

# **ACS718**

## **High Isolation Linear Current Sensor IC with 850 µΩ Current Conductor**

## **FEATURES AND BENEFITS IDESCRIPTION**

- IEC/UL 60950-1 Ed. 2 certified to:
- $\Box$  Dielectric Strength = 4800 Vrms (tested for 60 seconds)  $\Box$  Basic Isolation = 1550 Vpeak
- $\Box$  Reinforced Isolation = 800 Vpeak
- Small footprint, low-profile SOIC16 wide-body package suitable for space constrained applications that require high galvanic isolation
- 0.85 mΩ primary conductor for low power loss and high inrush current withstand capability
- Low, 350  $\mu A_{RMS}/\sqrt{Hz}$  noise density results in typical input referred noise of 70 mA(rms) at max bandwidth (40 kHz)
- 5.0 V, single supply operation
- Output voltage proportional to AC or DC current
- Factory-trimmed sensitivity and quiescent output voltage for improved accuracy
- Chopper stabilization results in extremely stable quiescent output voltage
- Ratiometric output from supply voltage





## **Package: 16-Pin SOICW (suffix MA)**



*Not to scale*

The Allegro™ ACS718 current sensor IC is an economical, high isolation solution for AC or DC current sensing in industrial, commercial, and communications systems. The small package is ideal for space constrained applications, though the wide-body provides the creepage and clearance needed for high isolation. Typical applications include motor control, load detection and management, switched-mode power supplies, and overcurrent fault protection.

The device consists of a low-offset, linear Hall sensor circuit with a copper conduction path located near the surface of the die. Applied current flowing through this copper conduction path generates a magnetic field which is sensed by the integrated Hall IC and converted into a proportional voltage. Device accuracy is optimized through the close proximity of the magnetic field to the Hall transducer. A proportional voltage is provided by the low-offset, chopper-stabilized BiCMOS Hall IC, which is programmed for accuracy after packaging. The output of the device has a positive slope when an increasing current flows through the primary copper conduction path (from pins 1 through 4, to pins 5 through 8), which is the path used for current sensing. The internal resistance of this conductive path is 0.85 mΩ typical, providing low power loss.

The terminals of the conductive path are electrically isolated from the sensor leads (pins 10 through 15 ). This allows the ACS718 current sensor IC to be used in high-side current sense applications without the use of high-side differential amplifiers or other costly isolation techniques.

The ACS718 is provided in a small, low profile surface mount SOICW16 package (suffix MA). The device is lead (Pb) free with 100% matte tin leadframe plating. The device is fully calibrated prior to shipment from the factory.



**The ACS718 outputs an analog signal, VIOUT , that changes, proportionally, with the bidirectional AC or DC primary sensed current, IP , within the**  specified measurement **range.**

## **SPECIFICATIONS**

#### **SELECTION GUIDE**



[1] Contact Allegro for additional packing options.

[2] Variant not intended for automotive applications.

#### **ABSOLUTE MAXIMUM RATINGS**



#### **ESD RATINGS**



#### **ISOLATION CHARACTERISTICS**



[1] In order to maintain this creepage in applications, the user should add a slit in the PCB under the package. Otherwise, the pads on the PCB will reduce the creepage.





## **Pinout Diagram and Terminal List Table**



**Package MA, 16-Pin SOICW**

#### **Terminal List**





#### **COMMON ELECTRICAL CHARACTERISTICS** [1]:  $T_A$  Range K, valid at  $T_A$  = -40°C to 125°C, V<sub>CC</sub> = 5 V, **unless otherwise specified**



[1] Device may be operated at higher primary current levels, I<sub>P</sub>, ambient temperatures, T<sub>A</sub>, and internal leadframe temperatures, provided the Maximum Junction Temperature, T<sub>J</sub>(max), is not exceeded.

[2] The sensor IC will continue to respond to current beyond the range of I<sub>P</sub> until the high or low saturation voltage; however, the nonlinearity in this region will be worse than through the rest of the measurement range.



## **xKMATR-10B PERFORMANCE CHARACTERISTICS: Valid at**  $T_A = -40^{\circ}$ **C to 125°C, V<sub>CC</sub> = 5 V,**

#### unless otherwise specified



 $[1]$  Typical values with  $\pm$  are 3 sigma values.

<sup>[2]</sup> Percentage of I<sub>P</sub>, with I<sub>P</sub> = I<sub>PR(max)</sub>.<br><sup>[3]</sup> A single part will not have both the maximum/minimum sensitivity error and maximum/minimum offset voltage, as that would violate the maximum/minimum total output error specification. Also, 3 sigma distribution values are combined by taking the square root of the sum of the squares. See Application Information section.

[4] Voltage Offset Error does not incorporate any error due to external magnetic fields. See section: Impact of External Magnetic Fields.



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## **CHARACTERISTIC PERFORMANCE**

#### **xKMATR-10B Key Parameters**







**Sensitivity Error vs. Temperature**







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# **High Isolation Linear Current Sensor IC with 850 µΩ Current Conductor ACS718**

## **xKMATR-20B Key Parameters**





# **Sensitivity vs. Temperature**



**Sensitivity Error vs. Temperature**









For information regarding bandwidth characterization methods used for the ACS718, see the "Characterizing System Bandwidth" application note (https://allegromicro.com/en/insights-and-innovations/technical-documents/hall-effect-sensor-ic-publications/ an296169-acs720-bandwidth-testing) on the Allegro website.



## **RESPONSE CHARACTERISTICS DEFINITIONS AND PERFORMANCE DATA**

## **Response Time (t**<sub>RESPONSE</sub>)

The time interval between a) when the sensed input current reaches 90% of its final value, and b) when the sensor output reaches 90% of its full-scale value.

## **Propagation Delay (t<sub>pd</sub>)**

The time interval between a) when the sensed input current reaches 20% of its full-scale value, and b) when the sensor output reaches 20% of its full-scale value.

## **Rise Time (t<sup>r</sup> )**

The time interval between a) when the sensor reaches 10% of its full-scale value, and b) when it reaches 90% of its full-scale value.

## **Output Slew Rate (SR)**

The rate of change  $[V/\mu s]$  in the output voltage from a) when the sensor reaches 10% of its full-scale value, and b) when it reaches 90% of its full-scale value.





Applied current step with  $10\%$ -90% rise time = 0.3 µs Test Conditions:  $T_A = 25^{\circ}C$ ,  $C_{\text{BYPASS}} = 0.1 \mu F$ ,  $C_L = 0 \mu F$ 

## **POWER ON FUNCTIONAL DESCRIPTION AND PERFORMANCE DATA**

## **Power-On Time (t<sub>PO</sub>)**

When the supply is ramped to its operating voltage, the device requires a finite amount of time to power its internal components before responding to an input magnetic field. Power-On Time  $(t_{PO})$  is defined as the time interval between a) the power supply has reached its minimum specified operating voltage  $(VCC(min))$ , and b) when the sensor output has settled within  $\pm 10\%$  of its steady-state value under an applied magnetic field.

#### **Power-On Profile**

After applying power, the part remains off in a known state referred to as Power-on Reset, or POR. The device stays in this state until the voltage reaches a point at which the device will remain powered. The power-on profile below illustrates the intended power on/off. A pull-down resistor was used on the output of the tested device.



Supply voltage ramp rate = 1V/ms





## **DEFINITIONS OF ACCURACY CHARACTERISTICS**

**Sensitivity (Sens).** The change in sensor IC output in response to a 1 A change through the primary conductor. The sensitivity is the product of the magnetic circuit sensitivity  $(G/A)$  (1 G = 0.1 mT) and the linear IC amplifier gain (mV/G). The linear IC amplifier gain is programmed at the factory to optimize the sensitivity (mV/A) for the full-scale current of the device.

**Nonlinearity (** $E_{LIN}$ **). The nonlinearity is a measure of how linear** the output of the sensor IC is over the full current measurement range. The nonlinearity is calculated as:

$$
100\left\{1-\left[\frac{\Delta \text{ gain} \times \frac{9}{6} \text{ sat } (V_{\text{IOUT}\_\text{full-scale amperes}} - V_{\text{IOUT}(Q)})}{2 (V_{\text{IOUT}\_\text{half-scale amperes}} - V_{\text{IOUT}(Q)})}\right]\right\}
$$

where  $V_{\text{IOUT}}(I_{\text{PR}}(\text{max}))$  is the output of the sensor IC with the maximum measurement current flowing through it and  $V_{\text{IOUT}}(I_{\text{PR}}(\text{max})/2)$  is the output of the sensor IC with half of the maximum measurement current flowing through it.

**Zero Current Output Voltage (V<sub>IOUT(O)</sub>).** The output of the sensor when the primary current is zero. For a unipolar supply voltage, it nominally remains at at  $0.5 \times V_{CC}$  for a bidirectional device and  $0.1 \times V_{CC}$  for a unidirectional device. For example, in the case of a bidirectional output device,  $V_{CC} = 5$  V translates into  $V_{\text{IOUT}(Q)} = 2.5$  V. Variation in  $V_{\text{IOUT}(Q)}$  can be attributed to the resolution of the Allegro linear IC quiescent voltage trim and thermal drift.

**Voltage Offset Error (** $V_{OE}$ **). The deviation of the device output** from its ideal quiescent value of  $0.5 \times V_{CC}$  (bidirectional) or 0.1  $\times$  V<sub>CC</sub> (unidirectional) due to nonmagnetic causes. To convert this voltage to amperes, divide by the device sensitivity, Sens.

**Total Output Error (E<sub>TOT</sub>).** The difference between the current measurement from the sensor IC and the actual current  $(I_p)$ , relative to the actual current. This is equivalent to the difference between the ideal output voltage and the actual output voltage, divided by the ideal sensitivity, relative to the current flowing through the primary conduction path:

$$
E_{\text{TOT}}(\text{I}_{\text{P}}) = \frac{V_{\text{IOUT\_ideal}}(\text{I}_{\text{P}}) - V_{\text{IOUT}}(\text{I}_{\text{P}})}{\text{Sens}_{\text{ideal}}(\text{I}_{\text{P}}) \times I_{\text{P}}} \times 100 \text{ (*)}
$$

The Total Output Error incorporates all sources of error and is a function of  $I_P$ . At relatively high currents,  $E_{TOT}$  will be mostly due to sensitivity error, and at relatively low currents,  $E_{TOT}$  will be mostly due to Voltage Offset Error ( $V_{OE}$ ). In fact, at I<sub>P</sub> = 0,  $E_{TOT}$  approaches infinity due to the offset. This is illustrated in figures 1 and 2. Figure 1 shows a distribution of output voltages versus  $I_p$  at 25 $\degree$ C and across temperature. Figure 2 shows the corresponding  $E_{TOT}$  versus  $I_P$ .



**Figure 1: Output Voltage versus Sensed Current** 



**Figure 2: Total Output Error versus Sensed Current** 



#### **APPLICATION INFORMATION**

#### **Impact of External Magnetic Fields**

The ACS718 works by sensing the magnetic field created by the current flowing through the package. However, the sensor cannot differentiate between fields created by the current flow and external magnetic fields. This means that external magnetic fields can cause errors in the output of the sensor. Magnetic fields which are perpendicular to the surface of the package affect the output of the sensor, as it only senses fields in that one plane. The error in Amperes can be quantified as:

$$
Error(B) = \frac{B}{C_F}
$$

where B is the strength of the external field perpendicular to the surface of the package in Gauss, and  $C_F$  is the coupling factor in G/A. Then, multiplying by the sensitivity of the part (Sens) gives the error in mV.

For example, an external field of 1 Gauss will result in around 0.22 A of error. If the ACS718KMATR-10B, which has a nominal sensitivity of 200 mV/A, is being used, that equates to 44 mV of error on the output of the sensor.





## **Estimating Total Error vs. Sensed Current**

The Performance Characteristics tables give distribution  $(\pm 3)$ sigma) values for Total Error at  $I_{PR(max)}$ ; however, one often wants to know what error to expect at a particular current. This can be estimated by using the distribution data for the components of Total Error, Sensitivity Error, and Voltage Offset Error. The  $\pm 3$  sigma value for Total Error ( $E_{TOT}$ ) as a function of the sensed current  $(I_P)$  is estimated as:

$$
E_{\text{ror}}(I_{\text{p}}) = \sqrt{E_{\text{SENS}}^2 + \left(\frac{100 \times V_{\text{OE}}}{\text{Sens} \times I_{\text{p}}}\right)^2}
$$

Here,  $E_{\text{SENS}}$  and  $V_{\text{OE}}$  are the  $\pm 3$  sigma values for those error terms. If there is an average sensitivity error or average offset voltage, then the average Total Error is estimated as:

$$
E_{\text{TOT}_{\text{AVG}}}(I_p) = E_{\text{SENS}_{\text{AVG}}} + \frac{100 \times V_{\text{OE}_{\text{AVG}}}}{\text{Sens} \times I_p}
$$

The resulting total error will be a sum of  $E_{TOT}$  and  $E_{TOT}$  AVG. Using these equations and the 3 sigma distributions for  $\overline{S}$ ensitivity Error and Voltage Offset Error, the Total Error vs. sensed current (I<sub>P</sub>) is below for the ACS718KMATR-20B. As expected, as one goes towards zero current, the error in percent goes towards infinity due to division by zero (refer to Figure 3).



**Figure 3: Predicted Total Error as a Function of Sensed Current for the ACS718KMATR-20B**



## **Thermal Rise vs. Primary Current**

Self-heating due to the flow of current should be considered during the design of any current sensing system. The sensor, printed circuit board (PCB), and contacts to the PCB will generate heat as current moves through the system.

The thermal response is highly dependent on PCB layout, copper thickness, cooling techniques, and the profile of the injected current. The current profile includes peak current, current "on-time", and duty cycle. While the data presented in this section was collected with Direct-Current (DC), these numbers may be used to approximate thermal response for both AC signals and current pulses.

The plot in Figure 4 shows the measured rise in steady-state die temperature of the ACS718 versus continuous current at an ambient temperature,  $T_A$ , of 25 °C. The thermal offset curves may be directly applied to other values of  $T_A$ . Conversely, Figure 5 shows the maximum continuous current at a given  $T_A$ . Surges beyond the maximum current listed in Figure 5 are allowed given the maximum junction temperature,  $T_{J(MAX)}$  (165°C), is not exceeded.







**Figure 5: Maximum continuous current at a given TA**

The thermal capacity of the ACS718 should be verified by the end user in the application's specific conditions. The maximum junction temperature,  $T_{J(MAX)}$  (165°C), should not be exceeded. Further information on this application testing is available in the DC and Transient Current Capability application note on the Allegro website.

## **ASEK718 Evaluation Board Layout**

Thermal data shown in Figure 4 and Figure 5 was collected using the ASEK718 Evaluation Board (TED-85-0667-002). This board includes 1500 mm2 of 4 oz. copper (0.1388 mm) connected to pins 1 through 4, and to pins 5 through 8, with thermal vias connecting the layers. Top and Bottom layers of the PCB are shown below in Figure 6.



**ASEK718 Evaluation Board**

Gerber files for the ASEK718 evaluation board are available for download from the Allegro website. Please see the technical documents section of the ACS718 device webpage.



## **HIGH ISOLATION PCB LAYOUT**





## **PACKAGE OUTLINE DRAWING**







#### **Revision History**



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