September 2015

FAN4800AU / FAN4800CU PFC/ PWM Controller Combination

Features

- Pin-to-Pin Compatible with ML4800, FAN4800, CM6800, and CM6800A
- PWM Configurable for Current-Mode or Feed-Forward Voltage-Mode Operation
- Internally Synchronized Leading-Edge PFC and Trailing-Edge PWM in One IC
- Low Operating Current
- Innovative Switching-Charge Multiplier Divider
- Average-Current-Mode for Input-Current Shaping
- **PFC Over-Voltage and Under-Voltage Protections**
- **PFC Feedback Open-Loop Protection**
- Cycle-by-Cycle Current Limiting for PFC/PWM
- **Power-on Sequence Control and Soft-Start**
- **Line Sagging Protection**
- $f_{\text{RTCT}} = 4 \cdot f_{\text{PFC}} = 4 \cdot f_{\text{PWM}}$ for FAN4800AU
- f_{RTCT}=4•f_{PFC}=2•f_{PWM} for FAN4800CU

Applications

- Desktop PC Power Supply
- Internet Server Power Supply
- **LCD TV/ Monitor Power Supply**
- **UPS**
- Battery Charger
- DC Motor Power Supply
- Monitor Power Supply
- Telecom System Power Supply
- Distributed Power

Related Resources

 *AN[-8027](http://www.fairchildsemi.com/an/AN/AN-8027.pdf:-.T�K���Ff�1z
L�) — FAN480X PFC+PWM Combination Controller Application*

Description

The highly integrated FAN4800AU/CU parts are specially designed for power supplies that consist of boost PFC and PWM. They require very few external components to achieve versatile protections and compensation. They are available in 16-pin DIP and SOP packages.

The PWM can be used in current or Voltage Mode. In Voltage Mode, feed-forward from the PFC output bus can reduce secondary output ripple.

To evaluate FAN4800AU/CU for replacing existing FAN4800A/C, FAN4800AS/CS, old version FAN4800 and ML4800 boards, six things must be completed before the fine-tuning procedure:

- 1. Change R_{AC} resistor from the old value to a higher resistor value: 6 M Ω to 8 M Ω .
- 2. Change RT/CT pin from the existing values to $R_T=6.8 \text{ k}\Omega$ and $C_T=1000 \text{ pF}$ to have f_{PFC}=64 kHz and f_{PWM}=64 kHz.
- 3. The VRMS pin needs to be 1.224 V at $V_{\text{IN}}=85$ V_{AC} for universal input application with line input from 85 V_{AC} to 270 V_{AC}.
- 4. Change ISENSE pin filter from the exiting values to $R_{Filter}=51 \Omega$ and $C_{Filter}=0.01 \mu F$ for higher bandwidth.
- 5. At full load, the average V_{VEA} must be ~4.5 V and ripple on V_{VFA} needs to be less than 400 mV.
- 6. For the SS pin, the soft-start current has been reduced to half the FAN4800 capacitor.

There are two differences from FAN4800AS/CS to FAN4800AU/CU:

- Add Line Sagging Protection
- Fix Inductance Current Instability during AC Cycle Drop Test

FAN4800AU/CU AN4800AU/CU — PFC/ PWM Controller Combination **PFC/ PWM Controller Combination**

Ordering Information

Block Diagram

Pin Configuration

Figure 6. Pin Configuration (Top View)

Pin Definitions

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Notes:

1. All voltage values, except differential voltage, are given with respect to GND pin.

2. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.

Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Electrical Characteristics

Continued on the following page…

Electrical Characteristics (Continued)

Unless otherwise noted, $V_{DD}=15$ V, $T_{A}=25^{\circ}C$, $T_{A}=T_{J}$, $R_{T}=6.8$ kΩ, and $C_{T}=1000$ pF.

Continued on the following page…

Electrical Characteristics (Continued)

Unless otherwise noted, $V_{DD}=15$ V, $T_{A}=25^{\circ}C$, $T_{A}=T_{J}$, $R_{T}=6.8$ kΩ, and $C_{T}=1000$ pF.

Notes:

3. This parameter, although guaranteed by design, is not 100% production tested.

4. This gain is the maximum gain of modulation with a given V_{RMS} voltage when V_{VEA} is saturated to HIGH.

Figure 17. VRMS-UVP vs. Temperature Figure 18. ΔVRMS-UVP vs. Temperature

FAN4800AU/CU

FAN4800AU/CU --- PFC/ PWM Controller Compination

PFC/ PWM Controller Combination

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Typical Characteristics

Figure 19. VGATE-CLAMP-PFC vs. Temperature Figure 20. VGATE-CLAMP-PWM vs. Temperature

Figure 21. DPFC-MAX vs. Temperature Figure 22. DPWM-MAX vs. Temperature

Figure 23. I_{ss} vs. Temperature **Figure 24.** V_{RMS-SAG} vs. Temperature

Functional Description

Oscillator

The internal oscillator frequency is determined by the timing resistor and capacitor on the RT/CT pins as shown in [Figure 25.](#page-12-0) The frequency of the internal oscillator is given:

$$
f_{osc} = \frac{1}{0.56 \cdot R_r \cdot C_r + 360 C_r} \tag{1}
$$

Because the PWM stage generally uses a forward converter, it is necessary to limit the maximum duty cycle at 50%. To have a small tolerance of the maximum duty cycle, a frequency divider with toggle flip-flops is used, as illustrated in [Figure 25.](#page-12-0) The operation frequency of PFC and PWM stage is 1/4 of oscillator frequency. (For FAN4800CU, the operation frequencies for PFC and PWM stages are 1/4 and 1/2 of oscillator frequency, respectively).

The dead time for the PFC gate drive signal is determined by:

$$
t_{DEAD} = 360C_T \tag{2}
$$

The dead time should be smaller than 2% of the switching period to minimize line current distortion around the line zero crossing.

[Figure 27](#page-12-1) shows the interleaved leading / trailing edge modulation, where the turn-off of the PFC drive signal is synchronized to the turn-on of the PWM drive signal. This technique allows the PFC output diode current to flow directly into the downstream DC/DC converter, minimizing the current ripple of PFC output capacitor.

Gain Modulator

Gain modulator is the key block for the PFC stage because it provides the reference to the current control error amplifier for the input current shaping, as shown in [Figure 28.](#page-12-2) The output current of the gain modulator is a function of V_{EA}, I_{AC,} and V_{RMS}. The gain of the gain modulator is given as a ratio between I_{MO} and I_{AC} with a given V_{RMS} when V_{EA} is saturated to HIGH. The gain is inversely proportional to $V_{RMS}²$, as shown in Figure 29, to implement line feed-forward. This automatically adjusts the reference of current control error amplifier according to the line voltage, such that the input power of PFC converter is not changed with line voltage (as shown i[n Figure 30\)](#page-13-1).

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Figure 29. Modulation Gain Characteristics

Figure 30. Line Feed-Forward Operation

To sense the RMS value of the line voltage, averaging circuit with two poles is typically employed, as shown in [Figure 28.](#page-12-2) Notice that the input voltage of the PFC is clamped at the peak of the line voltage once the PFC stops switching because the junction capacitance of the bridge diode is not discharged, as shown in [Figure 31.](#page-13-2) Therefore, the voltage divider for VRMS should be designed considering the brownout protection trip-point and minimum operation line voltage.

The rectified sinusoidal signal is obtained by the current flowing into the IAC pin. The resistor R_{IAC} should be large enough to prevent saturation of the gain modulator, calculating as:

$$
\frac{\sqrt{2}V_{LINE}}{R_{IAC}} \cdot G^{MAX} < 140\,\mu\text{A} \tag{3}
$$

where V_{LINEMIN} is the line voltage that trips brownout protection, G_{MAX} is the maximum modulator gain when V_{RMS} is 1.08 V (which can be found in the datasheet), and $140 \mu A$ is the maximum output current of the gain modulator.

Current Control of Boost Stage

The FAN4800AU/CU employs two control loops for power factor correction, as shown in [Figure 32:](#page-13-3) a current-control loop and a voltage-control loop. The current-control loop shapes inductor current as shown in [Figure 33](#page-13-4) based on the reference signal obtained at the IAC pin calculated as:

$$
I_L \cdot R_{CS1} = I_{MO} \cdot R_M = I_{AC} \cdot G \cdot R_M \tag{4}
$$

Figure 32. Gain Modulation Block

Figure 33. Inductor Current Shaping

The current-control feedback loop also has a pulse-bypulse current limit comparator that forces the PFC switch to turn off until the next switching cycle if the ISENSE pin voltage drops below -1.3 V.

Voltage Control of Boost Stage

The voltage-control loop regulates PFC output voltage using an internal error amplifier such that the FB voltage is the same as the internal reference of 2.5 V.

Brownout Protection

The built-in internal brownout protection comparator monitors the voltage of the VRMS pin. Once VRMS pin voltage is lower than 1.05 V, the PFC stage is shut down to protect the system from over current. FAN4800AU/CU starts up the boost stage once VRMS voltage increases above 1.9 V.

TriFault Detect™

To improve power supply reliability, reduce system component count, and simplify compliance to UL 1950 safety standards, the FAN4800AU/CU includes Fairchild's TriFault Detect technology.

In a feedback path failure, the output voltage of the PFC can exceed safe operating limits. TriFault Detect protects the power supply from a failure related to the output feedback by monitoring the FBPFC voltage.

TriFault Detect is an entirely internal circuit. It requires no external components to serve its protective function.

Figure 34. TriFault Detect™

PWM Stage

The PWM stage is capable of Current Mode or Voltage Mode operation. In Current-Mode, the PWM ramp (RAMP) is usually derived directly from a currentsensing resistor or current transformer in the primary side of the output stage, and is thereby representative of the current flowing in the converter's output stage. ILIMIT, which provides cycle-by-cycle current limiting, is typically connected to RAMP in such applications.

For Voltage-Mode operation, RAMP can be connected to a separate RC timing network to generate a voltage ramp against which the FBPWM voltage is compared. Under these conditions, the voltage feed-forward from the PFC bus can be used for better line transient response.

No voltage error amplifier is included in the PWM stage, as this function is generally performed by KA431, in the secondary side. To facilitate the design of opto-coupler feedback circuitry, an offset voltage is built into the inverting input of PWM comparator. This allows FBPWM to command a zero percent duty cycle when its pin voltage is below 1.5 V.

Figure 35. PWM Ramp Generation Circuit

PWM Current Limit

The ILIMIT pin is a direct input to the cycle-by-cycle current limiter for the PWM section. If the input voltage at this pin exceeds 1 V, the output of the PWM is disabled for until the start of the next PWM clock cycle.

VIN OK Comparator

The V_{IN} OK comparator monitors the output of the PFC stage and inhibits the PWM stage if this voltage is less than 2.4 V (96% of its nominal value). Once this voltage goes above 2.4 V, the PWM stage begins soft-start. The PWM stage is shut down when FBPFC voltage drops below 1.3 V.

PWM Soft-Start (SS)

PWM startup is controlled by the soft-start capacitor. A current source of 10 µA supplies the charging current for the soft-start capacitor. PWM startup is prohibited until the soft-start capacitor voltage reaches 1.5 V.

AC Line Drops Out

FAN4800AU/CU is designed such that the operation of PFC part is not perturbed by AC line dropout. Once line voltage disappears, the error amplifier can be saturated, resulting in abnormal current waveforms when the line voltage is recovered if proper preventive measures are not employed.

With a limited gain modulator operation, FAN4800AU /CU guarantees stable PFC operation even when AC line is recovered from dropout, as shown in [Figure 36.](#page-15-0)

Figure 36. AC Cycle Drop

Line Sag Protection

When the line sags below its normal operational range, the PFC part keeps operating until the brownout protection is triggered, which has 1 s debounce time. Due to the low line voltage, the gain modulator for current loop is saturated and input current of PFC is limited, resulting in a drop of the PFC output voltage at heavy-load condition. Since the PWM part has a V_{IN} OK comparator that shuts down PWM operation when the FBPFC voltage drops below 1.3 V, the downstream DC-DC converter can stop operation while the PFC output voltage drops during line sag. Once the downstream converter stops operation, even the limited PFC input current can charge up the PFC output since the PFC part has no load current. Because this can cause repeated startup and shutdown of downstream converter during line sag, FAN4800AU/CU has line sag protection.

There are two conditions that trigger line sag protection, as shown in [Figure 37](#page-15-1) and [Figure 38.](#page-15-2) The first condition is when V_{RMS} is lower than $V_{RMS-SAG}$ $(0.85 V)$ for longer than t_{SAG} $(33 ms)$, as shown in [Figure 37.](#page-15-1) The second condition is when V_{RMS} is lower than VRMS-SAG (0.85 V) and VFBPFC is lower than VIN-OFF (1.3 V), as shown in [Figure 38.](#page-15-2) Once line sag protection is triggered, the PWM and the PFC stop operation until V_{RMS} increases above 1.9 V.

Figure 37. The First Condition of Sag Protection

Figure 38. The Second condition of Sag Protection

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