TRF3701

0.4 GHz to 1.5 GHz QUADRATURE MODULATOR

FEATURES

- **P1dB of 7 dBm**
- **−156 dBm/Hz Noise Floor**
- **−150 dBm/Hz Noise at P_{OUT} = 0 dBm**
- **Typical Unadjusted Carrier Suppression > 35 dBc at 1 GHz**
- **Typical Unadjusted Sideband Suppression > 40 dBc at 1 GHz**
- **Differential or Single-Ended I, Q Inputs**
- **Convenient Single-Ended LO Input**
- **Silicon Germanium Technology**

APPLICATIONS

- **Cellular Base Transceiver Station Transmit Channel**
- **IF Sampling Applications**
- **TDMA: GSM, IS-136, EDGE/UWC-136**
- **CDMA: IS-95, UMTS, CDMA2000**
- **Wireless Local Loop**
- **Wireless LAN IEEE 802.11**
- **LMDS, MMDS**
- **Wideband Baseband Transceivers**

RHC PACKAGE
(TOP VIEW)

```
            GND QREF IREF IVIN QVIN
              1   16   15   14   13
GND   2  ┌─────────────────────┐  12   GND
GND   3  │                     │  11   GND
LO    4  │                     │  10   VCC
              5    6    7    8    9
            GND  VCC  PWD RFOUT GND
```

DESCRIPTION

The TRF3701 is an ultralow-noise direct quadrature modulator that is capable of converting complex input signals from baseband or IF directly up to RF. An internal analog combiner sums the real and imaginary components of the RF outputs. This combined output can feed the RF preamp directly at frequencies of up to 1.5 GHz. The modulator is implemented as a double-balanced mixer. An internal local oscillator (LO) phase splitter accommodates a single-ended LO input, eliminating the need for a costly external balun.
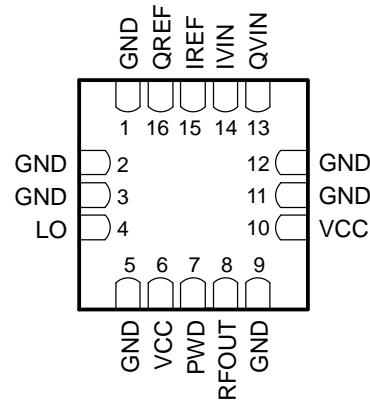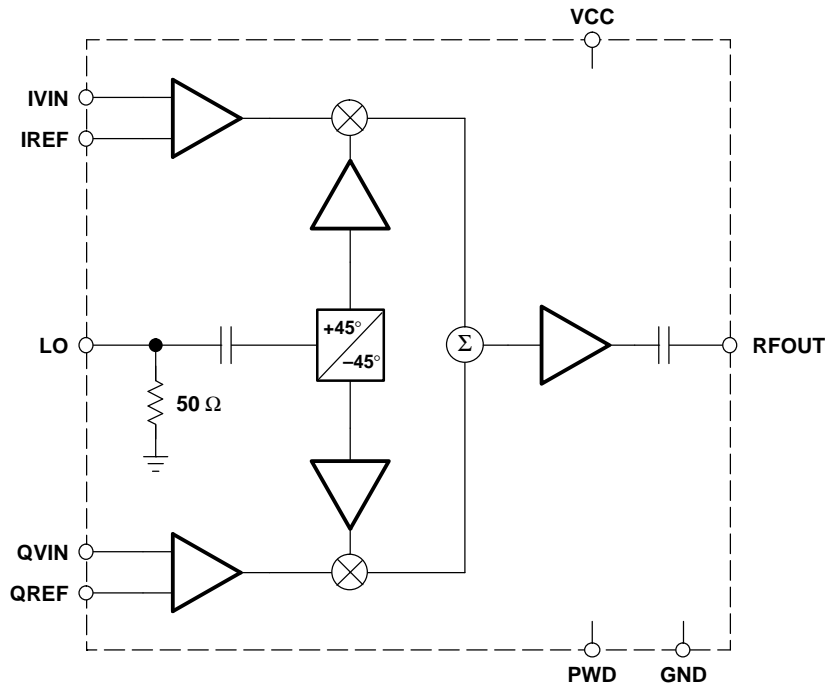
AVAILABLE OPTIONS

T_A	4-mm × 4-mm 16-Pin RHC (QFN) Package
−40°C to 85°C	TRF3701IRHC
	TRF3701IRHCR (Tape and Reel)

TRF3701

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FUNCTIONAL BLOCK DIAGRAM

TERMINAL FUNCTIONS

TERMINAL		I/O	DESCRIPTION
NAME	NO.		
GND	1, 2, 3, 5, 9, 11, 12		Ground
IREF	15	I	In-phase (I) reference voltage/differential input
IVIN	14	I	In-phase (I) signal input
LO	4	I	Local oscillator input
PWD	7	I	Power down
QREF	16	I	Quadrature (Q) reference voltage/differential input
QVIN	13	I	Quadrature (Q) signal input
RFOUT	8	O	RF output
VCC	6, 10		Supply voltage

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)[1][2]

V_{CC}	Supply voltage range	−0.5 V to 6 V
	LO input power level	10 dBm
	Baseband input voltage level (single-ended)	3 Vp-p
T_A	Operating free-air temperature range	−40°C to 85°C
	Lead temperature for 10 seconds	260°C

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
(2) Measured with respect to ground

2

RECOMMENDED OPERATING CONDITIONS

		MIN	NOM	MAX	UNIT
Supplies and References					
V_{CC}	Analog supply voltage	4.5	5	5.5	V
	VCM (IVIN, QVIN, IREF, QREF input common-mode dc voltage)		3.7		V
Local Oscillator Input (LO)					
	Input frequency	400		1500	MHz
	Power level (measured into 50 Ω)	−6	0	6	dBm
Signal Inputs (IVIN, QVIN)					
	Input bandwidth		700		MHz

ELECTRICAL CHARACTERISTICS

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V, f_{LO} = 942.5 MHz at 0 dBm, T_A = 25°C (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
Power Supply						
I_{CC}	Total supply current	V(PWD) = 5 V		145		mA
		V(PWD) = 0 V		13		
	Power-down input impedance			11		kΩ
	Turnon time			120		ns
	Turnoff time			20		ns
Local Oscillator (LO) Input						
	Input impedance			40 + j4.8		Ω
Signal Inputs (IVIN, QVIN, IREF, QREF)						
	Input bias current	V(IVIN) = V(IREF) = V(QVIN) = V(QREF) = VCM = 3.7 V		16		µA
	Input impedance	Single-ended input		250		kΩ
		Differential input		125		

TRF3701

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RF OUTPUT PERFORMANCE

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V, f_{LO} = 942.5 MHz at 0 dBm, T_A = 25°C (unless otherwise noted)[1]

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Single and Two-Tone Specifications						
	Output power		−3.5	−1		dBm
	Second baseband harmonic (USB or LSB)[3]	I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz		−50	−45	dBc
	Third baseband harmonic (USB or LSB)[3]			−61	−55	dBc
	IMD$_3$	I, Q[2] = 1 Vp-p (two-tone signal, f_{BB1} = 928 kHz, f_{BB2} = 992 kHz)		−55	−45	dBc
	P1dB (output compression point)			6.5		dBm
NSD	Noise spectral density	I, Q[4] = VCM = 3.7 VDC		−156		dBm/Hz
		6-MHz offset from carrier, P_{out} = −10 dBm, over temperature		−153	−151[5]	
		6-MHz offset from carrier, P_{out} = −5 dBm, over temperature		−152	−150[5]	
		6-MHz offset from carrier, P_{out} = 0 dBm, over temperature		−150	−148[5]	
	RFOUT pin impedance			26 + j3		Ω
	Carrier suppression	I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, unadjusted	30	35		dBc
		I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, optimized		55		
		I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, over temperature		35		
	Sideband suppression	I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, unadjusted	37	50		dBc
		I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, optimized		55		
		I, Q[2] = 1 Vp-p, f_{BB} = 928 kHz, over temperature		38		

(1) Baseband inputs are differential; equivalent performance is attained by using single-ended drive.
(2) I , Q = 1 Vp-p implies that the magnitude of the signal at each input pin IVIN, IREF, QVIN, QREF is equal to 500 mVp-p.
(3) USB = upper sideband. LSB = lower sideband.
(4) All input pins tied to VCM
(5) Maximum noise values are assured by statistical characterization only, not production testing. The values specified are over the entire temperature range, T_A = −40°C to 85°C.

DEFINITIONS OF SELECTED SPECIFICATIONS

Unadjusted Carrier Suppression

This specification measures the amount by which the local oscillator component is attenuated in the output spectrum of the modulator relative to the carrier. It is assumed that the baseband inputs delivered to the pins of the TRF3701 are perfectly matched to have the same dc offset (VCM). This includes all four baseband inputs: IVIN, QVIN, IREF and QREF. Unadjusted carrier suppression is measured in dBc.

Adjusted (Optimized) Carrier Suppression

This differs from the unadjusted suppression number in that the dc offsets of the baseband inputs are iteratively adjusted around their theoretical value of VCM in order to yield the maximum suppression of the LO component in the output spectrum. Adjusted carrier suppression is measured in dBc.

Unadjusted Sideband Suppression

This specification measures the amount by which the unwanted sideband of the input signal is attenuated in the output of the modulator, relative to the wanted sideband. It is assumed that the baseband inputs delivered to the modulator input pins are perfectly matched in amplitude and are exactly 90° out of phase. Unadjusted sideband suppression is measured in dBc.

DEFINITIONS OF SELECTED SPECIFICATIONS (continued)
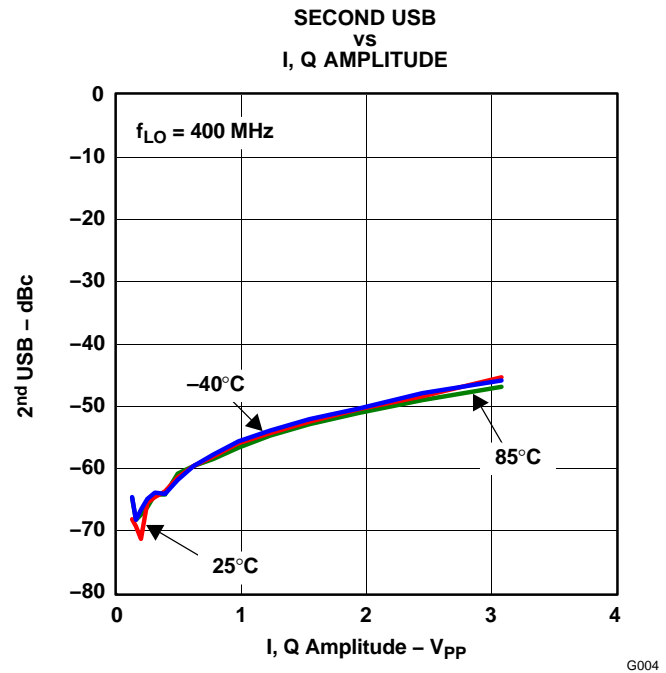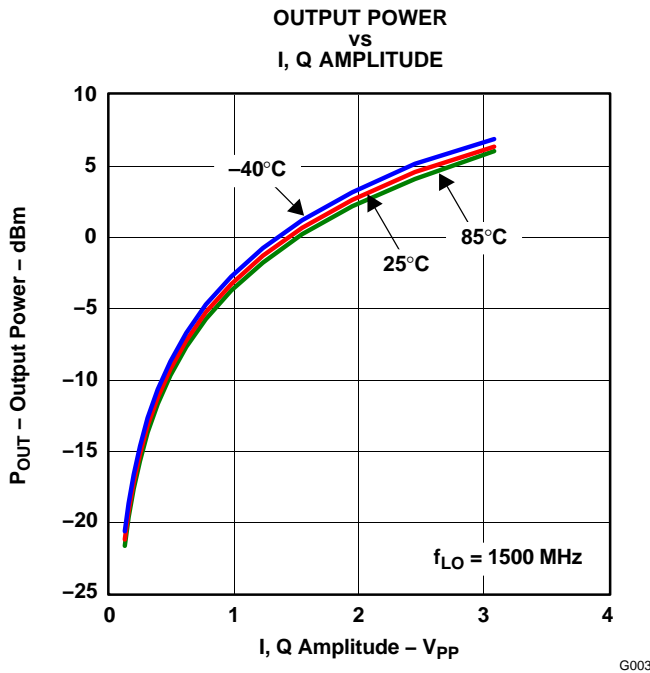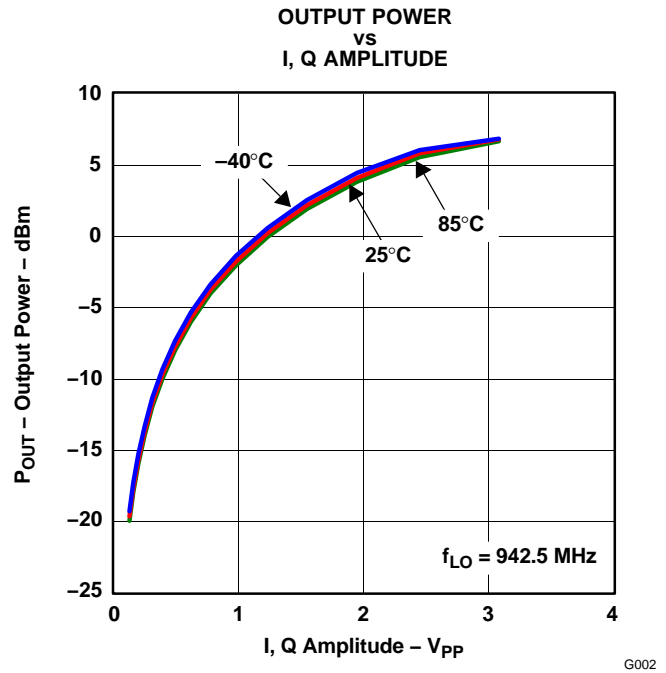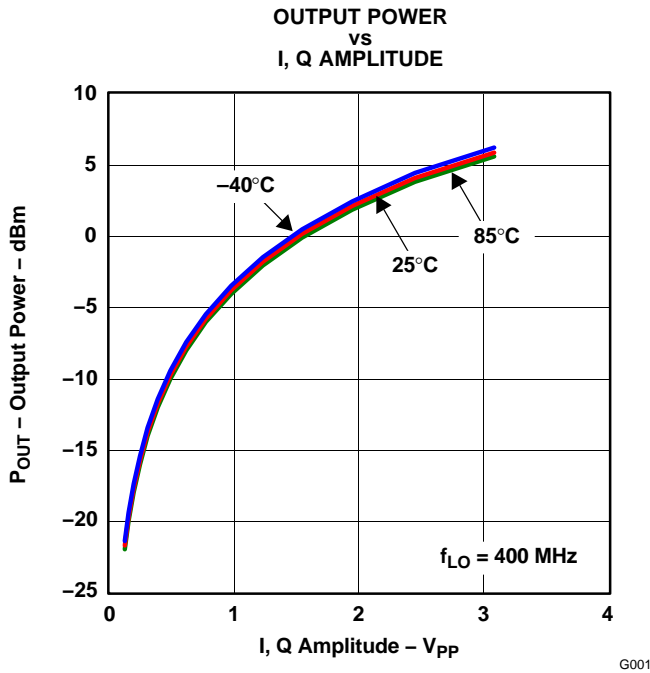
Adjusted (Optimized) Sideband Suppression

This differs from the unadjusted sideband suppression in that the baseband inputs are iteratively adjusted around their theoretical values to maximize the amount of sideband suppression. Adjusted sideband suppression is measured in dBc.

Suppressions Over Temperature

This specification assumes that the user has gone through the optimization process for the suppression in question, and set the optimal settings for the I, Q inputs at room temperature. This specification then measures the suppression when temperature conditions change after the initial calibration is done.

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TYPICAL CHARACTERISTICS

For all the performance plots in this section, the following conditions were used, unless otherwise noted: T_A = −40°C to 85°C, VCC = 5 V, VCM = 3.7 V, f_{LO} = 942.5 MHz at P_{LO} = 0 dBm, I and Q inputs driven differentially at a frequency of 50 kHz for an output power level P_{out} = 0 dBm. In the case of optimized suppressions, the point of optimization is noted and is always at nominal conditions and room temperature. A level of >50 dBc is assumed to be optimized.

OUTPUT POWER
vs
I, Q AMPLITUDE

Figure 1.

OUTPUT POWER
vs
I, Q AMPLITUDE

Figure 2.

OUTPUT POWER
vs
I, Q AMPLITUDE

Figure 3.

SECOND USB
vs
I, Q AMPLITUDE

Figure 4.

TYPICAL CHARACTERISTICS (continued)

SECOND USB
vs
I, Q AMPLITUDE

f_{LO} = 942.5 MHz

2nd USB – dBc

−40°C

25°C   85°C

I, Q Amplitude – V_{PP}

G005

Figure 5.

SECOND USB
vs
I, Q Amplitude

f_{LO} = 1500 MHz

2nd USB – dBc

−40°C

85°C   25°C

I, Q Amplitude – V_{PP}

G006

Figure 6.

UNADJUSTED CARRIER SUPPRESSION
vs
OUTPUT POWER

f_{LO} = 400 MHz   85°C

CS – Unadjusted Carrier Suppression – dBc

25°C   −40°C

P_{OUT} – Output Power – dBm

G007

Figure 7.

UNADJUSTED CARRIER SUPPRESSION
vs
OUTPUT POWER

f_{LO} = 942.5 MHz

−40°C

CS – Unadjusted Carrier Suppression – dBc

25°C

85°C

P_{OUT} – Output Power – dBm

G008

Figure 8.

TYPICAL CHARACTERISTICS (continued)

UNADJUSTED CARRIER SUPPRESSION
vs
OUTPUT POWER

Figure 9.

UNADJUSTED SIDEBAND SUPPRESSION
vs
OUTPUT POWER

Figure 10.

UNADJUSTED SIDEBAND SUPPRESSION
vs
OUTPUT POWER

Figure 11.

UNADJUSTED SIDEBAND SUPPRESSION
vs
OUTPUT POWER
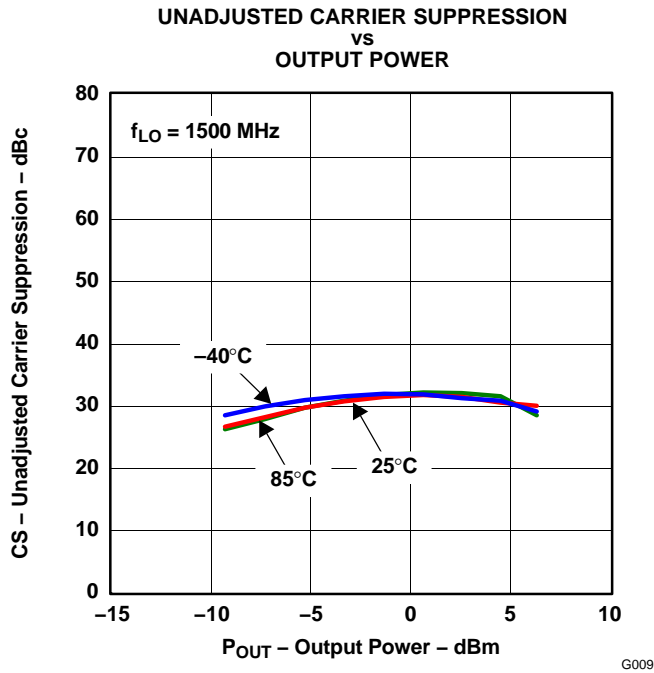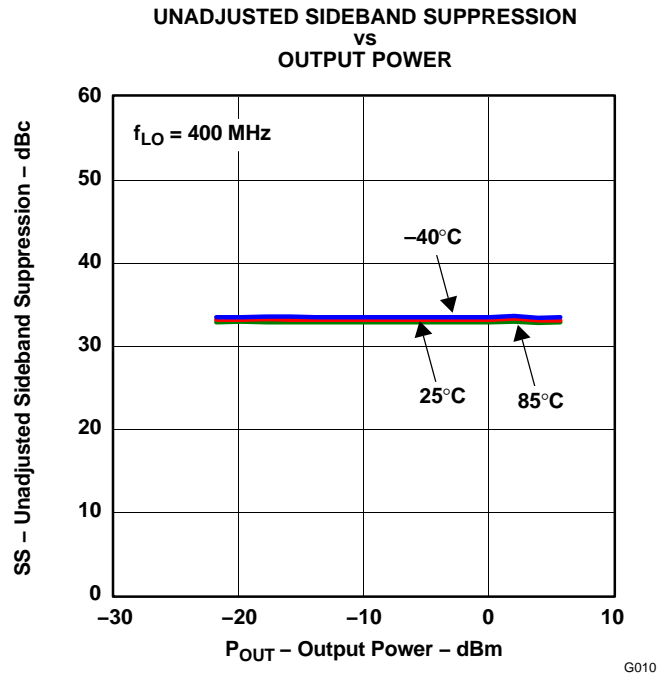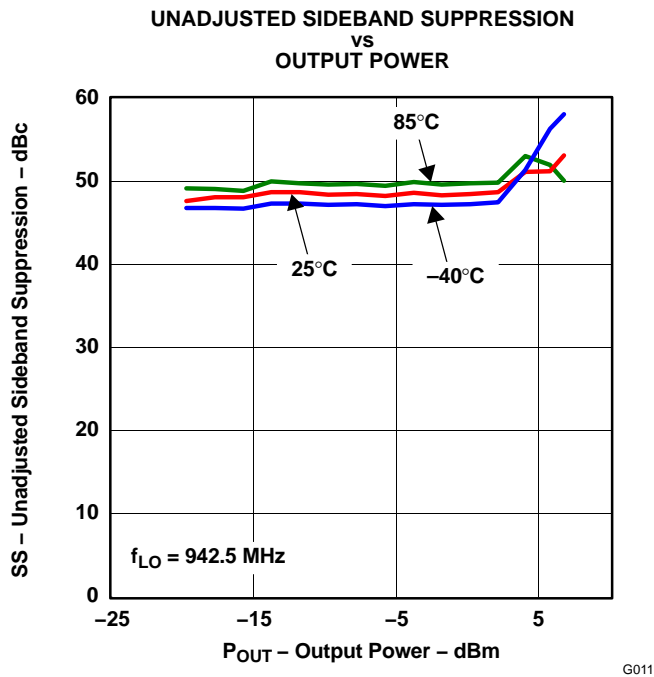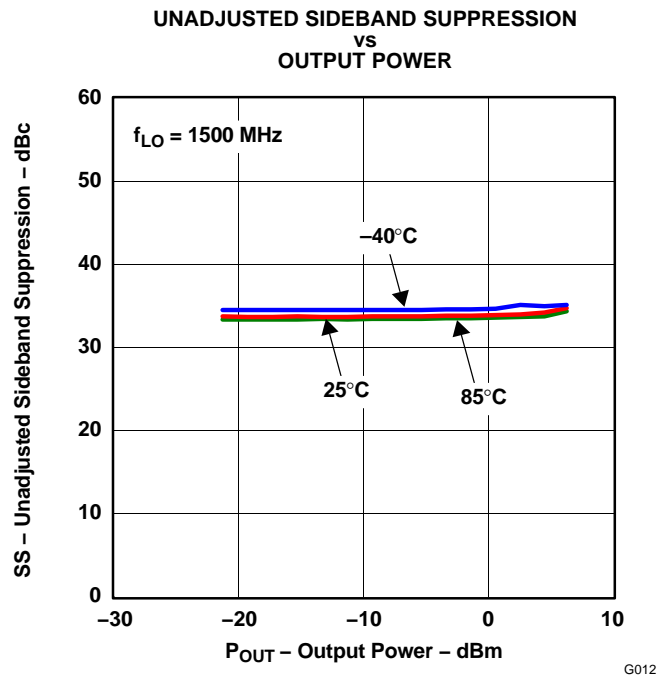
Figure 12.

TYPICAL CHARACTERISTICS (continued)

**THIRD LSB
vs
OUTPUT POWER**

Figure 13.

**THIRD LSB
vs
OUTPUT POWER**

Figure 14.

**THIRD LSB
vs
OUTPUT POWER**

Figure 15.

**IMD3
vs
OUTPUT POWER PER TONE**
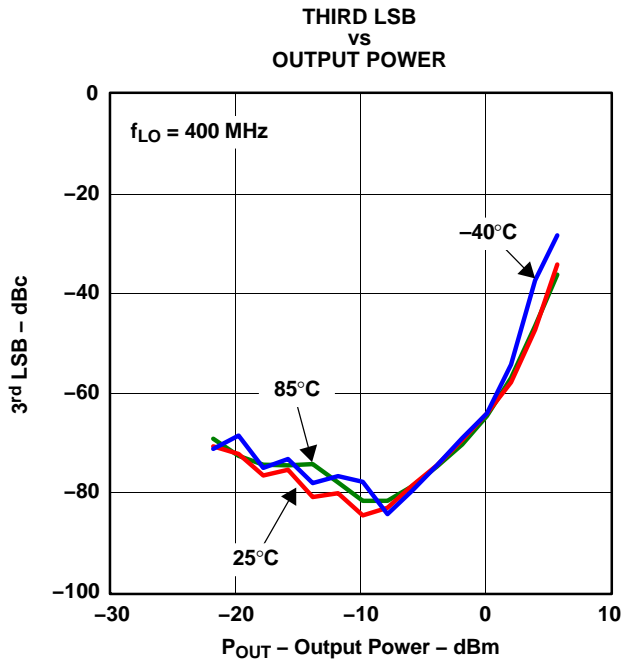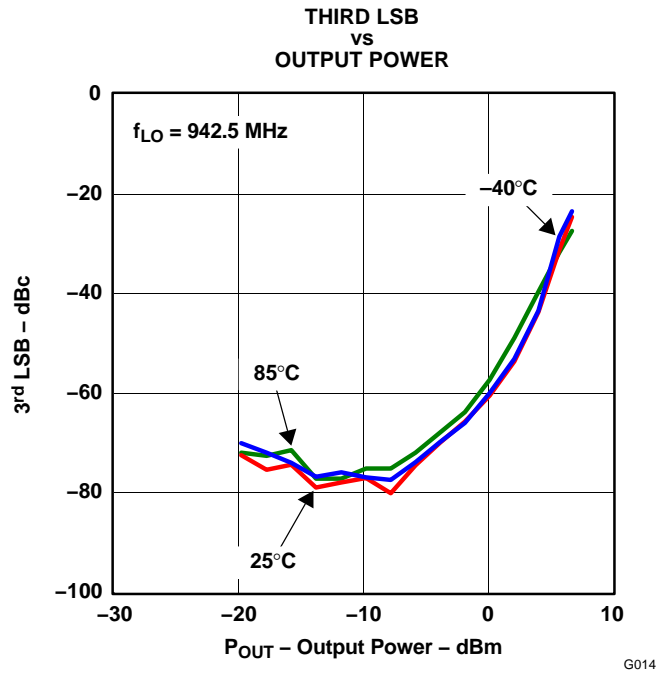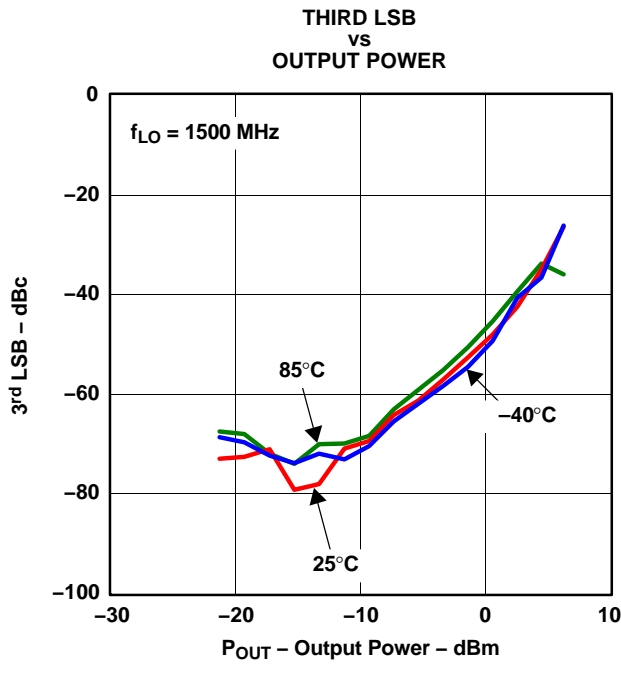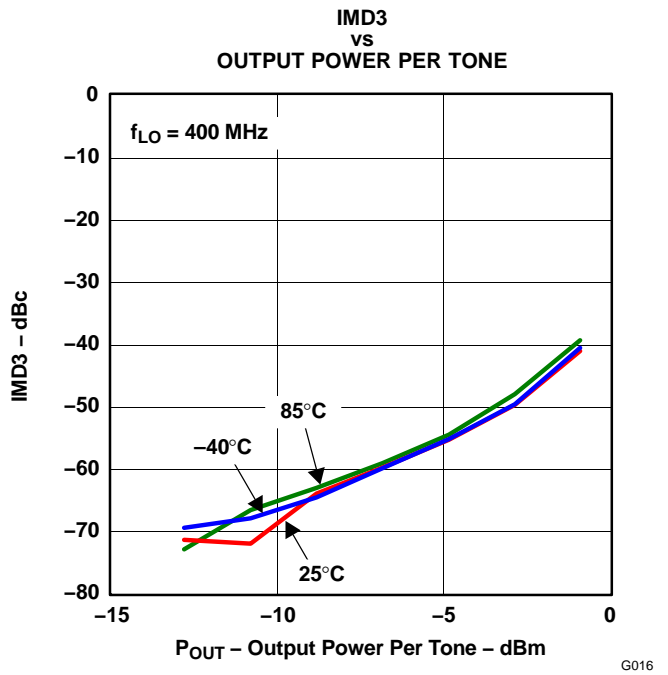
Figure 16.

TYPICAL CHARACTERISTICS (continued)

IMD3
vs
OUTPUT POWER PER TONE

Figure 17.

IMD3
vs
OUTPUT POWER PER TONE

Figure 18.

P1dB
vs
FREQUENCY

Figure 19.

UNADJUSTED CARRIER SUPPRESSION
vs
FREQUENCY

Figure 20.

![Texas Instruments logo]
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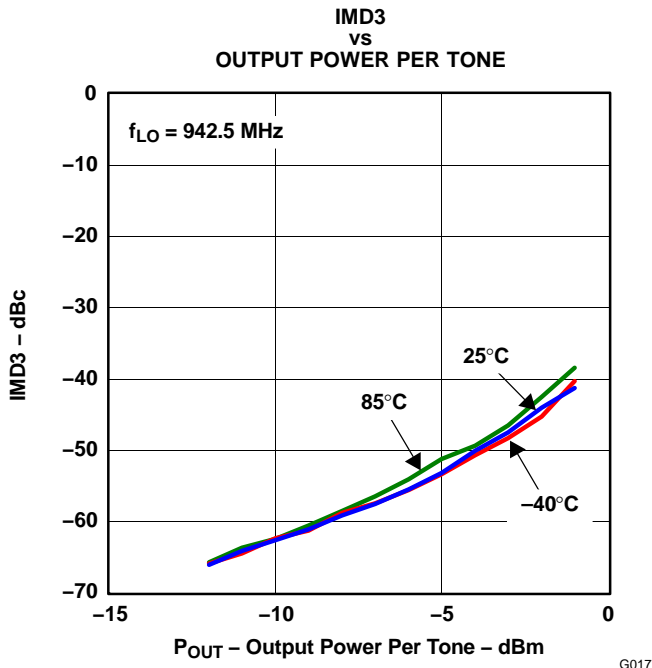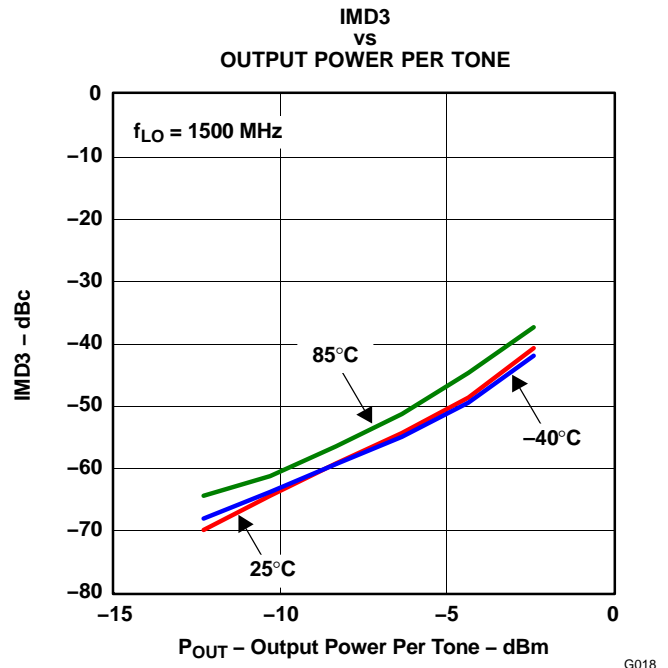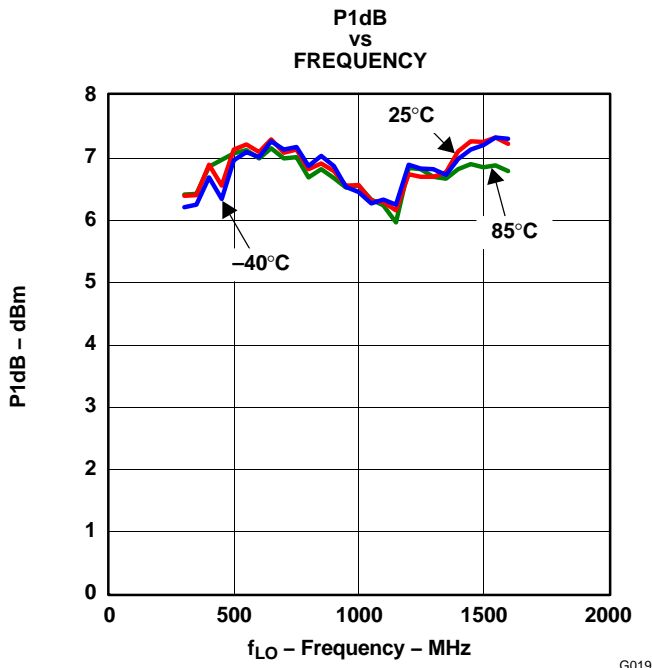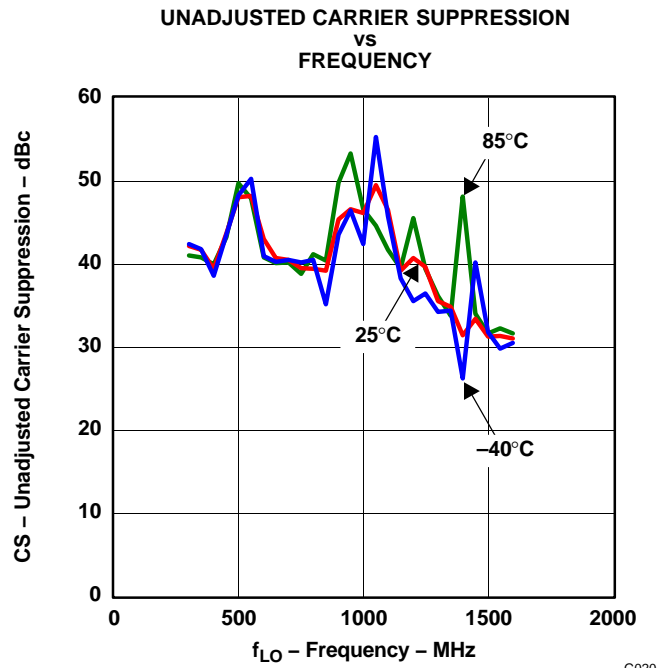
TYPICAL CHARACTERISTICS (continued)

**UNADJUSTED SIDEBAND SUPPRESSION
vs
FREQUENCY**
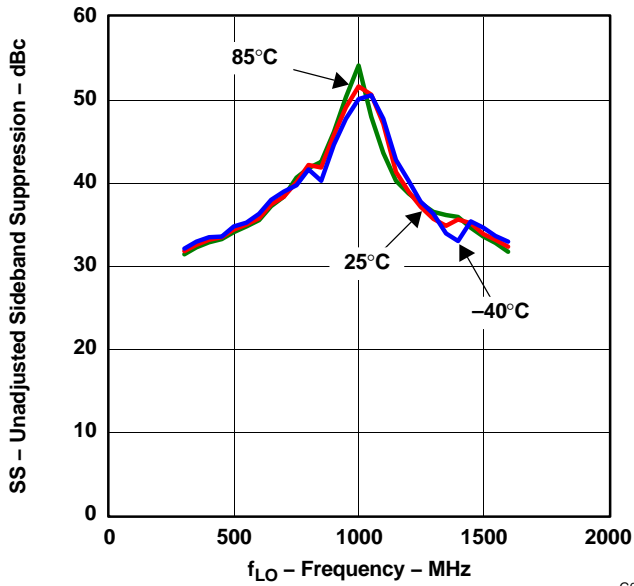
Figure 21.

**OUTPUT POWER FLATNESS
vs
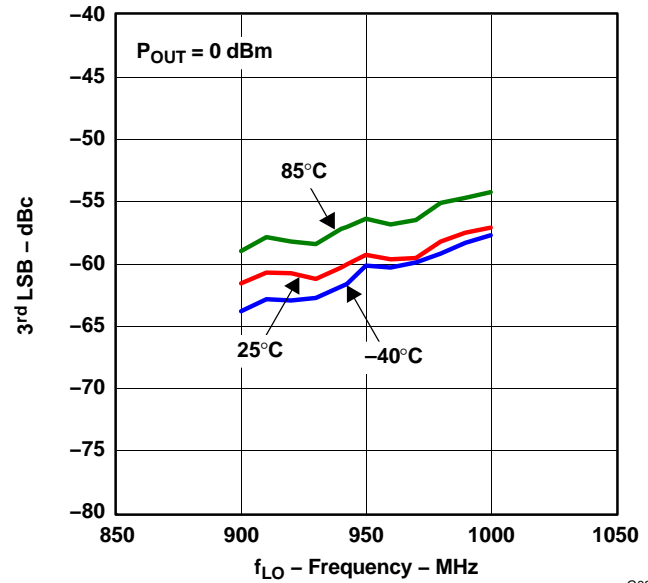FREQUENCY (P_{OUT} = 0, −10 dBm NOMINAL)**
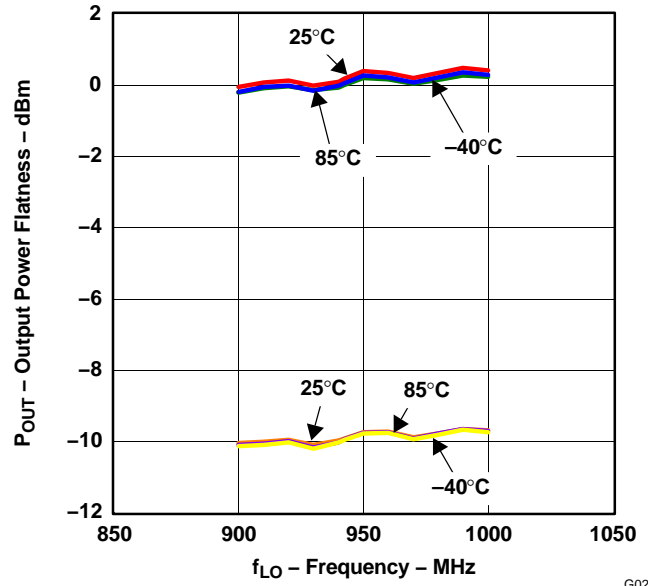
Figure 22.

**SECOND USB
vs
FREQUENCY**
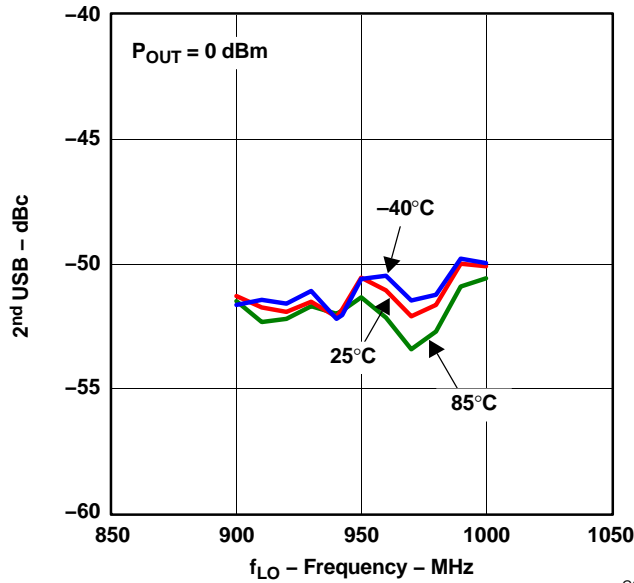
Figure 23.

**THIRD LSB
vs
FREQUENCY**

Figure 24.

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TYPICAL CHARACTERISTICS (continued)

CARRIER SUPPRESSION
vs
FREQUENCY

Figure 25.

SIDEBAND SUPPRESSION
vs
FREQUENCY

Figure 26.

OUTPUT POWER FLATNESS
vs
VCM (P_{OUT} = 0 dBm NOMINAL)

Figure 27.

CARRIER SUPPRESSION
vs
VCM
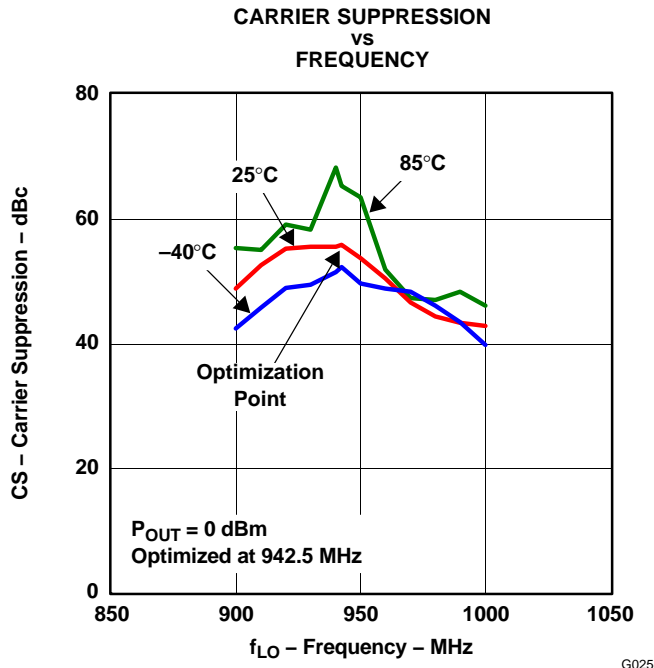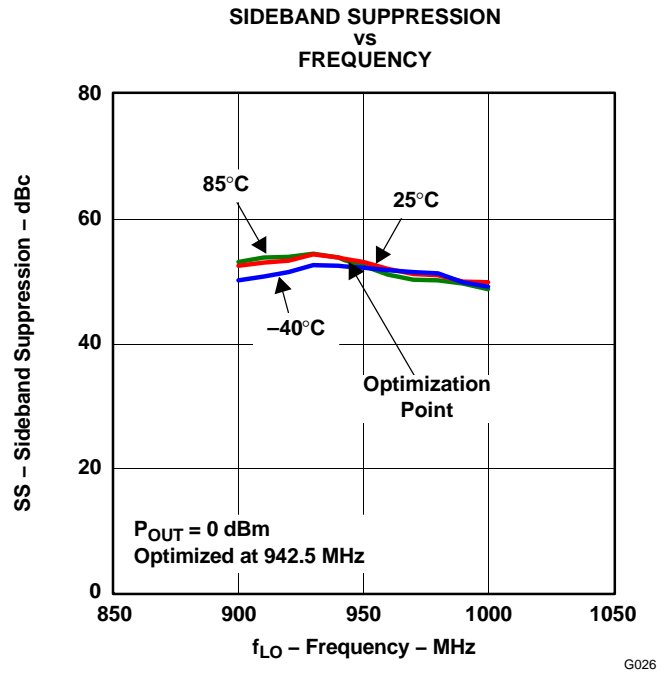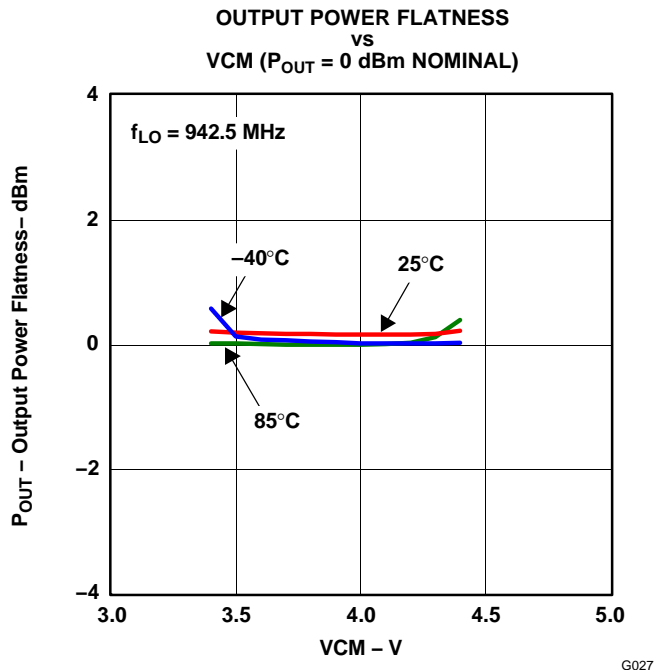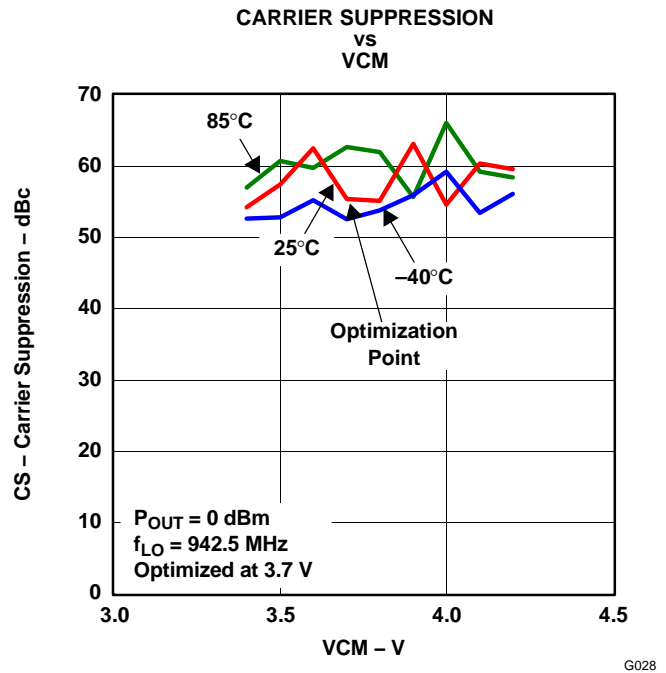
Figure 28.

TYPICAL CHARACTERISTICS (continued)
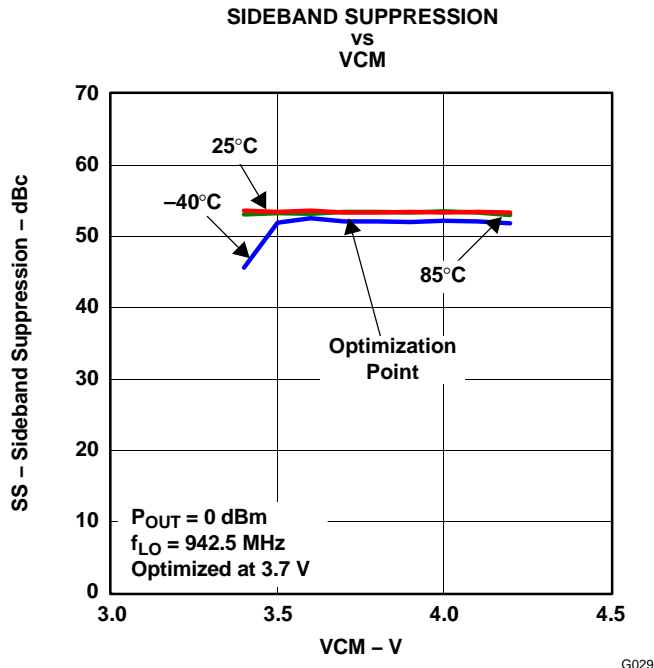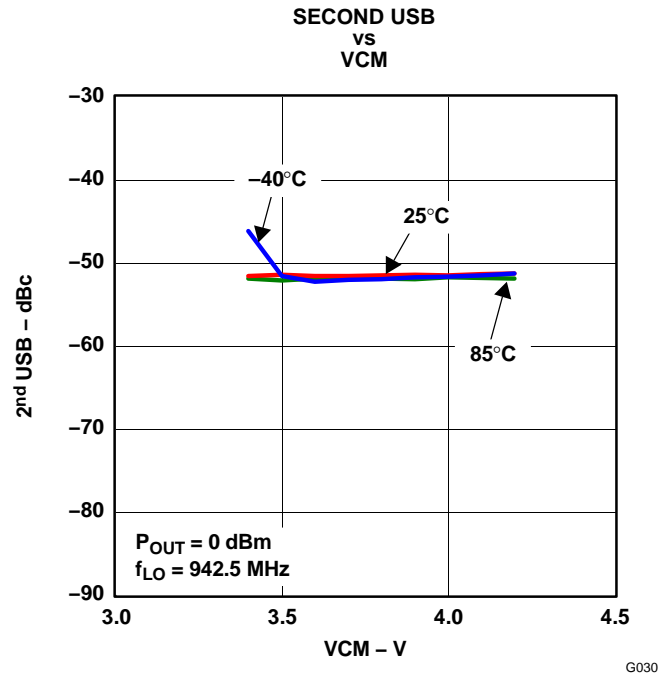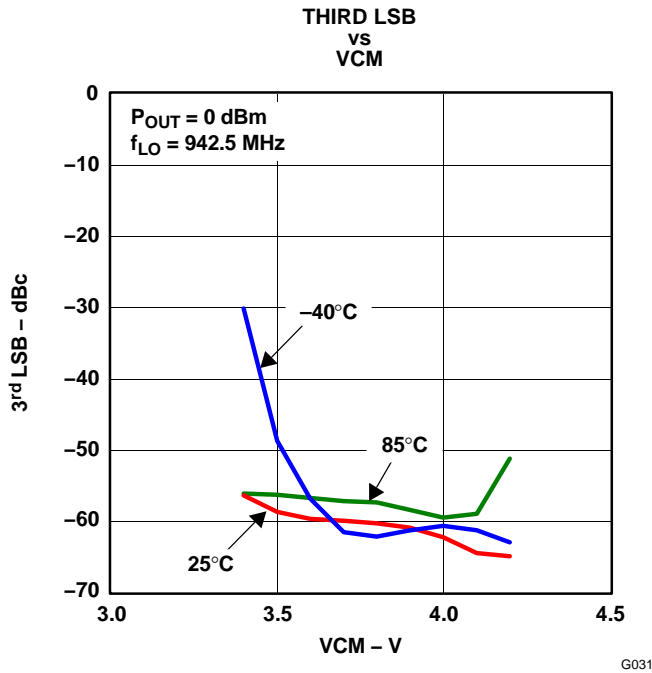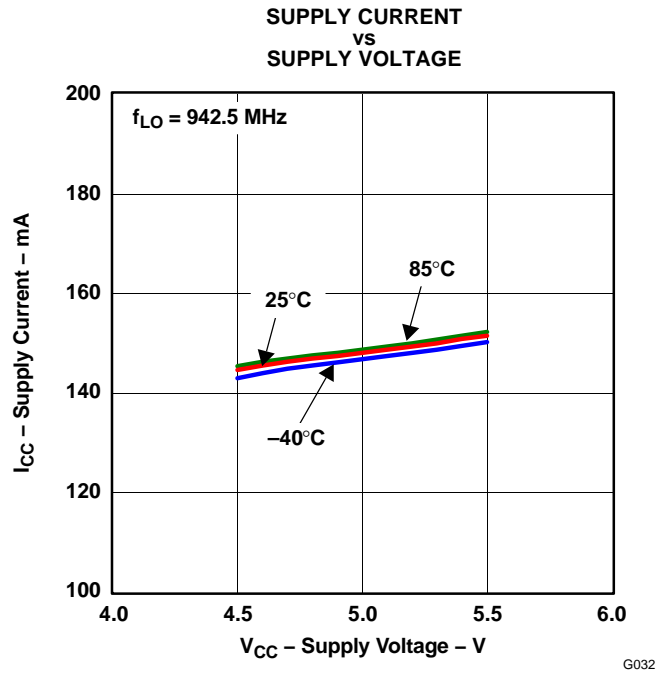
**SIDEBAND SUPPRESSION
vs
VCM**

Figure 29.

**SECOND USB
vs
VCM**

Figure 30.

**THIRD LSB
vs
VCM**

Figure 31.

**SUPPLY CURRENT
vs
SUPPLY VOLTAGE**

Figure 32.

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TYPICAL CHARACTERISTICS (continued)

OUTPUT POWER FLATNESS
vs
SUPPLY VOLTAGE (P_{OUT} = 0 dBm NOMINAL)

Figure 33.

CARRIER SUPPRESSION
vs
SUPPLY VOLTAGE

Figure 34.

SIDEBAND SUPPRESSION
vs
SUPPLY VOLTAGE

Figure 35.

SECOND USB
vs
SUPPLY VOLTAGE
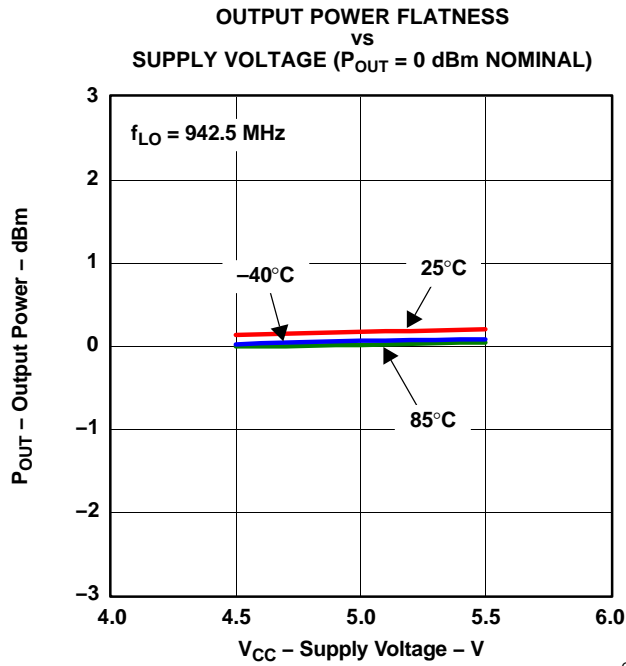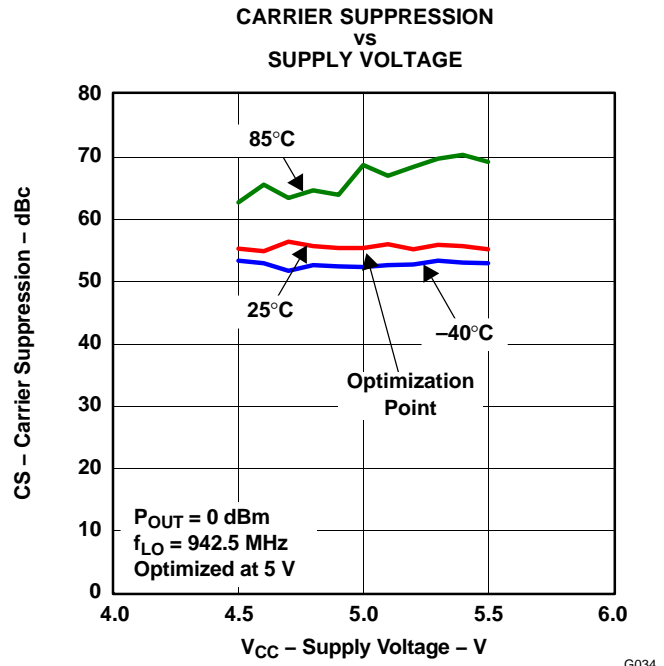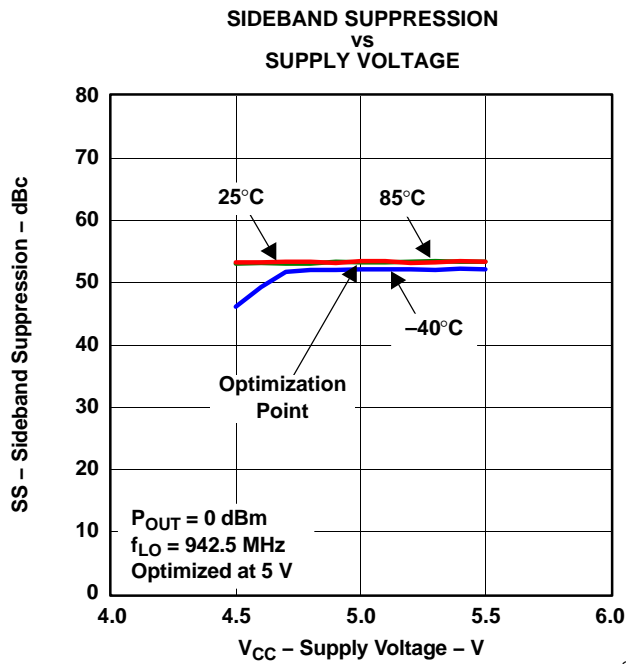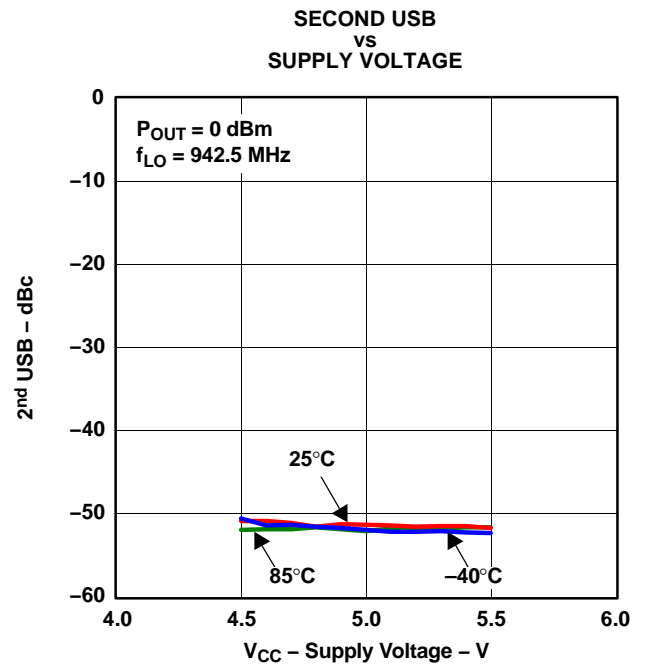
Figure 36.

TYPICAL CHARACTERISTICS (continued)

**THIRD LSB
vs
SUPPLY VOLTAGE**

G037

Figure 37.

**OUTPUT POWER FLATNESS
vs
LO INPUT POWER (P_{OUT} = 0 dBm NOMINAL)**

G038

Figure 38.

**CARRIER SUPPRESSION
vs
LOCAL OSCILLATOR INPUT POWER**

G039
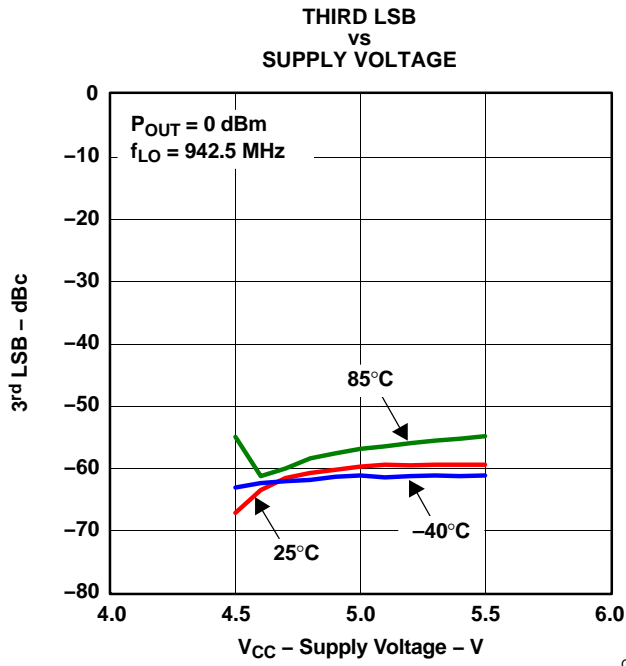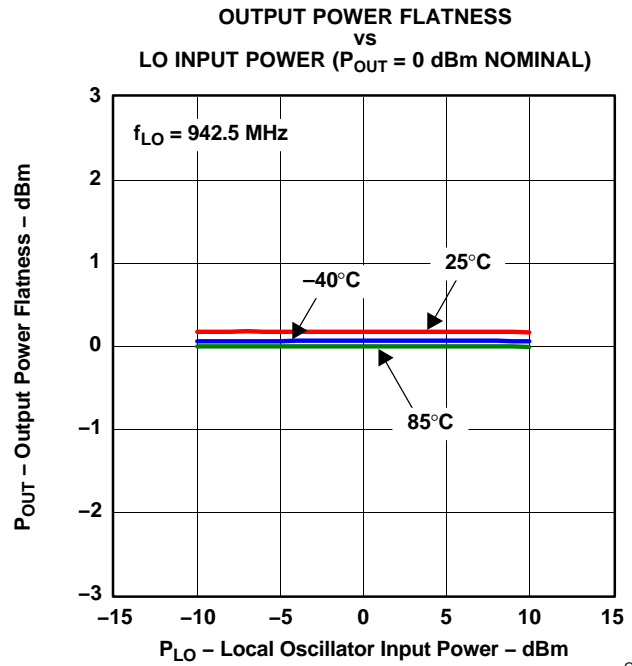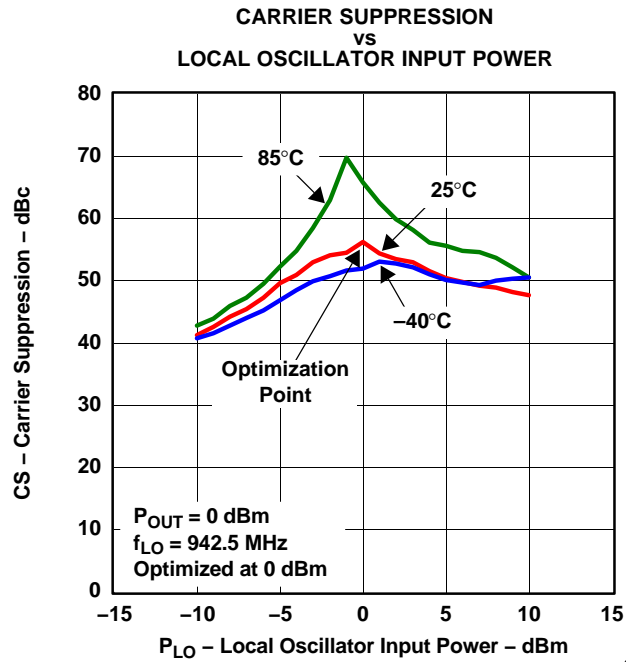
Figure 39.

Table 1. RFOUT and LO Pin Impedance

Frequency (MHz)	Z (RFOUT Pin)	Z (LO Pin)
100	8.59 − j 130.2	33.95 − j 106.93
200	7.12 − j 61.22	29.54 − j 52.57
300	8.52 − j 36.37	28.65 - j 31.83
400	10.5 − j 23.72	29.371 − j 19.33
500	12.82 − j 15.51	30.78 − j 11.42
600	15.26 − j 9.33	32.64 − j 6.06
700	187.1 − j 4.77	34.99 − j 1.65
800	20.8 − j 1.2	36.55 + j 1.65
900	24.2 + j 2.0	38.52 + j 3.98
1000	28.7 + j 4.9	40.29 + j 5.92
1100	32.35 + j 6.61	42.21 + j 6.98
1200	37.15 + j 6.88	44.09 + j 7.55
1300	40.55 + j 6.64	45.7 + j 7.96
1400	43.76 + j 6.4	47 + j 7.76
1500	46.6 + j 6.03	48.28 + j 7.39
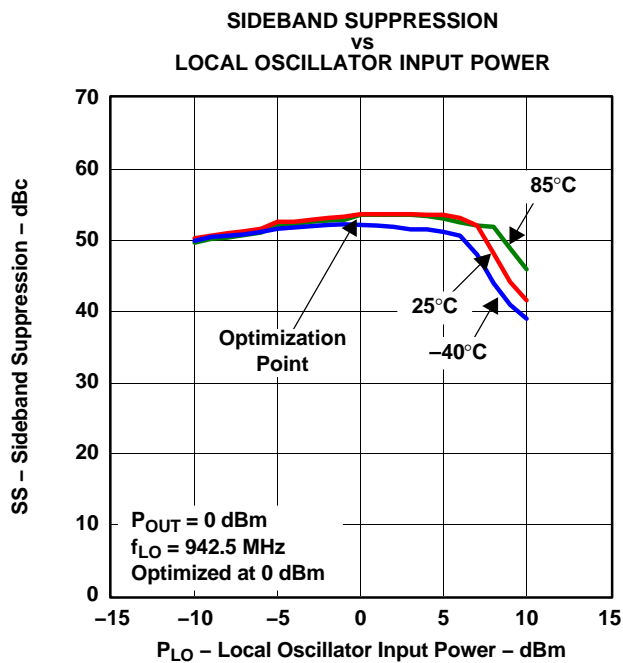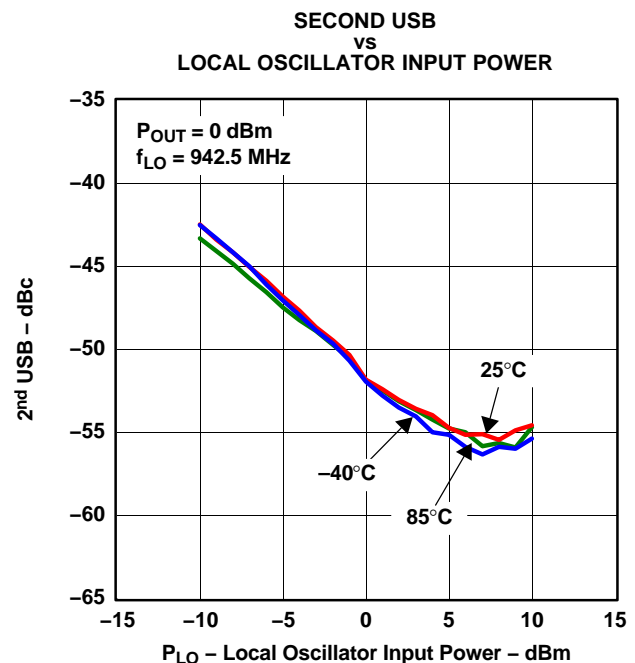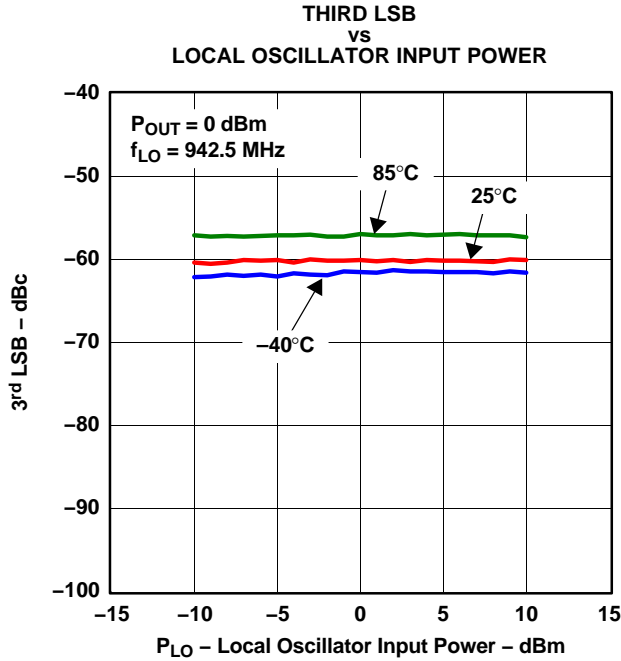
SIDEBAND SUPPRESSION
vs
LOCAL OSCILLATOR INPUT POWER

Figure 40.

SECOND USB
vs
LOCAL OSCILLATOR INPUT POWER

Figure 41.

THIRD LSB
vs
LOCAL OSCILLATOR INPUT POWER

Figure 42.

NOISE DISTRIBUTION AT 6 MHZ
OFFSET OVER TEMPERATURE

Figure 43.

NOISE DISTRIBUTION AT 6 MHZ
OFFSET OVER TEMPERATURE

Figure 44.

NOISE DISTRIBUTION AT 6 MHZ
OFFSET OVER TEMPERATURE

Figure 45.

**NOISE AT 6 MHz OFFSET
vs
OUTPUT POWER**

G046

Figure 46.

**GMSK SPECTRAL PERFORMANCE
vs
CHANNEL POWER**

G047

Figure 47.

**GSM EDGE EVM
vs
CHANNEL POWER**
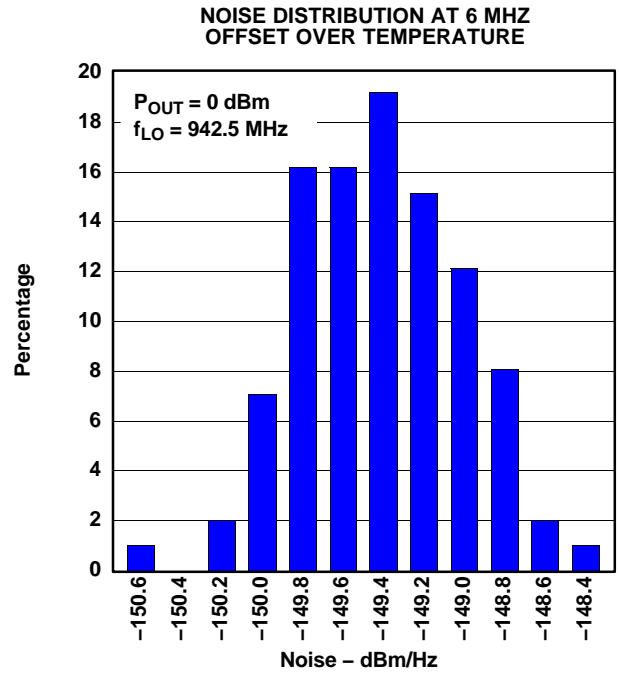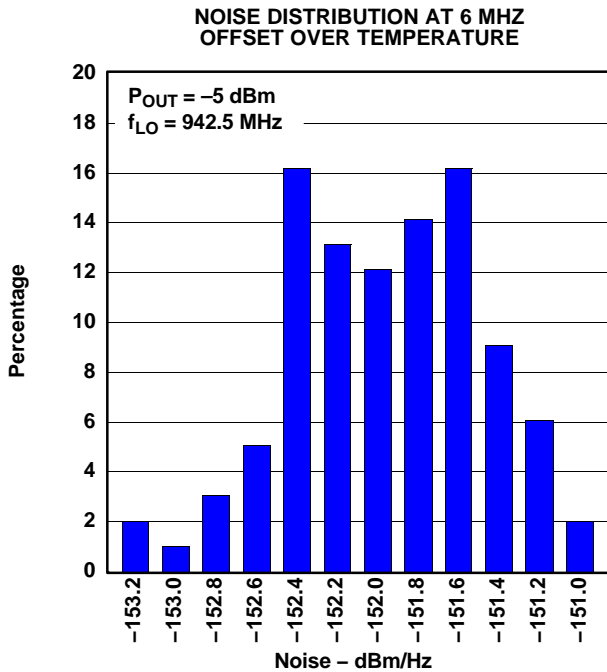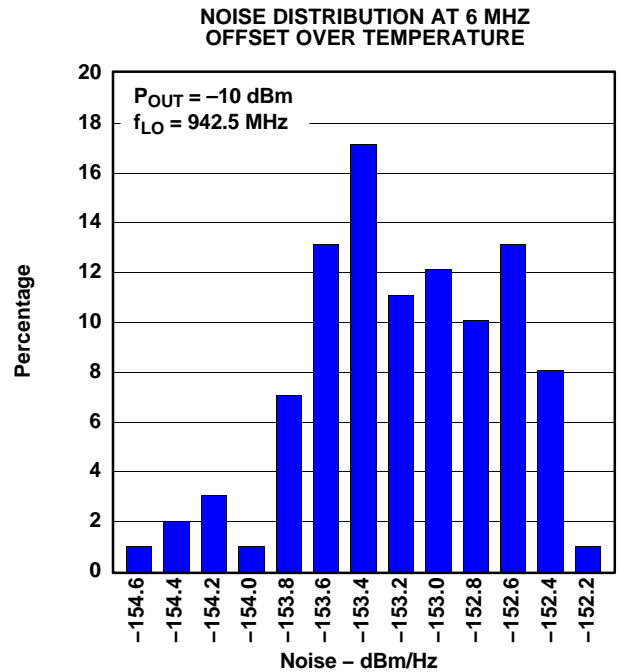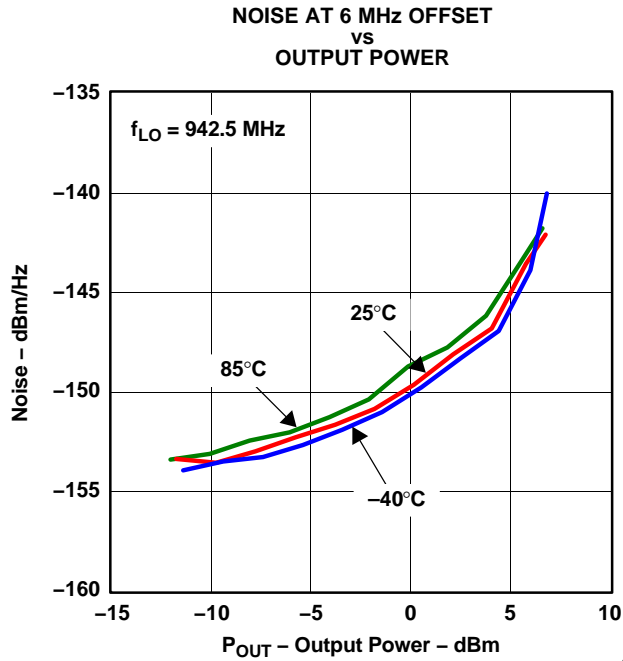
G048

Figure 48.

THEORY OF OPERATION

The TRF3701 employs a double-balanced mixer architecture in implementing the direct I, Q upconversion. The I, Q inputs can be driven single-endedly or differentially, with comparable performance in both cases. The common mode level (VCM) of the four inputs (IVIN, IREF, QVIN, QREF) is typically set to 3.7 V and needs to be driven externally. These inputs go through a set of differential amplifiers and through a V-I converter feed the double-balanced mixers. The AC-coupled LO input to the device goes through a phase splitter to provide the in-phase and quadrature signals that in turn drive the mixers. The outputs of the mixers are then summed, converted to single-ended signals, and amplified before they are fed to the output port RFOUT. The output of the TRF3701 is ac-coupled and can drive 50-Ω loads.
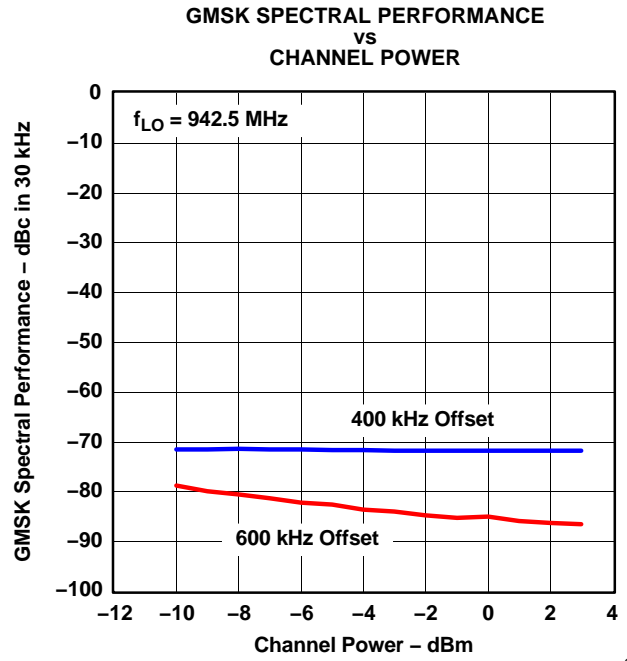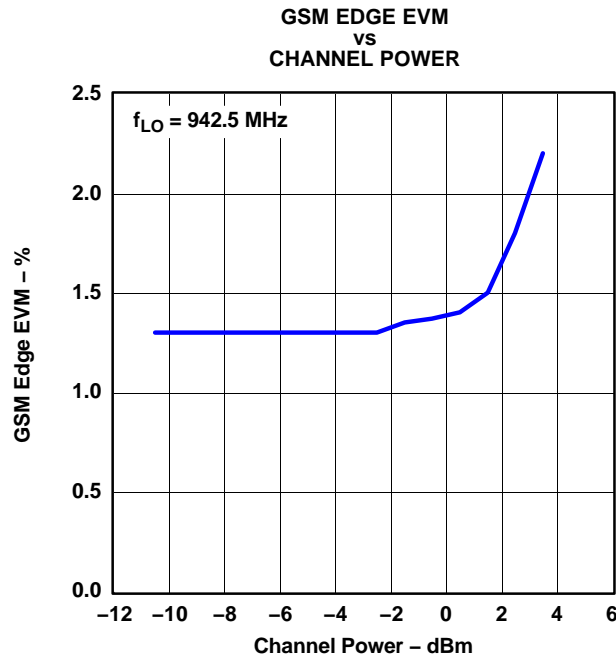
EQUIVALENT CIRCUITS

Figure 49 through Figure 52 show equivalent schematics for the main inputs and outputs of the device.
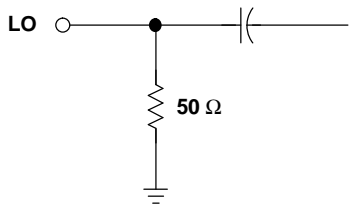
S0001-01

Figure 49. LO Equivalent Input Circuit

S0002-01

Figure 50. IVIN, QVIN, IREF, QREF Equivalent Circuit

S0003-01

Figure 51. RFOUT Equivalent Circuit

S0004-01

Figure 52. Power-Down (PWD) Equivalent Circuit

APPLICATION INFORMATION

DRIVING THE I, Q INPUTS

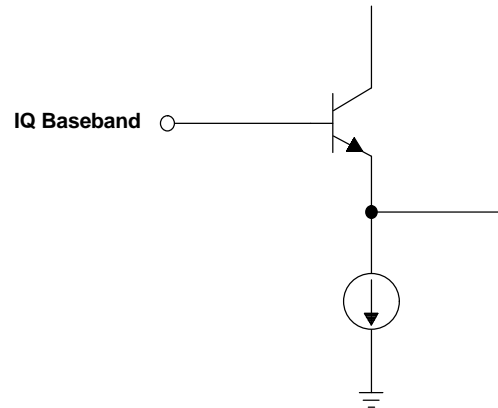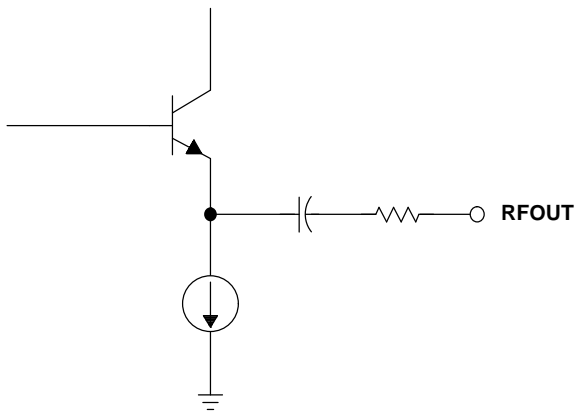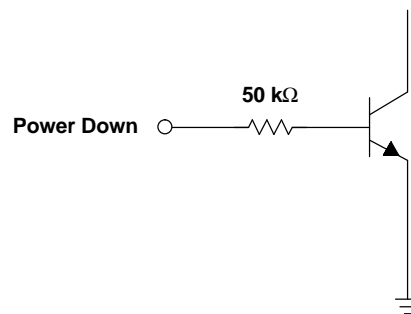There are several ways to drive the four baseband inputs of the TRF3701 to the required amplitude and dc offset. The optimal configuration depends on the end application requirements and the signal levels desired by the designer.

The TRF3701 is by design a differential part, meaning that ideally the user should provide fully complementary signals. However, similar performance in every respect can be achieved if the user only has single-ended signals available. In this case, the IREF and QREF pins just need to have the VCM dc offset applied.

Implementing a Single-to-Differential Conversion for the I, Q inputs

In case differential I, Q signals are desired but not available, the THS4503 family of wideband, low-distortion, fully differential amplifiers can be used to provide a convenient way of performing this conversion. Even if differential signals are available, the THS4503 can provide gain in case a higher voltage swing is required. Besides featuring high bandwidth and high linearity, the THS4503 also provides a convenient way of applying the VCM to all four inputs to the modulator through the VOCM pin (pin 2). The user can further adjust the dc levels for optimum carrier suppression by injecting extra dc at the inputs to the operational amplifier, or by individually adding it to the four outputs. Figure 53 shows a typical implementation of the THS4503 as a driver for the TRF3701. Gain can be easily incorporated in the loop by adjusting the feedback resistors appropriately. For more details, see the THS4503 data sheet at www.ti.com.

APPLICATION INFORMATION (continued)
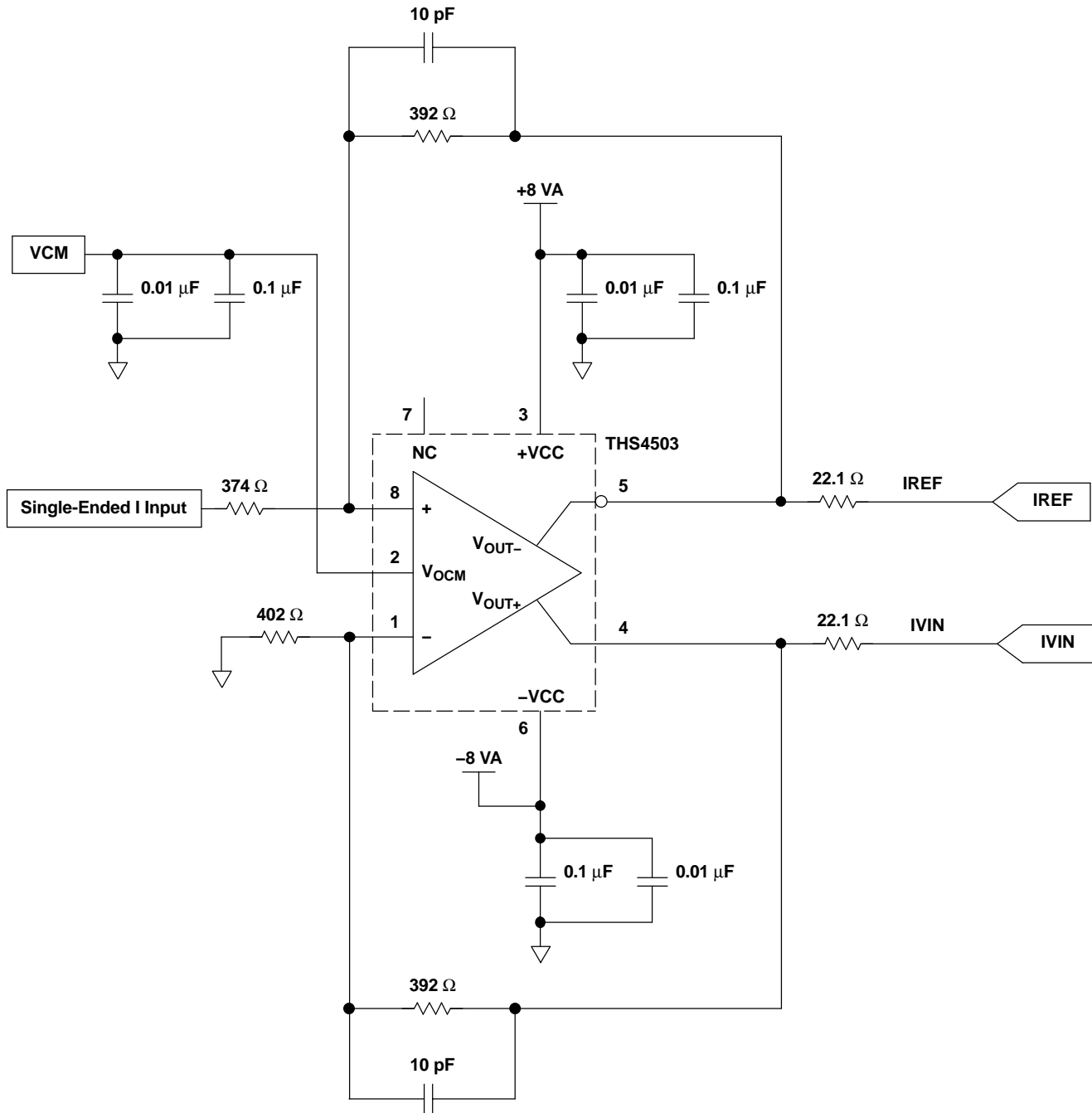
S0005-02

Figure 53. Using the THS4503 to Condition the Baseband Inputs to the TRF3701 (I Channel Shown)

DRIVING THE LOCAL OSCILLATOR INPUT

The LO pin is internally terminated to 50 Ω, thus enabling easy interface to the LO source without the need for external impedance matching. The power level of the LO signal should be in the range of −6 to 6 dBm. For characterization purposes, a power level of 0 dBm was chosen. An ideal way of driving the LO input of the TRF3701 is by using the TRF3750, an ultralow-phase-noise integer-N PLL from Texas Instruments. Combining the TRF3750 with an external VCO can complete the loop and provide a flexible, convenient and cost-effective

APPLICATION INFORMATION (continued)

solution for the local oscillator of the transmitter. Figure 54 shows a typical application for the LO driver network that incorporates the TRF3750 integer-N PLL synthesizer into the design. Depending on the VCO output and the amount of signal loss, an optional gain stage may be added to the output of the VCO before it is applied to the TRF3701 LO input.
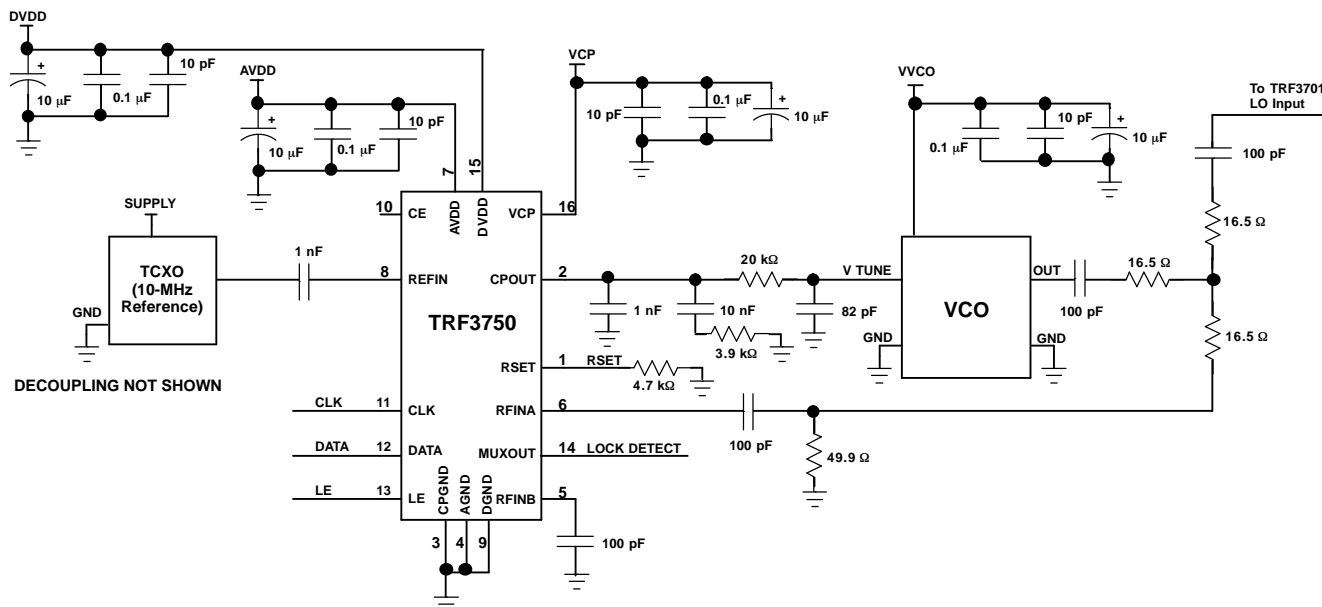

Figure 54. Typical Application Circuit for Generating the LO Signal for the TRF3701 Modulator

PCB LAYOUT CONSIDERATIONS

The TRF3701 is a high-performance RF device; hence, care should be taken in the layout of the PCB in order to ensure optimum performance. Proper decoupling with low ESR capacitors is needed for the VCC supplies (pins 6 and 10). Typical values used are in the order of 1 pF in parallel to 0.1 µF, with the lower-valued capacitors placed closer to the device pins. In addition, a larger tank capacitor in the order of 10 µF should be placed on the supply line as layout permits. At least a 4-layer board is recommended for the PCB. If possible, a solid ground plane and a ground pour is also recommended, as is a power plane for the supplies. Because the balance of the four I, Q inputs to the modulator can be critical to device performance, care should be taken to ensure that the trace runs for all four inputs are equidistant. In the case of single-ended drive of the I, Q inputs, the two unused pins IREF and QREF are fed with the VCM dc voltage only, and should be decoupled with a 0.1-µF capacitor (or smaller). The LO input trace should be minimized in length and have controlled impedance of 50 Ω. No external matching components are needed because there is an internal 50-Ω termination. The RFOUT pin should also have a relatively small trace to minimize parasitics and coupling, and should also be controlled to 50 Ω. An impedance-matching network can be used to optimize power transfer, but is not critical. All the results shown in the data sheet were taken with no impedance matching network used (RFOUT directly driving an external 50-Ω load).

The exposed thermal and ground pad on the bottom of the TRF3701 should be soldered to ground to ensure optimum electrical and thermal performance. The landing pattern on the PCB should include a solid pad and 4 thermal vias. These vias typically have 1,2-mm pitch and 0,3-mm diameter. The vias can be arranged in a 2×2 array. The thermal pad on the PCB should be at least 1.65×1.65 mm.

IMPLEMENTING A DIRECT UPCONVERSION TRANSMITTER USING A TI CommsDAC

The TRF3701 is ideal for implementing a direct upconversion transmitter, where the input I, Q data can originate from an ASIC or a DAC. Texas Instruments' line of digital-to-analog converters (DAC) is ideally suited for interfacing to the TRF3701. Such DACs include, among others, the DAC290x series, DAC5672, and DAC5686.

APPLICATION INFORMATION (continued)

This section illustrates the use of the DAC5686, which offers a unique set of features that make interfacing to the TRF3701 easy and convenient. The DAC5686 is a 16-bit, 500 MSPS, 2×−16× interpolating dual-channel DAC, and it features I, Q adjustments for optimal interface to the TRF3701. User-selectable, 11-bit offset and 12-bit gain adjustments can optimize the carrier and sideband suppression of the modulator, resulting in enhanced performance and relaxed filtering requirements at RF. The preferred mode of operation of the DAC5686 for direct interface with the TRF3701 at baseband is the dual-DAC mode. The user also has the flexibility of selecting any one of the four possible complex spectral bands to be fed into the TRF3701. For details on the available modes and programming, see the DAC5686 data sheet available at www.ti.com.

Figure 55 shows the DAC5686 in dual-DAC mode, which is best-suited for zero-IF interface to the TRF3701. In this mode, a seamless, passive interface between the DAC output and the input to the modulator is used, so that no extra components are needed between the two devices. The optimum dc offset level for the inputs to the TRF3701 (VCM) is approximately 3.7 V. The output of the DAC should be centered around 3.3 V or less (depending on signal swing), in order to ensure that its output compliance limits are not exceeded. The resistive network shown in Figure 55 allows for this dc offset transition while still providing a dc path between the DAC output and the modulator. This ensures that the dc offset adjustments on the DAC5686 can still be applied to optimize the carrier suppression at the modulator output. The combination of the DAC5686 and the TRF3701 provides a unique signal-chain solution with state-of-the-art performance for wireless infrastructure applications.
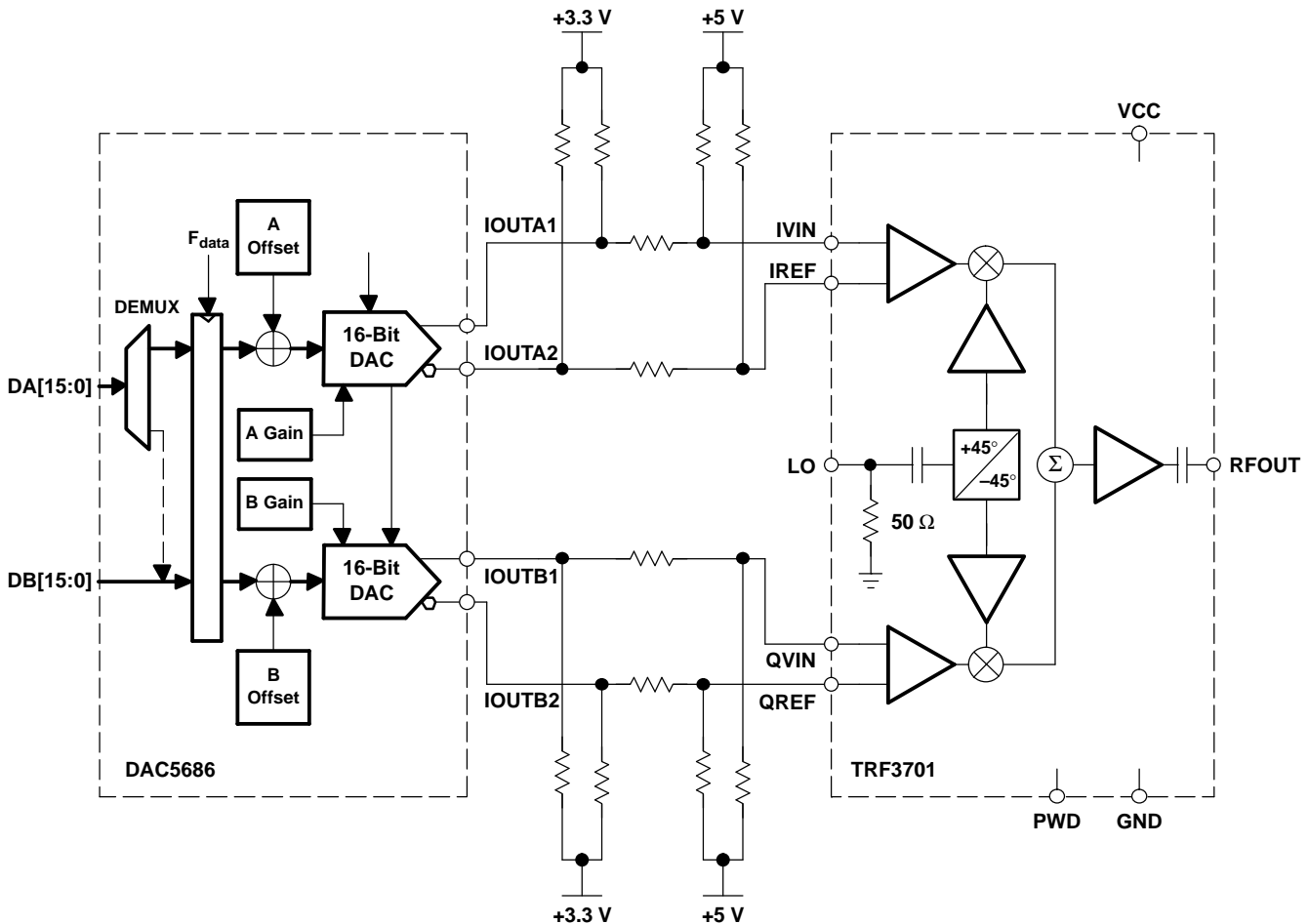
Figure 55. DAC5686 in Dual-DAC Mode with Quadrature Modulator

RHC (S–PQFP–N16)   **(CUSTOM PACKAGE)**   **PLASTIC QUAD FLATPACK**

4204353/A 05/02
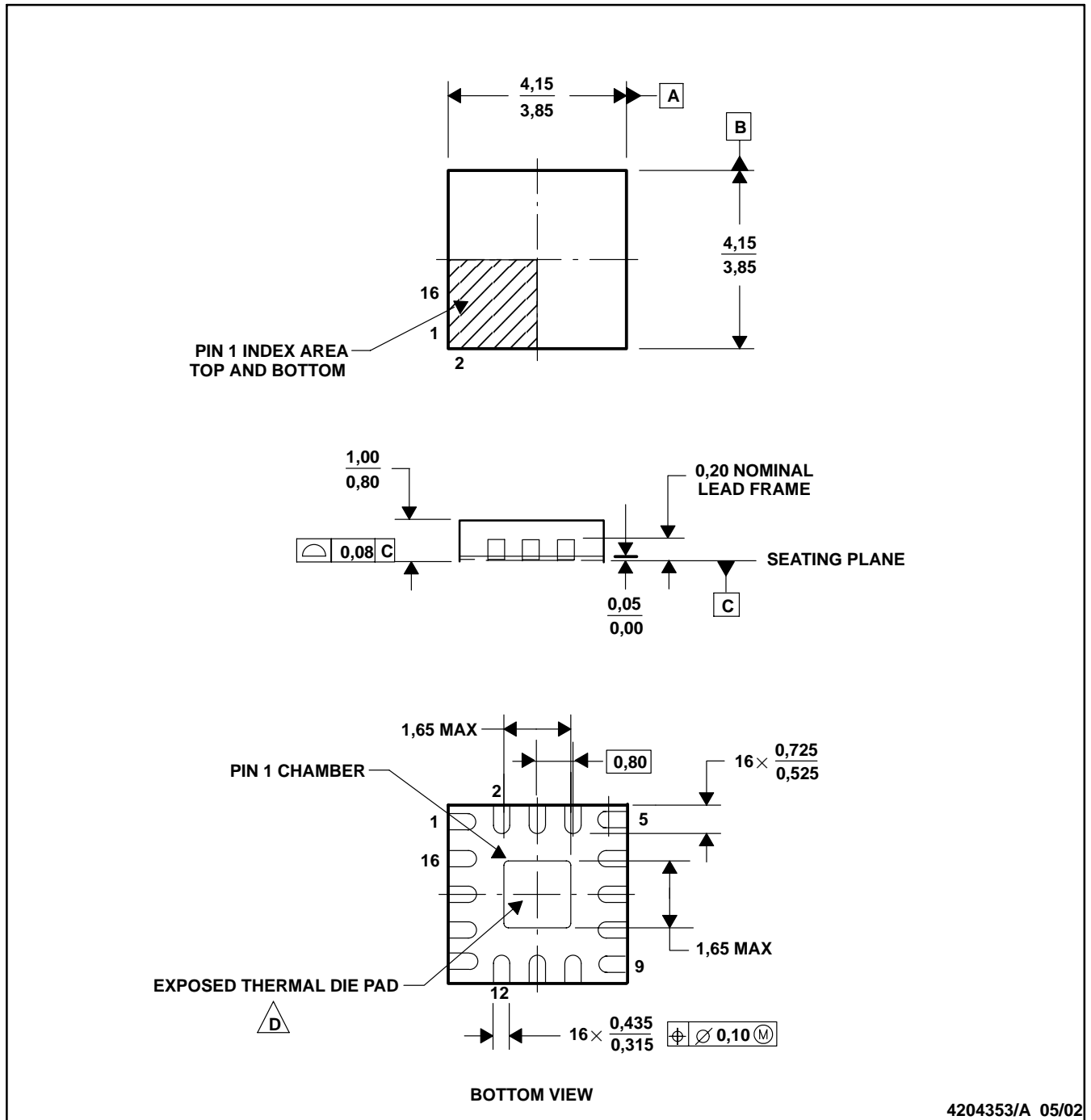
NOTES: A. All linear dimensions are in millimeters.
       B. This drawing is subject to change without notice.
       C. QFN (Quad Flatpack No–Lead) Package configuration.
       D. The Package thermal performance may be enhanced by bonding the thermal die pad to an external thermal plane. This pad is electrically and thermally connected to the backside of the die and possibly selected ground leads.

RHC (S−PQFP−N16)   (CUSTOM PACKAGE)   PLASTIC QUAD FLATPACK

$\dfrac{4,15}{3,85}$

A

B

$\dfrac{4,15}{3,85}$

16

1

2

PIN 1 INDEX AREA
TOP AND BOTTOM

$\dfrac{1,00}{0,80}$

0,20 NOMINAL
LEAD FRAME

⌓ 0,08 C

SEATING PLANE

$\dfrac{0,05}{0,00}$

C

16X $\dfrac{0,725}{0,525}$

0,80

2

1

5

16

9

12

EXPOSED THERMAL PAD

△D

16X $\dfrac{0,435}{0,315}$ ⊕ 0,10 Ⓜ

BOTTOM VIEW
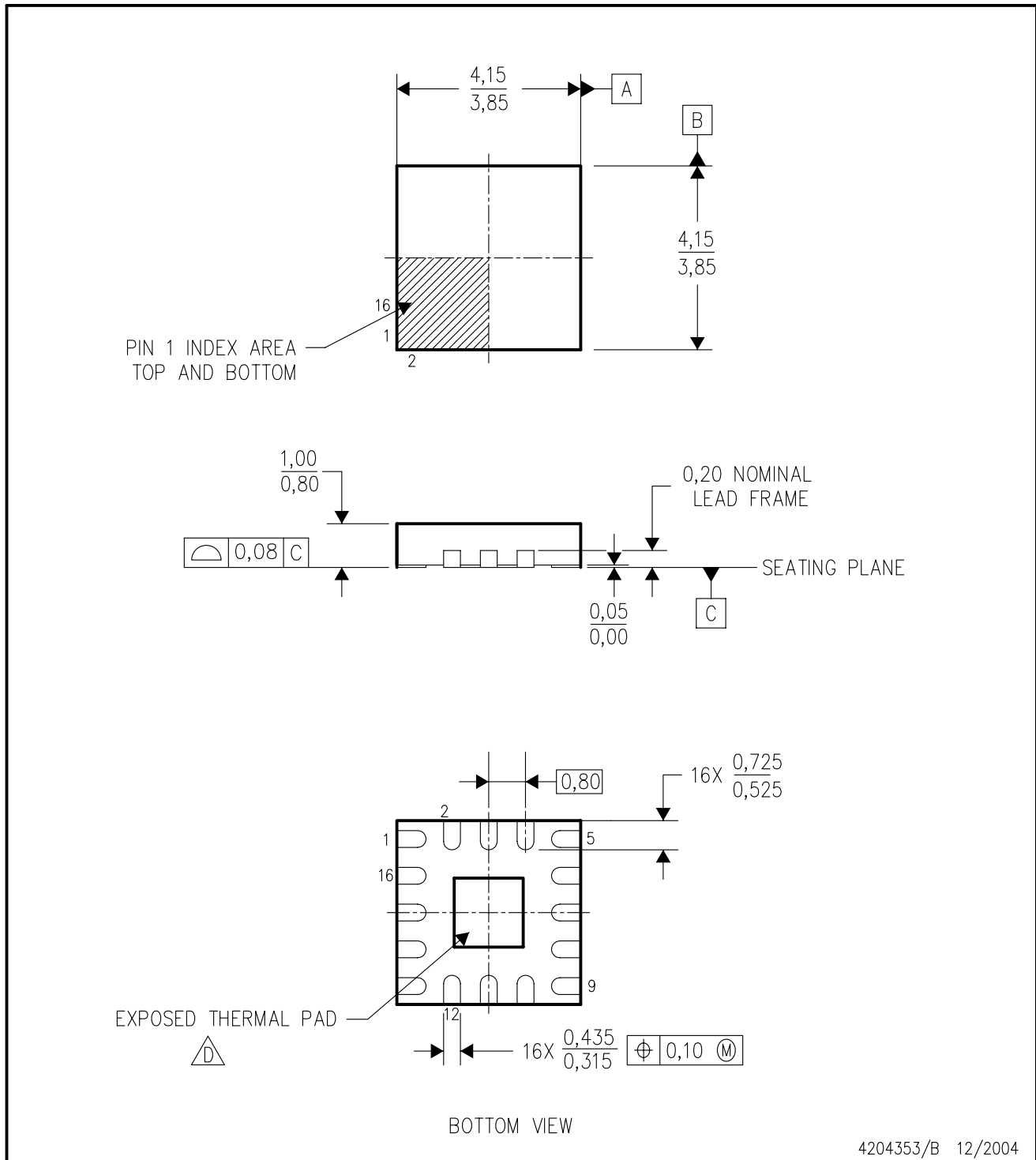
4204353/B   12/2004

NOTES: A.   All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M−1994.
          B.   This drawing is subject to change without notice.
          C.   QFN (Quad Flatpack No−Lead) Package configuration.
      △D   The package thermal pad must be soldered to the board for thermal and mechanical performance.
            See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

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