**THS0842**

**DUAL-INPUT, 8-BIT, 40 MSPS LOW-POWER ANALOG-TO-DIGITAL CONVERTER**

**WITH SINGLE OR DUAL PARALLEL BUS OUTPUT**

#### **features**

- $\bullet$ **Dual Simultaneous Sample and Hold Inputs**
- $\bullet$ **Differential or Single-Ended Analog Inputs**
- $\bullet$  **8-Bit Resolution 40 MSPS Sampling Analog-to-Digital Converter (ADC)**
- $\bullet$ **Single or Dual Parallel Bus Output**
- $\bullet$  **Low Power Consumption: 275 mW Typ Using External References**
- $\bullet$ **Wide Analog Input Bandwidth: 600 MHz Typ**
- $\bullet$ **3.3 V Single-Supply Operation**
- $\bullet$ **3.3 V TTL/CMOS-Compatible Digital I/O**
- $\bullet$  **Internal or External Bottom and Top Reference Voltages**
- $\bullet$ **Adjustable Reference Input Range**
- $\bullet$ **Power-Down (Standby) Mode**
- $\bullet$  **48-Pin Thin Quad Flat Pack (TQFP) Package**

#### **applications**

- $\bullet$  **Digital Communications (Baseband Sampling)**
- $\bullet$ **Cable Modems**
- $\bullet$ **Set Top Boxes**
- $\bullet$ **Test Instruments**

#### **description**

The THS0842 is a dual 8-bit 40 MSPS high-speed A/D converter. It alternately converts each analog input signal into 8-bit binary-coded digital words up to a maximum sampling rate of 40 MSPS with an 80 MHz clock. All digital inputs and outputs are 3.3 V TTL/CMOS-compatible.

Thanks to an innovative single-pipeline architecture implemented in a CMOS process and the 3.3 V supply, the device consumes very little power. In order to provide maximum flexibility, both bottom and top voltage references can be set from user supplied voltages. Alternately, if no external references are available, on-chip references can be used which are also made available externally. The full-scale range is 1 Vpp, depending on the analog supply voltage. If external references are available, the internal references can be powered down independently from the rest of the chip, resulting in an even greater power saving.

The device is specifically suited for the baseband sampling of wireless local loop (WLL) communication, cable modems, set top boxes (STBs), and test instruments.







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## **functional block diagram**





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## **ADC pipeline block diagram**



The single-pipeline architecture uses 6 ADC/DAC stages and one final flash ADC. Each stage produces a resolution of 2 bits. Digital correction logic generates its result using the 2-bit result from the first stage, 1 bit from each of the 5 succeeding stages, and 1 bit from the final stage in order to arrive at an 8-bit result. The correction logic ensures no missing codes over the full operating temperature range.

## **circuit diagrams of inputs and outputs**





## **Terminal Functions**





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#### **absolute maximum ratings over operating free-air temperature (unless otherwise noted)†**



† Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### **recommended operating conditions over operating free-air temperature range**

#### **power supply**



#### **analog and reference inputs**



#### **digital inputs**





**electrical characteristics over recommended operating conditions with fCLK = 80 MSPS and use of internal voltage references, AVDD = DVDD = DRVDD = 3 V, TA = TMIN to TMAX, dual output bus mode (unless otherwise noted)**

#### **power supply**



#### **logic inputs**



 $\dagger$  I<sub>IH</sub> leakage current on other digital inputs (OE, STDBY, PWDN\_REF) is not measured since these inputs have an internal pull-down resistor of  $4$  K $\Omega$  to DGND.

#### **logic outputs**





**electrical characteristics over recommended operating conditions with fCLK = 80 MSPS and use of internal voltage references,**  $AV_{DD} = DV_{DD} = DRV_{DD} = 3V$ **,**  $T_A = T_{MIN}$  **to**  $T_{MAX}$ **, dual output bus mode (unless otherwise noted) (continued)**

#### **dc accuracy**



NOTES: 1. Integral nonlinearity refers to the deviation of each individual code from a line drawn from zero to full scale. The point used as zero occurs 1/2 LSB before the first code transition. The full–scale point is defined as a level 1/2 LSB beyond the last code transition. The deviation is measured from the center of each particular code to the best fit line between these two endpoints.

2. An ideal ADC exhibits code transitions that are exactly 1 LSB apart. DNL is the deviation from this ideal value. Therefore this measure indicates how uniform the transfer function step sizes are. The ideal step size is defined here as the step size for the device under test (i.e., (last transition level – first transition level)  $+(2^n-2)$ ). Using this definition for DNL separates the effects of gain and offset error. A minimum DNL better than –1 LSB ensures no missing codes.

3. Offset error is defined as the difference in analog input voltage – between the ideal voltage and the actual voltage – that will switch the ADC output from code 0 to code 1. The ideal voltage level is determined by adding the voltage corresponding to 1/2 LSB to the bottom reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

Gain error is defined as the difference in analog input voltage – between the ideal voltage and the actual voltage – that will switch the ADC output from code 254 to code 255. The ideal voltage level is determined by subtracting the voltage corresponding to 1.5 LSB from the top reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

- 4. Offset match is the change in offset error between I and Q channels.
- 5. Gain match is the change in gain error between I and Q channels.

#### **analog input**



#### $reference input (AV<sub>DD</sub> = DV<sub>DD</sub> = DRV<sub>DD</sub> = 3.6 V)$



#### **reference outputs**





**electrical characteristics over recommended operating conditions with fCLK = 80 MSPS and use of internal voltage references, AVDD = DVDD = DRVDD = 3 V, TA = TMIN to TMAX, dual output bus mode (unless otherwise noted) (continued)**

#### **dynamic performance†**



 $\uparrow$  Based on analog input voltage of  $-1$  dBFS referenced to a 1.3  $\lor_{\text{pp}}$  full-scale input range.

NOTE 6: The analog input bandwidth is defined as the maximum frequency of a -1 dBFS input sine that can be applied to the device for which an extra 3 dB attenuation is observed in the reconstructed output signal.

#### **timing requirements**



NOTE 7: Conversion rate is  $1/2$  the clock rate,  $f_{\text{Clk}}$ .



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NOTE A: The relationship between CLK and C<sub>OUT</sub>/C<sub>OUT</sub> is not fixed and depends on the power-on conditions. Data out should be referenced to COUT and COUT.

**Figure 1. Timing Diagram, Single Bus Output**



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NOTE A: The relationship between CLK and C<sub>OUT</sub>/C<sub>OUT</sub> is not fixed and depends on the power-on conditions. Data out should be referenced to  $C_{\text{OUT}}$  and  $\overline{C_{\text{OUT}}}.$ 

**Figure 2. Timing Diagram, Dual Bus Output**



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## **TYPICAL CHARACTERISTICS†**



**TYPICAL CHARACTERISTICS†**



**Figure 6**









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## **TYPICAL CHARACTERISTICS†**



**–140 –120 –100 –80 –60 –40 –20 0 0 2 4 6 8 10 12 14 16 18 20 f – Frequency – MHz Power – dBFS I Input Channel AIN = 15.1 MHz FAST FOURIER TRANSFORM**







**FAST FOURIER TRANSFORM 0 I Input Channel –20 AIN = 20 MHz –40 Power – dBFS –60 –80** ШТ T'III انا آبادین VIY 117 x **–100 –120 –140 0 2 4 6 8 10 12 14 16 18 20 f – Frequency – MHz Figure 12 FAST FOURIER TRANSFORM 0 Q Input Channel –20 AIN = 20 MHz –40 Power – dBFS –60** ահա **–80** dina Laur **–100 –120 –140 0 2 4 6 8 10 12 14 16 18 20 f – Frequency – MHz Figure 13**

**TYPICAL CHARACTERISTICS†**



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## **TYPICAL CHARACTERISTICS†**







**TYPICAL CHARACTERISTICS†**



**Figure 17**



## **PRINCIPLES OF OPERATION**

#### **definitions of specifications and terminology**

#### **integral nonlinearity (INL)**

Integral nonlinearity refers to the deviation of each individual code from a line drawn from zero through full scale. The point used as zero occurs 1/2 LSB before the first code transition. The full-scale point is defined as level 1/2 LSB beyond the last code transition. The deviation is measured from the center of each particular code to the true straight line between these two endpoints.

#### **differential nonlinearity (DNL)**

An ideal ADC exhibits code transitions that are exactly 1 LSB apart. DNL is the deviation from this ideal value. Therefore this measure indicates how uniform the transfer function step sizes are. The ideal step size is defined here as the step size for the device under test, i.e. (last transition level – first transition level)/(2n –2). Using this definition for DNL separates the effects of gain and offset error. A minimum DNL better than –1 LSB ensures no missing codes.

#### **offset and gain error**

Offset error is defined as the difference in analog input voltage – between the ideal voltage and the actual voltage – that will switch the ADC output from code 0 to code 1. The ideal voltage level is determined by adding the voltage corresponding to 1/2 LSB to the bottom reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

Gain error is defined as the difference in analog input voltage – between the ideal voltage and the actual voltage – that will switch the ADC output from code 254 to code 255. The ideal voltage level is determined by subtracting the voltage corresponding to 1.5 LSB from the top reference level. The voltage corresponding to 1 LSB is found from the difference of top and bottom references divided by the number of ADC output levels (256).

#### **analog input bandwidth**

The analog input bandwidth is defined as the maximum frequency of a 1-dBFS input sine wave that can be applied to the device for which an extra 3-dB attenuation is observed in the reconstructed output signal.

#### **output timing**

Output timing  $t_{d(0)}$  is measured from the 1.5-V level of the CLK input falling edge to the 10%/90% level of the digital output. The digital output load is not higher than 10 pF.

Output hold time t<sub>h(o)</sub> is measured from the 1.5-V level of the CLK input falling edge to the10%/90% level of the digital output. The digital output load is not less than 2 pF.

Aperture delay  $t_{d(A)}$  is measured from the 1.5-V level of the CLK input to the actual sampling instant.

The OE signal is asynchronous.

OE timing t<sub>dis</sub> is measured from the V<sub>IH(min)</sub> level of OE to the high-impedance state of the output data. The digital output load is not higher than 10 pF.

OE timing t<sub>en</sub> is measured from the V<sub>IL(max)</sub> level of OE to the instant when the output data reaches V<sub>OH(min)</sub> or  $V_{\text{OL} (max)}$  output levels. The digital output load is not higher than 10 pF.



## **PRINCIPLES OF OPERATION**

## **definitions of specifications and terminology (continued)**

#### **pipeline delay (latency)**

The number of clock cycles between conversion initiation on an input sample and the corresponding output data being made available from the ADC pipeline. Once the data pipeline is full, new valid output data is provided on every clock cycle. In order to know when data is stable on the output pins, the output delay time  $t_{d(0)}$  (i.e., the delay time through the digital output buffers) needs to be added to the pipeline latency. Note that since the max t<sub>d(o)</sub> is more than 1/2 clock period at 80 MHz, data cannot be reliably clocked in on a rising edge of CLK at this speed. The falling edge should be used.

The THS0842 implements a high-speed 40 MSPS converter in a cost effective CMOS process. Powered from 3.3 V, the single pipeline design architecture ensures low power operation and 8-bit accuracy. Signal inputs are differential and the clock signal is single ended. The digital inputs are 3.3 V TTL/CMOS compatible. Internal voltage references are included for both bottom and top voltages. Therefore, the converter forms a self-contained solution. Alternatively, the user may apply externally generated reference voltages. In doing so, both input offset and input range can be modified to suit the application.

The analog input signal is captured by a high speed sampling and hold. Multiple stages will generate the output code with a pipeline delay of 6.5 CLK cycles. Correction logic combines the multistage data and aligns the 8-bit output word. All digital logic operates at the rising edge of CLK.

## **analog input**



**Figure 18. Simplified Equivalent Input Circuit**

A first-order approximation for the equivalent analog input circuit of the THS0842 is shown in Figure 18. The equivalent input capacitance C<sub>I</sub> is 5 pF typical. The input must charge/discharge this capacitance within the sample period of one half of a clock cycle. When a full-scale voltage step is applied, the input source provides the charging current through the switch resistance  $R_{SM}$  (200  $\Omega$ ) of S1 and quickly settles. In this case the input impedance is low. Alternatively, when the source voltage equals the value previously stored on C<sub>I</sub>, the hold capacitor requires no input current and the equivalent input impedance is very high.



## **PRINCIPLES OF OPERATION**

## **analog input (continued)**

To maintain the frequency performance outlined in the specifications, the total source impedance should be limited to the following equation with f<sub>CLK</sub> = 80 MHz, C<sub>I</sub> = 5 pF, R<sub>SW</sub> = 200 Ω:

$$
\displaystyle R_{S} \; < \; \Bigl[1 \, \div \, \Bigl(2f_{CLK} \times C_{I} \times \ln(256)\Bigr) \! - \! R_{SW}\Bigr]
$$

So, for applications running at a lower  $f_{\text{CI K}}$ , the total source resistance can increase proportionally.

The analog input of the THS0842 is a differential input that can be configured in various ways depending on the signal source and the required level of performance. A fully differential connection (Figure 20) will deliver the best performance from the converter. A dc voltage source, CML, equal to 1.5 V (typical for AV<sub>DD</sub> = 3 V), is made available to the user to help simplify circuit design when using an ac coupled differential input. This low output impedance voltage source(300 Ω, typical) is not designed to be a reference or to be loaded, but makes an excellent dc bias source and stays well within the analog input common mode voltage range over temperature. If load on that pin is foreseen, the use of an external buffer is recommended. Defining VREFD = VREFT – VREFB, each single-ended analog input is limited to be between VCML + VREFD/2 and VCML – VREFD/2. See Table 1 for the minimum and maximum reference input levels.

For the ac-coupled differential input with  $AV_{DD} = 3$  V (see Figure 23), full scale is achieved when the +I/Q and –I/Q input signals are 0.5 VPP, with –I/Q being 180 degrees out of phase with +I/Q. The converter will be at positive full scale when the +I/Q input is at CML +  $0.25$  V and the  $-$ I/Q input is at CML  $-$  0.25 V (+I/Q + I/Q  $= 0.5$  V). Conversely, the converter will be at negative full scale when the  $+1/Q$  input is equal to CML – 0.25 V and  $-1/Q$  is at CML + 0.25 V ( $1/Q$ + +  $1/Q$ – =  $-0.5$  V) (see Figure 19).



## **PRINCIPLES OF OPERATION**

## **analog input (continued)**





The analog input can be dc coupled (see Figure 21) as long as the inputs are within the analog input common mode voltage range. For example (see Figure 21), V+ and V– are signals centered on GND with a peak-to-peak voltage of 2 V, and the circuit in Figure 21 is used to interface it with the THS0842. Assume AV<sub>DD</sub> of the converter is 3 V. Two problems have to be solved. The first is to shift CML from 0 V to 1.5 V (AV<sub>DD</sub>/2). To do that, a V<sub>bias</sub> voltage and an adequate ratio of R1 and R2 have to be selected. For instance, if  $V_{bias} = AV_{DD} = 3 V$ , then R1  $=$  R2. The second is that the differential voltage has to be reduced from 4 V (2 x 2 V) to 1 V, and for that an attenuation of 4 to1 is needed. The attenuation is determined by the relation: (R3||2R2)/((R3||2R2) + 2R1). One possible solution is R1 = R2 = R3 = 150 Ω. In this case, moreover, the input impedance (2R1 + (R3||2R2)) will be 400  $\Omega$ . The values can be changed to match any other input impedance. A capacitor, C, connected from I/Q IN+ to I/Q IN– will help filter any high frequency noise on the inputs, also improving performance. Note, that the chosen value of capacitor C must take into account the highest frequency component of the analog input signal.



**PRINCIPLES OF OPERATION**

#### **ac coupled input**



**Figure 20. AC-Coupled Differential Input Circuits**

**(b)**

**C2**

**CML**

**REFT REFB**

**PRINCIPLES OF OPERATION**

## **ac coupled input (continued)**



**Figure 21. DC-Coupled Differential Input Circuit**

For many applications, ac coupling offers a convenient way for biasing the analog input signal at the proper signal range. Figure 20 shows a typical configuration. To maintain the outlined specifications, the component values need to be carefully selected. The most important issue is the positioning of the 3 dB high-pass corner point f<sub>-3 dB</sub>, which is a function of R (R<sub>S</sub> + R<sub>SW</sub> as shown in Figure 18) and the parallel combination of C<sub>1</sub> and  $C_2$ , called  $C_{eq}$ . This is given by the following equation:

$$
f_{-3 \text{ dB}} = 1 \div (2\pi \times R \times C_{\text{eq}})
$$

Since C1 is typically a large electrolytic or tantalum capacitor, the impedance becomes inductive at higher frequencies. Adding a small ceramic or polystyrene capacitor, C2 of approximately 0.01 µF, which is not inductive within the frequency range of interest, maintains low impedance.

## **analog input, single-ended connection**

The configuration shown in Figure 23 may be used with a single-ended ac coupled input. If I/Q is a 1  $V_{\text{pp}}$ sinewave, then I/Q IN+ is a 1  $V_{DD}$  sinewave riding on a positive voltage equal to CML (see Figure 22). The converter will be at positive full scale when  $I/Q IN+$  is at CML+0.5V ( $I/Q IN+$  –  $I/Q IN-$  = 0.5 V) and will be at negative full scale when I/Q IN+ is equal to  $CML - 0.5$  V (I/Q IN+  $-$  I/Q IN-  $= -0.5$  V). Sufficient headroom must be provided such that the input voltage never goes above 3.3 V or below AGND. The simplest way is to use the dc bias source output (CML) of the THS0842.



## **PRINCIPLES OF OPERATION**

#### **analog input, single-ended connection (continued)**

The single ended analog input can be dc coupled (Figure 24) as long as the input is within the analog input common mode voltage range. A capacitor, C, connected from I/Q IN+ to I/Q IN– will help filter any high frequency noise on the inputs, also improving performance. Note, that the value of capacitor C chosen must take into account the highest frequency component of the analog input signal.



**Figure 22. Single-Ended Input Waveform With AV<sub>DD</sub> = 3 V** 

A single-ended source may give better overall system performance if it is first converted to differential before driving the THS0842.



**Figure 23. AC-Coupled Input**



**PRINCIPLES OF OPERATION**

## **dc coupled input**





For dc-coupled systems, an op-amp can level shift a ground referenced input signal. A circuit like Figure 24(b) could be used. In this case, the AIN voltage is given by:  $AIN = -V_{IN} + V_{CMI}$ 

### **reference terminals**

The THS0842 input voltage range is determined by the voltages on terminals REFBI and REFTI. Since the device has an internal voltage reference generator, it must be placed in power down before applying an external voltage to the REFT and REFB pins. Especially at higher sampling rates, it is advantageous to have a wider analog input range. This can be achievable by using external voltage references (e.g., at  $AV<sub>DD</sub> = 3.3 V$ , the full scale range can be extended from 1  $V_{pp}$  (internal reference) to 1.3  $V_{pp}$  (external reference) as shown in Table 1). These voltages should not be derived via a voltage divider from a power supply source. Instead, use a bandgap-derived voltage reference to derive both references via an op-amp circuit. Refer to the schematic of the THS0842 evaluation module in this datasheet for an example circuit.

When using external references, the full-scale ADC input range and its dc position can be adjusted. The full-scale ADC range is always equal to  $V_{REFT} - V_{REFB}$ . The maximum full-scale range is dependent on AV<sub>DD</sub> as shown in the specification section. Next to the constraint on their difference, there are limitations on the useful range of  $V_{REFT}$  and  $V_{REFB}$  individually as well, dependent also on  $AV_{DD}$ .

Table 1 summarizes these limits for 3 cases.

<b>AV<sub>DD</sub></b>	VREFB(min)	$V$ REFB(max)	$V$ REFT(min)	$V$ REFT $(max)$	$[V_{REFT}-V_{REFB}]_{max}$
3V	0.8V	1.2V	1.8V	2.2V	
3.3V	0.8V	1.2V	2.1V	2.5V	1.3V
3.6V	0.8V	1.2V	2.4V	2.8V	1.6V

**Table 1. Min/Max Reference Input Levels**



## **PRINCIPLES OF OPERATION**

## **digital inputs**

The digital inputs are CLK, STDBY, PWDN\_REF, and OE. All these signals, except CLK, have an internal pulldown resistor to connect to digital ground. This provides a default active operation mode using internal references when left unconnected.

The CLK signal at high frequencies should be considered as an analog input. Overshoot/undershoot should be minimized by proper termination of the signal close to the THS0842. An important cause of performance degradation for a high-speed ADC is clock jitter. Clock jitter causes uncertainty in the sampling instant of the ADC, in addition to the inherent uncertainty on the sampling instant caused by the part itself, as specified by its aperture jitter. There is a theoretical relationship between the frequency (f) and resolution ( $2^N$ ) of a signal that needs to be sampled and the maximum amount of aperture error  $d_{max}$  that is tolerable. The following formula shows the relation:

$$
dt_{\text{max}} = 1 \div \left[ \pi \ f \ 2^{\left(N+1\right)} \right]
$$

As an example, for an 8-bit converter with a 15-MHz input, the jitter needs to be kept <41 pS in order not to have changes in the LSB of the ADC output due to the total aperture error.

## **digital outputs**

The output of THS0842 is straight binary code. Capacitive loading on the output should be kept as low as possible (a maximum loading of 10 pF is recommended) to provide best performance. Higher output loading causes higher dynamic output currents and can increase noise coupling into the device analog front end. To drive higher loads, use an output buffer is recommended. See Figure 25 through Figure 28 for examples.

When clocking output data from the THS0842, it is important to observe its timing relation to COUT. See Note 6 in the specification section for more details.



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**Figure 25. Single Bus Connection Example**



**Figure 26. Dual Bus Connection Example**

NOTE: The SN74ALVCH16841 latches are used to buffer the THS8042 and C<sub>OUT</sub> pins.



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## **PRINCIPLES OF OPERATION**



**Figure 27. Single Bus FIFO Connection to DSP Example**



**Figure 28. Dual Bus FIFO Connection to DSP Example**

## **layout, decoupling and grounding rules**

Proper grounding and layout of the PCB on which the THS0842 is populated are essential to achieve the stated performance. It is advisable to use separate analog and digital ground planes that are spliced underneath the device. The THS0842 has digital and analog terminals on opposite sides of the package to make this easier. Since there is no internal connection between analog and digital grounds, they have to be joined on the PCB. It is advisable to do this at one point in close proximity to the THS0842.

As for power supplies, separate analog and digital supply terminals are provided on the device (AV<sub>DD</sub>/DV<sub>DD</sub>). The supply to the digital output drivers is kept separate also (DRV<sub>DD</sub>). Lowering the voltage on this supply to 3 V instead of the nominal 3.3 V improves performance because of the lower switching noise caused by the output buffers.

Because of the high sampling rate and switched-capacitor architecture, THS0842 generates transients on the supply and reference lines. Proper decoupling of these lines is essential. Decoupling as shown in the schematic of the THS0842 EVM is recommended.



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**MECHANICAL DATA**

**PFB (S-PQFP-G48) PLASTIC QUAD FLATPACK**



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Falls within JEDEC MS-026





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## **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

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**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

**(6)** Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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## **TEXAS INSTRUMENTS**

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# **PACKAGE MATERIALS INFORMATION**

## **TRAY**



Chamfer on Tray corner indicates Pin 1 orientation of packed units.

\*All dimensions are nominal



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