

Large Current External FET Controller Type Switching Regulator

Dual-output, high voltage, high-efficiency step-down switching controller



BD9012KV

●Overview

The BD9012KV is a 2-ch synchronous controller with rectification switching for enhanced power management efficiency. It supports a wide input range, enabling low power consumption ecodeign for an array of electronics.

●Features

- 1) Wide input voltage range: 4.5V to 30V
- 2) Precision voltage references: $0.8V \pm 1\%$
- 3) FET direct drive
- 4) Rectification switching for increased efficiency
- 5) Variable frequency: 250k to 1200kHz (external synchronization to 1200kHz)
- 6) Built-in selected auto remove over current protection
- 7) Built-in independent power up/power down sequencing control
- 8) Make various application , step-down , step-up and step-up-down
- 9) Small footprint packages: VQFP48C

●Applications

Car audio and navigation systems, CRTTV, LCDTV, PDPTV, STB, DVD, and PC systems, portable CD and DVD players, etc.

●Absolute Maximum Ratings (Ta=25°C)

| Parameter | Symbol | Limits | Unit | Parameter | Symbol | Limits | Unit |
|-----------------------|---------------|--------|------|------------------------------|--------------|-------------|------|
| VCC Voltage | VCC | 34 *1 | V | VREG33 Voltage | VREG33 | VREG5 | V |
| EXTVCC Voltage | EXTVCC | 34 *1 | V | SS1,2, FB1,2 Voltage | SS1,2, FB1,2 | | |
| VCCCL1,2 Voltage | VCCCL1,2 | 34 | V | COMP1,2 Voltage | COMP1,2 | | |
| CL1,2 Voltage | CL1,2 | 34 | V | DET1,2 Voltage | DET1,2 | | |
| SW1,2 Voltage | SW1,2 | 34 *1 | V | RT, SYNC Voltage | RT, SYNC | | |
| BOOT1,2 Voltage | BOOT1,2 | 40 *1 | V | Power Dissipation | Pd | 1.1 *2 | W |
| BOOT1,2-SW1,2 Voltage | BOOT1,2-SW1,2 | 7 *1 | V | Operating Temperature Range | Topr | -40 to +105 | °C |
| STB, EN1,2 Voltage | STB, EN1,2 | VCC | V | Storage Temperature Range | Tstg | -55 to +150 | °C |
| VREG5,5A Voltage | VREG5,5A | 7 *1 | V | Maximum Junction Temperature | Tj | +150 | °C |

*1 Regardless of the listed rating, do not exceed Pd in any circumstances.

*2 Pd de-rated at 7mW/°C for temperature above Ta=25°C, Mounted on PCB 70mm×70mm×1.6mm.

●Operating conditions (Ta=25°C)

| Parameter | Symbol | Min. | Typ. | Max. | Unit |
|------------------------|---------|----------------------|------|----------------------|------|
| Input voltage 1 | EXTVCC | 4.5 ^{*1 *2} | 12 | 30 | V |
| Input voltage 2 | VCC | 4.5 ^{*1 *2} | 12 | 30 | V |
| BOOT—SW voltage | BOOT—SW | 4.5 | 5 | VREG5 | V |
| Carrier frequency | OSC | 250 | 300 | 1200 | kHz |
| Synchronous frequency | SYNC | OSC | - | 1200 ^{*3*4} | kHz |
| Synchronous pulse duty | Duty | 40 | 50 | 60 | % |
| Min OFF pulse | TMIN | - | 150 | - | nsec |

★This product is not designed to provide resistance against radiation.

*1 After more than 4.5V, voltage range.

*2 In case of using less than 6V, Short to VCC, EXTVCC and VREG5.

*3 Please do not exceed OSC×1.5.

*4 Do not do such things as switching over to internal oscillating frequency while external synchronization frequency is used.

●Electrical characteristics (Unless otherwise specified, Ta=25°C VCC=12V STB=5V EN1,2=5V)

| Parameter | Symbol | Limit | | | Unit | Conditions |
|--|------------|-------|-------|-------|------|---------------------------|
| | | Min. | Typ. | Max. | | |
| VIN bias current | IIN | - | 6 | 10 | mA | |
| Shutdown mode current | IST | - | 0 | 10 | μA | VSTB=0V |
| [Error Amp Block] | | | | | | |
| Feedback reference voltage | VOB | 0.792 | 0.800 | 0.808 | V | |
| Feedback reference voltage (Ta=-40 to 105°C) | VOB+ | 0.784 | 0.800 | 0.816 | V | Ta=-40 to 105°C ※ |
| Open circuit voltage gain | Averr | - | 46 | - | dB | |
| VO input bias current | IVo+ | - | - | 1 | μA | |
| [Oscillator] | | | | | | |
| Carrier frequency | FOSC | 900 | 1000 | 1100 | kHz | RT=27 kΩ |
| Synchronous frequency | Fsync | - | 1200 | - | kHz | RT=27 kΩ, SYNC=1200kHz |
| [Over Current Protection Block] | | | | | | |
| CL threshold voltage | Vswth | 70 | 90 | 110 | mV | |
| CL threshold voltage (Ta=-40 to 105°C) | Vswth+ | 67 | 90 | 113 | mV | Ta=-40 to 105°C ※ |
| [VREG Block] | | | | | | |
| VREG5 output voltage | VREG5 | 4.8 | 5 | 5.2 | V | IREF=6mA |
| VREG33 reference voltage | VREG33 | 3.0 | 3.3 | 3.6 | V | IREG=6mA |
| VREG5 threshold voltage | VREG_UVLO | 2.6 | 2.8 | 3.0 | V | VREG:Sweep down |
| VREG5 hysteresis voltage | DVREG_UVLO | 50 | 100 | 200 | mV | VREG:Sweep up |
| [Soft start block] | | | | | | |
| Charge current | ISS | 6.5 | 10 | 13.5 | μA | VSS=1V |
| Charge current (Ta=-40 to 105°C) | ISS+ | 6 | 10 | 14 | μA | VSS=1V, Ta=-40 to 105°C ※ |

Note: Not all shipped products are subject to outgoing inspection.

●Reference data (Unless otherwise specified, Ta=25°C)

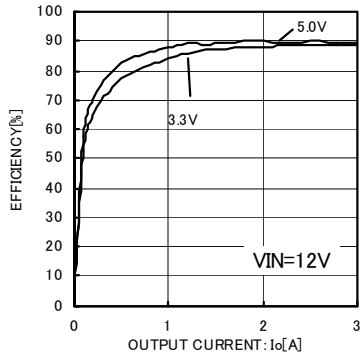


Fig.1 Efficiency 1

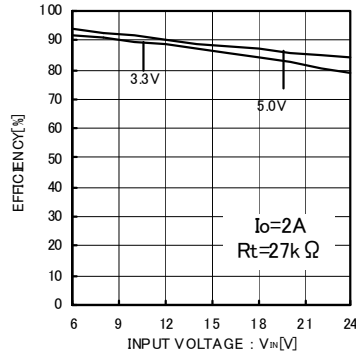


Fig.2 Efficiency 2

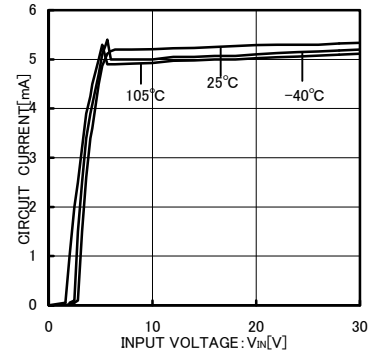


Fig.3 Circuit current

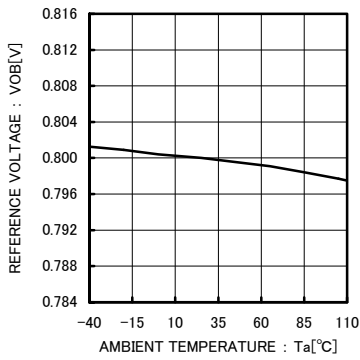


Fig.4 Reference voltage vs. temperature characteristics

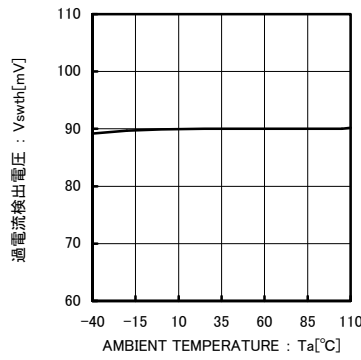


Fig.5 Over current detection vs. temperature characteristics

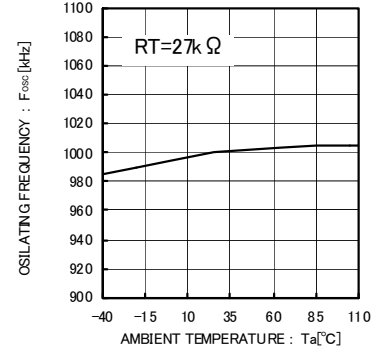


Fig.6 Frequency vs. temperature characteristics

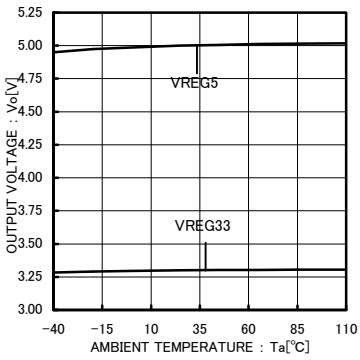


Fig.7 Internal Reg vs. temperature characteristics

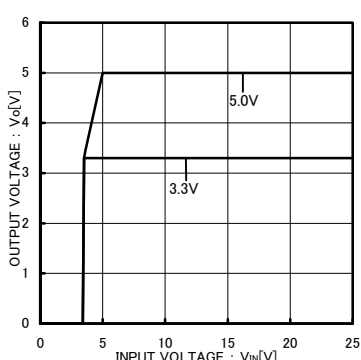


Fig.8 Line regulation

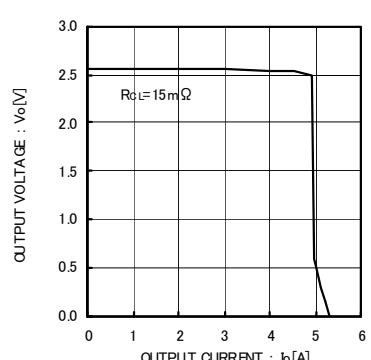


Fig.9 Load regulation

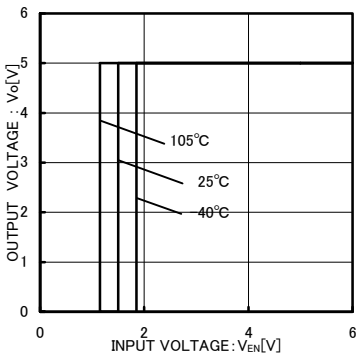


Fig.10 EN threshold voltage

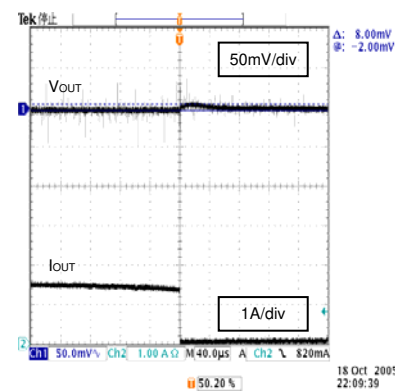


Fig.11 Load transient response 1

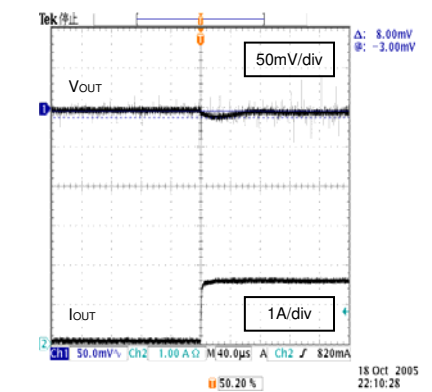


Fig.12 Load transient response 2

● Block diagram

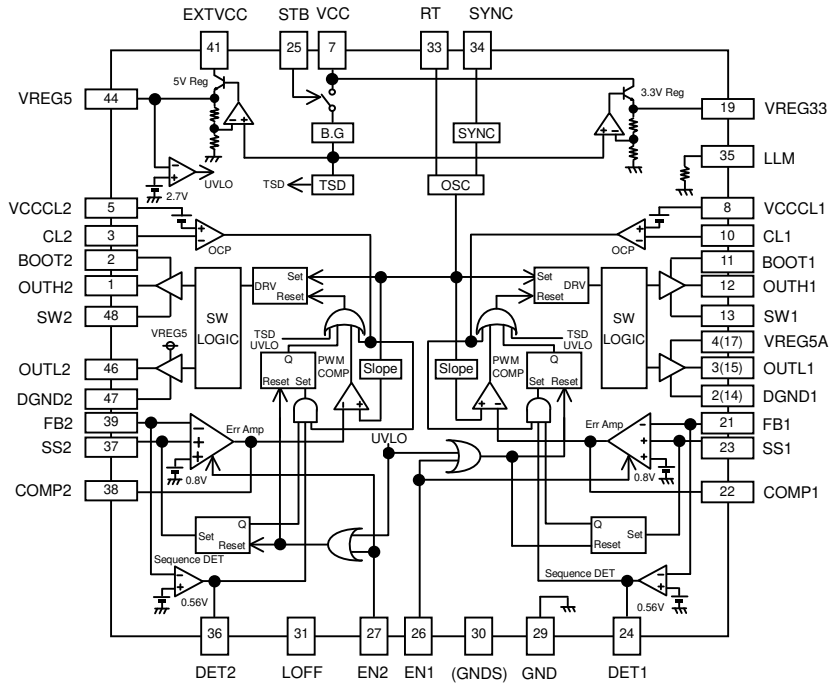


Fig-13

● Pin configuration

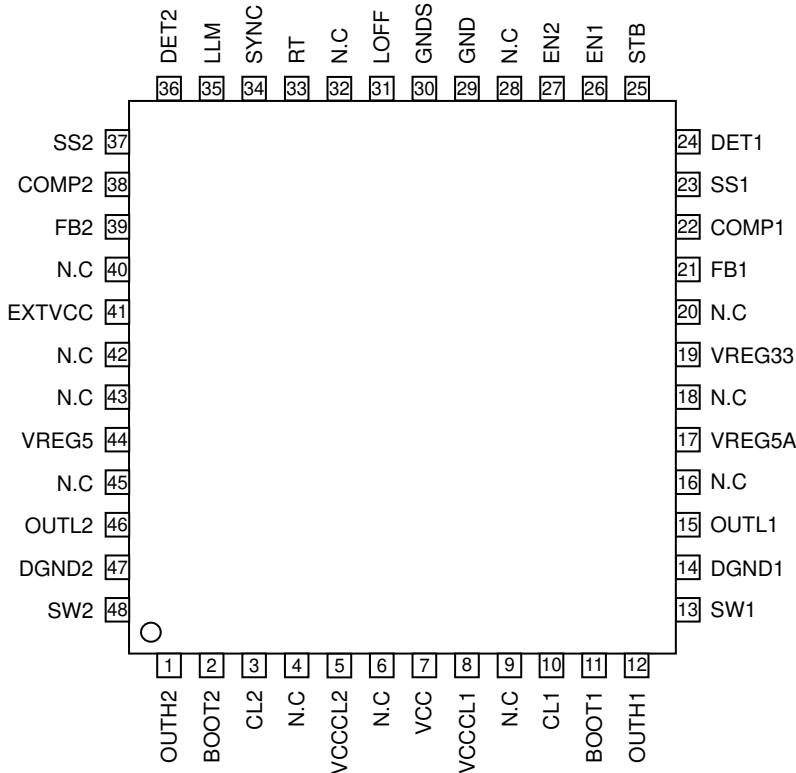


Fig-15

● Pin function table

| Pin No. | Pin name | Function |
|---------|----------|--------------------------------------|
| 1 | OUTH2 | High side FET gate drive pin 2 |
| 2 | BOOT2 | OUTH2 driver power pin |
| 3 | CL2 | Over current detection pin 2 |
| 4 | N.C | Non-connect (unused) pin |
| 5 | VCCCL2 | Over current detection VCC2 |
| 6 | N.C | Non-connect (unused) pin |
| 7 | VCC | Input power pin |
| 8 | VCCCL1 | Over current detection CC1 |
| 9 | N.C | Non-connect (unused) pin |
| 10 | CL1 | Over current detection setting pin 1 |
| 11 | BOOT1 | OUTH1 driver power pin |
| 12 | OUTH1 | High side FET gate drive pin 1 |
| 13 | SW1 | High side FET source pin 1 |
| 14 | DGND1 | Low side FET source pin 1 |
| 15 | OUTL1 | Low side FET gate drive pin 1 |
| 16 | N.C | Non-connect (unused) pin |
| 17 | VREG5A | FET drive REG input |
| 18 | N.C | Non-connect (unused) pin |
| 19 | VREG33 | Reference input REG output |
| 20 | N.C | Non-connect (unused) pin |
| 21 | FB1 | Error amp input 1 |
| 22 | COMP1 | Error amp output 1 |
| 23 | SS1 | Soft start setting pin 1 |
| 24 | DET1 | FB detector output 1 |
| 25 | STB | Standby ON/OFF pin |
| 26 | EN1 | Output 1 ON/OFF pin |
| 27 | EN2 | Output 2 ON/OFF pin |
| 28 | N.C | Non-connect (unused) pin |
| 29 | GND | Ground |
| 30 | GNDS | Sense ground |
| 31 | LOFF | Test Mode Terminal |
| 32 | N.C | Non-connect (unused) pin |
| 33 | RT | Switching frequency setting pin |
| 34 | SYNC | External synchronous pulse input pin |
| 35 | LLM | Built-in pull-down resistor pin |
| 36 | DET2 | FB detector output 2 |
| 37 | SS2 | Soft start setting pin 2 |
| 38 | COMP2 | Error amp output 2 |
| 39 | FB2 | Error amp input 2 |
| 40 | N.C | Non-connect (unused) pin |
| 41 | EXTVCC | External power input pin |
| 42 | N.C | Non-connect (unused) pin |
| 43 | N.C | Non-connect (unused) pin |
| 44 | VREG5 | FET drive REG output |
| 45 | N.C | Non-connect (unused) pin |
| 46 | OUTL2 | Low side FET gate drive pin 2 |
| 47 | DGND2 | Low side FET source pin 2 |
| 48 | SW2 | High side FET source pin 2 |

● Block functional descriptions

- Error amp
The error amp compares output feedback voltage to the 0.8V reference voltage and provides the comparison result as COMP voltage, which is used to determine the switching Duty. COMP voltage is limited to the SS voltage, since soft start at power up is based on SS pin voltage.
- Oscillator (OSC)
Oscillation frequency is determined by the switching frequency pin (RT) in this block. The frequency can be set between 250kHz and 550kHz.
- SLOPE
The SLOPE block uses the clock produced by the oscillator to generate a triangular wave, and sends the wave to the PWM comparator.
- PWM COMP
The PWM comparator determines switching Duty by comparing the COMP voltage, output from the error amp, with the triangular wave from the SLOPE block. Switching duty is limited to a percentage of the internal maximum duty, and thus cannot be 100% of the maximum.
- Reference voltage (5Vreg, 33Vreg)
This block generates the internal reference voltages: 5V and 3.3V.
- External synchronization (SYNC)
Determines the switching frequency, based on the external pulse applied.
- Over current protection (OCP)
Over current protection is activated when the VCCCL-CL voltage reaches or exceeds 90mV. When over current protection is active, Duty is low, and output voltage also decreases. When LOFF=L, the output voltage has fallen to 70% or below and output is latched OFF. The OFF latch mode ends when the latch is set to STB, EN.
- Sequence control (Sequence DET)
Compares FB voltage with reference voltage (0.56V) and outputs the result as DET.
- Protection circuits (UVLO/TSD)
The UVLO lock out function is activated when VREG falls to about 2.8V, while TSD turns outputs OFF when the chip temperature reaches or exceeds 150°C. Output is restored when temperature falls back below the threshold value.

● Application circuit example (Parentheses indicate VQFP48C pin numbers)

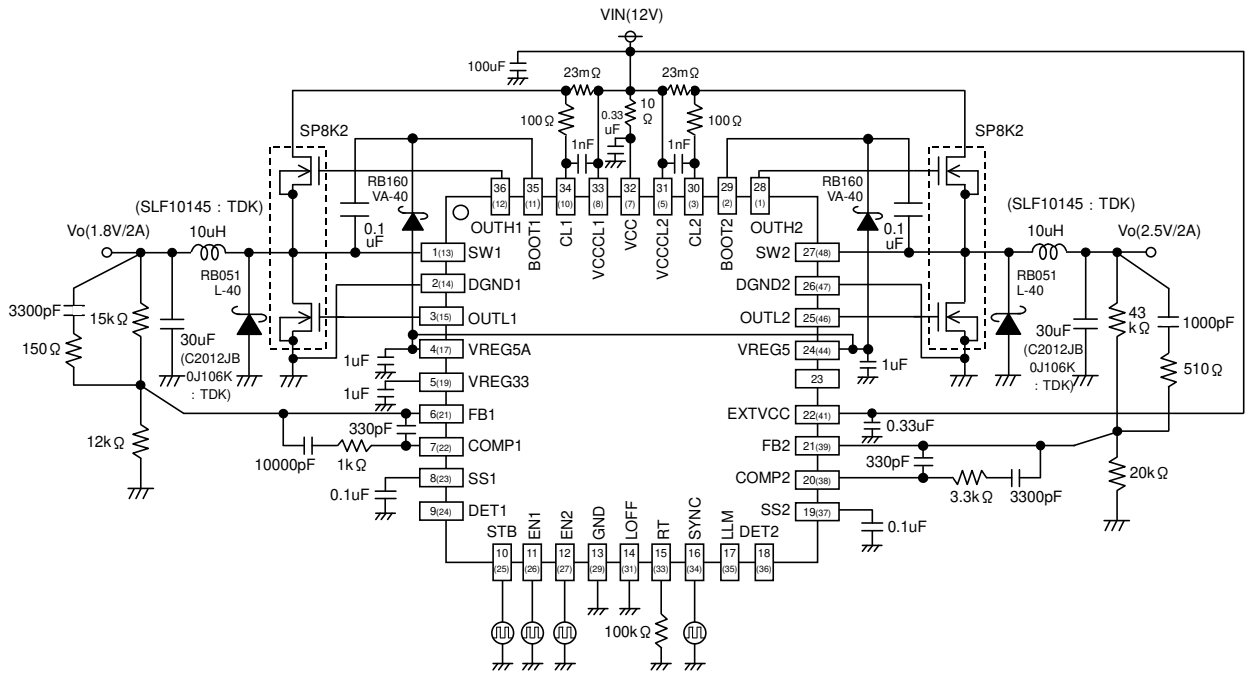


Fig-16B (Step-Down : Cout=Ceramic Capacitor)

There are many factors(The PCB board layout, Output Current, etc.)that can affect the DCDC characteristics. Please verify and confirm using practical applications.

●Application component selection

(1) Setting the output L value

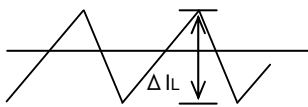


Fig-17

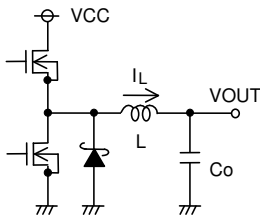


Fig-18

Output ripple current

The coil value significantly influences the output ripple current. Thus, as seen in equation (5), the larger the coil, and the higher the switching frequency, the lower the drop in ripple current.

$$\Delta I_L = \frac{(V_{CC} - V_{OUT}) \times V_{OUT}}{L \times V_{CC} \times f} \quad [A] \dots (5)$$

The optimal output ripple current setting is 30% of maximum current.

$$\Delta I_L = 0.3 \times I_{OUTmax} [A] \dots (6)$$

$$L = \frac{(V_{CC} - V_{OUT}) \times V_{OUT}}{\Delta I_L \times V_{CC} \times f} \quad [H] \dots (7)$$

(ΔI_L : output ripple current f : switching frequency)

※Outputting a current in excess of the coil current rating will cause magnetic saturation of the coil and decrease efficiency.

Please establish sufficient margin to ensure that peak current does not exceed the coil current rating.

※Use low resistance (DCR, ACR) coils to minimize coil loss and increase efficiency.

(2) Setting the output capacitor Co value

Select the output capacitor with the highest value for ripple voltage (VPP) tolerance and maximum drop voltage (at rapid load change). The following equation is used to determine the output ripple voltage.

$$\text{Step down} \quad \Delta V_{PP} = \Delta I_L \times R_{ESR} + \frac{\Delta I_L}{C_o} \times \frac{V_o}{V_{cc}} \times \frac{1}{f} \quad [V] \quad \text{Note: } f : \text{ switching frequency}$$

Be sure to keep the output Co setting within the allowable ripple voltage range.

※Please allow sufficient output voltage margin in establishing the capacitor rating. Note that low-ESR capacitors enable lower output ripple voltage.

Also, to meet the requirement for setting the output startup time parameter within the soft start time range, please factor in the conditions described in the capacitance equation (9) for output capacitors, below.

$$C_o \leq \frac{T_{SS} \times (\text{Limit} - I_{OUT})}{V_{OUT}} \dots (9) \quad \begin{array}{l} T_{SS} : \text{ soft start time} \\ I_{Limit} : \text{ over current detection value (2/16) reference} \end{array}$$

Note: less than optimal capacitance values may cause problems at startup.

(3) Input capacitor selection

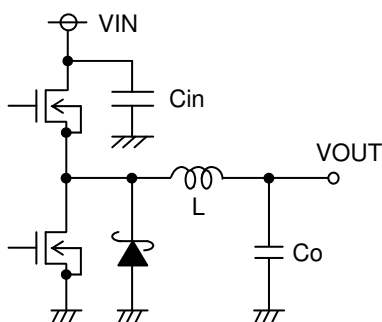


Fig-19

Input capacitor

The input capacitor serves to lower the output impedance of the power source connected to the input pin (VCC). Increased power supply output impedance can cause input voltage (VCC) instability, and may negatively impact oscillation and ripple rejection characteristics. Therefore, be certain to establish an input capacitor in close proximity to the VCC and GND pins. Select a low-ESR capacitor with the required ripple current capacity and the capability to withstand temperature changes without wide tolerance fluctuations. The ripple current IRMSS is determined using equation (10).

$$I_{RMS} = I_{OUT} \times \frac{\sqrt{V_{OUT} (V_{CC} - V_{OUT})}}{V_{CC}} \quad [A] \dots (10)$$

Also, be certain to ascertain the operating temperature, load range and MOSFET conditions for the application in which the capacitor will be used, since capacitor performance is heavily dependent on the application's input power characteristics, substrate wiring and MOSFET gate drain capacity.

(4) Feedback resistor design

Please refer to the following equation in determining the proper feedback resistance. The recommended setting is in a range between 10kΩ and 330kΩ. Resistance less than 10kΩ risks decreased power efficiency, while setting the resistance value higher than 330kΩ will result in an internal error amp input bias current of 0.2uA increasing the offset voltage. Please use it with 150nsec or more so that there is a possibility that the output becomes unstable when the output pulse width is small. (12)

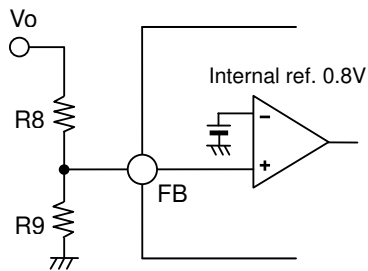


Fig-20

$$V_o = \frac{R8 + R9}{R9} \times 0.8 [V] \dots (11)$$

$$\frac{V_o}{V_{in}} \times \frac{1}{f} \geq 150ns \dots (12)$$

(5) Setting switching frequency

The triangular wave switching frequency can be set by connecting a resistor to the RT 15(33) pin. The RT sets the frequency by adjusting the charge/discharge current in relation to the internal capacitor. Refer to the figure below in determining proper RT resistance, noting that the recommended resistance setting is between 50kΩ and 130kΩ. Settings outside this range may render the switching function inoperable, and proper operation of the controller overall cannot be guaranteed when unsupported resistance values are used.

Fig-21 RT vs. switching frequency

(6) Setting the soft start delay

The soft start function is necessary to prevent an inrush of coil current and output voltage overshoot at startup. The figure below shows the relation between soft start delay time and capacitance, which can be calculated using equation (12) at right.

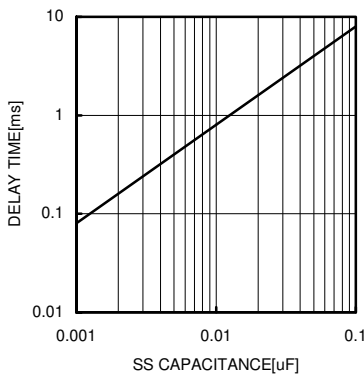


Fig-22 SS capacitance vs. delay time

$$TSS = \frac{0.8V(typ.) \times CSS}{ISS(10 \mu A Typ.)} [sec] \dots (12)$$

Recommended capacitance values are between 0.01uF and 0.1uF. Capacitance lower than 0.01uF may generate output overshoots. Please use high accuracy components (such as X5R) when implementing sequential startups involving other power sources. Be sure to test the actual devices and applications to be used, since the soft start time varies, depending on input voltage, output voltage and capacitance, coils and other characteristics.

(7) Setting over current detection values

The current limit value (ILimit) is determined by the resistance of the RCL established between CL and VCCCL.

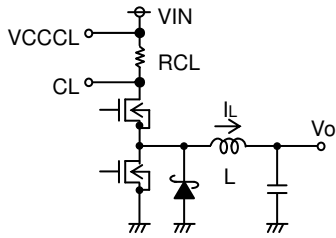


Fig-23

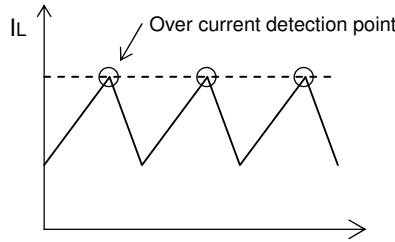


Fig-24

$$I_{Limit} = \frac{90m}{RCL} [A] \dots (13)$$

When the current goes beyond the threshold value, the current can be limited by reducing the ON Duty Cycle. When the load goes back to the normal operation, the output voltage also becomes back on to the specific level.

The current limit value

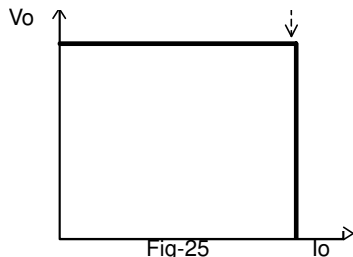


Fig-25

(8) Method for determining phase compensation

Conditions for application stability

Feedback stability conditions are as follows:

- When gain is 1 (0dB) and phase shift is 150° or less (i.e., phase margin is at least 30°): a dual-output high-frequency step-down switching regulator is required

Additionally, in DC/DC applications, sampling is based on the switching frequency; therefore, overall GBW may be set at no more than 1/10 the switching frequency. In summary, target characteristics for application stability are:

- Phase shift of 150° or less (i.e., phase margin of 30° or more) with gain of 1 (0dB)
- GBW (i.e., gain 0dB frequency) no more than 1/10 the switching frequency.

Stability conditions mandate a relatively higher switching frequency, in order to limit GBW enough to increase response.

The key to achieving successful stabilization using phase compensation is to cancel the secondary phase margin/delay (-180°) generated by LC resonance, by employing a dual phase lead. In short, adding two phase leads stabilizes the application.

GBW (the frequency at gain 1) is determined by the phase compensation capacitor connected to the error amp. Thus, a larger capacitor will serve to lower GBW if desired.

- ① General use integrator (low-pass filter) ② Integrator open loop characteristics

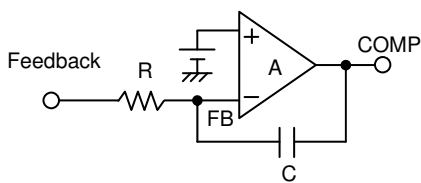


Fig-26

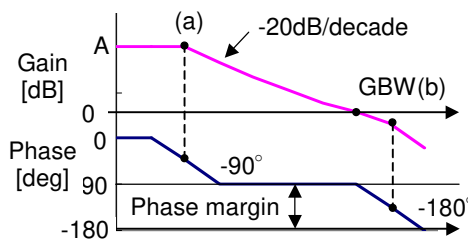


Fig-27

$$\text{point (a) } f_a = \frac{1}{2\pi RCA} \cdot 1.25[\text{Hz}]$$

$$\text{point (b) } f_b = \text{GBW} \cdot \frac{1}{2\pi RC} [\text{Hz}]$$

The error amp is provided with phase compensation similar to that depicted in figures ① and ② above and thus serves as the system's low-pass filter.

In DC/DC converter applications, R is established parallel to the feedback resistance.

When electrolytic or other high-ESR output capacitors are used:

Phase compensation is relatively simple for applications employing high-ESR output capacitors (on the order of several Ω). In DC/DC converter applications, where LC resonance circuits are always incorporated, the phase margin at these locations is -180° . However, wherever ESR is present, a 90° phase lead is generated, limiting the net phase margin to -90° in the presence of ESR. Since the desired phase margin is in a range less than 150° , this is a highly advantageous approach in terms of the phase margin. However, it also has the drawback of increasing output voltage ripple components.

③ LC resonance circuit

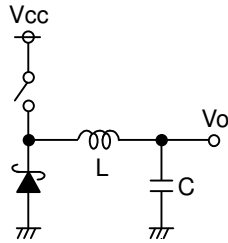


Fig-28

$$f_r = \frac{1}{2\pi\sqrt{LC}} \text{ [Hz]}$$

Resonance point phase margin -180°

④ ESR connected

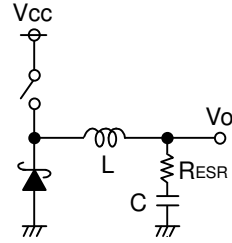


Fig-29

$$f_r = \frac{\text{resonance point 1}}{2\pi\sqrt{LC}} \text{ [Hz] : Resonance Point}$$

$$f_{ESR} = \frac{1}{2\pi R_{ESR}C} \text{ [Hz] : Zero}$$

-90° : Pole

Since ESR changes the phase characteristics, only one phase lead need be provided for high-ESR applications. Please choose one of the following methods to add the phase lead.

⑤ Add C to feedback resistor

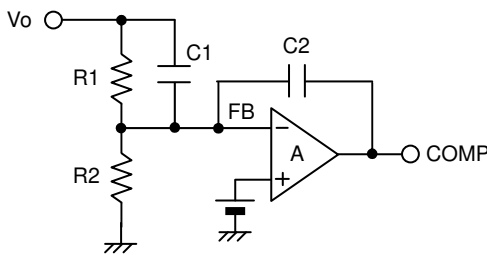


Fig-30

$$\text{Phase lead } f_z = \frac{1}{2\pi C_1 R_1} \text{ [Hz]}$$

⑥ Add R3 to aggregator

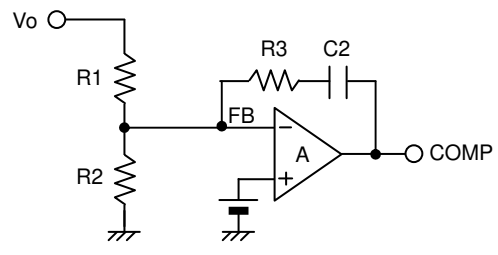


Fig-31

$$\text{Phase lead } f_z = \frac{1}{2\pi C_2 R_3} \text{ [Hz]}$$

Set the phase lead frequency close to the LC resonance frequency in order to cancel the LC resonance.

When using ceramic, OS-CON, or other low-ESR capacitors for the output capacitor:

Where low-ESR (on the order of tens of $m\Omega$) output capacitors are employed, a two phase-lead insertion scheme is required, but this is different from the approach described in figure ③~⑥, since in this case the LC resonance gives rise to a 180° phase margin/delay. Here, a phase compensation method such as that shown in figure ⑦ below can be implemented.

⑦ Phase compensation provided by secondary (dual) phase lead

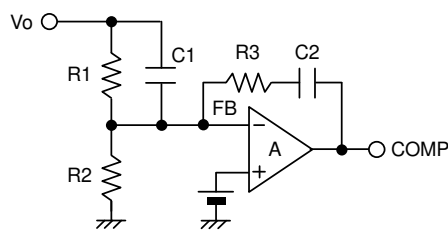


Fig-32

$$\text{Phase lead } f_{z1} = \frac{1}{2\pi R_1 C_1} \text{ [Hz]}$$

$$\text{Phase lead } f_{z2} = \frac{1}{2\pi R_3 C_2} \text{ [Hz]}$$

$$\text{LC resonance frequency } f_r = \frac{1}{2\pi\sqrt{LC}} \text{ [Hz]}$$

Once the phase-lead frequency is determined, it should be set close to the LC resonance frequency.

This technique simplifies the phase topology of the DCDC Converter. Therefore, it might need a certain amount of trial-and-error process. There are many factors(The PCB board layout, Output Current, etc.)that can affect the DCDC characteristics. Please verify and confirm using practical applications.

(9) MOSFET selection

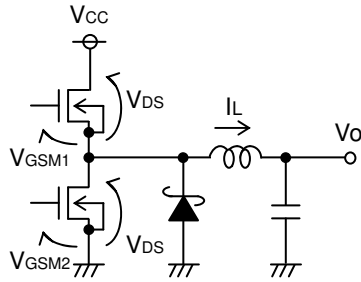


Fig-33

FET uses Nch MOS

- $V_{DS} > V_{CC}$
- $V_{GSM1} > \text{BOOT-SW interval voltage}$
- $V_{GSM2} > V_{REG5}$
- Allowable current $>$ voltage current + ripple current
- ※ Should be at least the over current protection value
- ※ Select a low ON-resistance MOSFET for highest efficiency

- The shoot-through may happen when the input parasitic capacitance of FET is extremely big or the Duty ratio is less than or equal to 10%. Less than or equal to 1000pF input parasitic capacitance is recommended. Please confirm operation on the actual application since this character is affected by PCB layout and components.

(10) Schottky barrier diode selection

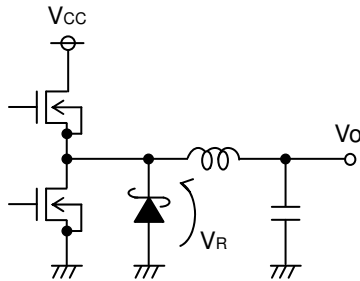


Fig-34

- Reverse voltage $V_R > V_{CC}$
- Allowable current $>$ voltage current + ripple current
- ※ Should be at least the over current protection value
- ※ Select a low forward voltage, fast recovery diode for highest efficiency

(11) Sequence function

● Circuit diagram

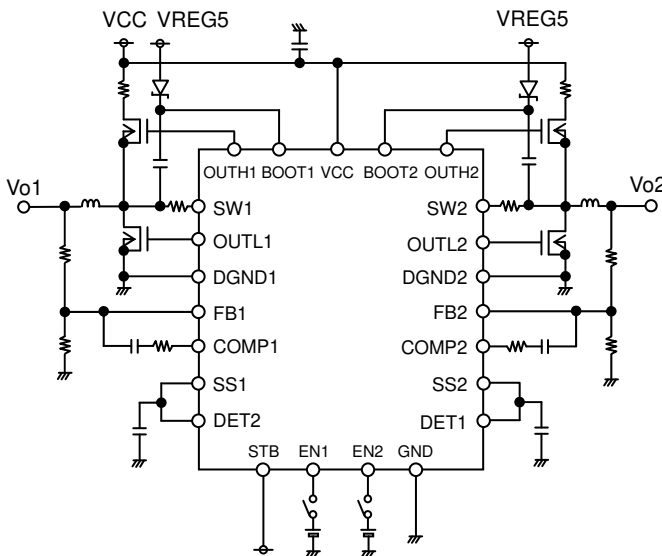
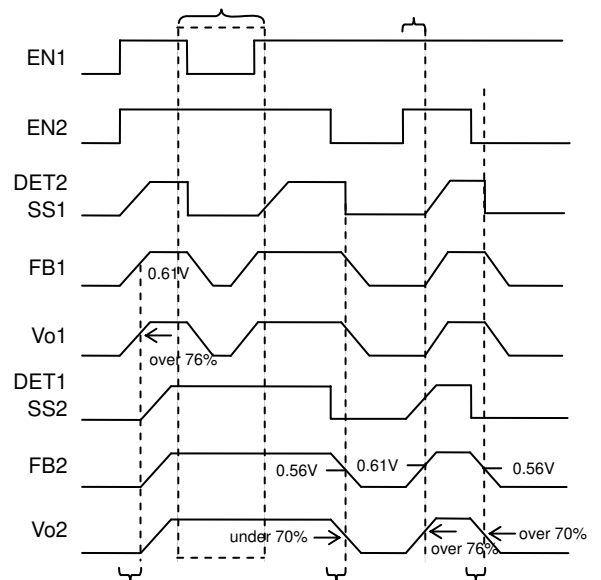


Fig-35

● Timing chart

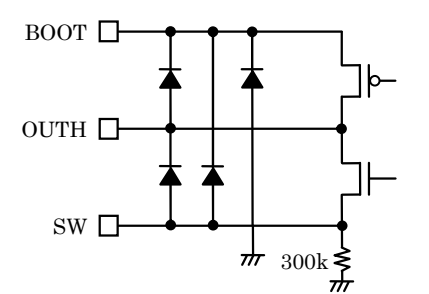
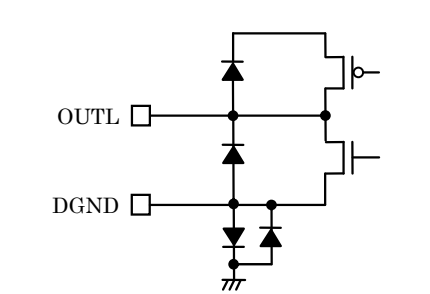
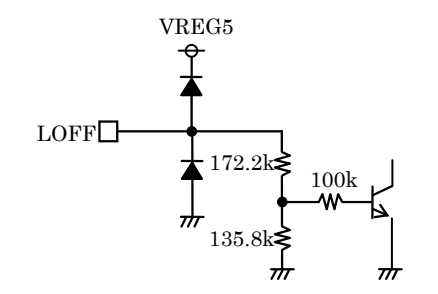
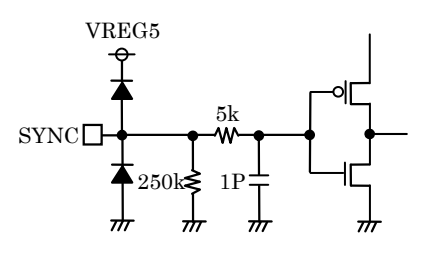
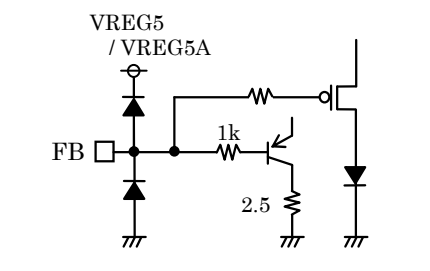
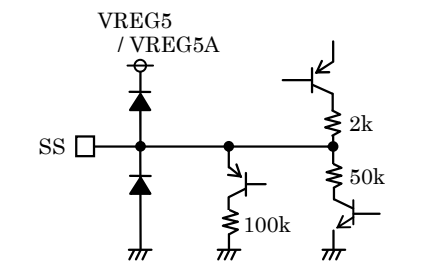
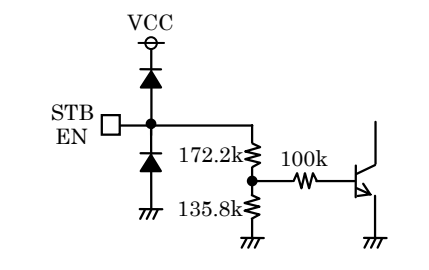
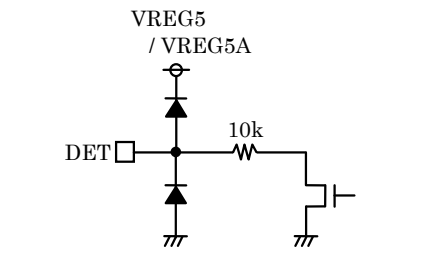
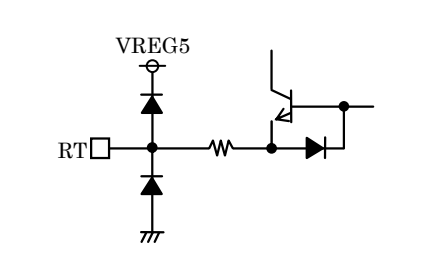
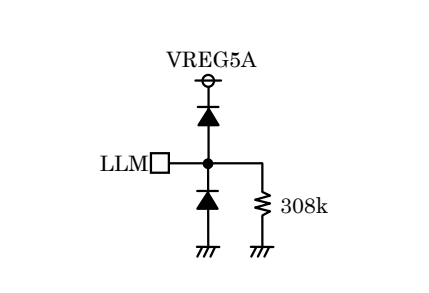
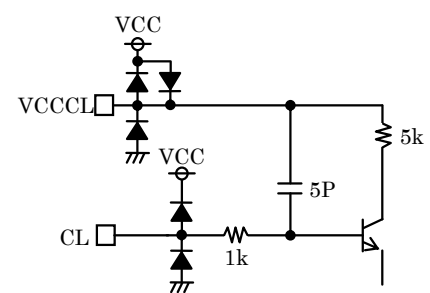
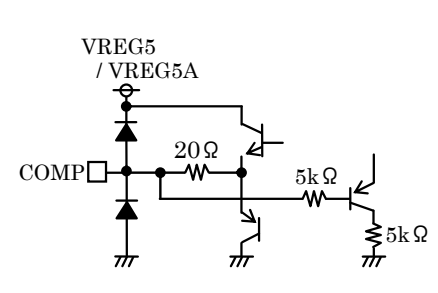
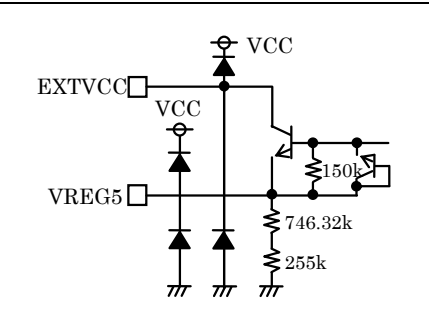
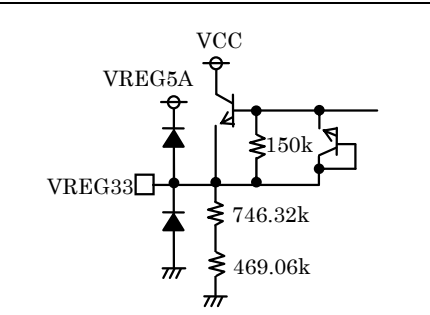
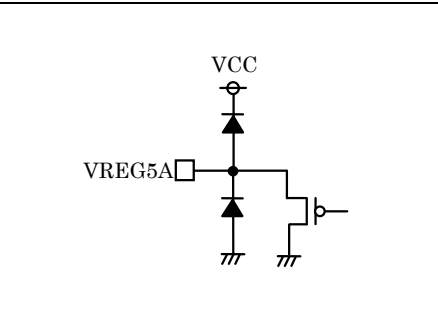
With EN1, 2 at "H" level, when EN1 goes "L", Vo1 turns OFF, but Vo2 output continues.
When EN1 stays "H" and EN2 returns to "H", DET1 is in open state, thus SS2 is asserted, and Vo2 output starts. If Vo2 is 76% of the voltage setting or higher, DET2 goes open and SS1 is asserted, starting Vo1 output.



With EN1,2 at "H" level, if Vo1 starts at 76% or more of voltage setting, DET goes open and SS1 is asserted, starting Vo2 output. (A) With EN2 set "L", if Vo2 goes below 70% the voltage setting, DET2 shorts and SS1 is asserted, turning Vo1 OFF. (A) Same as "A" at left

Fig-36

● Input/Output equivalent circuits

| | | |
|---|---|---|
| <p>13, 48PIN (SW1, SW2) 2, 11PIN (BOOT2, BOOT1) 1, 15PIN (OUTH1, OUTH2)</p>  | <p>14, 47PIN (DGND1, DGND2) 15, 46PIN (OUTL1, OUTL2) 44, 17PIN (VREG5, VREG5A)</p>  | <p>31PIN (LOFF)</p>  |
| <p>34PIN (SYNC)</p>  | <p>21, 39PIN (FB1, FB2)</p>  | <p>23, 37PIN (SS1, SS2)</p>  |
| <p>25, 26, 27PIN (STB, EN1, EN2)</p>  | <p>24, 36PIN (DET1, DET2)</p>  | <p>33PIN (RT)</p>  |
| <p>35PIN (LLM)</p>  | <p>3, 10PIN (CL2, CL1) 5, 8PIN (VCCCL2, VCCCL1)</p>  | <p>22, 38PIN (COMP1, COMP2)</p>  |
| <p>41PIN (EXTVCC) 44PIN (VREG5)</p>  | <p>19PIN (VREG33)</p>  | <p>17PIN (VREG5A)</p>  |

● Operation notes

1) Absolute maximum ratings

Exceeding the absolute maximum ratings for supply voltage, operating temperature or other parameters can damage or destroy the IC. When this occurs, it is impossible to identify the source of the damage as a short circuit, open circuit, etc. Therefore, if any special mode is being considered with values expected to exceed absolute maximum ratings, consider taking physical safety measures to protect the circuits, such as adding fuses.

2) GND electric potential

Keep the GND terminal potential at the lowest (minimum) potential under any operating condition.

3) Thermal design

Be sure that the thermal design allows sufficient margin for power dissipation (Pd) under actual operating conditions.

4) Inter-pin shorts and mounting errors

Use caution when positioning the IC for mounting on printed surface boards. Connection errors may result in damage or destruction of the IC. The IC can also be damaged when foreign substances short output pins together, or cause shorts between the power supply and GND.

5) Operation in strong electromagnetic fields

Use caution when operating in the presence of strong electromagnetic fields, as this may cause the IC to malfunction.

6) Testing on application boards

Connecting a capacitor to a low impedance pin for testing on an application board may subject the IC to stress. Be sure to discharge the capacitors after every test process or step. Always turn the IC power supply off before connecting it to or removing it from any of the apparatus used during the testing process. In addition, ground the IC during all steps in the assembly process, and take similar antistatic precautions when transporting or storing the IC.

7) The output FET

The shoot-through may happen when the input parasitic capacitance of FET is extremely big or the Duty ratio is less than or equal to 10%. Less than or equal to 1000pF input parasitic capacitance is recommended. Please confirm operation on the actual application since this character is affected by PCB layout and components.

8) This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated.

P-N junctions are formed at the intersection of these P layers with the N layers of other elements, creating a parasitic diode or transistor. Relations between each potential may form as shown in the example below, where a resistor and transistor are connected to a pin:

- With the resistor, when $GND > \text{Pin A}$, and with the transistor (NPN), when $GND > \text{Pin B}$:
The P-N junction operates as a parasitic diode

- With the transistor (NPN), when $GND > \text{Pin B}$:
The P-N junction operates as a parasitic transistor by interacting with the N layers of elements in proximity to the parasitic diode described above.

Parasitic diodes inevitably occur in the structure of the IC. Their operation can result in mutual interference between circuits, and can cause malfunctions, and, in turn, physical damage or destruction. Therefore, do not employ any of the methods under which parasitic diodes can operate, such as applying a voltage to an input pin lower than the (P substrate) GND.

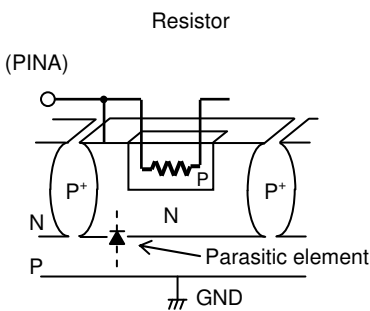


Fig-37

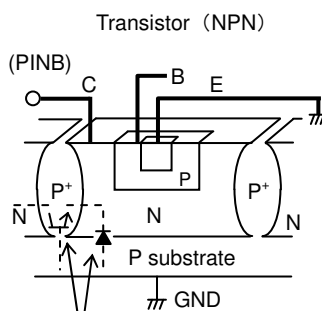


Fig-38

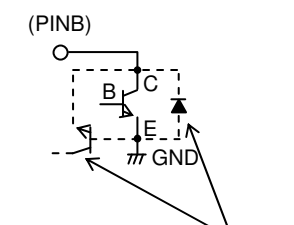


Fig-39

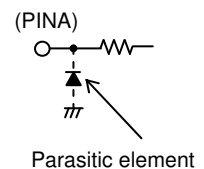


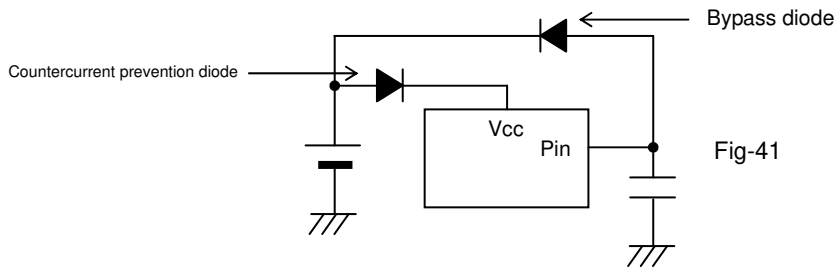
Fig-40

9) GND wiring pattern

When both a small-signal GND and high current GND are present, single-point grounding (at the set standard point) is recommended, in order to separate the small-signal and high current patterns, and to be sure voltage changes stemming from the wiring resistance and high current do not cause any voltage change in the small-signal GND. In the same way, care must be taken to avoid wiring pattern fluctuations in any connected external component GND.

10) In some application and process testing, Vcc and pin potential may be reversed, possibly causing internal circuit or element damage. For example, when the external capacitor is charged, the electric charge can cause a Vcc short circuit to the GND.

In order to avoid these problems, limiting output pin capacitance to 100 μ F or less and inserting a Vcc series countercurrent prevention diode or bypass diode between the various pins and the Vcc is recommended.

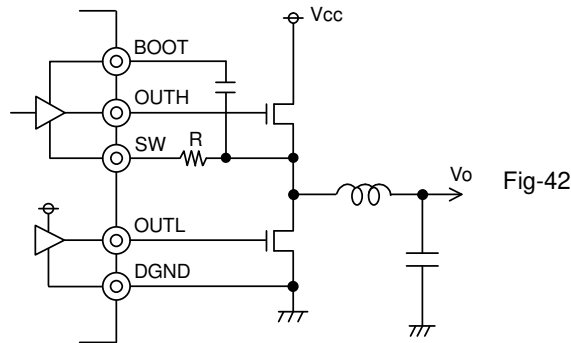


11) Thermal shutdown (TSD)

This IC is provided with a built-in thermal shutdown (TSD) circuit, which is designed to prevent thermal damage to or destruction of the IC. Normal operation should be within the power dissipation parameter, but if the IC should run beyond allowable Pd for a continued period, junction temperature (Tj) will rise, thus activating the TSD circuit, and turning all output pins OFF. When Tj again falls below the TSD threshold, circuits are automatically restored to normal operation. Note that the TSD circuit is only asserted beyond the absolute maximum rating. Therefore, under no circumstances should the TSD be used in set design or for any purpose other than protecting the IC against overheating

12) The SW pin

When the SW pin is connected in an application, its coil counter-electromotive force may give rise to a single electric potential. When setting up the application, make sure that the SW pin never exceeds the absolute maximum value. Connecting a resistor of several Ω will reduce the electric potential. (See Fig. 43)



13) Dropout operation

When input voltage falls below approximately output voltage / 0.9 (varying depending on operating frequency) the ON interval on the OUTL side MOS is lost, making boost applications and wrap operation impossible. If a small differential between input and output voltage is envisioned for a prospective application, connect the load such that the SW voltage drops to the GND level. Managing this load requires discharging the SW line capacitance (SW pin capacitance: approx. 500pF; OUTL side MOS D-S capacitance; Schottky capacitance). Supported loads can be calculated using the equation below.

$$I_{LOAD} = \frac{\text{Output voltage} \times \text{SW line capacitance}}{25n}$$

Note that SW line capacitance is lower with smaller loads, and more stable operation is attained when low voltage bias circuits are configured as in the example below (Fig. 44). However, the degree to which line capacitance is reduced or operational stability is attained will vary depending on the board layout and components. Therefore, be certain to confirm the effectiveness of these design factors in actual operation before entering mass production.

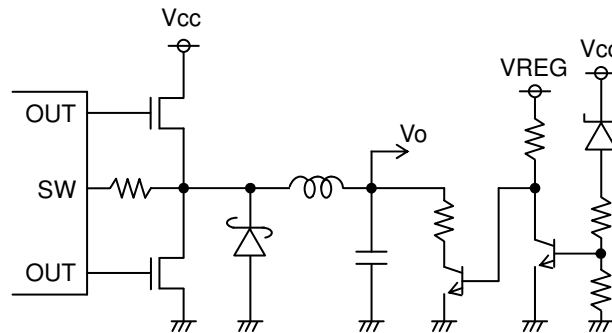


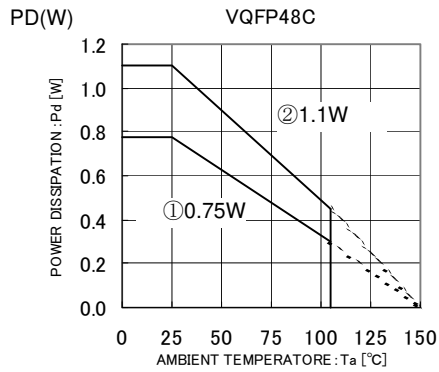
Fig-43

14) Logic of Output

When each function operates, each output is as follows.

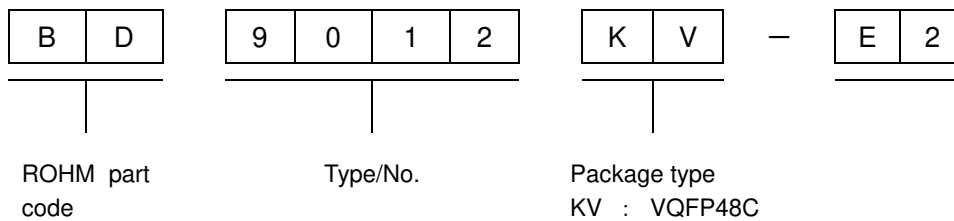
| Function | Upper side FET | OUTH | Lower side FET | OUTL |
|----------|----------------|------|----------------|------|
| EN= L | OFF | L | OFF | L |
| OCP | OFF | L | ON | H |
| UVLO | OFF | L | OFF | L |
| TSD | OFF | L | OFF | L |

●Power dissipation vs. temperature characteristics

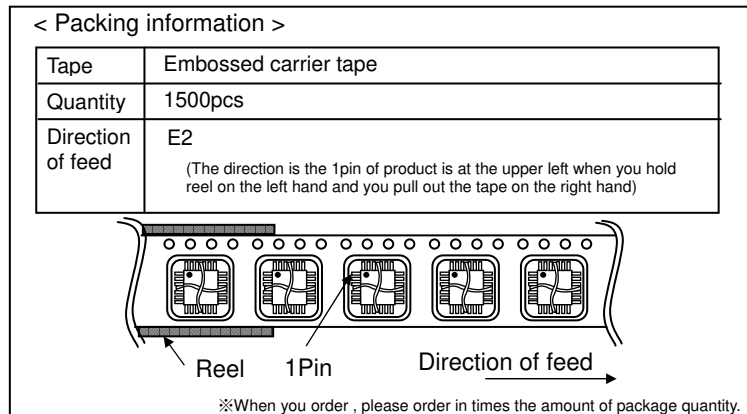
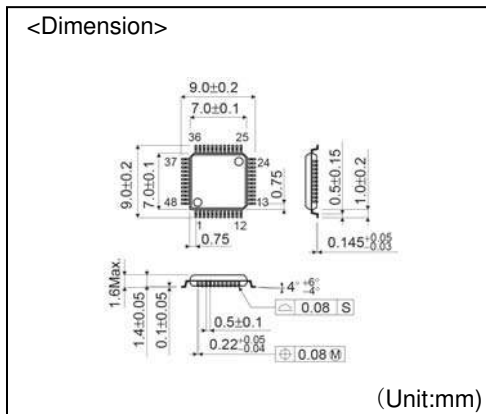


- ① : Stand-alone IC
- ② : Mounted on Rohm standard board
(70mm x 70mm x 1.6mm glass-epoxy board)

●Part order number



VQFP48C



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