

# 3-V TO 6-V INPUT, 3-A OUTPUT, SYNCHRONOUS BUCK PWM SWITCHER WITH INTEGRATED FETs (SWIFT™)

## FEATURES

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- Controlled Baseline
  - One Assembly Site
  - One Test Site
  - One Fabrication Site
- **Extended Temperature Performance of** –55°C to 125°C
- **Enhanced Diminishing Manufacturing Sources** (DMS) Support
- **Enhanced Product-Change Notification**
- Qualification Pedigree (1)
- 60-mΩ MOSFET Switches for High Efficiency at 3-A Continuous Output Source or Sink Current
- Component gualification in accordance with JEDEC and (1) industry standards to ensure reliable operation over an extended temperature range. This includes, but is not limited to, Highly Accelerated Stress Test (HAST) or biased 85/85, temperature cycle, autoclave or unbiased HAST, electromigration, bond intermetallic life, and mold compound life. Such qualification testing should not be viewed as justifying use of this component beyond specified performance and environmental limits.

- Adjustable Output Voltage Down to 0.9 V With 1% Accuracy
- **Externally Compensated for Design Flexibility**
- **Fast Transient Response**
- Wide PWM Frequency: Fixed 350 kHz, 550 • kHz, or Adjustable 280 kHz to 700 kHz
- Load Protected by Peak Current Limit and Thermal Shutdown
- Integrated Solution Reduces Board Area and **Total Cost**

## APPLICATIONS

- Low-Voltage High-Density Systems With Power Distributed at 5 V or 3.3 V
- Point of Load Regulation for High-Performance DSPs, FPGAs, ASICs, and Microprocessors
- Broadband, Networking, and Optical **Communications Infrastructure**
- Portable Computing/Notebook PCs

## DESCRIPTION/ORDERING INFORMATION

As members of the SWIFT<sup>™</sup> family of dc/dc regulators, the TPS54310 low input voltage high output current synchronous buck PWM converter integrates all required active components. Included on the substrate with the listed features are a true, high performance, voltage error amplifier that provides high performance under transient conditions; an undervoltage-lockout circuit to prevent start-up until the input voltage reaches 3 V; an internally and externally set slow-start circuit to limit in-rush currents; and a power good output useful for processor/logic reset, fault signaling, and supply sequencing.

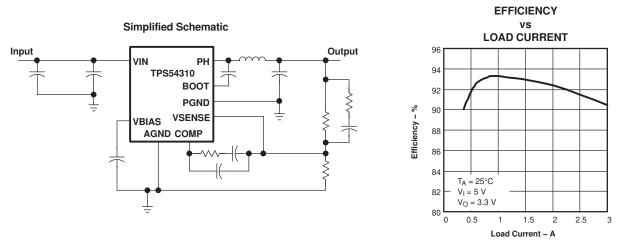
The TPS54310 device is available in a thermally enhanced 20-pin TSSOP (PWP) PowerPAD<sup>™</sup> package, which eliminates bulky heatsinks. TI provides evaluation modules and the SWIFT designer software tool to aid in quickly achieving high-performance power supply designs to meet aggressive equipment development cycles.



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. SWIFT, PowerPAD are trademarks of Texas Instruments.



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## **ORDERING INFORMATION**<sup>(1)</sup>

Tj	OUTPUT VOLTAGE	PACKAGED DEVICES PLASTIC HTSSOP (PWP) <sup>(2)(3)</sup>	TOPSIDE MARKING
–55°C to 125°C	Adjustable Down to 0.9 V	TPS54310MPWPREP	54310EP

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

(2) Package drawings, thermal data, and symbolization are available at www.ti.com/packaging.

(3) The PWP package is shipped taped and reeled with 2000 units per reel. See the application section of this data sheet for PowerPAD drawing and layout information.

## **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

			TPS54310	UNIT
		VIN, SS/ENA, SYNC	–0.3 to 7	V
v	Input voltage range	RT	-0.3 to 6	V
VI	input voltage range	VSENSE	-0.3 to 4	V
		BOOT	–0.3 to 17	V
v		VBIAS, PWRGD, COMP	–0.3 to 7	V
Vo	Output voltage range	РН	-0.6 to 10	V
	Output valtage renge	РН	Internally Limited	
I <sub>O</sub>	Output voltage range	COMP, VBIAS	6	mA
		РН	6	Α
	Sink current	COMP	6	mA
		SS/ENA, PWRGD	10	mA
	Voltage differential	AGND to PGND	±0.3	V
	Continuous power dissipa	tion	See Package Dissipation Rating	
TJ	Operating virtual-junction	temperature range	-55 to 150	°C
T <sub>stg</sub>	Storage temperature		-65 to 150	°C

(1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.



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## **RECOMMENDED OPERATING CONDITIONS**

		MIN	MAX	UNIT
VI	Input voltage	3	6	V
$T_J$	Operating virtual-junction temperature	-55	125	°C

## PACKAGE DISSIPATION RATINGS<sup>(1)</sup> <sup>(2)</sup>

PACKAGE	THERMAL IMPEDANCE JUNCTION-TO-AMBIENT	T <sub>A</sub> = 25°C POWER RATING	T <sub>A</sub> = 70°C POWER RATING	T <sub>A</sub> = 85°C POWER RATING
20-Pin PWP with solder	26°C/W	3.85 W <sup>(3)</sup>	2.12 W	1.54 W
20-Pin PWP without solder	57.5°C/W	1.73 W	0.96 W	0.69 W

(1) For more information on the PWP package, refer to TI technical brief, literature number SLMA002.

Test board conditions: (2)

a. 3 inch  $\times$  3 inch, 2 layers, Thickness: 0.062 inch

b. 1.5 oz copper traces located on the top of the PCB

c. 1.5 oz copper ground plane on the bottom of the PCB

d. Ten thermal vias (see recommended land pattern in application section of this data sheet)

(3) Maximum power dissipation may be limited by overcurrent protection.

## **ELECTRICAL CHARACTERISTICS**

 $T_{.1} = -55^{\circ}C$  to  $125^{\circ}C$ , VIN = 3 V to 6 V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPI	PLY VOLTAGE, VIN					
	VIN input voltage range		3		6	V
		$f_s = 350 \text{ kHz}, \text{ SYNC} = 0.8 \text{ V}, \text{ RT open}$		6.2	9.6	
	Quiescent current	$\rm f_s$ = 550 kHz, SYNC $\geq$ 2.5 V, RT open, phase pin open		8.4	12.8	mA
		Shutdown, SS/ENA = 0 V		1	1.4	
UND	ERVOLTAGE LOCKOUT					
	Start threshold voltage, UVLO			2.95	3	v
	Stop threshold voltage, UVLO		2.70	2.80		v
	Hysteresis voltage, UVLO		0.10	0.16		V
	Rising and falling edge deglitch, UVLO <sup>(1)</sup>			2.5		μs
BIAS	VOLTAGE					
Vo	Output voltage, VBIAS	$I_{(VBIAS)} = 0$	2.70	2.80	2.95	V
v <sub>O</sub>	Output current, VBIAS <sup>(2)</sup>				100	μA
CUM	ULATIVE REFERENCE					
$V_{\text{ref}}$	Accuracy		0.880	0.891	0.900	V
REG	ULATION					
	Line regulation <sup>(1) (3)</sup>	$I_L = 1.5 \text{ A}, f_s = 350 \text{ kHz}, T_J = 85^{\circ}\text{C}$			0.07	%/V
		$I_L = 1.5 \text{ A}, f_s = 550 \text{ kHz}, T_J = 85^{\circ}\text{C}$			0.07	70/ V
	Load regulation <sup>(1) (3)</sup>	$I_L = 0$ A to 3 A, $f_s = 350$ kHz, $T_J = 85^{\circ}C$			0.03	%/A
		I <sub>L</sub> = 0 A to 3 A, f <sub>s</sub> = 550 kHz, T <sub>J</sub> = 85°C			0.03	%/A

Specified by design (1)

(2) (3) Static resistive loads only

Specified by the circuit used in Figure 10.

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# **ELECTRICAL CHARACTERISTICS (continued)**

 $T_J = -55^{\circ}C$  to  $125^{\circ}C$ , VIN = 3 V to 6 V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
OSCIL	LATOR	1				1
	Internally set free-running frequency range	SYNC ≤ 0.8 V, RT open	255	350	450	kHz
	internally set nee-running nequency range	SYNC ≥ 2.5 V, RT open	400	550	700	KI IZ
		RT = 180 k $\Omega$ (1% resistor to AGND) <sup>(4)</sup>	245	280	313	
	Externally set free-running frequency range	RT = 100 k $\Omega$ (1% resistor to AGND)	450	500	550	kHz
		$RT = 68 k\Omega (1\% resistor to AGND)$	650	700	775	l
	High-level threshold voltage, SYNC		2.5			V
	Low-level threshold voltage, SYNC				0.8	V
	Pulse duration, SYNC <sup>(5)</sup>		50			
	Frequency range, SYNC <sup>(5)</sup>		330		700	kHz
	Ramp valley <sup>(4)</sup>			0.75		V
	Ramp amplitude (peak-to-peak) <sup>(4)</sup>			1		V
	Minimum controllable on time				200	ns
	Maximum duty cycle		90%			
ERROF	R AMPLIFIER					
	Error amplifier open loop voltage gain	1 kΩ COMP to AGND <sup>(5)</sup>	90	110		dB
	Error amplifier unity gain bandwidth	Parallel 10 k $\Omega$ , 160 pF COMP to AGND <sup>(5)</sup>	3	5		MHz
	Error amplifier common-mode input voltage range	Powered by internal LDO <sup>(5)</sup>	0	0	VBIAS	V
	Input bias current, VSENSE	VSENSE = V <sub>ref</sub>	0	60	250	nA
I <sub>IB</sub> V <sub>O</sub>	Output voltage slew rate (symmetric), COMP			1.4	230	V/µs
-				1.4		v/µs
	PWM comparator propagation delay time, PWM comparator input to PH pin (excluding dead time)	10 mV overdrive <sup>(5)</sup>		70	85	ns
SLOW	-START/ENABLE					-
	Enable threshold voltage, SS/ENA		0.82	1.20	1.45	V
	Enable hysteresis voltage, SS/ENA <sup>(4)</sup>			0.03		V
	Falling edge deglitch, SS/ENA <sup>(4)</sup>			2.5		μs
	Internal slow-start time		2.2	3.35	4.1	ms
	Charge current, SS/ENA	SS/ENA = 0 V	2.5	5	8	μA
	Discharge current, SS/ENA	SS/ENA = 0.2 V, V <sub>1</sub> = 2.7 V	1.2	2.3	4	mA
POWF	R GOOD				-	
	Power good threshold voltage	VSENSE falling		90		%V <sub>ret</sub>
	Power good hysteresis voltage <sup>(4)</sup>			3		%V <sub>ret</sub>
	Power good falling edge deglitch <sup>(4)</sup>			35		μs
	Output saturation voltage, PWRGD	1 = 2.5 mA		0.18	0.30	μs V
		I <sub>(sink)</sub> = 2.5 mA		0.10		
	Leakage current, PWRGD	V <sub>1</sub> = 5.0 V			1	μA
CURRI		$V_{1} = 2 V_{1}$ subsut shows a $(5)$		0.5		
	Current limit trip point	$V_{I} = 3 V$ , output shorted <sup>(5)</sup>	4	6.5		А
	<ul> <li>Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.Α.</li></ul>	$V_{I} = 6 V$ , output shorted <sup>(5)</sup>	4.5	7.5		ŀ
	Current limit leading edge blanking time <sup>(4)</sup>			100		ns
	Current limit total response time <sup>(4)</sup>			200		ns
THERN	AL SHUTDOWN					[
	Thermal shutdown trip point <sup>(4)</sup>		135	150	165	°C
	Thermal shutdown hysteresis <sup>(4)</sup>			10		°C
Ουτρι	JT POWER MOSFETS	1				
r <sub>bo</sub> , s	Power MOSFET switches	$I_{O} = 0.5 \text{ A}, \text{ VI} = 6 \text{ V}^{(6)}$		59	88	mΩ
r <sub>DS(on)</sub>		$I_{O} = 0.5 \text{ A}, \text{ VI} = 3 \text{ V}^{(6)}$		85	136	11152

(4)

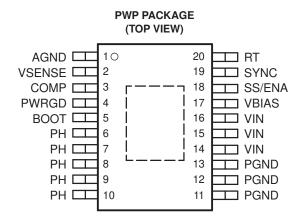
Specified by design Specified by design for  $T_J = -40^{\circ}$ C to 125°C Matched MOSFETs, low side  $r_{DS(on)}$  production tested, high side  $r_{DS(on)}$  specified by design. (5) (6)

# **TPS54310-EP**



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## **PIN ASSIGNMENTS**



## **TERMINAL FUNCTIONS**

TERM	IINAL	DESCRIPTION							
NAME	NO.	DESCRIPTION							
AGND	1	Analog ground. Return for compensation network/output divider, slow-start capacitor, VBIAS capacitor, RT resistor and SYNC pin. Make PowerPAD connection to AGND.							
BOOT	5	Bootstrap input. 0.022 $\mu$ F to 0.1 $\mu$ F low-ESR capacitor connected from BOOT to PH generates floating drive for the high-side FET driver.							
COMP	3	Error amplifier output. Connect compensation network from COMP to VSENSE.							
PGND	11–13	Power ground. High current return for the low-side driver and power MOSFET. Connect PGND with large copper areas to the input and output supply returns, and negative terminals of the input and output capacitors.							
PH	6–10	Phase input/output. Junction of the internal high and low-side power MOSFETs, and output inductor.							
PWRGD	4	Power good open drain output. High when VSENSE ≥ 90% V <sub>ref</sub> , otherwise PWRGD is low. Note that output is low when SS/ENA is low or internal shutdown signal active.							
RT	20	Frequency setting resistor input. Connect a resistor from RT to AGND to set the switching frequency, fs.							
SS/ENA	18	Slow-start/enable input/output. Dual function pin which provides logic input to enable/disable device operation and capacitor input to externally set the start-up time.							
SYNC	19	Synchronization input. Dual function pin which provides logic input to synchronize to an external oscillator or pin select between two internally set switching frequencies. When used to synchronize to an external signal, a resistor must be connected to the RT pin.							
VBIAS	17	Internal bias regulator output. Supplies regulated voltage to internal circuitry. Bypass VBIAS pin to AGND pin with a high quality, low ESR 0.1 $\mu$ F to 1.0 $\mu$ F ceramic capacitor.							
VIN	14–16	Input supply for the power MOSFET switches and internal bias regulator. Bypass VIN pins to PGND pins close to device package with a high quality, low ESR $1-\mu$ F to $10-\mu$ F ceramic capacitor.							
VSENSE	2	Error amplifier inverting input.							

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## FUNCTIONAL BLOCK DIAGRAM

VBIAS AGND VIN Enable Comparator VBIAS < REG Falling SHUTDOWN Л Edge ILIM VIN ţ 1.2 V – 6 V Deglitch Thermal Comparator 3 Hysteresis: 0.03 Leading Shutdown 2.5 us ٧ 150°C Edge Л Blanking VIN UVLO Falling Comparator 100 ns and VIN BOOT Rising Л 2.95 V Edge Hysteresis: 0.16 Deglitch 30 mΩ 4 -|i∙ V 2.5 μs SS\_DIS SHUTDOWN LOUT PH Internal/External Slow-start Adaptive Dead-Time Co R Q (Internal Slow-start Time = 3.35 ms Π and s Control Logic Error PWM Amplifier Reference VIN Comparator VREF = 0.891 V 30 mΩ ามม OSC PGND Powergood Comparator PWRGD VSENSE Falling Л 0.90 V<sub>ref</sub> Edge TPS54610 Deglitch Hysteresis: 0.03 Vref SHUTDOWN 35 µs VSENSE COMP RT SYNC ł(

## **ADDITIONAL 3-A SWIFT DEVICES**

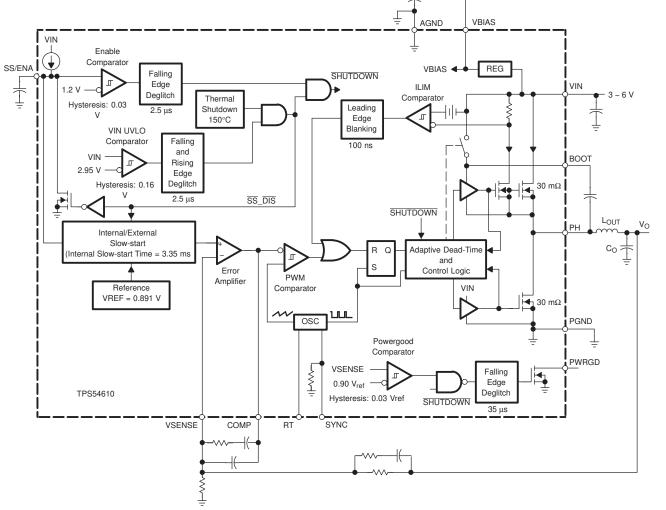
DEVICE	OUTPUT VOLTAGE	DEVICE	OUTPUT VOLTAGE	DEVICE	OUTPUT VOLTAGE
TPS54311	0.9 V	TPS54314	1.8 V	TPS54372	DDR/Adjustable
TPS54312	1.2 V	TPS54315	2.5 V	TPS54373	Prebias/Adjustable
TPS54313	1.5 V	TPS54316	3.3 V	TPS54380	Sequencing/Adjustable

## **RELATED DC/DC PRODUCTS**

- TPS40000 dc/dc controller
- PT5500 series 3-A plug-in modules
- TPS757xx 3-A low dropout regulator .



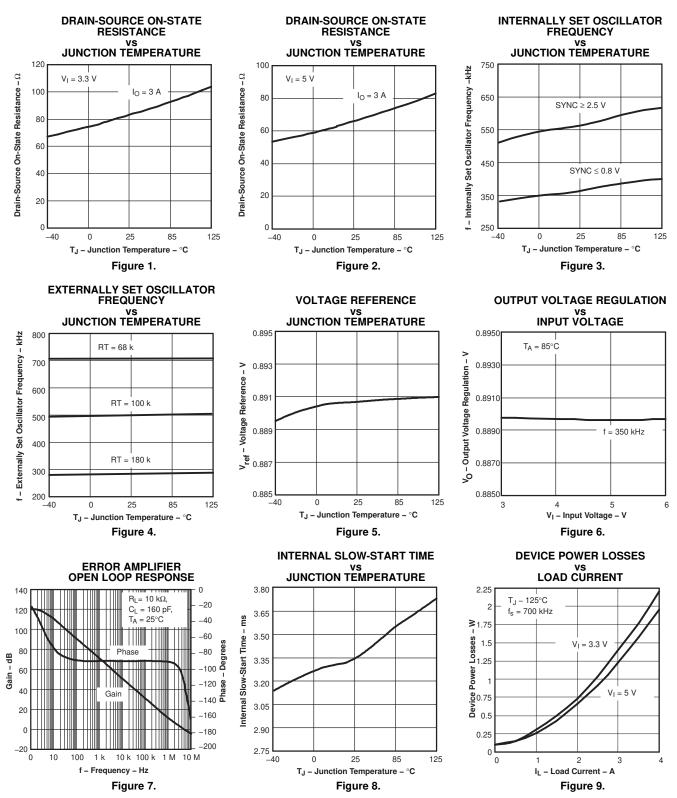
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## **TYPICAL CHARACTERISTICS**





## APPLICATION INFORMATION

Figure 10 shows the schematic diagram for a typical TPS54310 application. The TPS54310 (U1) can provide up to 3 A of output current at a nominal output voltage of 3.3 V. For proper thermal performance, the thermal pad under the TPS54310 integrated circuit needs to be soldered well to the printed-circuit board.

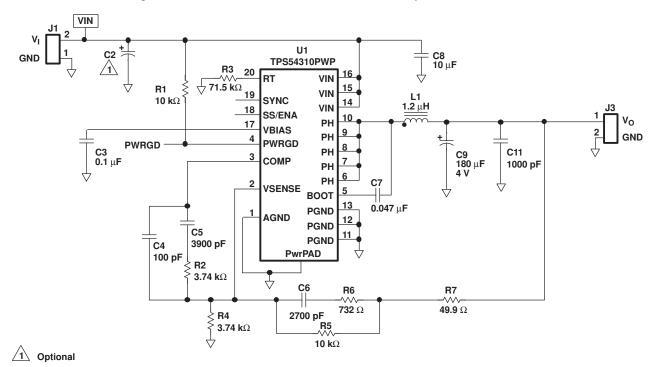


Figure 10. TPS54310 Schematic

## **INPUT VOLTAGE**

The input to the circuit is a nominal 5 VDC, applied at J1. The optional input filter (C2) is a 220- $\mu$ F POSCAP capacitor, with a maximum allowable ripple current of 3 A. C8 is the decoupling capacitor for the TPS54310 and must be located as close to the device as possible.

## FEEDBACK CIRCUIT

The resistor divider network of R5 and R4 sets the output voltage for the circuit at 3.3 V. R5, along with R2, R6, C4, C5, and C6 forms the loop compensation network for the circuit. For this design, a Type 3 topology is used.

## SETTING THE OUTPUT VOLTAGE

The output voltage of the TPS54310 can be set by feeding back a portion of the output to the VSENSE pin using a resistor divider network. In the application circuit of Figure 10, this divider network is comprised of resistors R5 and R4. To calculate the resistor values to generate the required output voltage use Equation 1.

$$R4 = \frac{R5 \times 0.891}{V_{O} - 0.891}$$
(1)

Start with a fixed value of R5 and calculate the required R4 value. Assuming a fixed value of 10 k $\Omega$  for R5, the following table gives the appropriate R4 value for several common output voltages:

OUTPUT VOLTAGE (V)	R4 VALUE (KΩ)
1.2	28.7
1.5	14.7
1.8	9.76
2.5	5.49
3.3	3.74



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## **OPERATING FREQUENCY**

In the application circuit, the 350-kHz operation is selected by leaving RT and SYNC open. Connecting a 68-k $\Omega$  to 180-k $\Omega$  resistor between RT (pin 20) and analog ground can be used to set the switching frequency from 280 kHz to 700 kHz. To calculate the RT resistor, use the Equation 2:

 $\mathsf{R} = \frac{100 \text{ k}\Omega}{f_{\mathsf{SW}}} \times 500 \text{ kHz}$ 

(2)

## **OUTPUT FILTER**

The output filter is composed of a 1.2- $\mu$ H inductor and 180- $\mu$ F capacitor. The inductor is a low dc resistance (0.017  $\Omega$ ) type, Coilcraft DO1813P-122HC. The capacitor used is a 4-V special polymer type with a maximum ESR of 0.015  $\Omega$ . The feedback loop is compensated so that the unity gain frequency is approximately 75 kHz.

## PCB LAYOUT

Figure 11 shows a generalized PCB layout guide for the TPS54310.

The VIN pins should be connected together on the printed circuit board (PCB) and bypassed with a low ESR ceramic bypass capacitor. Care should be taken to minimize the loop area formed by the bypass capacitor connections, the VIN pins, and the TPS54X10 ground pins. The minimum recommended bypass capacitance is  $10-\mu$ F ceramic with a X5R or X7R dielectric and the optimum placement is closest to the VIN pins and the PGND pins.

The TPS54310 has two internal grounds (analog and power). Inside the TPS54310, the analog ground ties to all of the noise sensitive signals, while the power ground ties to the noisier power signals. Noise injected between the two grounds can degrade the performance of the TPS54310, particularly at higher output currents. Ground noise on an analog ground plane can also cause problems with some of the control and bias signals. For these reasons, separate analog and power ground traces are recommended.

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There should be an area of ground one the top laver directly under the IC, with an exposed area for connection to the PowerPAD. Use vias to connect this ground area to any internal ground planes. Use additional vias at the ground side of the input and output filter capacitors as well. The AGND and PGND pins should be tied to the PCB ground by connecting them to the ground area under the device as shown. The only components that should tie directly to the power ground plane are the input capacitors, the output capacitors, the input voltage decoupling capacitor, and the PGND pins of the TPS54310. Use a separate wide trace for the analog ground signal path. This analog ground should be used for the voltage set point divider, timing resistor RT, slow start capacitor and bias capacitor grounds. Connect this trace directly to AGND (pin 1).

The PH pins should be tied together and routed to the output inductor. Since the PH connection is the switching node, inductor should be located very close to the PH pins and the area of the PCB conductor minimized to prevent excessive capacitive coupling.

Connect the boot capacitor between the phase node and the BOOT pin as shown. Keep the boot capacitor close to the IC and minimize the conductor trace lengths.

Connect the output filter capacitor(s) as shown between the VOUT trace and PGND. It is important to keep the loop formed by the PH pins, Lout, Cout and PGND as small as practical.

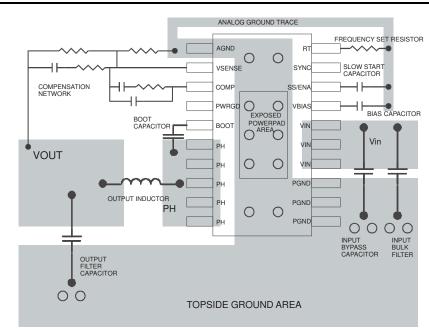
Place the compensation components from the VOUT trace to the VSENSE and COMP pins. Do not place these components too close to the PH trace. Due to the size of the IC package and the device pinout, they will have to be routed somewhat close, but maintain as much separation as possible while still keeping the layout compact.

Connect the bias capacitor from the VBIAS pin to analog ground using the isolated analog ground trace. If a slow-start capacitor or RT resistor is used, or if the SYNC pin is used to select 350-kHz operating frequency, connect them to this trace as well.

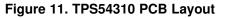
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○ VIA to Ground Plane



# LAYOUT CONSIDERATIONS FOR THERMAL PERFORMANCE

For operation at full rated load current, the analog ground plane must provide adequate heat dissipating area. A 3 inch by 3 inch plane of 1 ounce copper is recommended, though not mandatory, depending on ambient temperature and airflow. Most applications have larger areas of internal ground plane available, and the PowerPAD should be connected to the largest area available. Additional areas on the top or bottom layers also help dissipate heat, and any area available should be used when 3 A or greater operation is desired. Connection from the exposed area of the PowerPAD to the analog ground plane layer should be made using 0.013 inch diameter vias to avoid solder wicking through the vias. Six vias should be in the PowerPAD area with four additional vias located under the device package. The size of the vias under the package, but not in the exposed thermal pad area, can be increased to 0.018. Additional vias beyond the ten recommended that enhance thermal performance should be included in areas not under the device package.







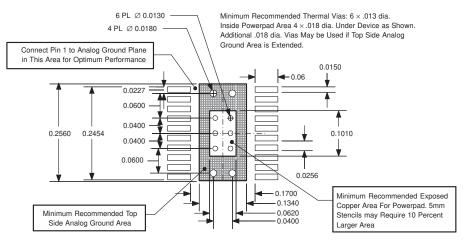
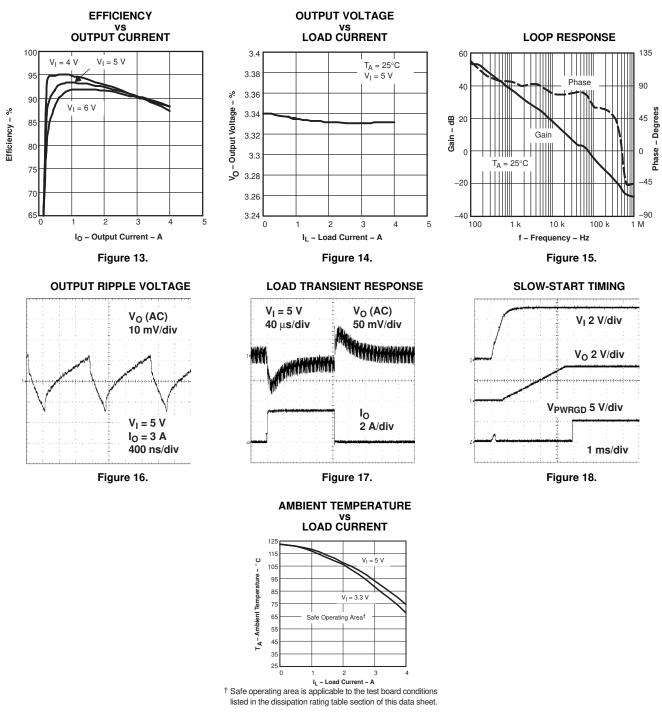


Figure 12. Recommended Land Pattern for 20-Pin PWP PowerPAD

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## **PERFORMANCE GRAPHS**







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## DETAILED DESCRIPTION

## Under Voltage Lock Out (UVLO)

The TPS54310 incorporates an under voltage lockout circuit to keep the device disabled when the input voltage (VIN) is insufficient. During power up, internal circuits are held inactive until VIN exceeds the nominal UVLO threshold voltage of 2.95 V. Once the UVLO start threshold is reached, device start-up begins. The device operates until VIN falls below the nominal UVLO stop threshold of 2.8 V. Hysteresis in the UVLO comparator, and a 2.5- $\mu$ s rising and falling edge deglitch circuit reduce the likelihood of shutting the device down due to noise on VIN.

## Slow-Start/Enable (SS/ENA)

The slow-start/enable pin provides two functions; first, the pin acts as an enable (shutdown) control by keeping the device turned off until the voltage exceeds the start threshold voltage of approximately 1.2 V. When SS/ENA exceeds the enable threshold, device start up begins. The reference voltage fed to the error amplifier is linearly ramped up from 0 V to 0.891 V in 3.35 ms. Similarly, the converter output voltage reaches regulation in approximately 3.35 ms. Voltage hysteresis and a 2.5-µs falling edge deglitch circuit reduce the likelihood of triggering the enable due to noise.

The second function of the SS/ENA pin provides an external means of extending the slow-start time with a low-value capacitor connected between SS/ENA and AGND. Adding a capacitor to the SS/ENA pin has two effects on start-up. First, a delay occurs between release of the SS/ENA pin and start up of the output. The delay is proportional to the slow-start capacitor value and lasts until the SS/ENA pin reaches the enable threshold. The start-up delay is approximately:

$$t_{d} = C_{(SS)} \times \frac{1.2 \text{ V}}{5 \mu \text{A}}$$
(3)

Second, as the output becomes active, a brief ramp-up at the internal slow-start rate may be observed before the externally set slow-start rate takes control and the output rises at a rate proportional to the slow-start capacitor. The slow-start time set by the capacitor is approximately:

$$t_{(SS)} = C_{(SS)} \times \frac{0.7 \text{ V}}{5 \mu \text{A}}$$
(4)

The actual slow-start is likely to be less than the above approximation due to the brief ramp-up at the internal rate.

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## VBIAS Regulator (VBIAS)

The VBIAS regulator provides internal analog and digital blocks with a stable supply voltage over variations in junction temperature and input voltage. A high quality, low-ESR, ceramic bypass capacitor is required on the VBIAS pin. X7R or X5R grade dielectrics are recommended because their values are more stable over temperature. The bypass capacitor should be placed close to the BVIAS pin and returned to AGND. External loading on VBIAS is allowed, with the caution that internal circuits require a minimum BVIAS of 2.7 V, and external loads on VBIAS with ac or digital switching noise may degrade performance. The VBIAS pin may be useful as a reference voltage for external circuits.

## Voltage Reference

The voltage reference system produces a precise  $V_{ref}$  signal by scaling the output of a temperature stable bandgap circuit. During manufacture, the bandgap and scaling circuits are trimmed to produce 0.891 V at the output of the error amplifier, with the amplifier connected as a voltage follower. The trim procedure adds to the high precision regulation of the TPS54310, since it cancels offset errors in the scale and error amplifier circuits

## Oscillator and PWM Ramp

The oscillator frequency can be set to internally fixed values of 350 kHz or 550 kHz using the SYNC pin as a static digital input. If a different frequency of operation is required for the application, the oscillator frequency can be externally adjusted from 280 kHz to 700 kHz by connecting a resistor to the RT pin to ground and floating the SYNC pin. The switching frequency is approximated by the following equation, where R is the resistance from RT to AGND:

SWITCHING FREQUENCY = 
$$\frac{100 \text{ k}\Omega}{\text{R}} \times 500 \text{ kHz}$$
 (5)

External synchronization of the PWM ramp is possible over the frequency range of 330 kHz to 700 kHz by driving a synchronization signal into SYNC and connecting a resistor from RT to AGND. Choose an RT resistor that sets the free-running frequency to 80% of the synchronization signal. Table 1 summarizes the frequency selection configurations.

Table 1. Summa	y of the Fre	quency Selectio	n Configurations
----------------	--------------	-----------------	------------------

SWITCHING FREQUENCY	SYNC PIN	RT PIN
350 kHz, internally set	Float or AGND	Float
550 kHz, internally set	≥ 2.5 V	Float
Externally set 280 kHz to 700 kHz	Float	R = 68 k to 180 k
Externally synchronized frequency	Synchronization signal	R = RT value for 80% of external synchronization frequency

## **Error Amplifier**

The high performance, wide bandwidth, voltage error amplifier sets the TPS54310 apart from most dc/dc converters. The user is given the flexibility to use a wide range of output L and C filter components to suit the particular needs of the application. Type 2 or type 3 compensation can be employed using external compensation components.

## **PWM Control**

Signals from the error amplifier output, oscillator, and current limit circuit are processed by the PWM control logic. Referring to the internal block diagram, the control logic includes the PWM comparator, OR gate, PWM latch, and portions of the adaptive dead-time and control logic block. During steady-state operation below the current limit threshold, the PWM comparator output and oscillator pulse train alternately reset and set the PWM latch. Once the PWM latch is set, the low-side FET remains on for a minimum duration set by the oscillator pulse duration. During this period, the PWM ramp discharges rapidly to its valley voltage. When the ramp begins to charge back up, the low-side FET turns off and high-side FET turns on. As the PWM ramp voltage exceeds the error amplifier output voltage, the PWM comparator resets the latch, thus turning off the high-side FET and turning on the low-side FET. The low-side FET remains on until the next oscillator pulse discharges the PWM ramp.

During transient conditions, the error amplifier output could be below the PWM ramp valley voltage or above the PWM peak voltage. If the error amplifier is high, the PWM latch is never reset and the high-side FET remains on until the oscillator pulse signals the control logic to turn the high-side FET off and the low-side FET on. The device operates at its maximum duty cycle until the output voltage rises to the regulation set-point, setting VSENSE to approximately the same voltage as  $V_{ref}$ . If the error amplifier output is low, the PWM latch is continually reset and the high-side FET does not turn on. The

low-side FET remains on until the VSENSE voltage decreases to a range that allows the PWM comparator to change states. The TPS54310 is capable of sinking current continuously until the output reaches the regulation set-point.

If the current limit comparator trips for longer than 100 ns, the PWM latch resets before the PWM ramp exceeds the error amplifier output. The high-side FET turns off and low-side FET turns on to decrease the energy in the output inductor and consequently the output current. This process is repeated each cycle in which the current limit comparator is tripped.

## **Dead-Time Control and MOSFET Drivers**

Adaptive dead-time control prevents shoot-through current from flowing in both N-channel power MOSFETs during the switching transitions by actively controlling the turn-on times of the MOSFET drivers. The high-side driver does not turn on until the gate drive voltage to the low-side FET is below 2 V. The low-side driver does not turn on until the voltage at the gate of the high-side MOSFETs is below 2 V. The high-side and low-side drivers are designed with 300-mA source and sink capability to quickly drive the power MOSFETs gates. The low-side driver is supplied from VIN, while the high-side drive is supplied from the BOOT pin. A bootstrap circuit uses an external BOOT capacitor and an internal 2.5-Ω bootstrap switch connected between the VIN and BOOT pins. The integrated bootstrap switch improves drive efficiency and reduces external component count.

## **Overcurrent Protection**

The cycle by cycle current limiting is achieved by sensing the current flowing through the high-side MOSFET and differential amplifier and comparing it to the preset overcurrent threshold. The high-side MOSFET is turned off within 200 ns of reaching the current limit threshold. A 100-ns leading edge blanking circuit prevents false tripping of the current limit. Current limit detection occurs only when current flows from VIN to PH when sourcing current to the output filter. Load protection during current sink operation is provided by thermal shutdown.



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## **Thermal Shutdown**

The device uses the thermal shutdown to turn off the power MOSFETs and disable the controller if the junction temperature exceeds 150°C. The device is released from shutdown when the junction temperature decreases to 10°C below the thermal shutdown trip point and starts up under control of the slow-start circuit. Thermal shutdown provides protection when an overload condition is sustained for several milliseconds. With a persistent fault condition, the device cycles continuously; starting up by control of the soft-start circuit, heating up due to the fault, and then shutting down upon reaching the thermal shutdown point.

## Power Good (PWRGD)

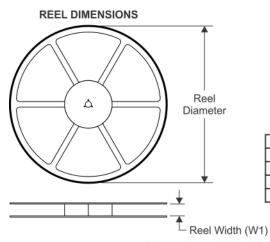
The power good circuit monitors for under voltage conditions on VSENSE. If the voltage on VSENSE is 10% below the reference voltage, the open-drain PWRGD output is pulled low. PWRGD is also pulled low if VIN is less than the UVLO threshold, or SS/ENA is low, or thermal shutdown is asserted. When VIN = UVLO threshold, SS/ENA = enable threshold, and VSENSE > 90% of V<sub>ref</sub>, the open drain output of the PWRGD pin is high. A hysteresis voltage equal to 3% of V<sub>ref</sub> and a 35-µs falling edge deglitch circuit prevent tripping of the power good comparator due to high frequency noise.

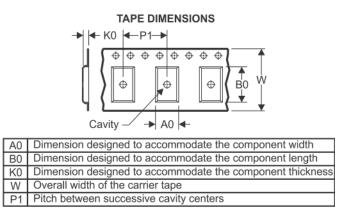
# PACKAGE MATERIALS INFORMATION

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## TAPE AND REEL INFORMATION





## QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



,	All dimensions are nominal												
	Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
	TPS54310MPWPREP	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1

TEXAS INSTRUMENTS

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12-Feb-2019

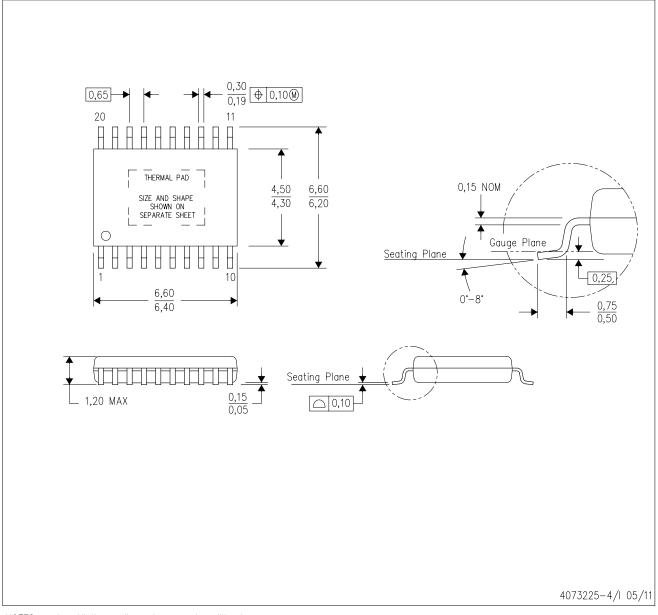


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS54310MPWPREP	HTSSOP	PWP	20	2000	350.0	350.0	43.0

PWP (R-PDSO-G20)

PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



All linear dimensions are in millimeters. NOTES: Α.

- Β. This drawing is subject to change without notice.
- Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side. C.
- This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad D.
- Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>. E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions. E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



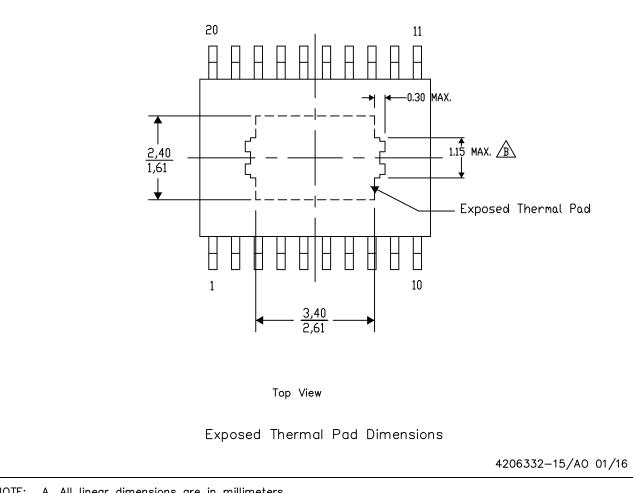
#### PowerPAD<sup>™</sup> SMALL PLASTIC OUTLINE PWP (R-PDSO-G20)

#### THERMAL INFORMATION

This PowerPAD<sup>™</sup> package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.

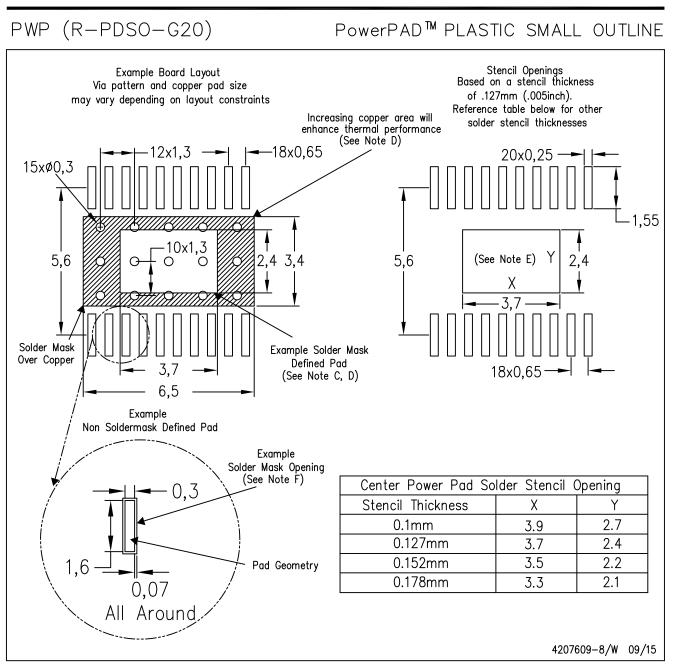


NOTE: A. All linear dimensions are in millimeters

B. Exposed tie strap features may not be present.

PowerPAD is a trademark of Texas Instruments





NOTES:

Α.

B. This drawing is subject to change without notice.

All linear dimensions are in millimeters.

- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com> Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



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