HCPL-4562 and HCNW4562

High Bandwidth, Analog/Video Optocouplers

Data Sheet

Description

The HCPL-4562 and HCNW4562 optocouplers provide wide-bandwidth isolation for analog signals. They are ideal for video isolation when combined with their application circuit ([Figure 4](#page-9-0)). High linearity and low phase shift are achieved through an AlGaAs LED combined with a high-speed detector. These single-channel optocouplers are available in 8-pin DIP and wide-body package configurations.

Functional Diagram

Applications

- Video isolation for the following standards/formats: NTSC, PAL, SECAM, S-VHS, ANALOG RGB
- **Low drive current feedback element in switching power** supplies (for ISDN networks, as an example)
- A/D converter signal isolation
- Analog signal ground isolation
- High-voltage insulation

Features

- Wide bandwidth $[1]$:
	- **—** 17 MHz (HCPL-4562)
	- **—** 9 MHz (HCNW4562)
- High voltage gain^[1]:
	- **—** 2.0 (HCPL-4562)
	- **—** 3.0 (HCNW4562)
- Low GV temperature coefficient: –0.3 %/°C
- Highly linear at low drive currents
- High-speed AlGaAs emitter
- Safety approval:
	- UL Recognized: 3750V_{RMS} for 1 minute (5000V_{RMS} for 1 minute for HCPL-4562#020 and HCNW4562) per UL 1577
	- **—** CSA Approved
	- **IEC/EN/DIN EN 60747-5-5 Approved: V_{IORM} =** 1414V_{peak} for HCNW4562
- Available in 8-pin DIP and wide-body packages
- **CAUTION** It is advised that normal static precautions be taken in the handling and assembly of this component to prevent damage and/or degradation which may be induced by ESD. The components featured in this data sheet are not to be used in military or aerospace applications or environments.

Selection Guide

Ordering Information

HCPL-4562 is UL Recognized with 3750V_{RMS} for 1 minute per UL1577 unless otherwise specified. HCNW4562 is UL Recognized with 5000V_{RMS} for 1 minute per UL1577.

a. IEC/EN/DIN EN 60747-5-5 $V_{IORM} = 630V_{peak}$ Safety Approval.

b. IEC/EN/DIN EN 60747-5-5 $V_{\text{IORM}} = 1414V_{\text{peak}}$ Safety Approval.

To order, choose a part number from the part number column and combine with the desired option from the option column to form an order entry.

Example 1:

HCPL-4562-520E to order product of Gull Wing Surface Mount package in Tape and Reel packaging with UL 5000V_{RMS}/1 minute rating and RoHS compliant.

Example 2:

HCNW4562 to order product of 8-Pin Wide-body DIP package in Tube packaging with IEC/EN/DIN EN 60747-5-5 V_{IORM} = 1414V_{peak} Safety Approval and UL 5000V_{RMS}/1 minute rating and non RoHS compliant.

Option data sheets are available. Contact your Broadcom sales representative or authorized distributor for information.

Remarks: The notation '#XXX' is used for existing products, while (new) products launched since July 15, 2001 and RoHS compliant will use '–XXXE.'

Package Outline Drawings

8-Pin DIP Package (HCPL-4562)

NOTE: FLOATING LEAD PROTRUSION IS 0.25 mm (10 mils) MAX.

8-Pin DIP Package with Gull Wing Surface Mount Option 300 (HCPL-4562)

NOTE: FLOATING LEAD PROTRUSION IS 0.25 mm (10 mils) MAX.

8-Pin Wide-Body DIP Package (HCNW4562)

8-Pin Wide-Body DIP Package with Gull Wing Surface Mount Option 300 (HCNW4562)

Schematic

Reflow Soldering Profile

The recommended reflow soldering conditions are per JEDEC Standard J-STD-020 (latest revision). Non-halide flux should be used.

Regulatory Information

The devices contained in this data sheet have been approved by the following organizations:

- IEC/EN/DIN EN 60747-5-5:
- UL: Recognized under UL 1577, Component Recognition Program, File E55361.
- CSA: Approval under CSA Component Acceptance Notice #5, File CA 88324.

Insulation and Safety Related Specifications

Option 300: surface-mount classification is Class A in accordance with CECC 00802.

IEC/EN/DIN EN 60747-5-5 Insulation Characteristics

a. Refer to the front of the optocoupler section of the current catalog, under Product Safety Regulations section IEC/EN/DIN EN 60747-5-5, for a detailed description.

NOTE These optocouplers are suitable for "safe electrical isolation" only within the safety limit data. Maintenance of the safety limit data shall be ensured by means of protective circuits.

Absolute Maximum Ratings

Recommended Operating Conditions

Electrical Specifications (DC)

T_A = 25°C, I_F = 6 mA for HCPL-4562 and I_F = 10 mA for HCNW4562 (meaning Recommended IFQ) unless otherwise specified.

Small Signal Characteristics (AC)

 $\sf T_A$ = 25°C, I_F = 6 mA for HCPL-4562 and I_F = 10 mA for HCNW4562 (i.e., Recommended I_{FO}) unless otherwise specified.

a. The Input-Output Momentary Withstand Voltage is a dielectric voltage rating that should not be interpreted as an input-output continuous voltage rating. For the continuous voltage rating refer to the VDE 0884 Insulation Related Characteristics Table (if applicable), your equipment level safety specification or Avago Application Note 1074 entitled "Optocoupler Input-Output Endurance Voltage," publication number 5963-2203E.

Notes:

1. When used in the circuit of <mark>Figure 1 or [Figure 4;](#page-9-0) G_V = V_{OUT}/V_{IN}; I_{FQ} = 6 mA (HCPL-4562), I_{FQ} = 10 mA (HCNW4562).</mark>

- 2. Derate linearly above 70°C free-air temperature at a rate of 2.0 mW/°C (HCPL-4562).
- 3. Maximum variation from the best fit line of l_{PB} vs. I_F expressed as a percentage of the peak-to-peak full scale output.
- 4. Current transfer ratio (CTR) is defined as the ratio of output collector current, I_O, to the forward LED input current, I_F, times 100%.
- 5. Device considered a two-terminal device: Pins 1, 2, 3, and 4 shorted together and Pins 5, 6, 7, and 8 shorted together.
- 6. Flat-band, small-signal voltage gain.
- 7. The frequency at which the gain is 3 dB below the flat-band gain.
- 8. Differential gain is the change in the small-signal gain of the optocoupler at 3.58 MHz as the bias level is varied over a given range.
- 9. Differential phase is the change in the small-signal phase response of the optocoupler at 3.58 MHz as the bias level is varied over a given range.
- 10. Total harmonic distortion (THD) is defined as the square root of the sum of the square of each harmonic distortion component. The THD of the isolated video circuit is measured using a 2.6 kΩ load in series with the 50Ω input impedance of the spectrum analyzer.
- 11. Isolation mode rejection ratio (IMRR), a measure of the optocoupler's ability to reject signals or noise that may exist between input and output terminals, is defined by 20 log_{10} [(V_{OUT}/V_{IN})/(V_{OUT}/V_{IM})], where V_{IM} is the isolation mode voltage signal.
- 12. In accordance with UL 1577, each optocoupler is proof-tested by applying an insulation test voltage ≥4500V_{RMS} for 1 second (leakage detection current limit, I_{I-O} ≤5 μA). This test is performed before the 100% Production test shown in the IEC/EN/DIN EN 60747-5-5 Insulation Related Characteristics Table, if applicable.
- 13. In accordance with UL 1577, each optocoupler is proof tested by applying an insulation test voltage ≥6000V_{RMS} for 1 second (leakage detection current limit, I_{I-O} ≤5 μA). This test is performed before the 100% Production test shown in the IEC/EN/DIN EN 60747-5-5 Insulation Related Characteristics Table, if applicable.

Figure 1 Gain and Bandwidth Test Circuit

NOTE: ALL RESISTORS ARE 1% TOLERANCE

Figure 2 Base Photo Current Test Circuit Figure 3 Base Photo Current Frequency Response Test Circuit

Figure 4 Recommended Isolated Video Interface Circuit

Figure 9 Small-Signal Response vs. Input Current (HCPL-4562) Figure 10 Small-Signal Response vs. Input Current (HCNW4562)

Figure 5 Input Current vs. Forward Voltage (HCPL-4562) Figure 6 Input Current vs. Forward Voltage (HCNW4562)

Figure 7 Base Photo Current vs. Input Current (HCPL-4562) Figure 8 Base Photo Current vs. Input Current (HCNW4562)

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Figure 15 Base Photo Current Variation vs. Bias Conditions (HCPL-4562)

Figure 11 Current Transfer Ratio vs. Temperature (HCPL-4562) Figure 12 Current Transfer Ratio vs. Temperature (HCNW4562)

Figure 16 Base Photo Current variation vs. Bias Conditions (HCNW4562)

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Figure 19 Normalized Base Photo Current vs. Frequency (HCPL-4562)

Figure 17 Normalized Voltage Gain vs. Frequency (HCPL-4562) Figure 18 Normalized Voltage Gain vs. Frequency (HCNW4562)

Figure 20 Normalized Base Photo Current vs. Frequency (HCNW4562)

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Figure 23 Isolation Mode Rejection Ratio vs. Frequency (HCPL-4562)

Figure 25 DC Output Voltage vs. Transistor Current Gain (HCPL-4562)

Figure 27 Output Buffer Stage for Low-Impedance Loads Figure 28 Thermal Derating Curve (Dependence of Safety Limiting

Figure 24 Isolation Mode Rejection Ratio vs. Frequency (HCNW4562)

Figure 26 DC Output Voltage vs. Transistor Current Gain (HCNW4562)

h_{FE} - TRANSISTOR CURRENT GAIN

Value with Case Temperature per IEC/EN/DIN EN 60747-5-5)

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Conversion from HCPL4562 to HCNW4562

In order to obtain similar circuit performance when converting from the HCPL-4562 to the HCNW4562, it is recommended to increase the Quiescent Input Current, I_{FO} , from 6 mA to 10 mA. If the application circuit in [Figure 4](#page-9-0) is used, then potentiometer R_4 should be adjusted appropriately.

Design Considerations of the Application Circuit

The application circuit in [Figure 4](#page-9-0) incorporates several features that help maximize the bandwidth performance of the HCPL-4562/HCNW4562. Most important of these features is peaked response of the detector circuit that helps extend the frequency range over which the voltage gain is relatively constant. The number of gain stages, the overall circuit topology, and the choice of DC bias points are all consequences of the desire to maximize bandwidth performance.

To use the circuit, first select R₁ to set V_E for the desired LED quiescent current by:

$$
I_{FQ} = \frac{V_E}{R_4} \gg \frac{G_V V_E R_{10}}{(\frac{I_{PB}}{I_E}) R_7 R_9}
$$
 (1)

For a constant value V_{INp-p} , the circuit topology (adjusting the gain with R_4) preserves linearity by keeping the modulation factor (MF) dependent only on V_E.

$$
i_{F_{p-p}} \gg V_{IN}/R_4 \tag{2}
$$

$$
\frac{i_{F_{|P\supset P}}}{I_{FQ}} \gg \frac{i_{PB_{|P\supset P}}}{I_{PBQ}} = \frac{V_{|N_{|P\supset P}}}{V_{E}}
$$
(3)

Modulation:

Factor (MF):
$$
\frac{i_{F_{1(p-p)}}}{21_{FQ}} = \frac{V_{1N_{p-p}}}{2V_{E}}
$$
 (4)

For a given G_V, V_E, and V_{CC}, DC output voltage will vary only with hFEX.:

$$
V_{\rm O} = V_{\rm CC} - V_{\rm BE_4} - \frac{R_9}{R_{10}} [V_{\rm BEX} - (I_{\rm PBQ} - I_{\rm BXQ}) R_7] \tag{5}
$$

Where:

$$
I_{PBQ} \propto \frac{G_V V_E R_{10}}{R_7 R_9}
$$
 (6)

and,

$$
I_{\rm BXQ} \propto \frac{V_{\rm CC} - 2 V_{\rm BE}}{R_6 h_{\rm FEX}} \tag{7}
$$

[Figure 25](#page-13-0) and [Figure 26](#page-13-1) shows the dependency of the DC output voltage on h_{FFX} .

For $9V < V_{CC}$ < 12V, select the value of R₁₁ such that:

$$
I_{C_{Q4}} \gg \frac{V_0}{R_{11}} \frac{4.25V}{470} \quad 9.0 \text{ mA}
$$
 (8)

The voltage gain of the second state (Q₃) is approximately equal to:

$$
\frac{R_9}{R_{10}} * \frac{1}{1 + s R_9 \left[C_{CQ_3} + \frac{1}{2 R_{11} f_{T_4}} \right]}
$$
(9)

Increasing R'_{11} (R'₁₁ includes the parallel combination of R₁₁ and the load impedance) or reducing R₉ (keeping R₉/R₁₀ ratio constant) will improve the bandwidth.

If it is necessary to drive a low-impedance load, bandwidth may also be preserved by adding an additional emitter following the buffer stage (Q₅ in [Figure 16](#page-11-5)), in which case R₁₁ can be increased to set $I_{CO4} \approx 2$ mA.

Finally, adjust R_4 to achieve the desired voltage gain:

$$
G_V \gg \frac{V_{OUT}}{V_{IN}} \gg \frac{I_{PB}}{I_F} \left[\frac{R_7 R_9}{R_4 R_{10}} \right]
$$
 (10)

where typically $\frac{I_{PB}}{I}$ $\frac{P_{\text{p}}}{I_{\text{F}}}$ = 0.0032

Definitions:

- \blacksquare G_V = Voltage Gain
- I_{FO} = Quiescent LED forward current
- i_{Fp-p} = Peak-to-peak small-signal LED forward current
- V_{1Np-p} = Peak-to-peak small-signal input voltage
- i_{PBD-D} = Peak-to-peak small-signal base photo current
- $I_{PBO} =$ Quiescent base photo current
- V_{BFX} = Base-Emitter voltage of HCPL-4562/HCNW4562 transistor
- I_{BXO} = Quiescent base current of HCPL-4562/HCNW4562 transistor
- h_{FEX} = Current Gain (I_C/I_B) of HCPL-4562/HCNW4562 transistor
- \blacksquare \blacksquare $\sf V_{\sf E}$ = Voltage across emitter degeneration resistor R₄
- f_{T4} = Unity gain frequency of Q₅
- \blacksquare C_{CQ3} = Effective capacitance from collector of Q₃ to ground

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