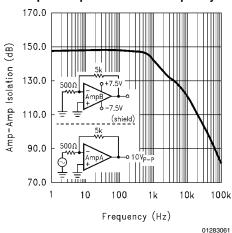
#### Amp to Amp Isolation vs. Frequency



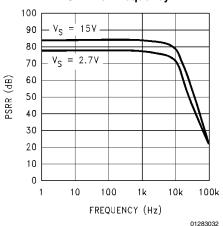
#### Input Noise vs. Frequency

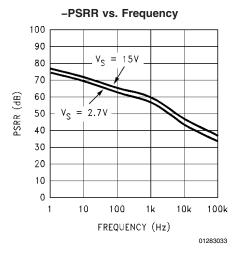


#### Amp to Amp Isolation vs. Frequency

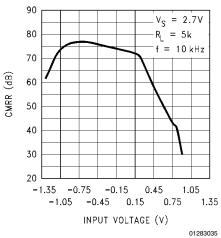


#### +PSRR vs. Frequency

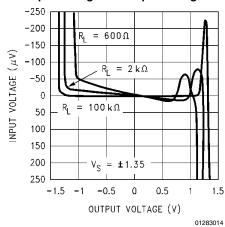




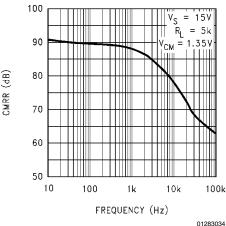
#### CMRR vs. Input Voltage



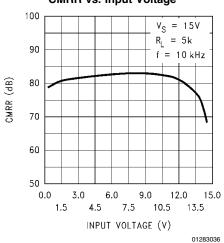
#### Input Voltage vs. Output Voltage



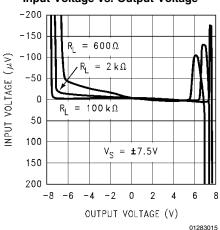
### CMRR vs. Frequency



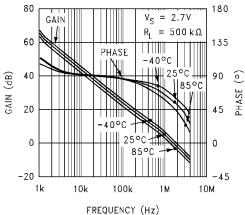
#### CMRR vs. Input Voltage



#### Input Voltage vs. Output Voltage

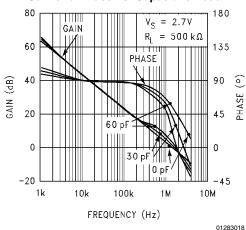






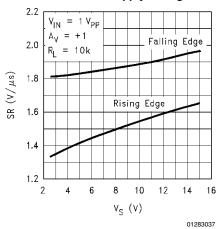
01283016

#### Gain and Phase vs. Capacitive Load

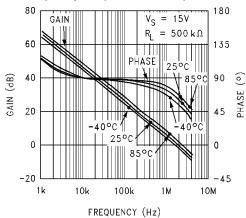


012

#### Slew Rate vs. Supply Voltage

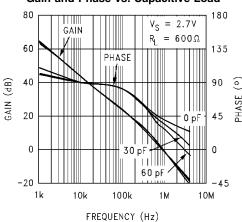


Frequency Response vs. Temperature



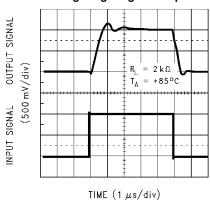
01283017

#### Gain and Phase vs. Capacitive Load



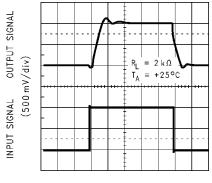
01283019

#### Non-Inverting Large Signal Response



01283020

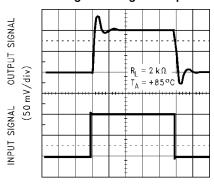
#### **Non-Inverting Large Signal Response**



TIME (1  $\mu$ s/div)

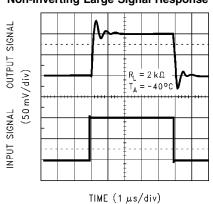
012830

### Non-Inverting Small Signal Response



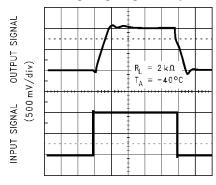
TIME (1  $\mu$ s/div)

### Non-Inverting Large Signal Response



01283025

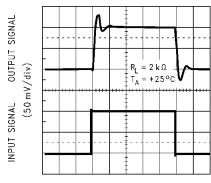
#### Non-Inverting Large Signal Response



TIME  $(1 \mu s/div)$ 

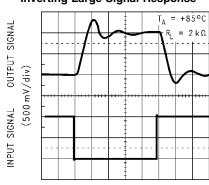
012830

#### Non-Inverting Small Signal Response



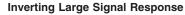
TIME  $(1 \mu s/div)$ 

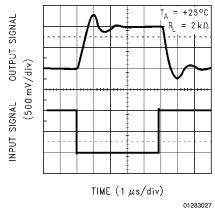
#### **Inverting Large Signal Response**



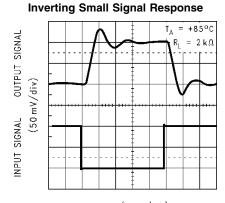
TIME (1  $\mu$ s/div)

01283026



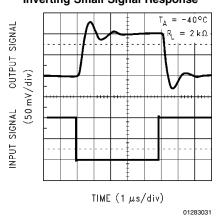


#### L'ANDREA DE LA COMPANION DE LA

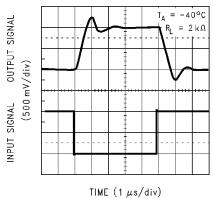


TIME  $(1 \mu s/div)$ 

## Inverting Small Signal Response

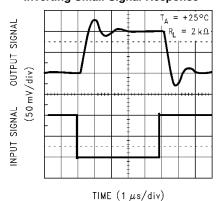


#### **Inverting Large Signal Response**



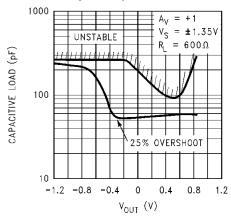
0128302

#### **Inverting Small Signal Response**



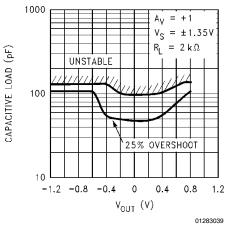
- TIME (1 pas) dity

#### Stability vs. Capacitive Load

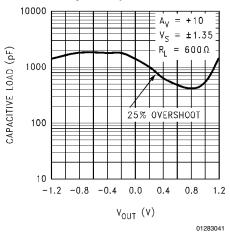


01283038

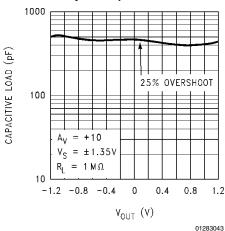




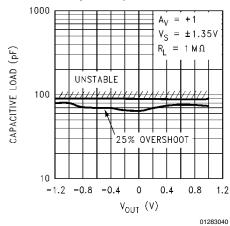
#### Stability vs. Capacitive Load



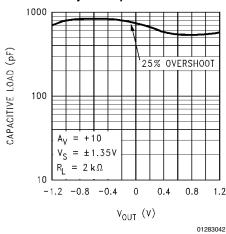
#### Stability vs. Capacitive Load



#### Stability vs. Capacitive Load



#### Stability vs. Capacitive Load



## 1.0 Application Notes

#### 1.1 Background

The LMC6035/6 is exceptionally well suited for low voltage applications. A desirable feature that the LMC6035/6 brings to low voltage applications is its output drive capability—a hallmark for National's CMOS amplifiers. The circuit of Figure 1 illustrates the drive capability of the LMC6035/6 at 3V of supply. It is a differential output driver for a one-to-one audio transformer, like those used for isolating ground from the telephone lines. The transformer (T1) loads the op amps with about  $600\Omega$  of AC load, at 1 kHz. Capacitor C1 functions to block DC from the low winding resistance of T1. Although the value of C1 is relatively high, its load reactance (Xc) is negligible compared to inductive reactance (X<sub>1</sub>) of T1.

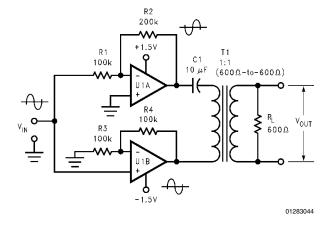


FIGURE 1. Differential Driver

The circuit in *Figure 1* consists of one input signal and two output signals. U1A amplifies the input with an inverting gain of -2, while the U1B amplifies the input with a non-inverting gain of +2. Since the two outputs are 180° out of phase with each other, the gain across the differential output is 4. As the differential output swings between the supply rails, one of the op amps sources the current to the load, while the other op amp sinks the current.

How good a CMOS op amp can sink or source a current is an important factor in determining its output swing capability. The output stage of the LMC6035/6—like many op amps—sources and sinks output current through two complementary transistors in series. This "totem pole" arrangement translates to a channel resistance (R<sub>dson</sub>) at each supply rail which acts to limit the output swing. Most CMOS op amps are able to swing the outputs very close to the rails—except, however, under the difficult conditions of low supply voltage and heavy load. The LMC6035/6 exhibits exceptional output swing capability under these conditions.

The scope photos of Figure 2 and Figure 3 represent measurements taken directly at the output (relative to GND) of U1A, in Figure 1. Figure 2 illustrates the output swing capability of the LMC6035, while Figure 3 provides a benchmark comparison. (The benchmark op amp is another low voltage (3V) op amp manufactured by one of our reputable competitors.)

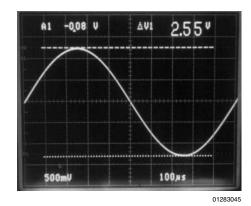


FIGURE 2. Output Swing Performance of the LMC6035 per the Circuit of Figure 1

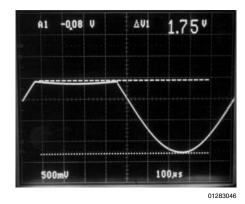


FIGURE 3. Output Swing Performance of Benchmark
Op Amp per the Circuit of Figure 1

Notice the superior drive capability of LMC6035 when compared with the benchmark measurement—even though the benchmark op amp uses twice the supply current.

Not only does the LMC6035/6 provide excellent output swing capability at low supply voltages, it also maintains high open loop gain (A  $_{\rm VOL}$ ) with heavy loads. To illustrate this, the LMC6035 and the benchmark op amp were compared for their distortion performance in the circuit of Figure 1. The graph of Figure 4 shows this comparison. The y-axis represents percent Total Harmonic Distortion (THD plus noise) across the loaded secondary of T1. The x-axis represents the input amplitude of a 1 kHz sine wave. (Note that T1 loses about 20% of the voltage to the voltage divider of R $_{\rm L}$  (600 $\Omega$ ) and T1's winding resistances—a performance deficiency of the transformer.)

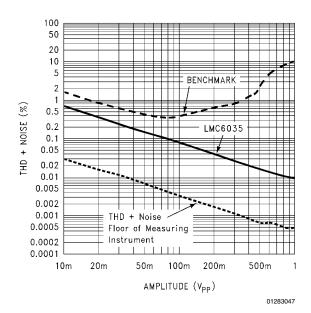


FIGURE 4. THD+Noise Performance of LMC6035 and "Benchmark" per Circuit of *Figure 1* 

Figure 4 shows the superior distortion performance of LMC6035/6 over that of the benchmark op amp. The heavy loading of the circuit causes the  $A_{VOL}$  of the benchmark part to drop significantly which causes increased distortion.

#### 1.2 APPLICATION CIRCUITS

#### 1.2.1 Low-Pass Active Filter

A common application for low voltage systems would be active filters, in cordless and cellular phones for example. The ultra low input currents ( $I_{\rm IN}$ ) of the LMC6035/6 makes it well suited for low power active filter applications, because it allows the use of higher resistor values and lower capacitor values. This reduces power consumption and space.

Figure 5 shows a low pass, active filter with a Butterworth (maximally flat) frequency response. Its topology is a Sallen and Key filter with unity gain. Note the normalized component values in parenthesis which are obtainable from standard filter design handbooks. These values provide a 1Hz cutoff frequency, but they can be easily scaled for a desired cutoff frequency ( $f_c$ ). The bold component values of Figure 5 provide a cutoff frequency of 3kHz. An example of the scaling procedure follows Figure 5.

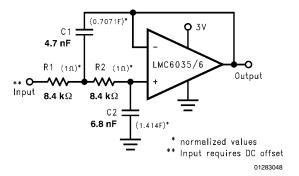


FIGURE 5. 2-Pole, 3kHz, Active, Sallen and Key, Lowpass Filter with Butterworth Response

#### 1.2.1.1 Low-Pass Frequency Scaling Procedure

The actual component values represented in bold of *Figure 5* were obtained with the following scaling procedure:

 First determine the frequency scaling factor (FSF) for the desired cutoff frequency. Choosing f<sub>c</sub> at 3kHz, provides the following FSF computation:

 $FSF = 2\pi \times 3kHz$  (desired cutoff freq.) = 18.84 x 10<sup>-3</sup>

- 2. Then divide all of the normalized capacitor values by the FSF as follows: C1' =  $C_{(Normalized)}$ /FSF C1' = 0.707/18.84 x 10³ = 37.93 x 10<sup>-6</sup> C2' = 1.414/18.84 x 10³ = 75.05 x 10<sup>-6</sup> (C1' and C2': prior to impedance scaling)
- Last, choose an impedance scaling factor (Z). This Z factor can be calculated from a standard value for C2. Then Z can be used to determine the remaining component values as follows:

$$Z = C2'/C2_{(chosen)} = 75.05 \text{ x } 10^{-6}/6.8 \text{nF} = 8.4 \text{k}$$
  
 $C1 = C1'/Z = 37.93 \text{ x } 10^{-6}/8.4 \text{k} = 4.52 \text{nF}$ 

(Standard capacitor value chosen for C1 is **4.7nF** ) R1 = R1<sub>(normalized)</sub> x Z =  $1\Omega$  x  $8.4k = 8.4k\Omega$  R2 =  $R2_{(normalized)}$  x Z =  $1\Omega$  x  $8.4k = 8.4k\Omega$ 

(Standard value chosen for R1 and R2 is  $8.45k\Omega$ )

#### 1.2.2 High Pass Active Filter

The previous low-pass filter circuit of *Figure 5* converts to a high-pass active filter per *Figure 6*.

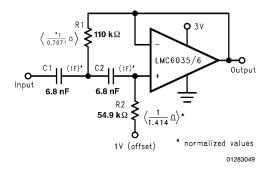


FIGURE 6. 2 Pole, 300Hz, Sallen and Key, High-Pass Filter

#### 1.2.2.1 High-Pass Frequency Scaling Procedure

Choose a standard capacitor value and scale the impedances in the circuit according to the desired cutoff frequency (300Hz) as follows: C = C1 = C2 Z = 1 Farad/ $C_{(chosen)}$  x  $2\pi$  x (desired cutoff freq.) = 1 Farad/**6.8nF** x  $2\pi$  x 300 Hz = 78.05k

R1 = Z x R1<sub>(normalized)</sub> = 78.05k x (1/0.707) = 110.4k $\Omega$  (Standard value chosen for R1 is **110k\Omega** )

R2 = Z x R2<sub>(normalized)</sub> = 78.05k x (1/1.414) =  $55.2k\Omega$  (Standard value chosen for R1 is  $\mathbf{54.9k}\Omega$ )

#### 1.2.3 Dual Amplifier Bandpass Filter

The dual amplifier bandpass (DABP) filter features the ability to independently adjust  $f_c$  and Q. In most other bandpass topologies, the  $f_c$  and Q adjustments interact with each other. The DABP filter also offers both low sensitivity to component values and high Qs. The following application of *Figure 7*, provides a 1kHz center frequency and a Q of 100.

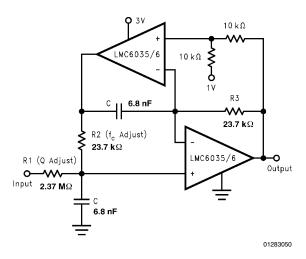


FIGURE 7. 2 Pole, 1kHz Active, Bandpass Filter

#### 1.2.3.1 DABP Component Selection Procedure

Component selection for the DABP filter is performed as follows:

- 1. First choose a center frequency (f<sub>c</sub>). Figure 7 represents component values that were obtained from the following computation for a center frequency of 1kHz. R2 = R3 =  $1/(2 \pi f_c C)$  Given: f<sub>c</sub> = 1kHz and C (chosen) = **6.8nF** R2 = R3 =  $1/(2\pi x \text{ 3kHz } x \text{ 6.8nF})$  = 23.4k $\Omega$  (Chosen standard value is **23.7k** $\Omega$ )
- 2. Then compute R1 for a desired Q ( $f_c$ /BW) as follows: R1 = Q x R2. Choosing a Q of 100, R1 = 100 x  $23.7k\Omega$  = **2.37M** $\Omega$ .

## 1.3 PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with < 1000pA of leakage current requires special layout of the PC board. If one wishes to take advantage of the ultra-low bias current of the LMC6035/6, typically < 0.04pA, it is essential to have an excellent layout. Fortunately, the techniques for obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may at times appear acceptably low. Under conditions of high humidity, dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6035 or LMC6036 inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op amp's inputs. See Figure 8. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of 10<sup>12</sup>Ω, which is normally considered a very large resistance, could leak 5pA if the trace were a 5V bus adjacent to the pad of an input. This would cause a 100 times degradation from the amplifiers actual performance. However, if a guard ring is held within 5mV of the inputs, then even a resistance of  $10^{11}\Omega$  would cause only 0.05pA of leakage current, or perhaps a minor (2:1) degradation of the amplifier's performance. See Figure 9a. b. c for typical connections of guard rings for standard op amp configurations. If both inputs are active and at high impedance, the guard can be tied to ground and still provide some protection; see Figure 9

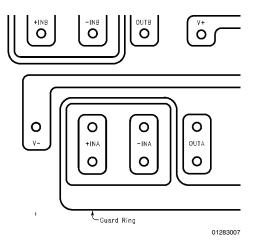
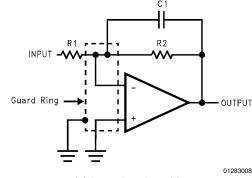
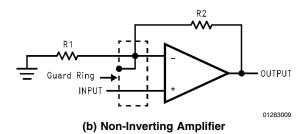
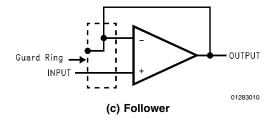


FIGURE 8. Example, using the LMC6036 of Guard Ring in P.C. Board Layout

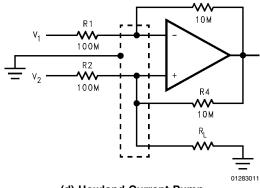


(a) Inverting Amplifier





R.3



(d) Howland Current Pump

FIGURE 9. Guard Ring Connections

#### 1.3.1 CAPACITIVE LOAD TOLERANCE

Like many other op amps, the LMC6035/6 may oscillate when its applied load appears capacitive. The threshold of oscillation varies both with load and circuit gain. The configuration most sensitive to oscillation is a unity-gain follower. See the Typical Performance Characteristics.

The load capacitance interacts with the op amp's output resistance to create an additional pole. If this pole frequency is sufficiently low, it will degrade the op amp's phase margin so that the amplifier is no longer stable at low gains. As shown in Figure 10, the addition of a small resistor  $(50\Omega-100\Omega)$  in series with the op amp's output, and a capacitor (5pF-10pF) from inverting input to output pins, returns the phase margin to a safe value without interfering with lower-frequency circuit operation. Thus, larger values of capacitance can be tolerated without oscillation. Note that in all cases, the output will ring heavily when the load capacitance is near the threshold for oscillation.

#### 1.4 Micro SMD Considerations

Contrary to what might be guessed, the micro SMD package does not follow the trend of smaller packages having higher thermal resistance. LMC6035 in micro SMD has thermal resistance of 220°C/W compared to 230°C/W in MSOP. Even when driving a 600 $\Omega$  load and operating from  $\pm 7.5$ V sup-

plies, the maximum temperature rise will be under 4.5°C. For application information specific to micro SMD, see Application note AN-1112.

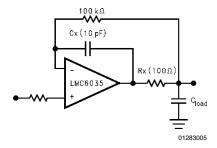


FIGURE 10. Rx, Cx Improve Capacitive Load Tolerance

Capacitive load driving capability is enhanced by using a pull up resistor to V $^+$  (*Figure 11*). Typically a pull up resistor conducting 500 $\mu$ A or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the amplifier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see Electrical Characteristics).

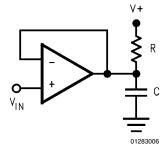
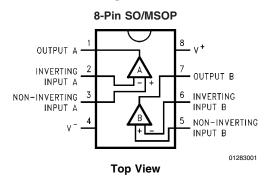
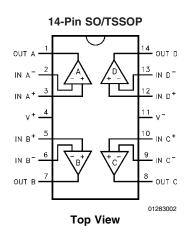


FIGURE 11. Compensating for Large Capacitive Loads with a Pull Up Resistor

## **Connection Diagrams**

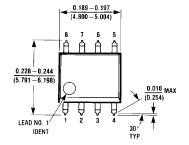


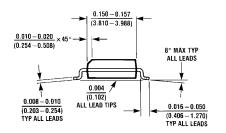


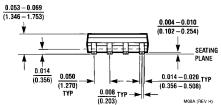
## **Ordering Information**

Package	Temperature Range	Transport Media	NSC Drawing	
	Industrial			
	-40°C to +85°C			
8-pin Small Outline (SO)	LMC6035IM	Rails	M08A	
	LMC6035IMX	2.5k Units Tape and Reel	IVIUOA	
8-pin Mini Small Outline	LMC6035IMM	1k Units Tape and Reel		
(MSOP)			MUA08A	
	LMC6035IMMX	3.5k Units Tape and Reel		
14-pin Small Outline (SO)	LMC6036IM	Rails	M14A	
	LMC6036IMX	2.5k Units Tape and Reel	- WITA	
14-pin Thin Shrink Small	LMC6036IMT	Rails	MTC14	
Outline (TSSOP)	LMC6036IMTX	2.5k Units Tape and Reel	WITC14	
8-Bump micro SMD	LMC6035IBP	250 Units Tape and Reel	BPA08FFB	
(Small Bump)	LMC6035IBPX	3k Units Tape and Reel	] DEAUGEED	
8-Bump Thin micro SMD	LMC6035ITL	250 Units Tape and Reel	TI 400 IO4	
(Large Bump)	LMC6035ITLX	3k Units Tape and Reel	TLA08JQA	

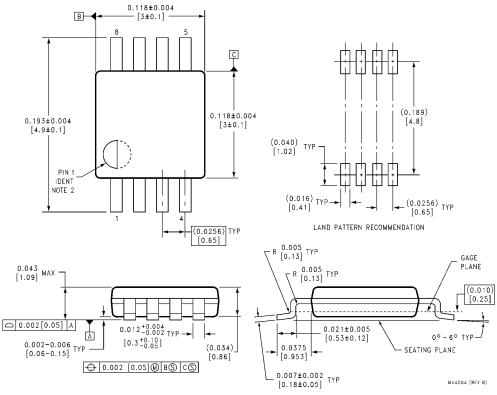
# **Physical Dimensions** inches (millimeters) unless otherwise noted





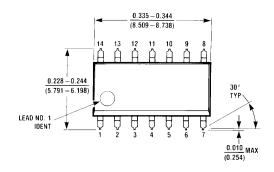


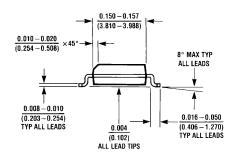
8-Lead (0.150" Wide) Molded Small Outline Package, JEDEC **NS Package Number M08A** 

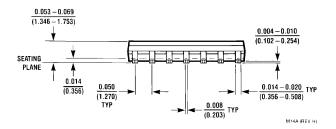


8-Lead (0.150" Wide) Molded Mini Small Outline Package, JEDEC **NS Package Number MUA08A** 

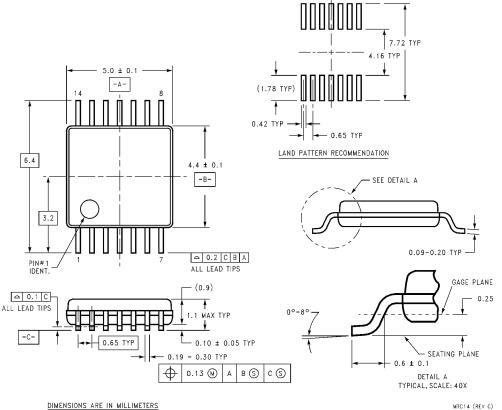
## Physical Dimensions inches (millimeters) unless otherwise noted (Continued)







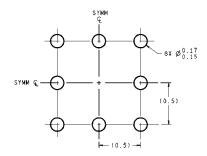
14-Lead (0.150" Wide) Molded Small Outline Package, JEDEC NS Package Number M14A



14-Pin TSSOP

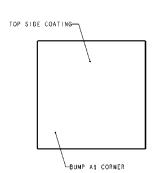
**NS Package Number MTC14** 

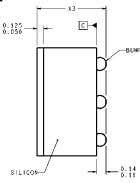
## Physical Dimensions inches (millimeters) unless otherwise noted (Continued)

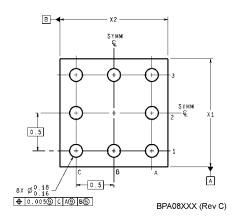


#### DIMENSIONS ARE IN MILLIMETERS

#### LAND PATTERN RECOMMENDATION





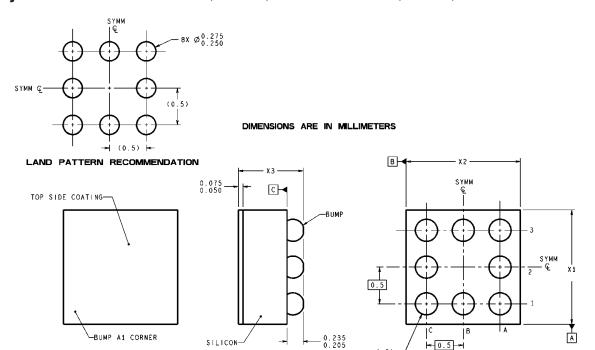


NOTE: UNLESS OTHERWISE SPECIFIED.

- 1. EPOXY COATING.
- 2. 63Sn/37Pb EUTECTIC BUMP.
- 3. RECOMMEND NON-SOLDER MASK DEFINED LANDING PAD.
- 4. PIN A1 IS ESTABLISHED BY LOWER LEFT CORNER WITH RESPECT TO TEXT ORIENTATION PINS ARE NUMBERED COUNTERCLOCKWISE.
- 5. XXX IN DRAWING NUMBER REPRESENTS PACKAGE SIZE VARIATION WHERE X1 IS PACKAGE WIDTH, X2 IS PACKAGE LENGTH AND X3 IS PACKAGE HEIGHT.
- 6. REFERENCE JEDEC REGISTRATION MO-211, VARIATION BC.

8-Bump micro SMD (6 mil bumps) NS Package Number BPA08FFB  $X_1 = 1.412$ mm  $X_2 = 1.412$ mm  $X_3 = 0.850$ mm

### Physical Dimensions inches (millimeters) unless otherwise noted (Continued)



NOTE: UNLESS OTHERWISE SPECIFIED.

- 1. EPOXY COATING.
- 2. 63Sn/37Pb EUTECTIC BUMP.
- 3. RECOMMEND NON-SOLDER MASK DEFINED LANDING PAD.
- 4. PIN A1 IS ESTABLISHED BY LOWER LEFT CORNER WITH RESPECT TO TEXT ORIENTATION PINS ARE NUMBERED COUNTERCLOCKWISE.
- 5. XXX IN DRAWING NUMBER REPRESENTS PACKAGE SIZE VARIATION WHERE X1 IS PACKAGE WIDTH, X2 IS PACKAGE LENGTH AND X3 IS PACKAGE HEIGHT.
- 6. REFERENCE JEDEC REGISTRATION MO-211. VARIATION BC.

8-Bump Thin micro SMD (12 mil bumps) NS Package Number TLA08JQA  $X_1 = 1.717$ mm  $X_2 = 1.869$ mm  $X_3 = 0.600$ mm

8X Ø 0 . 31

◆ 0.005⑤ C A⑤ B⑤

#### LIFE SUPPORT POLICY

NATIONAL'S PRODUCTS ARE NOT AUTHORIZED FOR USE AS CRITICAL COMPONENTS IN LIFE SUPPORT DEVICES OR SYSTEMS WITHOUT THE EXPRESS WRITTEN APPROVAL OF THE PRESIDENT AND GENERAL COUNSEL OF NATIONAL SEMICONDUCTOR CORPORATION. As used herein:

- 1. Life support devices or systems are devices or systems which, (a) are intended for surgical implant into the body, or (b) support or sustain life, and whose failure to perform when properly used in accordance with instructions for use provided in the labeling, can be reasonably expected to result in a significant injury to the user.
- 2. A critical component is any component of a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system, or to affect its safety or effectiveness.



Email: support@nsc.com

www.national.com

**National Semiconductor** Europe

Fax: +49 (0) 180-530 85 86 Email: europe.support@nsc.com Deutsch Tel: +49 (0) 69 9508 6208 English Tel: +44 (0) 870 24 0 2171 Français Tel: +33 (0) 1 41 91 8790

**National Semiconductor** Asia Pacific Customer Response Group Tel: 65-2544466 Fax: 65-2504466 Email: ap.support@nsc.com

**National Semiconductor** Tel: 81-3-5639-7560 Fax: 81-3-5639-7507

TLA08XXX (Rev A)