General Description

The MAX1667 provides the power control necessary to charge batteries of any chemistry. All charging functions are controlled through the Intel System Management Bus (SMBus™) interface. The SMBus 2-wire serial interface sets the charge voltage and current and provides thermal status information. The MAX1667 functions as a Level 2 charger, compliant with the Duracell/Intel Smart Battery Charger Specification.

In addition to the feature set required for a Level 2 charger, the MAX1667 generates interrupts to signal the host when power is applied to the charger or when a battery is installed or removed. Additional status bits allow the host to check whether the charger has enough input voltage, and whether the voltage on or current into the battery is being regulated. This allows the host to determine when lithium-ion (Li+) batteries have completed the charge without interrogating the battery.

The MAX1667 is available in a 20-pin SSOP with a 2mm profile height.

________________________Applications

Notebook Computers Charger Base Stations Personal Digital Assistants Phones

Pin Configuration appears at end of data sheet.

Features

- ♦ **Charges Any Battery Chemistry: Li+, NiCd, NiMH, Lead Acid, etc.**
- ♦ **SMBus 2-Wire Serial Interface**
- ♦ **Compliant with Duracell/Intel Smart Battery Charger Specification Rev. 1.0**
- ♦ **4A, 3A, or 1A (max) Battery Charge Current**
- ♦ **5-Bit Control of Charge Current**
- ♦ **Up to 18.4V Battery Voltage**
- ♦ **11-Bit Control of Voltage**
- ♦ **±1% Voltage Accuracy**
- ♦ **Up to +28V Input Voltage**
- ♦ **Battery Thermistor Fail-Safe Protection**
- ♦ **Greater than 95% Efficiency**
- ♦ **Synchronous Rectifier**

Ordering Information

Typical Operating Circuit

MAXIM

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For pricing, delivery, and ordering information, please contact Maxim/Dallas Direct! at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

ABSOLUTE MAXIMUM RATINGS

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

(VDCIN = 18V, internal reference, 1µF capacitor at REF, 1µF capacitor at VL, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at $T_A = +25^{\circ}C$, unless otherwise noted.)

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ELECTRICAL CHARACTERISTICS (continued)

(VDCIN = 18V, internal reference, 1µF capacitor at REF, 1µF capacitor at VL, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at $Ta = +25^{\circ}C$, unless otherwise noted.)

Note 1: When DCIN is less than 4V, VL is less than 3.2V, causing the battery current to be typically 2µA (CS plus BATT input current).

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ELECTRICAL CHARACTERISTICS

(VDCIN = 18V, internal reference, 1µF capacitor at REF, 1µF capacitor at VL, **TA = -40°C to +85°C**, unless otherwise noted. Typical values are at T_A = +25°C. Limits over this temperature range are guaranteed by design.)

TIMING CHARACTERISTICS (Figures 1 and 2)

(**TA = 0°C to +85°C**, unless otherwise noted.)

TIMING CHARACTERISTICS (Figures 1 and 2)

(**TA = -40°C to +85°C**, unless otherwise noted. Limits over this temperature range are guaranteed by design.)

Figure 1. SMBus Serial-Interface Timing—Address

Figure 2. SMBus Serial-Interface Timing—Acknowledge

0 105 15 20 25

Typical Operating Characteristics

Chemistry-Independent,

Level 2 Smart Battery Charger

ChargingVoltage() = 12,000mV ChargingCurrent() = 1500mA

LOAD CURRENT (mA)

(Circuit of Figure 7, $T_A = +25^{\circ}C$, unless otherwise noted.)

ChargingVoltage() = 12,000mV ChargingCurrent() = 1500mA

5.425

5.450

MAX1667 TOC03

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MAX1667 EFFICIENCY vs. LOAD CURRENT EFFICIENCY vs. BATT VOLTAGE VREF vs. TEMPERATURE (VOLTAGE REGULATION) (CURRENT REGULATION) 4.110 100 100 MAX1667 TOC07 A MAX1667 TOC08 MAX1667 TOC09 B 95 95 A 4.105 90 90 D E C C85 85 4.100 B EFFICIENCY (%) EFFICIENCY (%) EFFICIENCY (%) EFFICIENCY (%) 80 V REF (V) 80 4.095 75 75 70 70 4.090 A: $V_{DCIN} = 20V$, $V_{BAT} = 17V$ 65 65 $B: V_{DCIN} = 16V, V_{BAT} = 12.75V$ $C: V_{DCIN} = 20V, V_{BAT} = 12.75V$ 60 60 A: $V_{DCIN} = 16V$, $I_{LOAD} = 2A$ 4.085 $D: V_{DCIN} = 16V, V_{BATT} = 8.5V$ $B: V_{DCIN} = 20V, I_{LOAD} = 2A$ $V_{DCIN} = 20V$ 55 55 E: $V_{DCIN} = 20V$, $V_{BATT} = 8.5V$ C: $V_{DCIN} = 20V$, $I_{LOAD} = 600mA$ 4.080 -40 50 50 0 2 4 6 8 10 12 14 16 18 14 16 -40 4020-20 0 60 80 100 0 1000 2000 3000 4000 TEMPERATURE (°C) LOAD CURRENT (mA) BATT VOLTAGE (V) OUTPUT V-I CHARACTERISTIC OUTPUT V-I CHARACTERISTIC (LINEAR SOURCE) (SWITCHING REGULATOR) 0.001 8 MAX1667 TOC10 MAX1667 TOC11 DROP IN BATT OUTPUT VOLTAGE (%) DROP IN BATT OUTPUT VOLTAGE (%) 7 0.01 6 5 0.1 I_{IOUT} (mA) 4 1.0 3 $V_{DCIN} = 20V$ 2 $V_{DCIN} = 20V$

-5

0 500 1000 1500 2000 2500 3000 3500 4000

CODE

LOAD CURRENT ERROR

0 2 4 6 8 10 12 14 16 18 20

ChargingVoltage() = 17,408mV ChargingCurrent() = 1 to 127mA

VIOUT (V)

 $V_{DCIN} = 20V$ $V_{BATT} = 12.75V$ MEASURED AT AVAILABLE ChargingCurrent() CODES

0

5

BATT CURRENT ERROR (%)

BATT CURRENT ERROR (%)

10

15

 θ

1

Typical Operating Characteristics (continued)

(Circuit of Figure 7, $T_A = +25^{\circ}C$, unless otherwise noted.)

0 2k 4k 6k 8k 10k 12k 14k 16k 18k 20k

ChargingVoltage() CODE

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-1.0

Pin Description

Figure 3. Typical Single Smart Battery System

Smart Battery Charging System

A smart battery charging system, at a minimum, consists of a smart battery and smart battery charger compatible with the Smart Battery System specifications using Intel's system management bus (SMBus).

Smart Battery System Block Diagrams

A system may use one or more smart batteries. The block diagram of a smart battery charging system shown in Figure 3 depicts a single battery system. This is typically found in notebook computers, video cameras, cellular phones, and other portable electronic equipment.

Another possibility is a system that uses two or more smart batteries. A block diagram for a system featuring multiple batteries is shown in Figure 4. The smart battery selector is used to connect batteries to either the smart battery charger or the system, or to disconnect them, as appropriate. For a standard smart battery, the following connections must be made: power (the battery's positive and negative terminals), SMBus (clock and data), and safety signal (resistance, typically temperature dependent). Additionally, the system host must be able to query any battery in the system so it can display the state of all batteries present in the system.

Figure 4 shows a two-battery system where Battery 2 is being charged while Battery 1 is powering the system. This configuration may be used to "condition" Battery 1, allowing it to be fully discharged prior to recharge.

Smart Battery Charger Types

Two types of smart battery chargers are defined: Level 2 and Level 3. All smart battery chargers communicate with the smart battery using the SMBus; the two types differ in their SMBus communication mode and in whether they modify the charging algorithm of the smart battery as shown in Table 1. Level 3 smart battery chargers are supersets of Level 2 chargers and as such support all Level 2 charger commands.

Figure 4. Typical Multiple Smart Battery System

Table 1. Charger Type by SMBus Mode and Charge Algorithm Source

Note: Level 1 smart battery chargers are defined in the version 0.95a specification. While they can correctly interpret smart battery end-of-charge messages minimizing overcharge, they do not provide truly chemistry-independent charging. They are no longer defined by the Smart Battery Charger specification and are explicitly not compliant with this and subsequent Smart Battery Charger specifications.

Level 2 Smart Battery Charger

The Level 2 or "smart-battery-controlled" smart battery charger interprets the smart battery's critical warning

messages, and operates as an SMBus slave device that responds to ChargingVoltage() and Charging-Current() messages sent to it by a smart battery. The charger is obliged to adjust its output characteristics in direct response to the messages it receives from the battery. In Level 2 charging, the smart battery is completely responsible for initiating communication and for providing the charging algorithm to the charger. The smart battery is in the best position to tell the smart battery charger how it needs to be charged. The charging algorithm in the battery may request a static charge condition or may choose to periodically adjust the smart battery charger's output to meet its present needs. A Level 2 smart battery charger is truly chemistry independent, and since it is defined as an SMBus slave device only, it is relatively inexpensive and easy to implement.

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Figure 5. Output V-I Characteristic

Detailed Description

Output Characteristics

The MAX1667 contains both a voltage-regulation loop and a current-regulation loop. Both loops operate independently of each other. The voltage-regulation loop monitors BATT to ensure that its voltage never exceeds the voltage set point (V0). The current-regulation loop monitors current delivered to BATT to ensure that it never exceeds the current-limit set point (I0). The current-regulation loop is in control as long as BATT voltage is below V0. When BATT voltage reaches V0, the current loop no longer regulates, and the voltage-regulation loop takes over. Figure 5 shows the V-I characteristic at the BATT pin.

Setting V0 and I0

Set the MAX1667's voltage and current-limit set points via the Intel SMBus 2-wire serial interface. The MAX1667's logic interprets the serial-data stream from the SMBus interface to set internal digital-to-analog converters (DACs) appropriately. The power-on-reset value for V0 and I0 is 18.4V and 7mA, respectively. See Digital Section for more information.

_____________________Analog Section

The MAX1667 analog section consists of a currentmode pulse-width-modulated (PWM) controller and two transconductance error amplifiers—one for regulating current and the other for regulating voltage. The device uses DACs to set the current and voltage level, which are controlled via the SMBus interface. Since separate amplifiers are used for voltage and current control, both

control loops can be compensated separately for optimum stability and response in each state.

Whether the MAX1667 is controlling the voltage or current at any time depends on the battery's state. If the battery has been discharged, the MAX1667's output reaches the current-regulation limit before the voltage limit, causing the system to regulate current. As the battery charges, the voltage rises until the voltage limit is reached, and the charger switches to regulating voltage. The transition from current to voltage regulation is done by the charger and need not be controlled by the host. Figure 6 shows the MAX1667 block diagram.

Voltage Control

The internal GMV amplifier controls the MAX1667's output voltage. The voltage at the amplifier's noninverting input is set by an 11-bit DAC, which is controlled by a ChargingVoltage() command on the SMBus (see Digital Section for more information). The battery voltage is fed to the GMV amplifier through a 5:1 resistive voltage divider. The set voltage ranges between 0 and 18.416V with 16mV resolution. This allows up to four Li+ cells in series to be charged.

The GMV amplifier's output is connected to the CCV pin, which compensates the voltage-regulation loop. Typically, a series-resistor/capacitor combination can be used to form a pole-zero doublet. The pole introduced rolls off the gain starting at low frequencies. The zero of the doublet provides sufficient AC gain at midfrequencies. The output capacitor then rolls off the midfrequency gain to below 1 to guarantee stability before encountering the zero introduced by the output capacitor's equivalent series resistance (ESR). The GMV amplifier's output is internally clamped to between onefourth and three-fourths of the voltage at REF.

Current Control

An internal 7mA linear current source is used in conjunction with the PWM regulator to set the battery charge current. When the current is set to 0, the voltage regulator is on but no current is available. A current setting between 1mA and 127mA turns on the linear current source, providing a maximum of 7mA for trickle charging. For current settings above 127mA, the linear current source is disabled and the charging current is provided by the switching regulator set by the 5-bit current-control DAC.

The GMI amplifier's noninverting input is driven by a 4:1 resistive voltage divider, which is driven by the 5-bit DAC. With the internal 4.096V reference, this input is approximately 1.0V at full scale, and the resolution is 31mV. The current-sense amplifier drives the inverting input to the GMI amplifier. It measures the voltage

Figure 6. Functional Diagram

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across the current-sense resistor (RSEN) (which is between the CS and BATT pins), amplifies it by approximately 5.45, and level shifts it to ground. The full-scale current is approximately 0.16V/RSEN, and the resolution is 5mV/R_{SEN}.

The current-regulation loop is compensated by adding a capacitor to the CCI pin. This capacitor sets the currentfeedback loop's dominant pole. The GMI amplifier's output is clamped to between approximately one-fourth and three-fourths of the REF voltage. While the current is in regulation, the CCV voltage is clamped to within 80mV of the CCI voltage. This prevents the battery voltage from overshooting when the DAC voltage setting is updated. The converse is true when the voltage is in regulation and the current is not at the current DAC setting. Since the linear range of CCI or CCV is about 1.5V to 3.5V (about 2V), the 80mV clamp results in a relatively negligible overshoot when the loop switches from voltage to current regulation or vice versa.

PWM Controller

The battery voltage or current is controlled by the current-mode, PWM, DC-DC converter controller. This controller drives two external N-channel MOSFETs, which switch the voltage from the input source. This switched voltage feeds an inductor, which filters the switched rectangular wave. The controller sets the pulse width of the switched voltage so that it supplies the desired voltage or current to the battery.

The heart of the PWM controller is the multi-input comparator. This comparator sums three input signals to determine the pulse width of the switched signal, setting the battery voltage or current. The three signals are the current-sense amplifier's output, the GMV or GMI error amplifier's output, and a slope-compensation signal, which ensures that the controller's internal currentcontrol loop is stable.

The PWM comparator compares the current-sense amplifier's output to the lower output voltage of either the GMV or the GMI amplifier (the error voltage). This current-mode feedback corrects the duty ratio of the switched voltage, regulating the peak battery current and keeping it proportional to the error voltage. Since the average battery current is nearly the same as the peak current, the controller acts as a transconductance amplifier, reducing the effect of the inductor on the output filter LC formed by the output inductor and the battery's parasitic capacitance. This makes stabilizing the circuit easy, since the output filter changes from a complex second-order RLC to a first-order RC. To preserve the inner current-control loop's stability, slope compensation is also fed into the comparator. This damps out perturbations in the pulse width at duty ratios greater than 50%.

At heavy loads, the PWM controller switches at a fixed frequency and modulates the duty cycle to control the battery voltage or current. At light loads, the DC current through the inductor is not sufficient to prevent the current from going negative through the synchronous rectifier (Figure 7, M2). The controller monitors the current through the sense resistor RSEN; when it drops to zero, the synchronous rectifier turns off to prevent negative current flow.

MOSFET Drivers

The MAX1667 drives external N-channel MOSFETs to regulate battery voltage or current. Since the high-side N-channel MOSFET's gate must be driven to a voltage higher than the input source voltage, a charge pump is used to generate such a voltage. The capacitor C7 (Figure 7) charges to approximately 5V through D2 when the synchronous rectifier turns on. Since one side of C7 is connected to the LX pin (the source of M1), the high-side driver (DHI) can drive the gate up to the voltage at BST (which is greater than the input voltage) when the high-side MOSFET turns on.

The synchronous rectifier may not be completely replaced by a diode because the BST capacitor charges while the synchronous rectifier is turned on. Without the synchronous rectifier, the BST capacitor may not fully charge, leaving the high-side MOSFET with insufficient gate drive to turn on. Use a small MOS-FET, such as a 2N7002, to guarantee that the BST capacitor is allowed to charge. In this case, most of the current at high currents is carried by the Schottky diode and not by the synchronous rectifier.

Internal Regulator and Reference

The MAX1667 uses an internal low-dropout linear regulator to create a 5.4V power supply (VL), which powers its internal circuitry. VL can supply up to 20mA, less than 10mA powers the internal circuitry, and the remaining current can power the external circuitry. The current used to drive the MOSFETs comes from this supply, which must be considered when calculating how much power can be drawn. To estimate the current required to drive the MOSFETs, multiply the total gate charge of each MOSFET by the switching frequency (typically 250kHz). To ensure VL stability, bypass the VL pin with a 1µF or greater capacitor.

The MAX1667 has an internal, accurate 4.096V reference voltage. This guarantees a voltage-setting accuracy of ±1% max. Bypass the reference with a 1µF or greater capacitor.

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Table 2a. Component Selection

Digital Section

SMBus Interface

R5, R6 \vert 33Ω ±5%, 1/16W

The MAX1667 uses serial data to control its operation. The serial interface complies with the SMBus specification (see System Management Bus Specification, from the SBS forum at www.sbs-Forum.org or from Intel Architecture Labs: 800-253-3696). Charger functionality complies with the Duracell/Intel Smart Charger Specification for a Level 2 charger.

The MAX1667 uses the SMBus Read-Word and Write-Word protocols to communicate with the battery it is charging, as well as with any host system that monitors the battery to charger communications. The MAX1667 acts only as a slave device and never initiates communication on the bus; it receives commands and responds to queries for status information. Figures 8a and 8b show the SMBus Write-Word and Read-Word protocols.

Each communication with the MAX1667 begins with the master issuing a START condition, which is a high-tolow transition on SDA while SCL is high (Figure 1).

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Table 2b. Component Suppliers

When the master has finished communicating with the slave, the master issues a STOP condition, which is a low-to-high transition on SDA while SCL is high. The bus is then free for another transmission. Figures 1 and 2 show timing diagrams for signals on the SMBus interface. The address byte, control byte, and data bytes are transmitted between the START and STOP conditions. Data is transmitted in 8-bit words, and after each byte either the slave or the master issues an acknowledgment (Figure 2); therefore, nine clock cycles are required to transfer each byte. The SDA state is allowed to change only while SCL is low, except for the START and STOP conditions.

The MAX1667 7-bit address is preset to 0b0001001. The eighth bit indicates a Write-Word (\overline{W} = 0) or a Read-Word $(R = 1)$ command. This can also be denoted by the hexadecimal number 0x12 for a Write-Word command or a 0x13 for a Read-Word command.

The following commands use the Write-Word protocol (Figure 8a): ChargerMode(), ChargingVoltage(), ChargingCurrent(), and AlarmWarning(). The ChargerStatus command uses the Read-Word protocol (Figure 8b).

ChargerMode() The ChargerMode() command uses Write-Word protocol (Figure 8a). The command code for ChargerMode() is 0x12 (0b00010010). Table 3 describes the functions of the 16 data bits (D0–D15). Bit 0 refers to the D0 bit in the

Whenever the BATTERY_PRESENT status bit (bit 14) of ChargerStatus() is clear, the HOT_STOP bit is set, regardless of any previous ChargerMode() command.

To charge a battery that has a thermistor impedance in the HOT range (i.e., THERMISTOR_HOT = 1 and THERMISTOR_UR = 0), the host must use the ChargerMode() command to clear HOT_STOP **after** the battery is inserted. The HOT_STOP bit returns to its default power-up condition ('1') whenever the battery is removed.

ChargingVoltage()

The ChargingVoltage() command uses Write-Word protocol (Figure 8a). The command code for ChargingVoltage() is 0x15 (0b00010101). The 16-bit binary number formed by D15–D0 represents the voltage set point (V0) in millivolts; however, since the MAX1667 has only 16mV of resolution in setting V0, the D0, D1, D2, and D3 bits are ignored.

The maximum voltage delivered by the MAX1667 is 18.416V, corresponding to a ChargingVoltage() value of 0x47F0. This is also the floating voltage set by the power-on reset (POR). ChargingVoltage() values above 0x47F0 deliver the floating voltage and set the VOLT-AGE_OR status bit. Any time the BATTERY_PRESENT status bit is clear, the ChargingVoltage() register returns to its POR state.

Figure 9 shows the mapping between V0 (the voltageregulation-loop set point) and the ChargingVoltage() data.

ChargingCurrent()

The ChargingCurrent() command uses Write-Word protocol (Figure 8a). The command code for ChargingCurrent() is 0x14 (0b00010100). The 16-bit binary number formed by D15–D0 represents the current-limit set point (I0) in milliamps (Table 4). Connecting SEL to AGND selects a 0.896A maximum setting for I0. Leaving SEL open selects a 2.944A maximum setting for I0. Connecting SEL to VL selects a 3.968A maximum setting for I0.

Two sources of current in the MAX1667 charge the battery: a linear current source begins from IOUT, and a switching regulator controls the current flowing through the current-sense resistor (R1). IOUT provides a tricklecharge current to compensate for battery self-discharge, while the switching regulator provides large currents for fast charging.

IOUT sources 7mA, while the switching regulator sources from 128mA to 3968mA with a 5-bit resolution (LSB = 5.12 mV / RSENSE = 128mA with a 40m Ω sense resistor). In Table 4, DA4–DA0 denotes the bits in the current DAC code. Table 5 shows the relationship between the value programmed with the Charging-Current() command and IOUT source current. The CCV_LOW comparator checks to see if the output volt-

/VI /I XI /VI

Write-Word protocol.

Table 3. ChargerMode() Bit Functions

*Bit position in the D15–D0 data. **Power-on reset value.

N/A = Not applicable

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age is too high by comparing CCV to REF/4. If $CCV_LOW = 1$ (when $CCV < REF/4$), IOUT shuts off. This prevents the output voltage from exceeding the voltage set point specified by the ChargingVoltage() register. VOLTAGE_NOTREG = 1 whenever the internal clamp pulls down on CCV. (The internal clamp pulls down on CCV to keep its voltage close to CCI's voltage.)

With the switching regulator on, the current through R1 (Figure 7) is regulated by sensing the average voltage between CS and BATT. Figure 10 shows the relationship between the ChargingCurrent() data and the average voltage between CS and BATT.

When the switching regulator is off, DHI is forced to LX and DLO is forced to ground. This prevents current from flowing through inductor L1. Table 6 shows the relationship between the ChargingCurrent() register value and the switching regulator current DAC code (DA4–DA0).

To ensure that the actual output current matches the data value programmed with the ChargingCurrent() command, R1 should be as close as possible to 40mΩ. The SEL pin setting affects the full-scale current but not the step size. ChargingCurrent() values above the fullscale setting set the CURRENT_OR status bit. Note that whenever any current DAC bits are set, the linear-current source is turned off.

The power-on reset value for the ChargingCurrent() register is 0x0007. Any time the BATTERY_PRESENT status bit is clear (battery removed), the ChargingCurrent() register returns to its power-on reset state. This ensures that upon insertion of a battery, the initial charging current is 7mA.

AlarmWarning()

The AlarmWarning() command uses Write-Word protocol (Figure 8a). The command code for AlarmWarning() is 0x16 (0b00010110). The AlarmWarning() command sets the ALARM_INHIBITED status bit. The MAX1667 responds to the following alarms: OVER_CHARGED_ALARM (D15), TERMINATE_CHARGE_ALARM (D14), and OVER_TEMP_ ALARM (D12). Table 7 summarizes the AlarmWarning() command's function. The ALARM_INHIBITED status bit remains set until BATTERY_PRESENT = 0 (battery removed), a ChargerMode() command is written with the POR_RESET bit set, or a new ChargingVoltage() or ChargingCurrent() is written.

Figure 8. SMBus a) Write-Word and b) Read-Word Protocols

ChargerStatus()

The ChargerStatus() command uses Read-Word protocol (Figure 8b). The command code for ChargerStatus() is 0x13 (0b00010011). The ChargerStatus() command returns information about thermistor impedance and the MAX1667's internal state. The Read-Word protocol returns D15–D0. Table 8 describes the meaning of the individual bits. The latched bits, THERMISTOR_HOT and ALARM_INHIBITED, are cleared whenever BAT-TERY_PRESENT = 0 or ChargerMode() is written with POR _{RESET} = 1.

Interrupts and the Alert-Response Address

An interrupt is triggered (INT goes low) whenever power is applied to DCIN, the BATTERY_PRESENT bit changes, or the POWER_FAIL bit changes. BATTERY_PRESENT and POWER_FAIL have interrupt masks that can be set or cleared via the ChargerMode() command. INT stays low until the interrupt is cleared. There are two methods for clearing the interrupt: issuing a ChargerStatus() command, and using a modified Receive Byte protocol with a 0x19 (0b0011001) Alert-Response address. The MAX1667 responds to the Alert-Response address with its address (0x13) left justified as the most significant bits of the returned byte.

__________Applications Information

Negative Input Voltage Protection

In most portable equipment, the DC power to charge batteries enters through a two-conductor cylindrical power jack. It is easy for the end user to add an adapter to switch the DC power's polarity. Polarized capacitor C6 would be destroyed if a negative voltage were applied. Diode D4 in Figure 7 prevents this from happening.

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Figure 10. Average Voltage Between CS and BATT vs. Code Figure 11. Typical Thermistor Characteristics

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Table 4. ChargingCurrent() Bit Functions

When $SEL = VL$, values above 0x0F80 set the output current to 3.968A.

When SEL = OPEN, values above 0x0B80 set the output current to 2.944A.

When SEL = GND, values above 0x0380 set the output current to 0.896A.

** Values below 0x0080 set the output current to 7mA.

Table 5. Relationship Between IOUT Source Current and ChargingCurrent() Value

Note 1: THERMISTOR_HOT and HOT_STOP and NOT (THERMISTOR_UR).

If reverse-polarity protection for the DC input power is not necessary, diode D4 can be omitted. This eliminates the power lost due to the voltage drop on diode D4.

Thermistor Characterization

Figure 11 represents the expected electrical behavior of a 103ETB-type thermistor (nominally 10kΩ at +25°C ±5% or better) to be used with the MAX1667. The graph is typical of the suggested thermistor's characteristics.

THERMISTOR_OR bit is set only when the thermistor value is > 100kΩ. This indicates that the thermistor is open.

THERMISTOR_COLD bit is set only when the thermistor value is > 30kΩ. The thermistor indicates a cold battery.

THERMISTOR_HOT bit is set only when the thermistor value is $<$ 3kΩ.

THERMISTOR_UR bit is set only when the thermistor value is $<$ 500 $Ω$.

Multiple bits may be set depending on the values of the thermistor (e.g., a 450Ω thermistor will cause both the THERMISTOR_HOT and the THERMISTOR_UR bits to be set). The thermistor may be replaced by fixed-value resistors in battery packs that do not require the thermistor as a secondary fail-safe indicator. In this case, it is the responsibility of the battery pack to manipulate the resistance to obtain correct charger behavior.

Table 6. Relationship Between Current DAC Code and the ChargingCurrent() Value

Note 1: THERMISTOR_HOT and HOT_STOP and NOT (THERMISTOR_UR).

Table 7. Effect of the AlarmWarning() Command

Table 8. ChargerStatus() Bit Descriptions

*Bit position in the D15–D0 data

N/A = Not applicable

Figure 12. Kelvin Connections for the Current-Sense Resistors

PC Board Layout Considerations

Good PC board layout is required to achieve specified noise, efficiency, and stable performance. The PC board layout artist must be given explicit instructions, preferably a pencil sketch showing the placement of power-switching components and high-current routing. Refer to the PC board layout in the MAX1667 evaluation kit manual for examples. A ground plane is essential for optimum performance. In most applications, the circuit will be located on a multilayer board, and full use of the four or more copper layers is recommended. Use the top layer for high-current connections, the bottom layer for quiet connections (REF, CCV, CCI, DACV, GND), and the inner layers for an uninterrupted ground plane. Use the following step-by-step guide:

- 1) Place the high-power components (C1, C6, M1, M2, D1, L1, and R1) first, with their grounds adjacent:
	- Minimize current-sense resistor trace lengths and ensure accurate current sensing with Kelvin connections (Figure 12).
	- Minimize ground trace lengths in the high-current paths.
	- Minimize other trace lengths in the high-current paths:
		- Use > 5mm-wide traces.
		- Connect CIN to high-side MOSFET drain: 10mm max length.
		- Connect rectifier diode cathode to low side.
		- MOSFET: 5mm max length.
		- LX node (MOSFETs, rectifier cathode, inductor): 15mm max length.

Ideally, surface-mount power components are butted up to one another with their ground terminals almost touching. These high-current grounds are then connected to each other with a wide, filled zone of top-layer copper so they do not go through vias. The resulting top-layer subground plane is connected to the normal inner-layer ground plane at the output ground terminals, which ensures that the IC's analog ground is sensing at the supply's output terminals without interference from IR drops and ground noise. Other high-current paths should also be minimized, but focusing primarily on short ground and current-sense connections eliminates about 90% of all PC board layout problems.

- 2) Place the IC and signal components. Keep the main switching nodes (LX nodes) away from sensitive analog components (current-sense traces and REF capacitor). Place the IC and analog components on the opposite side of the board from the powerswitching node. **Important**: The IC must be no further than 10mm from the current-sense resistors. Keep the gate-drive traces (DH, DL, and BST) shorter than 20mm and route them away from CSH, CSL, and REF. Place ceramic bypass capacitors close to the IC. The bulk capacitors can be placed further away.
- 3) Use a single-point star ground where the input ground trace, power ground (subground plane), and normal ground plane meet at the supply's output ground terminal. Connect both IC ground pins and all IC bypass capacitors to the normal ground plane.

Upgrading from MAX1647 to MAX1667 The MAX1667 is a pin- and software-compatible upgrade to the MAX1647, with the following functional differences:

- 1) The PWM duty cycle has been extended to 97%.
- 2) The internal reference has been changed to +4.096V with 1% accuracy over line, load, and temperature.
- 3) The internal voltage DAC has been changed to allow a program voltage of 18,416mV. Up to four Li+ cells can be charged.
- 4) The linear current source (IOUT) has been reduced to 7mA and turns off when the switching regulator is on.
- 5) An internal diode has been added to the IOUT pin to prevent reverse current from BATT when the DC source is removed.
- 6) The internal current DAC was changed from 6-bit to 5-bit resolution.

- 7) The SEL pin digitally limits the output current to 4A, 3A, or 1A without a change in sense resistor value between the three modes.
- 8) The single count current-sense voltage has been changed to 5mV. R1 required is now 40mΩ.
- 9) After the AlarmWarning() message, the charger is not locked off. Subsequent ChargingVoltage() or ChargingCurrent() commands allow the MAX1667 to resume the charge.
- 10) The Alert-Response address is 0x13 (0b00010011).

When upgrading a MAX1647 design, follow these recommended or required changes (part numbers refer to Figure 3 of the MAX1647 data sheet):

- 1) Change R1 to 40mΩ (required).
- 2) Remove diodes D5 and D6, transistor Q1, and resistor R6. Connect IOUT directly to BATT (recommended).
- 3) Remove the external +4.096V reference (recommended).
- 4) Remove D6 (recommended). When doing this, also place a small-signal diode in series with R7 and connect it directly to the DC source (see D3 and R5 on Figure 3 of the MAX1647 data sheet).

Pin Configuration

MAX1667

MAX1667

Chip Information

TRANSISTOR COUNT: 6378 SUBSTRATE CONNECTED TO AGND

Package Information

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)

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MAX1667

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