

LITIX™ Power H-Bridge DC-DC controller

Features

- Single inductor high power buck-boost controller
- Switching frequency range from 200 kHz to 700 kHz
- Maximum efficiency in every condition (up to 96%)
- Constant current (LED) and constant voltage regulation
- EMC optimized device: spread spectrum always activated
- Overvoltage, shorted LED fault and overtemperature diagnostic output
- Enhanced dimming features: Analog and PWM dimming (from digital input or sourced by embedded PWM engine)
- LED current accuracy $\pm 3\%$



Potential applications

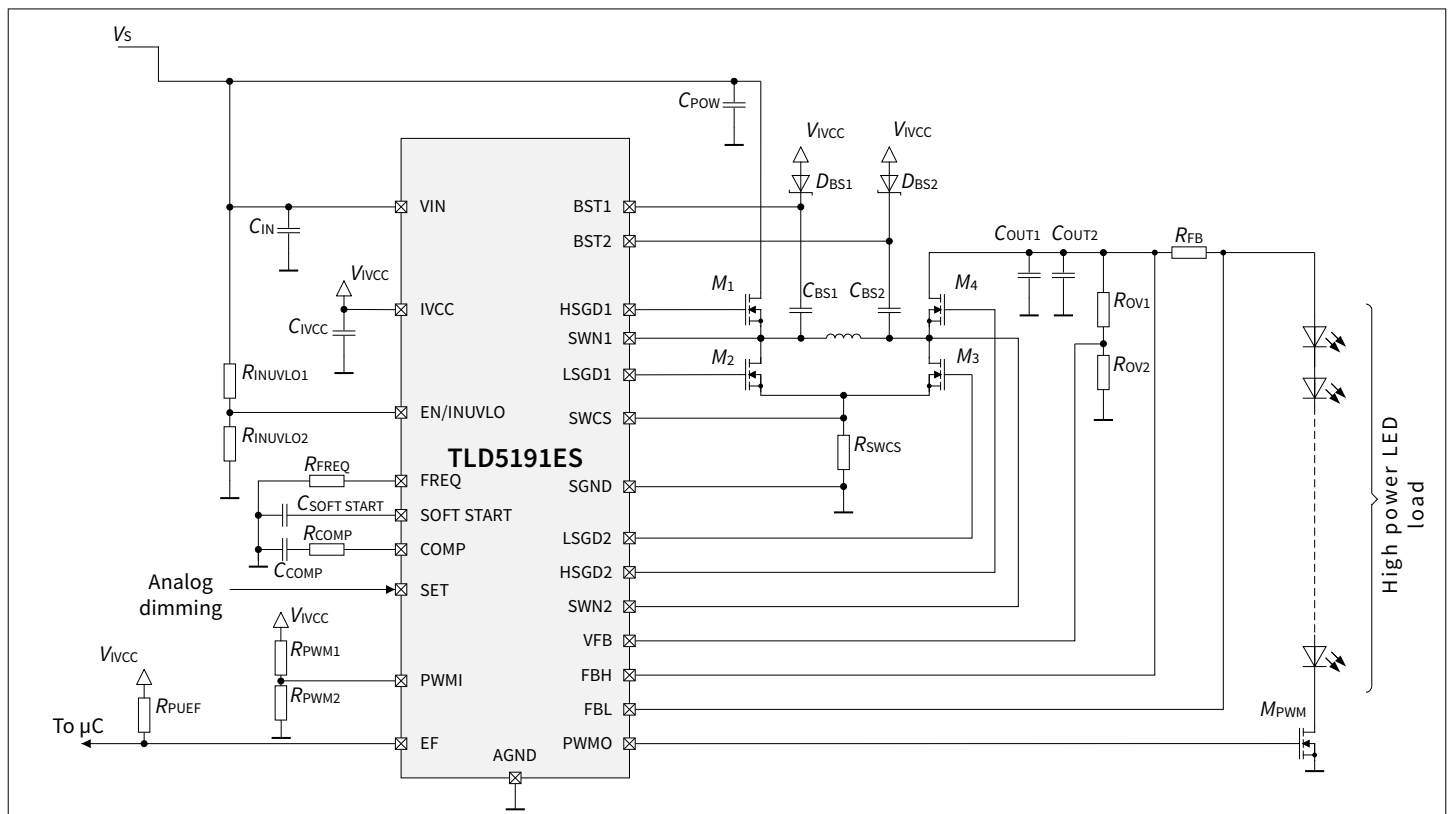
- Especially designed for driving high power LEDs in automotive applications
- Automotive exterior lighting: full LED headlamp assemblies (low beam, high beam, matrix beam, pixel light)
- Voltage pre-regulator for rear lamp assemblies
- General purpose DC-DC for constant current or constant voltage applications

Product validation

Product validation according to AEC-Q100, Grade1. Qualified for automotive applications.

Description

The TLD5191ES is a synchronous MOSFET H-Bridge DC-DC controller with built-in protection features. This concept is beneficial for driving high power LEDs with maximum system efficiency and minimum number of external components. The TLD5191ES offers analog and digital (PWM) dimming and embedded PWM engine. The switching frequency is adjustable in the range of 200 kHz to 700 kHz. A built-in spread spectrum switching frequency modulation and the forced continuous current regulation mode improve the overall EMC behavior. Furthermore the current mode regulation scheme provides a stable regulation loop maintained by small external compensation components. The adjustable soft start feature limits the current peak as well as voltage overshoot at start-up. The TLD5191ES is suitable for use in the automotive environment.



Description

Parameter	Symbol	Values
Power stage input voltage range	V_{POW}	4.5 V ... 55 V
Device input supply voltage range	V_{VIN}	4.5 V ... 40 V
Maximum output voltage (depending on the application conditions)	$V_{OUT(max)}$	55 V as LED driver boost mode 50 V as LED driver buck mode 50 V as voltage regulator
Switching frequency range	f_{SW}	200 kHz ... 700 kHz
Typical H-Bridge NMOS driver on-state resistance at $T_J = 25^\circ\text{C}$ (Gate pull-up)	$R_{DS(ON_PU)}$	2.3 Ω
Typical H-Bridge NMOS driver on-state resistance at $T_J = 25^\circ\text{C}$ (Gate pull-down)	$R_{DS(ON_PD)}$	1.2 Ω

Protective functions

- Overload protection of external MOSFETs
- Shorted load, output overvoltage protection
- Input undervoltage protection
- Thermal shutdown of device with autorestart behavior
- Electrostatic discharge protection (ESD)

Diagnostic functions

Diagnostic information via error flag: device overtemperature shutdown, output short to GND, output overvoltage

Type	Package	Marking
TLD5191ES	PG-TSDSO-24	TLD5191ES

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1 Block diagram

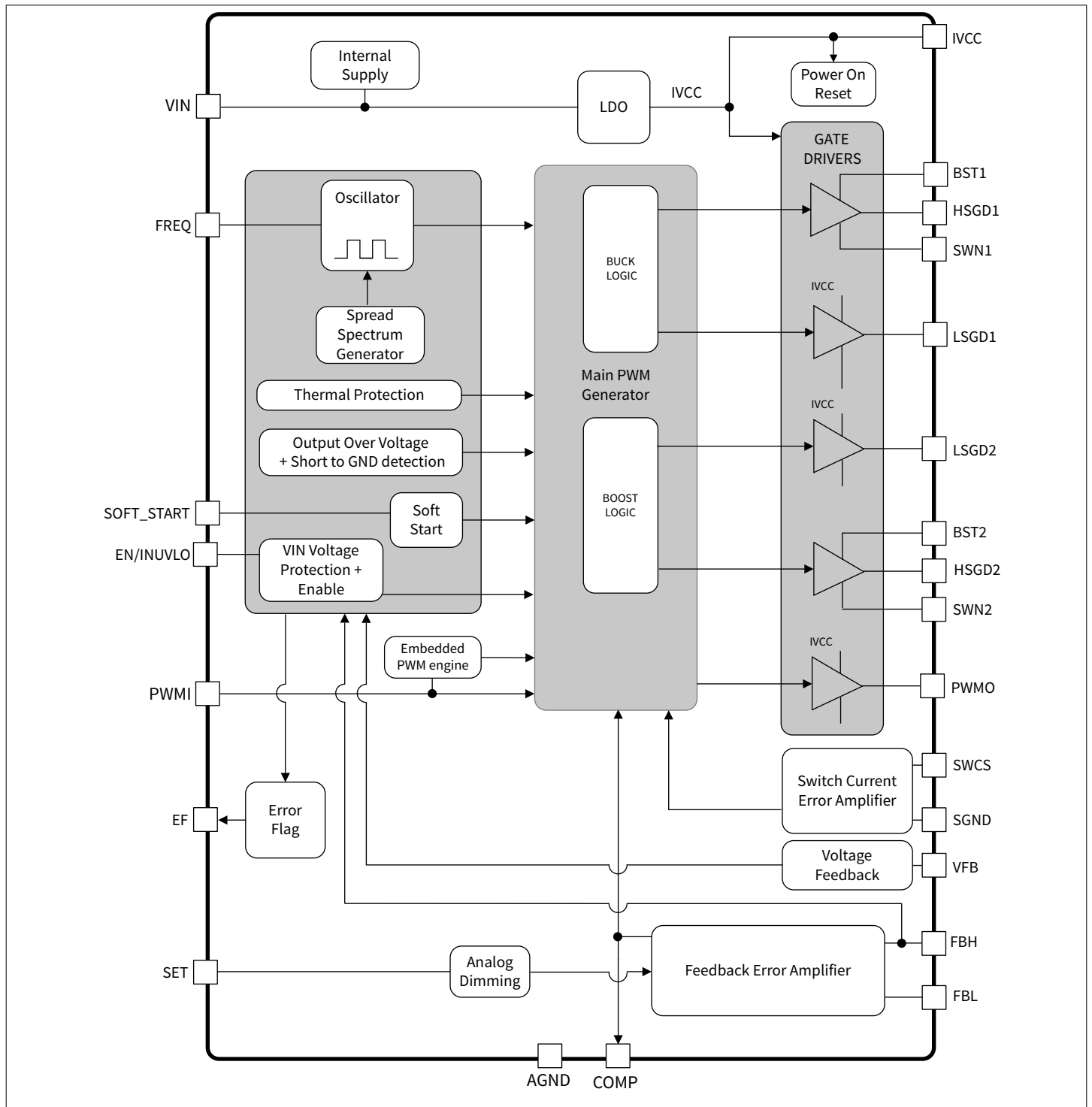


Figure 1 Block diagram TLD5191ES

2 Pin configuration

2.1 Pin assignment

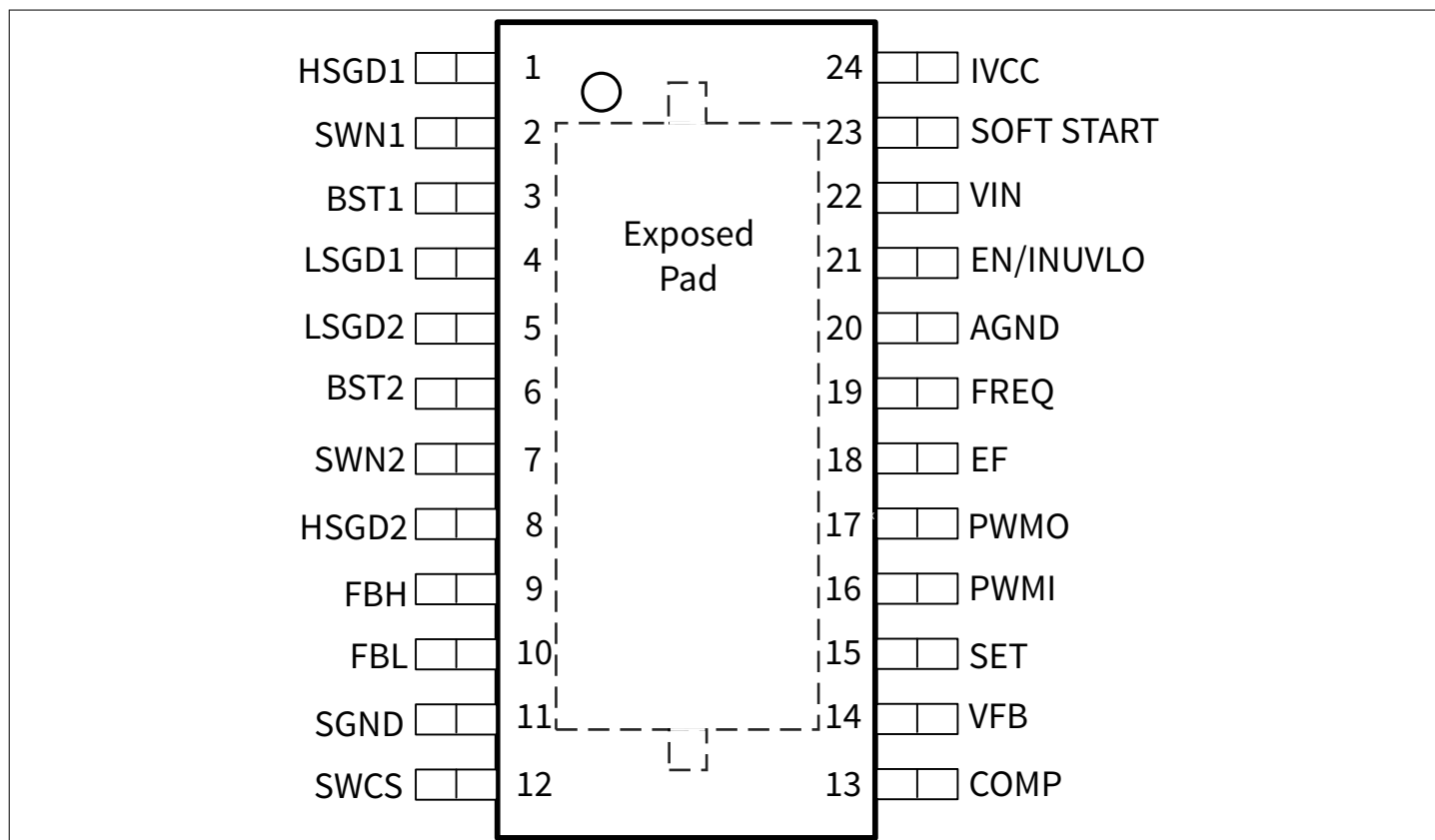


Figure 2 Pin configuration PG-TSDSO-24

2.2 Pin definitions and functions

Table 1 Pin definitions and functions

Pin	Symbol	I/O ¹⁾	Function
22	VIN	-	Power supply voltage Supply for internal biasing
20	AGND	-	Analog ground Ground reference
-	EP	-	Exposed pad Connect to external heatspreading Cu area (e.g. inner GND layer of multilayer PCB with thermal vias)
1	HSGD1	O	High-side gate driver output 1 Drives the top n-channel MOSFET with a voltage equal to V_{IVCC} superimposed on the switch node voltage SWN1. Connect to gate of external switching MOSFET

(table continues...)

Table 1 (continued) Pin definitions and functions

Pin	Symbol	I/O ¹⁾	Function
8	HSGD2	O	High-side gate driver output 2 Drives the top n-channel MOSFET with a voltage equal to V_{IVCC} superimposed on the switch node voltage SWN2. Connect to gate of external switching MOSFET
4	LSGD1	O	Low-side gate driver output 1 Drives the low-side n-channel MOSFET between GND and V_{IVCC} . Connect to gate of external switching MOSFET
5	LSGD2	O	Low-side gate driver output 2 Drives the low-side n-channel MOSFET between GND and V_{IVCC} . Connect to gate of external switching MOSFET
2	SWN1	IO	Switch node 1 SWN1 pin swings from a diode voltage drop below ground up to V_{IN}
7	SWN2	IO	Switch node 2 SWN2 pin swings from ground up to a diode voltage drop above V_{OUT}
24	IVCC	O	Internal LDO output Used for internal biasing and gate driver supply. Bypass with external capacitor close to the pin. Pin must not be left open
21	EN/INUVLO	I, PD	Enable/Input undervoltage lockout Used to put the device in a low current consumption mode, with additional capability to fix an undervoltage threshold via external components. Pin must not be left open
19	FREQ	I	Frequency select input Connect external resistor to GND to set frequency
16	PWMI	I, PD	PWM Control input Used to control the digital dimming via external PWM signal or via the embedded PWM engine
9	FBH	I	Output current feedback positive Non inverting Input (+)
10	FBL	I	Output current feedback negative Inverting Input (-)
3	BST1	IO	Bootstrap capacitor Used for internal biasing and to drive the high-side switch HSGD1. Bypass to SWN1 with external capacitor close to the pin. Pin must not be left open
6	BST2	IO	Bootstrap capacitor Used for internal biasing and to drive the high-side switch HSGD2. Bypass to SWN2 with external capacitor close to the pin. Pin must not be left open
12	SWCS	I	Current sense input Inductor current measurement - Non-inverting input (+)

(table continues...)

Table 1 (continued) Pin definitions and functions

Pin	Symbol	I/O ¹⁾	Function
11	SGND	I	Current sense / Power ground Inductor current sense - Inverting Input (-). Power ground, connect to GND
13	COMP	O	Compensation network pin Connect R and C network to pin for stability phase margin adjustment
23	SOFT_START	O	Softstart configuration pin Connect a capacitor C_{SOFT_START} to GND to fix a soft start ramp default time
14	VFB	I	Output voltage feedback pin Output voltage feedback to set output overvoltage protection function
15	SET	I	Analog current sense adjustment pin A voltage V_{SET} between 0.2 V and 1.4 V will adjust the I_{LED} or V_{OUT} in a linear relation
17	PWMO	O	PWM Digital dimming output Drives n-channel MOSFET between GND and V_{VCC} for dimming purposes
18	EF	O	Error flag output An open drain output which is pulled to LOW when an output short to GND, an output overvoltage or IC overtemperature occurs

1) O: Output, I: Input, PD: pull-down circuit integrated

3 General product characteristics

3.1 Absolute maximum ratings

Table 2 Absolute maximum ratings

$T_J = -40^\circ\text{C}$ to $+150^\circ\text{C}$; all voltages with respect to ground, positive current flowing into pin (unless otherwise specified)
Not subject to production test, specified by design

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Supply voltages							
VIN Supply Input	V_{VIN}	-0.3	-	60	V	-	PRQ-32
IVCC Internal linear voltage regulator output voltage	V_{IVCC}	-0.3	-	6	V	-	PRQ-33
Gate Driver Stages							
LSGD1,2 Low-side gatedriver voltage	$V_{LSGD1,2}$	-0.3	-	5.5	V	-	PRQ-34
HSGD1,2 - SWN1,2 High-side gate driver voltage	$V_{HSGD1,2-SWN1,2}$	-0.3	-	5.5	V	Differential signal (not referred to GND)	PRQ-35
SWN1, SWN2 Switching node voltage	$V_{SWN1,2}$	-1	-	60	V	-	PRQ-36
(BST1-SWN1), (BST2-SWN2) Bootstrap voltage	$V_{BST1,2-SWN1,2}$	-0.3	-	6	V	Differential signal (not referred to GND)	PRQ-37
BST1, BST2 Bootstrap voltage related to GND	$V_{BST1,2}$	-0.3	-	65	V	-	PRQ-38
SWCS Switch current sense input voltage	V_{SWCS}	-0.3	-	0.3	V	-	PRQ-39
SGND Switch current sense GND voltage	V_{SGND}	-0.3	-	0.3	V	-	PRQ-40
SWCS-SGND Switch current sense differential voltage	$V_{SWCS-SGND}$	-0.5	-	0.5	V	Differential signal (not referred to GND)	PRQ-41
PWMO Output voltage	V_{PWMO}	-0.3	-	5.5	V	-	PRQ-46
High voltage pins							
FBH, FBL Feedback error amplifier voltage	$V_{FBH, FBL}$	-0.3	-	60	V	-	PRQ-42
FBH-FBL Feedback error amplifier differential voltage	$V_{FBH-FBL}$	-0.5	-	0.5	V	Differential signal (not referred to GND)	PRQ-43
EN/INUVLO Device enable/input undervoltage lockout	$V_{EN/INUVLO}$	-0.3	-	60	V	-	PRQ-44

(table continues...)

Table 2 (continued) Absolute maximum ratings

$T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$; all voltages with respect to ground, positive current flowing into pin (unless otherwise specified)
Not subject to production test, specified by design

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			

Analog pins

PWMI Input voltage	V_{PWMI}	-0.3	–	5.5	V	–	PRQ-45
VFB Input voltage	V_{VFB}	-0.3	–	5.5	V	–	PRQ-47
EF Error flag output voltage	V_{EF}	-0.3	–	5.5	V	–	PRQ-48
SET Analog dimming input voltage	V_{SET}	-0.3	–	5.5	V	–	PRQ-49
COMP Compensation input voltage	V_{COMP}	-0.3	–	3.6	V	–	PRQ-205
SOFT_START Softstart voltage	$V_{\text{SOFT_START}}$	-0.3	–	3.6	V	–	PRQ-50
FREQ Voltage at frequency selection pin	V_{FREQ}	-0.3	–	3.6	V	–	PRQ-51

Temperatures

Junction Temperature	T_J	-40	–	150	$^{\circ}\text{C}$	–	PRQ-52
Storage Temperature	T_{stg}	-55	–	150	$^{\circ}\text{C}$	–	PRQ-53

ESD susceptibility

ESD resistivity of all pins	$V_{\text{ESD,HBM}}$	-2	–	2	kV	HBM ¹⁾	PRQ-54
ESD Resistivity to GND	$V_{\text{ESD,CDM}}$	-750	–	750	V	CDM ²⁾	PRQ-55

1) ESD susceptibility, Human Body Model “HBM” according to AEC Q100-002

2) ESD susceptibility, Charged Device Model “CDM” according to AECQ100-011

Notes:

1. Stresses above the ones listed here may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
2. Integrated protection functions are designed to prevent IC destruction under fault conditions described in the datasheet. Fault conditions are considered as “outside” normal operating range. Protection functions are not designed for continuous repetitive operation.

3.2 Functional range

Table 3 Functional Range

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Device extended supply voltage range	V_{VIN}	4.5		40	V	1)	PRQ-142
Device nominal supply voltage range	V_{VIN}	8	–	36	V	–	PRQ-57
Power stage voltage range	V_{POW}	4.5	–	55	V	1)	PRQ-58
Junction temperature	T_J	-40	–	150	°C	–	PRQ-59

1) Not subject to production test, specified by design.

Note: Within the functional range the IC operates as described in the circuit description. The electrical characteristics are specified within the conditions given in the related electrical characteristics table.

3.3 Thermal resistance

Note: This thermal data was generated in accordance with JEDEC JESD51 standards. For more information, go to www.jedec.org.

Table 4 Thermal Resistance

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Junction to case	R_{thJC}	–	7.78	–	K/W	1) 2)	PRQ-60
Junction to ambient	R_{thJA}	–	38.2	–	K/W	3) 2s2p	PRQ-61

1) Not subject to production test, specified by design

2) Specified R_{thJC} value is simulated at natural convection on a cold plate setup (all pins and the exposed pad are fixed to ambient temperature). $T_A = 25^\circ\text{C}$; The IC is dissipating 1 W

3) Specified R_{thJA} value is according to JEDEC 2s2p (JESD 51-7) + (JESD 51-5) and JEDEC 1s0p (JESD 51-3) + heatsink area at natural convection on FR4 board; The device was simulated on a 76.2 x 114.3 x 1.5 mm board. The 2s2p board has 2 outer copper layers (2 x 70 μm Cu) and 2 inner copper layers (2 x 35 μm Cu). A thermal via (diameter = 0.3 mm and 25 μm plating) array was applied under the exposed pad and connected the first outer layer (top) to the first inner layer and second outer layer (bottom) of the JEDEC PCB. $T_A = 25^\circ\text{C}$; The IC is dissipating 1 W

4 Power supply

4.1 Description

The TLD5191ES is supplied by the VIN (main supply voltage) pin.

The VIN supply provides internal supply voltages for the analog and digital blocks.

IVCC supplies the low side driver stages and the PWM driver.

This supply is used also to charge, through external Schottky diodes, the bootstrap capacitors which provide supply voltages to the high-side driver stages.

The supply pins VIN and IVCC have undervoltage detections.

If the voltage on IVCC goes below $V_{IVCC_RTH,d}$, driver stages are deactivated, thus stopping the switching activity.

The EN/INUVLO pin can be used as input undervoltage protection by placing a resistor divider from VIN to GND.

If the voltage on EN/INUVLO pin goes below $V_{EN/INUVLOth}$, IVCC voltage regulator is switched off, and switching activity is stopped.

Figure 3 shows a basic concept drawing of the supply domains and interactions among pins VIN and IVCC.

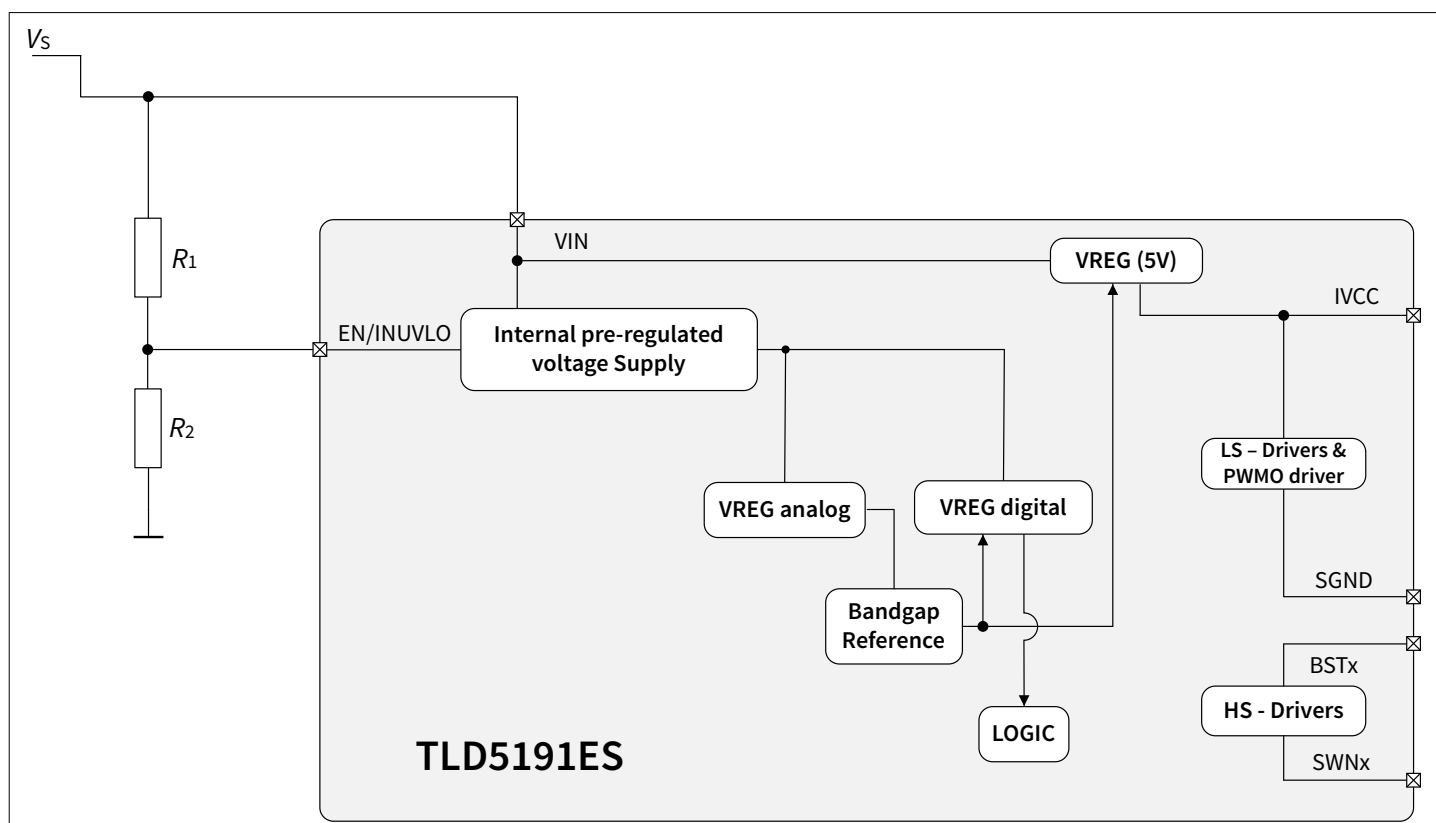


Figure 3 Power supply concept diagram

Usage of EN/INUVLO pin in different applications

The pin EN/INUVLO is a double function pin and can be used to put the device into a low current consumption mode. An undervoltage threshold should be fixed by placing an external resistor divider (A) in order to avoid low voltage operating conditions. This pin can be driven by a μ C-port as shown in (B) and (C) or directly connected to the input voltage supply as shown in (D).

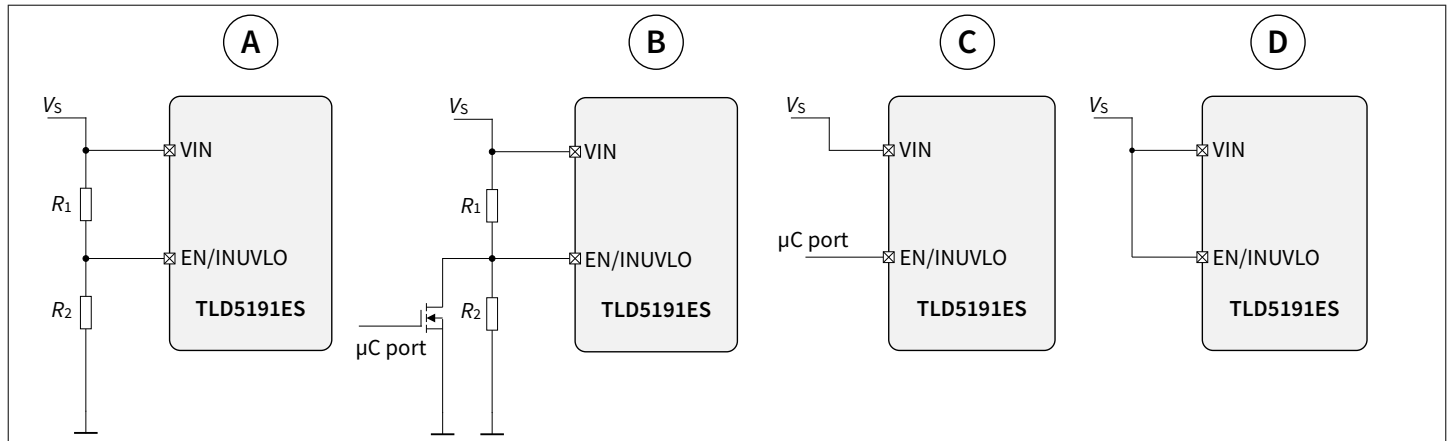


Figure 4 Usage of EN/INUVLO pin in different applications

4.2 Different power states

TLD5191ES has the following power states:

- SLEEP state
- IDLE state
- ACTIVE state

The transition between the power states is determined according to these variables:

- VIN level
- EN/INUVLO level
- IVCC level

The state diagram including the possible transitions is shown in [Figure 5](#)

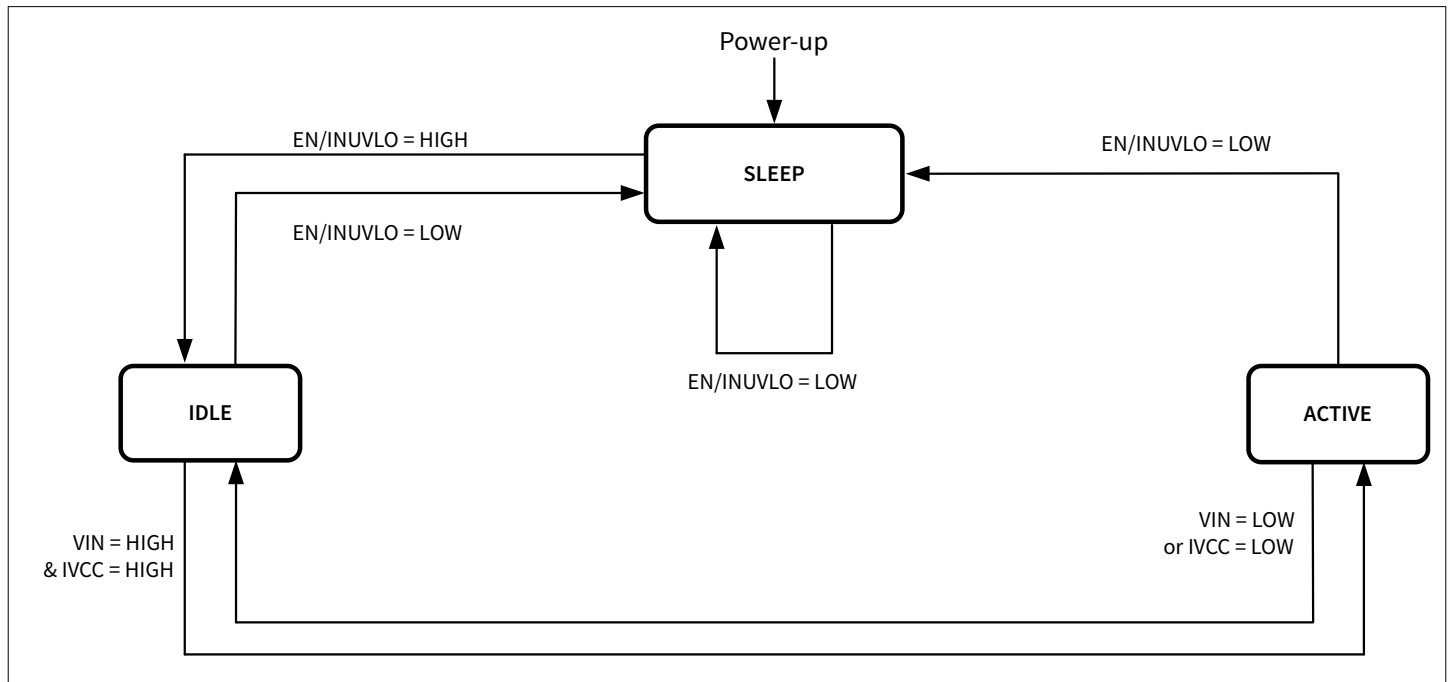


Figure 5 Simplified state diagram

The Power-up condition is entered when the supply voltage V_{VIN} exceeds its minimum supply voltage threshold $V_{VIN(ON)}$.

SLEEP

When the TLD5191ES is in the SLEEP state, all gate drivers and error flag are in OFF state, independently from the supply voltages V_{IN} , $IVCC$. The current consumption is lower than $I_{VIN(SLEEP)}$.

The transition from SLEEP to ACTIVE state requires a specified time: t_{ACTIVE} .

IDLE

In IDLE state the internal voltage regulator is working. The output drivers are switched OFF.

Diagnosis functions are not available.

ACTIVE

In active state the device will start switching activity to provide power at the output only when $PWMI = HIGH$ or $PWMI$ is in a valid range to enable the embedded PWM engine.

If the voltage between pins $BST1,2$ and $SWN1,2$ is higher than $V_{BST1,2} - V_{SWN1,2_UVth}$, high side gate drivers are enabled, otherwise they are disabled and no switching activity is permitted.

In active state the device current consumption via V_{IN} is dependent on the external MOSFETs used and the switching frequency f_{SW} .

Digital dimming PWM activity is mirrored on the $PWMO$ output pin unless a fault condition is detected (for details see [Chapter 6.1](#)).

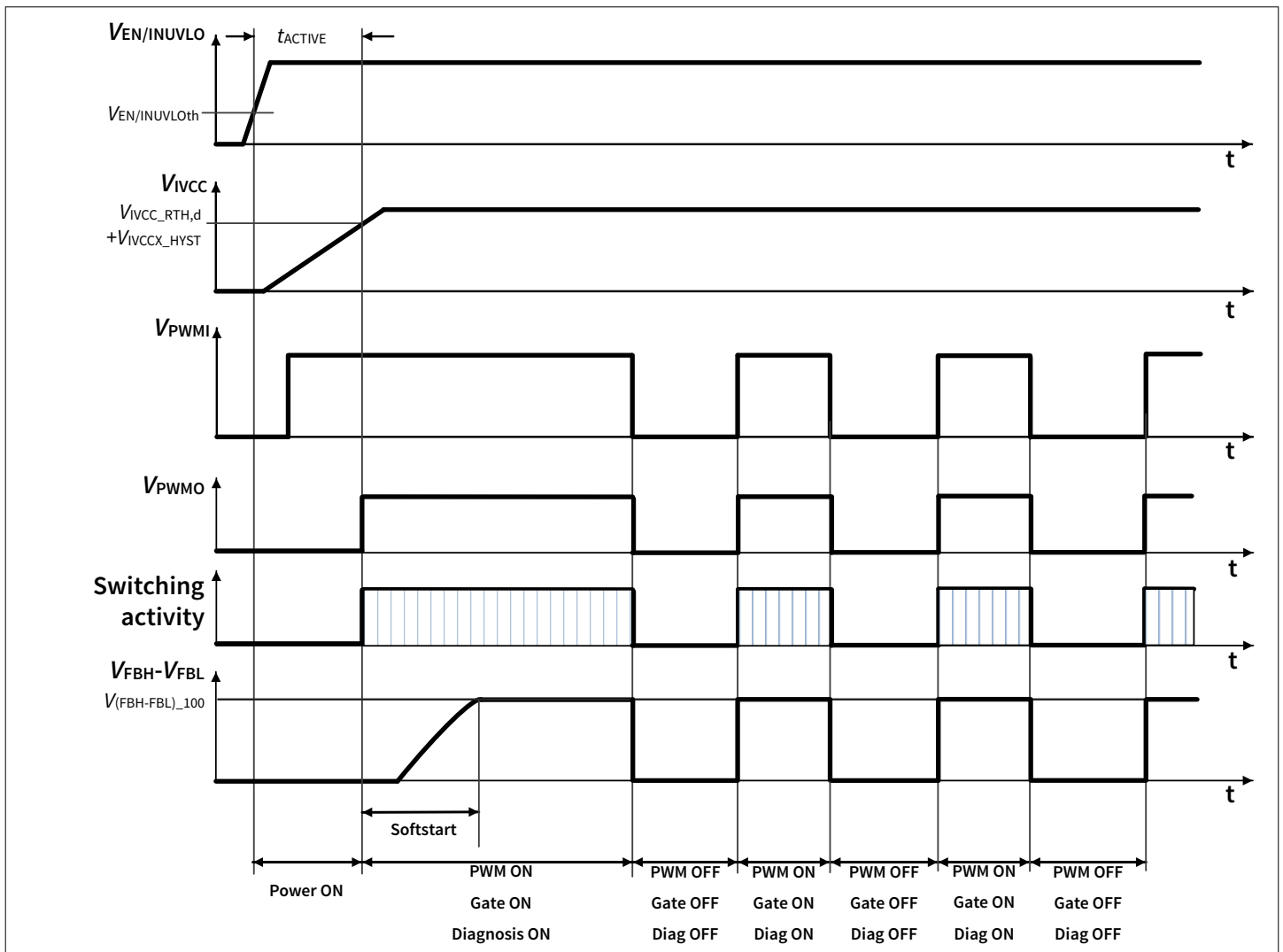


Figure 6 Timing diagram LED dimming and startup behavior example (V_{VIN} stable in the functional range and not during startup)

4.3 Electrical characteristics

Table 5 Electrical Characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Input voltage startup	$V_{VIN(ON)}$	–	–	4.7	V	V_{VIN} increasing; $V_{EN/INUVLO} = HIGH$; $I_{IVCC} = 0$ mA	PRQ-64
Input undervoltage switch OFF	$V_{VIN(OFF)}$	–	–	4.5	V	V_{VIN} decreasing; $V_{EN/INUVLO} = HIGH$; $I_{IVCC} = 10$ mA	PRQ-65
Device operating current	$I_{VIN(ACTIVE)}$	–	5	7	mA	¹⁾ ACTIVE mode; $V_{PWMI} = 0$ V	PRQ-66
VIN Sleep mode supply current	$I_{VIN(SLEEP)}$	–	–	1.5	μA	$V_{EN/INUVLO} = 0$ V; $V_{VIN} = 13.5$ V; $V_{IVCC} = 0$ V	PRQ-67
Input undervoltage falling threshold	$V_{EN/INUVLOth}$	1.6	1.75	1.9	V	–	PRQ-68
EN/INUVLO rising hysteresis	$V_{EN/INUVLO(hyst)}$	–	90	–	mV	¹⁾	PRQ-69
EN/INUVLO input current LOW	$I_{EN/INUVLO(LOW)}$	0.45	0.89	1.34	μA	$V_{EN/INUVLO} = 0.8$ V;	PRQ-70
EN/INUVLO input current HIGH	$I_{EN/INUVLO(HIGH)}$	1.1	2.2	3.3	μA	$V_{EN/INUVLO} = 2$ V;	PRQ-71
SLEEP mode to ACTIVE time	t_{ACTIVE}	–	–	0.7	ms	¹⁾ $C_{IVCC} = 10$ μF ; $V_{VIN} = 13.5$ V	PRQ-72

¹⁾ Not subject to production test, specified by design

5 Regulator

The TLD5191ES includes all of the functions necessary to provide constant current to the output as usually required to drive LEDs. A constant voltage regulation can also be implemented (refer to [Chapter 5.5](#)).

It is designed to control 4 gate driver outputs in a H-Bridge topology by using only one inductor and 4 external MOSFETs. This topology is able to operate in high power BOOST, BUCK-BOOST and BUCK mode applications with maximum efficiency.

The transition between the different regulation modes is done automatically by the device itself, with respect to the application boundary conditions.

The transition phase between modes is seamless.

5.1 Regulator diagram

An analog current control loop (with total gain = $IFB \times g_m$) connected to the sensing pins FBL, FBH regulates the output current.

The regulator function is implemented by a pulse width modulated (PWM) current mode controller. The error in the output current loop is used to determine the appropriate duty cycle to get a constant output current.

An external compensation network (RCOMP, CCOMP) is used to adjust the control loop to various application boundary conditions. The inductor current for the current mode loop is sensed by the RSWCS resistor. R_{SWCS} is used also to limit the maximum external switches / inductor current.

If the voltage across R_{SWCS} exceeds its overcurrent threshold (V_{SWCS_buck} or V_{SWCS_boost} for buck or boost operation respectively) the device reduces the duty cycle in order to bring the switches current below the imposed limit.

The current mode controller has a built-in slope compensation as well to prevent sub-harmonic oscillations.

The control loop logic block (LOGIC) provides a PWM signal to four internal gate drivers. The gate drivers (HSGD1,2 and LSGD1,2) are used to drive external MOSFETs in an H-Bridge setup.

Once V_{SOFT_START} exceeds $V_{Soft_Start_LOFF}$ or $V_{FBH-FBL}$ exceeds $V_{FBH_FBL_VALID}$, TLD5191ES forces CCM regulation mode.

The control loop block diagram displayed in [Figure 7](#) shows a typical constant current application. The voltage across R_{FB} sets the output current.

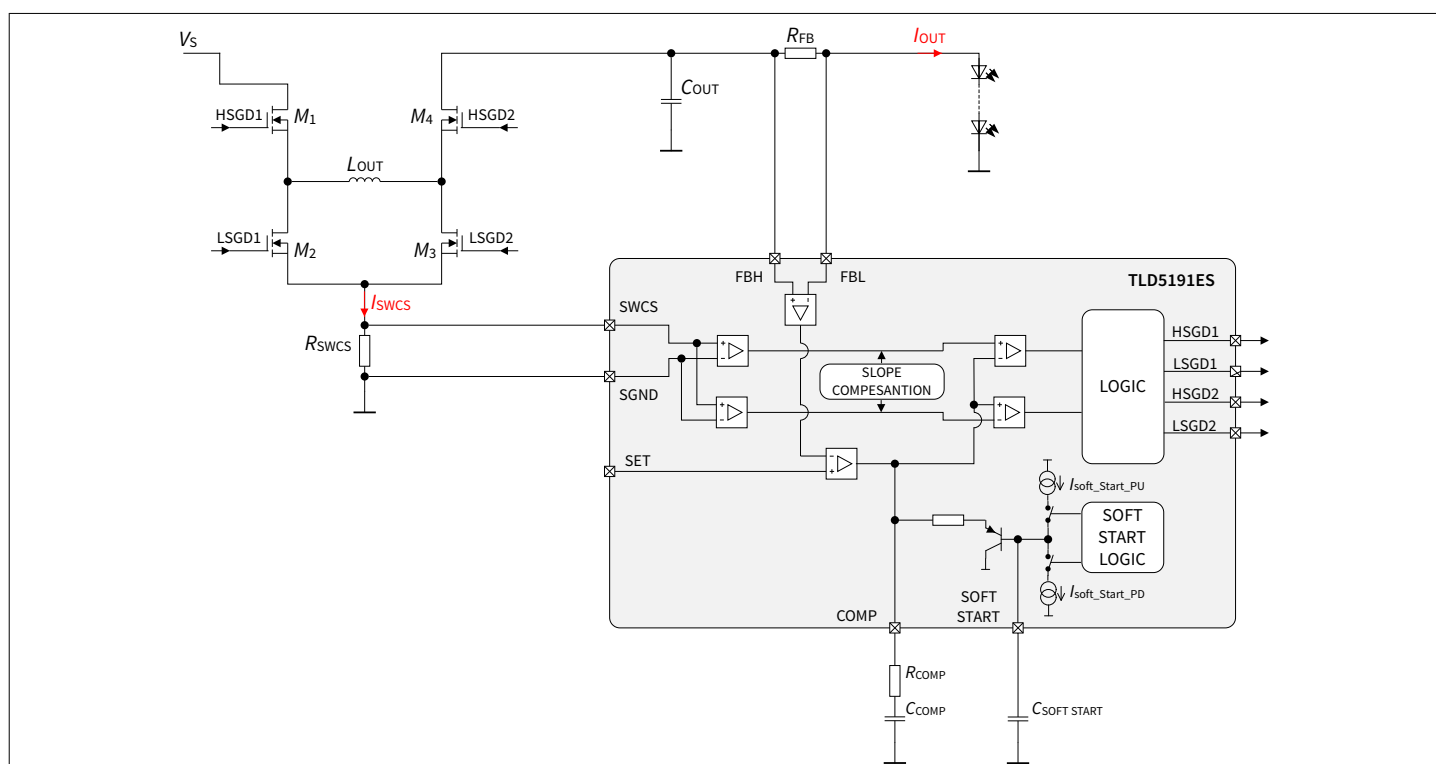


Figure 7 Regulator block diagram - TLD5191ES

5.2 Adjustable soft-start ramp

The soft-start routine limits the current through the inductor and the external MOSFET switches during initialization to minimize potential overshoots at the output.

The SOFT START pin is also used to implement a fault mask and wait-before-retry time, on rising and falling edge respectively.

See [Figure 8](#) and [Chapter 9.2](#) for details.

The soft start routine is applied if PWMI is above $V_{\text{PWMI,ON}}$ or PWMI is in a valid range to enable the embedded PWM engine, if one of the following conditions is verified:

- after IDLE to ACTIVE power state transition
- after PWMI has been kept below $V_{\text{PWMI,DC}_0}$ for more than $t_{\text{PWMI,OFF}}$
- after output short to GND detection

The soft start routine is active during the rising and falling edge of $V_{\text{SOFT_START}}$. The soft start timing is defined by a capacitor placed on the SOFT_START pin and both the soft start pull-up and pull-down current sources ($I_{\text{Soft_Start_PU}}$, $I_{\text{Soft_Start_PD}}$). Soft start rising edge time is approximately:

$$t_{\text{Soft_Start},r} = V_{\text{Soft_Start_LOFF}} \cdot \frac{C_{\text{Soft_Start}}}{I_{\text{Soft_Start_PU}}} \quad (1)$$

Note: Minimum value of soft start capacitor has to be designed such that, during startup, the output voltage exceeds the short to ground threshold ($V_{\text{FBH}} > V_{\text{FBH_S2G_inc}}$), before the soft start voltage reaches $V_{\text{SOFT_START_LOFF}}$. Minimum temperature and minimum input voltage shall be considered as worst case condition for the dimensioning.

The soft start routine limits the inrush current by clamping the COMP pin through a buffer like depicted in [Figure 7](#). Therefore this functionality is effective only when soft start capacitor is sufficiently larger than the COMP capacitor and its effect is visible mainly in buck-boost or boost regulation mode.

If a short circuit on the output is detected the pull-down current source $I_{\text{Soft_Start_PD}}$ is activated. This current discharges the $V_{\text{SOFT_START}}$ until $V_{\text{Soft_Start_RESET}}$ is reached. Afterwards the pull-up current source $I_{\text{Soft_Start_PU}}$ turns on again only if the PWMI signal is higher than $V_{\text{PWMI,DC}_0}$. If the fault condition hasn't been removed before $V_{\text{Soft_Start_LOFF}}$ is reached, the pull-down current source is reactivated initiating a new cycle.

During soft start rise time switching activity is observed, during the fall time instead the switching activity is halted like shown in [Figure 8](#). This hiccup mode will continue until the fault is removed.

It is possible to latch the fault condition on the TLD5191ES by sourcing a current higher than $I_{\text{Soft_Start_PD}}$ through an external pull-up resistor connected from IVCC to the SOFT START pin. In this condition the device will restart regulating only if EN/INUVLO pin is toggled or if PWMI is toggled after having kept it low for more than $t_{\text{PWMI,OFF}}$.

During rising edge of soft start, the internal PWM is extended till one of the 2 following condition is reached:

- Until $V_{\text{SOFT_START}}$ exceeds $V_{\text{Soft_Start_LOFF}}$
- Until $V_{\text{FBH-FBL}}$ exceeds $V_{\text{FBH_FBL_VALID}}$

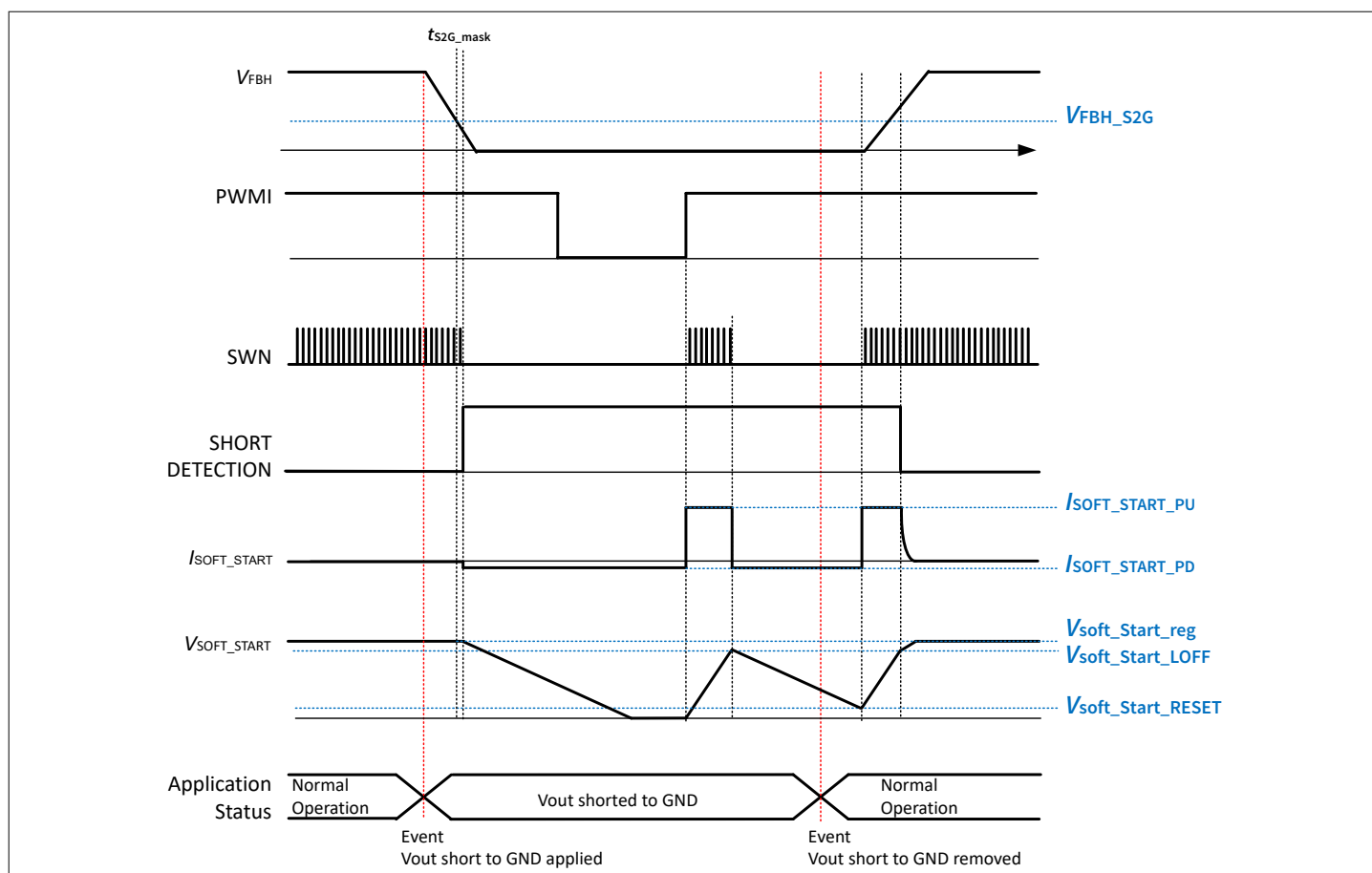


Figure 8 Soft start timing diagram on a short to ground detected by the FBH pin

5.3 Switching frequency setup

The switching frequency can be set from 200 kHz to 700 kHz by an external resistor connected from the FREQ pin to GND. Select the switching frequency with an external resistor according to the graph in [Figure 9](#) or the following approximated formulas.

$$f_{SW}[kHz] = 5375 * (R_{FREQ}[k\Omega])^{-0.8} \quad (2)$$

$$R_{FREQ}[k\Omega] = 46023 * (f_{SW}[kHz])^{-1.25} \quad (3)$$

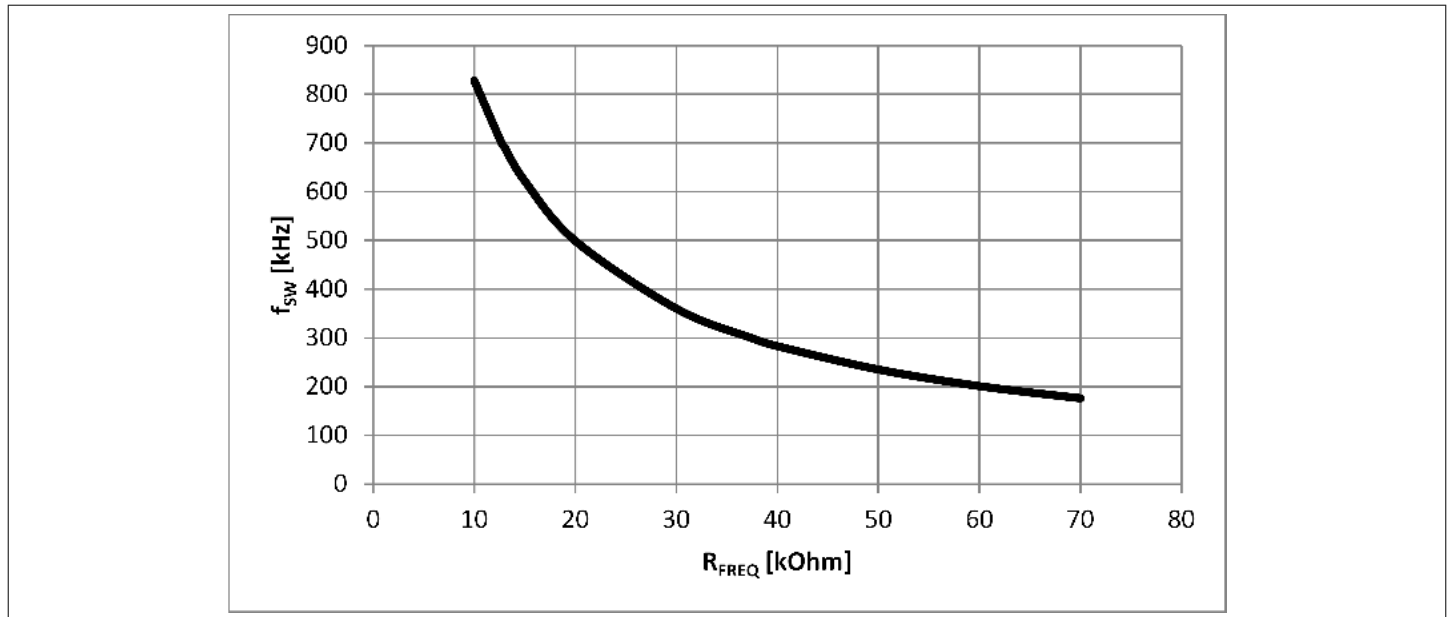


Figure 9 Switching frequency f_{SW} versus frequency select resistor to GND R_{FREQ}

5.4 Operation of 4 switches H-Bridge architecture

Inductor L_{OUT} connects in an H-Bridge configuration with 4 external n-channel MOSFETs (M_1 , M_2 , M_3 & M_4)

- Transistor M_1 and M_3 provides a path between V_{IN} and ground through L_{OUT} in one direction (Driven by top and bottom gate drivers HSGD1 and LSGD2)
- Transistor M_2 and M_4 provides a path between V_{OUT} and ground through L_{OUT} in the other direction (Driven by top and bottom gate drivers HSGD2 and LSGD1)
- Nodes SWN1, SWN2, voltage across R_{SWCS} and load current are also monitored by the TLD5191ES

Table 6 4 switches H-Bridge architecture transistor status summary

	BOOST mode	BUCK-BOOST mode	BUCK mode
M1	ON	PWM	PWM
M2	OFF	PWM	PWM
M3	PWM	PWM	OFF
M4	PWM	PWM	ON

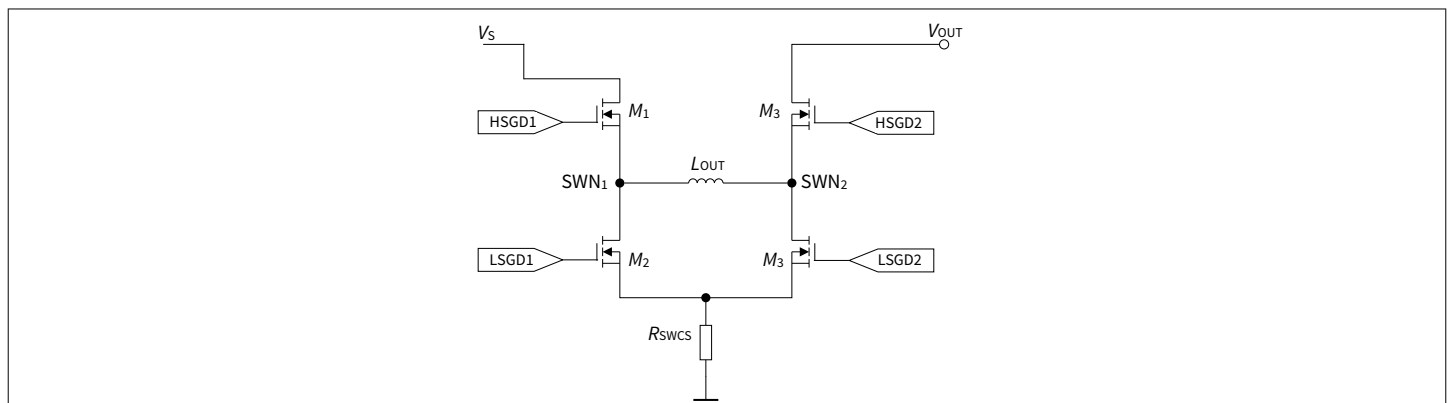


Figure 10 4 switches H-Bridge architecture overview

5.4.1 Boost mode ($V_{IN} < V_{OUT}$)

- M_1 is always ON, M_2 is always OFF
- Every cycle M_3 turns ON first and inductor current is sensed (peak current control)
- M_3 stays ON until the upper reference threshold is reached across R_{SWCS} (Energizing)
- M_3 turns OFF, M_4 turns ON until the end of the cycle (Recirculation)
- Switches M_3 and M_4 alternate, behaving like a typical synchronous boost regulator

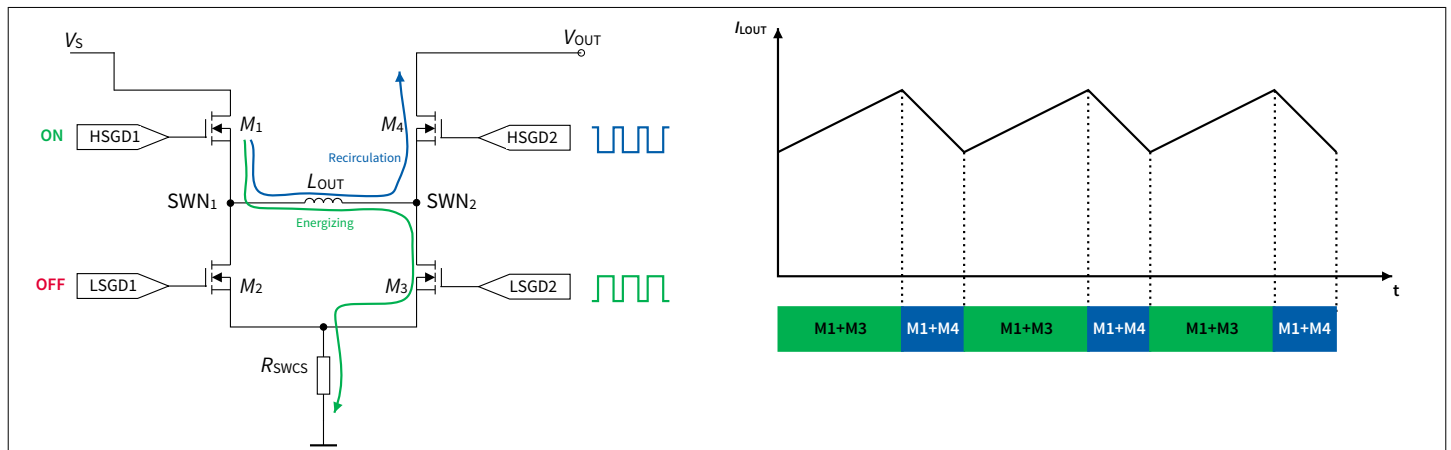


Figure 11 4 switches H-Bridge architecture in BOOST mode

Simplified comparison of 4 switches H-Bridge architecture to traditional asynchronous Boost approach

- M_2 is always OFF in this mode (open)
- M_1 is always ON in this mode (closed connection of inductor to V_{IN})
- M_4 acts as a synchronous diode, with significantly lower conduction power losses ($I^2 \times R_{DS(on)}$ vs. $0.7 V \times I$)

Note: Diode is source of losses and lower system efficiency!

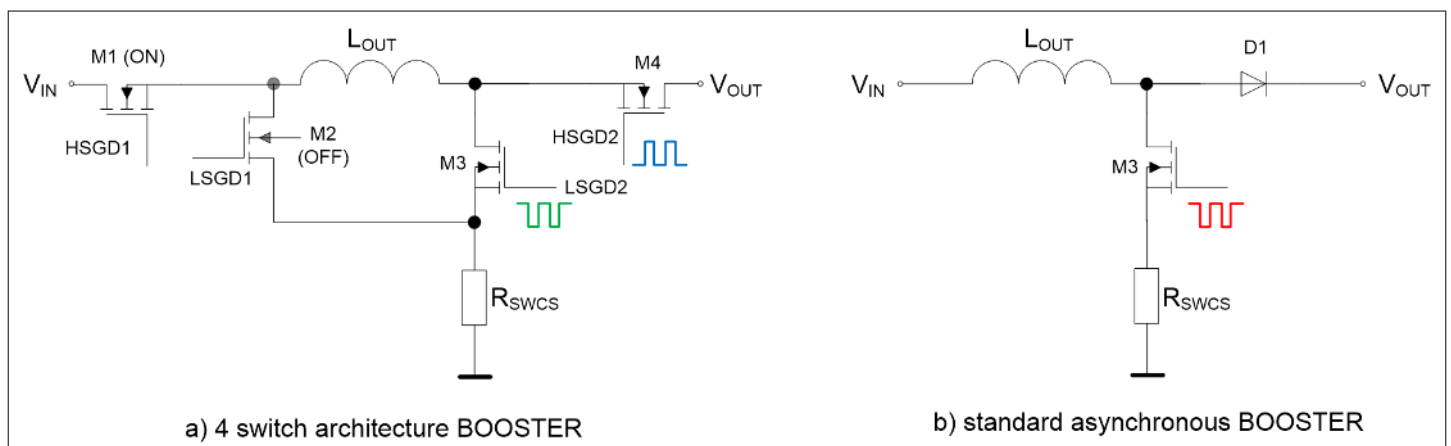


Figure 12 4 switches H-Bridge architecture in BOOST mode compared to standard async booster

5.4.2 Buck mode ($V_{IN} > V_{OUT}$)

- M_4 is always ON, M_3 is always OFF
- Every cycle M_2 turns ON and inductor current is sensed (valley current control)
- M_2 stays ON until the lower reference threshold is reached across R_{SWCS} (Recirculation)
- M_2 turns OFF, M_1 turns ON until the end of the cycle (Energizing)
- Switches M_1 and M_2 alternate, behaving like a typical synchronous BUCK Regulator

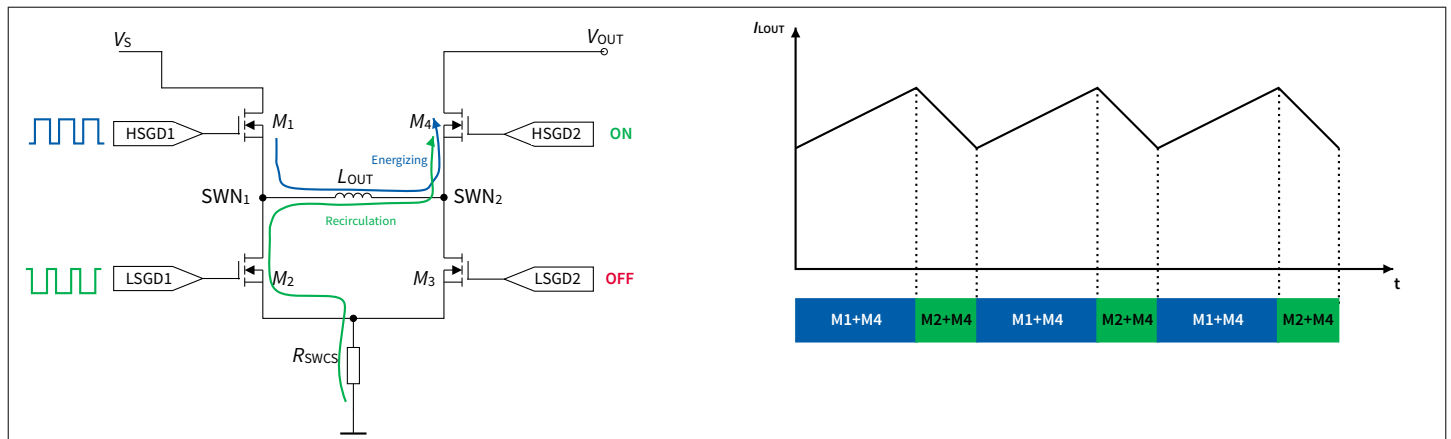


Figure 13 4 switches H-Bridge architecture in BUCK mode

Simplified comparison of 4 switches architecture to traditional asynchronous Buck approach

- M₃ is always OFF in this mode (open)
- M₄ is always ON in this mode (closed connection inductor to V_{OUT})
- M₂ acts as a synchronous diode, with significantly lower conduction losses ($I^2 \times R_{\text{DS(on)}}$ vs. $0.7 \text{ V} \times I$)

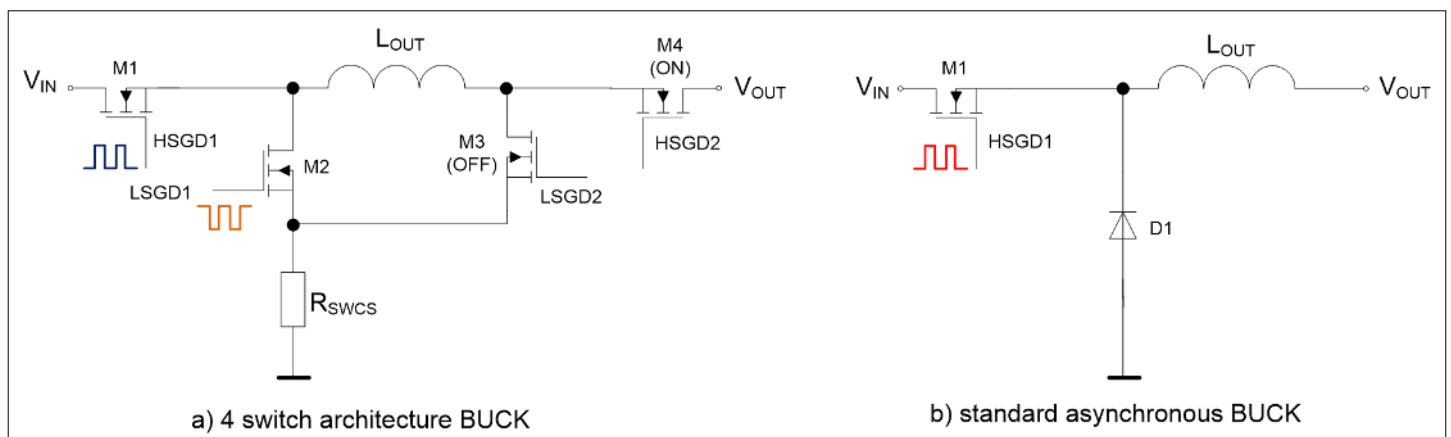


Figure 14 4 switches H-Bridge architecture in BUCK mode compared to standard async BUCK

5.4.3 Buck-Boost mode (V_{IN} ~ V_{OUT})

- When V_{IN} is close to V_{OUT} the controller is in Buck-Boost operation
- All switches are switching in buck-boost operation. The direct energy transfer from the input to the output (M₁+M₄ = ON) is beneficial to reduce ripple current and improves the energy efficiency of the buck-boost control scheme
- The two buck boost waveforms and switching behaviors are displayed in [Figure 15](#) below

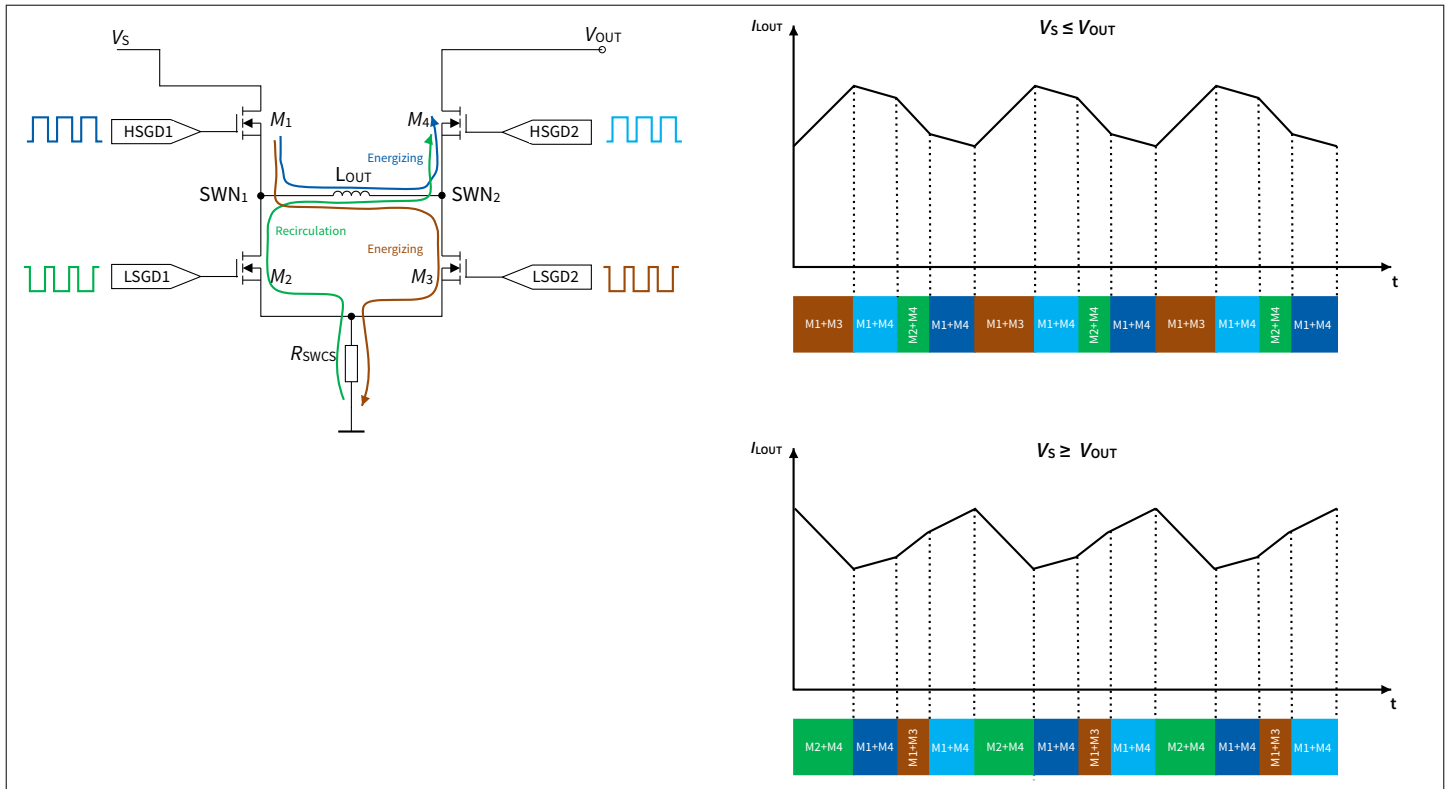


Figure 15 4 switches H-Bridge architecture in BUCK_BOOST mode

5.5 Programming output voltage (constant voltage regulation)

For a voltage regulator, the output voltage can be set by selecting the values R_{FB1} and R_{FB2} according to the following equation:

$$V_{OUT} = \left(\frac{V_{FBH} - V_{FBL}}{R_{FB1}} - I_{FBL} \right) \cdot R_{FB2} + V_{FBH} - V_{FBL} \quad (4)$$

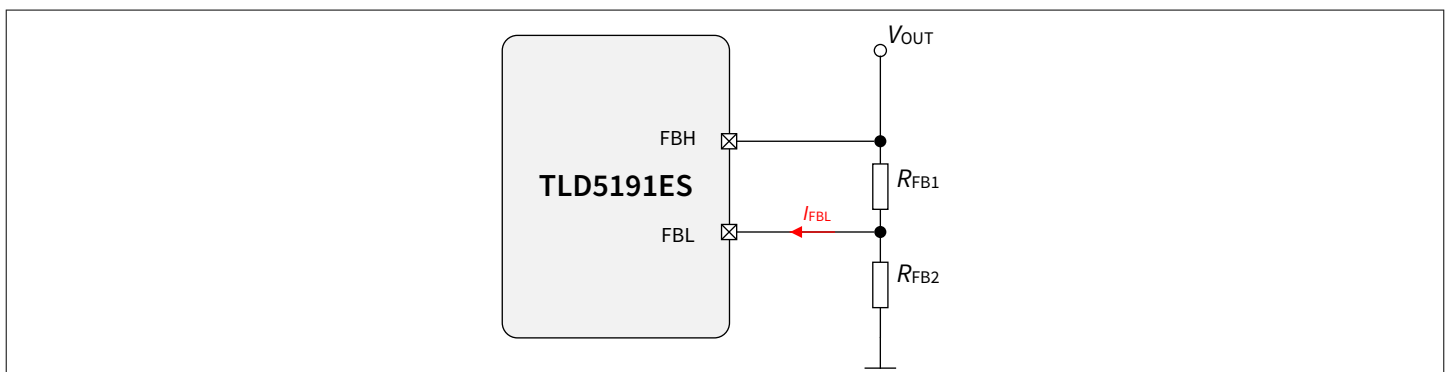


Figure 16 Programming output voltage (Constant voltage regulation)

5.6 Electrical characteristics

Table 7 Electrical characteristics

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
V(FBH-FBL) threshold @ analog dimming 100%	$V_{(\text{FBH-FBL})_{100}}$	145.5	150	154.5	mV	$V_{\text{SET}} = 2\text{ V}$; $V_{\text{FBH}} = 2\text{ V to }60\text{ V}$;	PRQ-73
V(FBH-FBL) threshold @ analog dimming 10%	$V_{(\text{FBH-FBL})_{10}}$	10	15	20	mV	$V_{\text{SET}} = 0.32\text{ V}$; $V_{\text{FBH}} = 2\text{ V to }60\text{ V}$	PRQ-74
FBH Bias current	I_{FBH}	65	110	155	μA	¹⁾ $V_{\text{FBL}} = 7\text{ V}$; $V_{\text{FBH-FBL}} = 150\text{ mV}$	PRQ-75
FBL Bias current	I_{FBL}	17	30	43	μA	¹⁾ $V_{\text{FBL}} = 7\text{ V}$; $V_{\text{FBH-FBL}} = 150\text{ mV}$	PRQ-76
V(FBH-FBL) valid range threshold	$V_{\text{FBH-FBL_VALID}}$	110	120	130	mV	$V_{\text{SET}} > 1.5\text{ V}$	PRQ-198
OUT Current sense amplifier gain	$I_{\text{FBX}}x_{\text{gm}}$	–	890	–	μS	¹⁾	PRQ-77
Maximum BOOST duty cycle	$D_{\text{BOOST_MAX}}$	89	91	93	%	¹⁾ $f_{\text{sw}} = 300\text{ kHz}$	PRQ-80
Switch peak over current threshold - BOOST	$V_{\text{SWCS_boost}}$	70	76	82	mV	¹⁾	PRQ-81
Switch peak over current threshold - BUCK	$V_{\text{SWCS_buck}}$	-60	-50	-40	mV	¹⁾	PRQ-82
Soft Start pull up current	$I_{\text{Soft_Start_PU}}$	22	26	32	μA	$V_{\text{Soft_Start}} = 1\text{ V}$	PRQ-83
Soft Start pull down current	$I_{\text{Soft_Start_PD}}$	2.2	2.6	3.2	μA	$V_{\text{Soft_Start}} = 1\text{ V}$	PRQ-84
Soft start latch-OFF threshold	$V_{\text{Soft_Start_LOFF}}$	1.65	1.75	1.85	V	–	PRQ-85
Soft start reset threshold	$V_{\text{Soft_Start_RESET}}$	0.1	0.2	0.3	V	–	PRQ-86
Soft start voltage during regulation	$V_{\text{Soft_Start_reg}}$	1.9	2	2.1	V	¹⁾ No Faults	PRQ-87
Average switching frequency	f_{sw}	280	300	320	kHz	$T_J = 25^\circ\text{C}$; $R_{\text{FREQ}} = 37.4\text{ k}\Omega$; Average value (spread spectrum modulator always on)	PRQ-88
Gate driver undervoltage threshold	$V_{\text{BST1,2-VSWN1,2_UVth}}$	3.4	–	4	V	$V_{\text{BST1,2-VSWN1,2}}$ decreasing; Differential signal (not referred to GND)	PRQ-89

(table continues...)

Table 7 (continued) Electrical characteristics

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
HSGD1,2 NMOS driver on-state resistance (Gate Pull Up)	$R_{DS(ON_PU)HS}$	1.4	2.3	3.7	Ω	$V_{BST1,2} - V_{SWN1,2} = 5\text{ V}$; $I_{source} = 100\text{ mA}$	PRQ-90
HSGD1,2 NMOS driver on-state resistance (Gate Pull Down)	$R_{DS(ON_PD)HS}$	0.6	1.2	2.2	Ω	$V_{BST1,2} - V_{SWN1,2} = 5\text{ V}$; $I_{sink} = 100\text{ mA}$	PRQ-91
LSGD1,2 NMOS driver on-state resistance (Gate Pull Up)	$R_{DS(ON_PU)LS}$	1.4	2.3	3.7	Ω	$V_{IVCC} = 5\text{ V}$; $I_{source} = 100\text{ mA}$	PRQ-92
LSGD1,2 NMOS driver on-state resistance (Gate Pull Down)	$R_{DS(ON_PD)LS}$	0.4	1.2	2.5	Ω	$V_{IVCC} = 5\text{ V}$; $I_{sink} = 100\text{ mA}$	PRQ-93
HSGD1,2 Gate driver peak sourcing current	$I_{HSGD1,2_SRC}$	380	–	–	mA	¹⁾ $V_{HSGD1,2} - V_{SWN1,2} = 1\text{ V to }4\text{ V}$; $V_{BST1,2} - V_{SWN1,2} = 5\text{ V}$	PRQ-161
HSGD1,2 Gate driver peak sinking current	$I_{HSGD1,2_SNK}$	410	–	–	mA	¹⁾ $V_{HSGD1,2} - V_{SWN1,2} = 4\text{ V to }1\text{ V}$; $V_{BST1,2} - V_{SWN1,2} = 5\text{ V}$	PRQ-162
LSGD1,2 Gate driver peak sourcing current	$I_{LSGD1,2_SRC}$	370	–	–	mA	¹⁾ $V_{LSGD1,2} = 1\text{ V to }4\text{ V}$; $V_{IVCC} = 5\text{ V}$	PRQ-163
LSGD1,2 Gate driver peak sinking current	$I_{LSGD1,2_SNK}$	550	–	–	mA	¹⁾ $V_{LSGD1,2} = 4\text{ V to }1\text{ V}$; $V_{IVCC} = 5\text{ V}$	PRQ-164
LSGD1,2 OFF to HSGD1,2 ON delay	$t_{LSOFF-HSON_delay}$	15	30	40	ns	¹⁾	PRQ-98
HSGD1,2 OFF to LSGD1,2 ON delay	$t_{HSOFF-LSON_delay}$	35	60	75	ns	¹⁾	PRQ-99

¹⁾ Not subject to production test, specified by design

6 Digital dimming function

PWM dimming is adopted to vary LEDs brightness with greatly reduced chromaticity shift. PWM dimming achieves brightness reduction by varying the duty cycle of a constant current in the LED string.

6.1 Description

PWM via direct interface

Pulse width modulated (PWM) signals can be applied to the PWMI pin. The gate drivers are enabled if the signal is on high level and they are disabled if the signal is at low level.

The applied PWM signal shall have a frequency above $f_{PWM,min}$.

PWMO pin replicates PWMI pin HIGH or LOW state, unless one of the following conditions occur:

- Output overvoltage event
- Output short to ground event
- Thermal shutdown

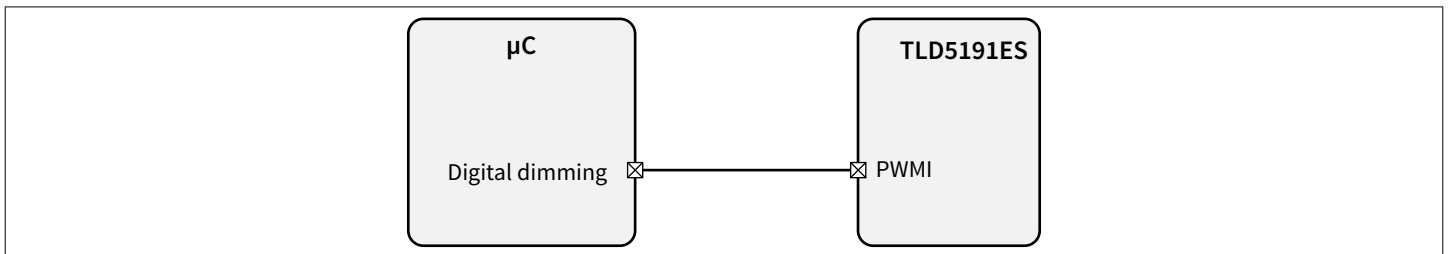


Figure 17 Digital dimming overview

PWM dimming in LOW states can be used to suspend the output current for long time intervals in a safe manner. Indeed a soft start routine is applied once the channel is enabled if the PWM input signal has been kept below V_{PWMI,DC_0} for at least $t_{PWMI,OFF}$.

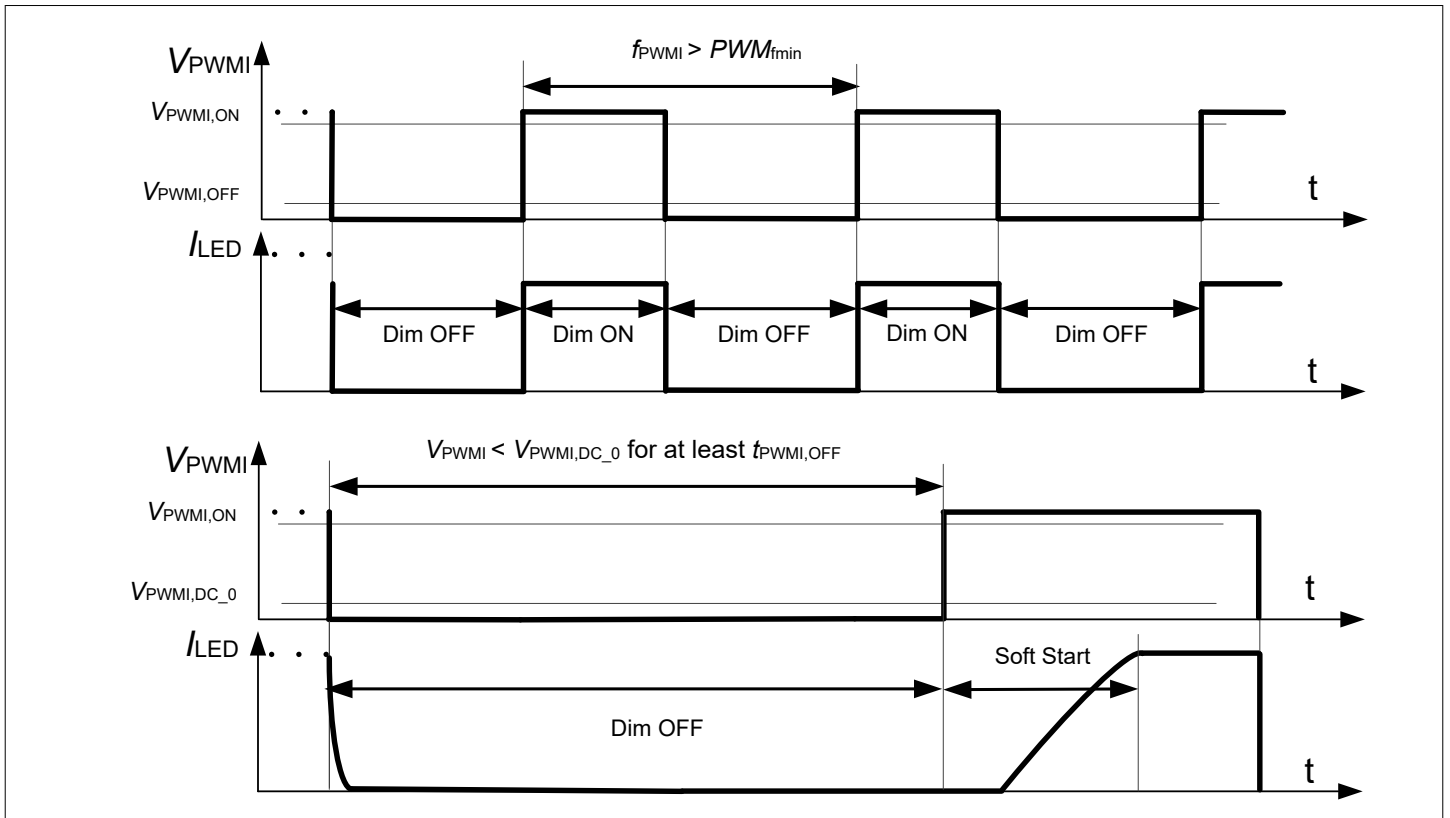


Figure 18 PWMI timings diagrams

PWM via embedded PWM engine

If an analog signal in between V_{PWMI,DC_0} and V_{PWMI,DC_100} is applied, embedded PWM is activated. The embedded PWM engine has an 8 bit resolution with a fixed internal frequency of f_{PWM} .

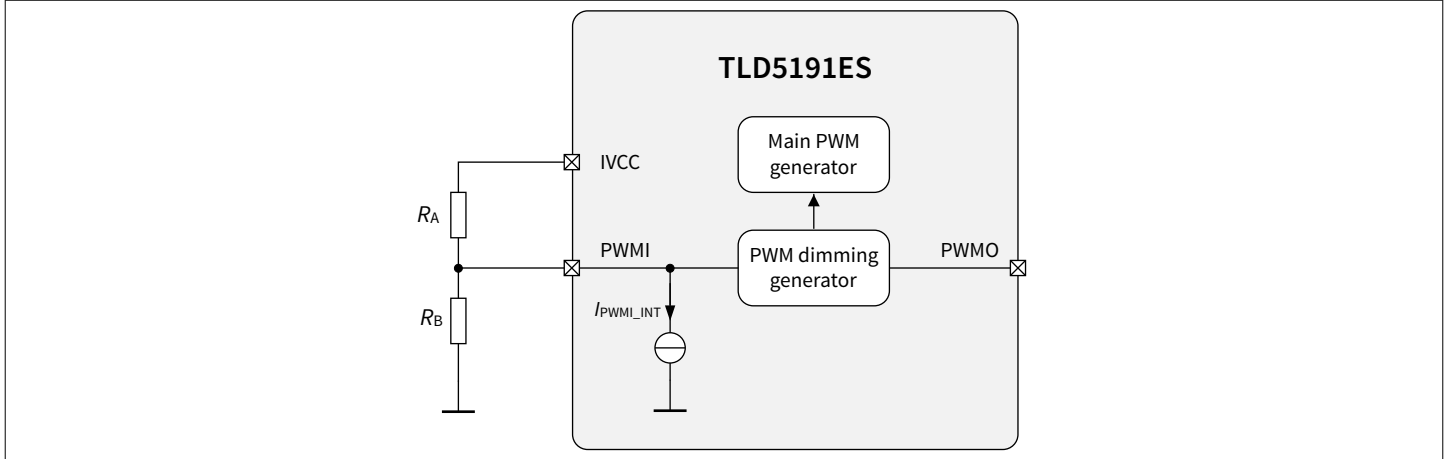


Figure 19 Block diagram of embedded PWM generator

Note: A non linear embedded PWM engine is implemented to guarantee high accuracy for low values of duty cycle. It helps the headlamp designers to achieve high LED brightness accuracy when dimming to low duty cycle values. Moreover it helps to produce smooth fading curve, compensating the logarithmic change in the perceived brightness.

PWMO pin replicates the frequency and duty cycle of the embedded PWM engine, unless one of the following conditions occur:

- Output overvoltage event
- Output short to ground event
- Thermal shutdown

The duty cycle produced by the embedded PWM engine is a function of the voltage applied on PWMI pin.

The duty cycle is quantized with different LSB step values in the following V_{PWMI} ranges:

- 0.142% for $V_{PWMI,DC_0} \leq V_{PWMI} \leq 0.23 \cdot V_{IVCC}$
- 0.284% for $0.23 \cdot V_{IVCC} < V_{PWMI} \leq 0.28 \cdot V_{IVCC}$
- 0.569% for $0.28 \cdot V_{IVCC} < V_{PWMI} \leq V_{PWMI,DC_100}$

and can be calculated by the following formulas:

$$DC \% = 63 \cdot \left(\frac{V_{PWMI} - 0.18 \cdot V_{IVCC}}{0.05 \cdot V_{IVCC}} \right) \cdot 0.142 \% \quad \text{for } V_{PWMI,DC_0} \leq V_{PWMI} \leq 0.23 \cdot V_{IVCC} \quad (5)$$

$$DC \% = 8.95 \% + 64 \cdot \left(\frac{V_{PWMI} - 0.23 \cdot V_{IVCC}}{0.05 \cdot V_{IVCC}} \right) \cdot 0.284 \% \quad \text{for } 0.23 \cdot V_{IVCC} < V_{PWMI} \leq 0.28 \cdot V_{IVCC} \quad (6)$$

$$DC \% = 27.13 \% + 128 \cdot \left(\frac{V_{PWMI} - 0.28 \cdot V_{IVCC}}{0.1 \cdot V_{IVCC}} \right) \cdot 0.569 \% \quad \text{for } 0.28 \cdot V_{IVCC} < V_{PWMI} \leq V_{PWMI,DC_100} \quad (7)$$

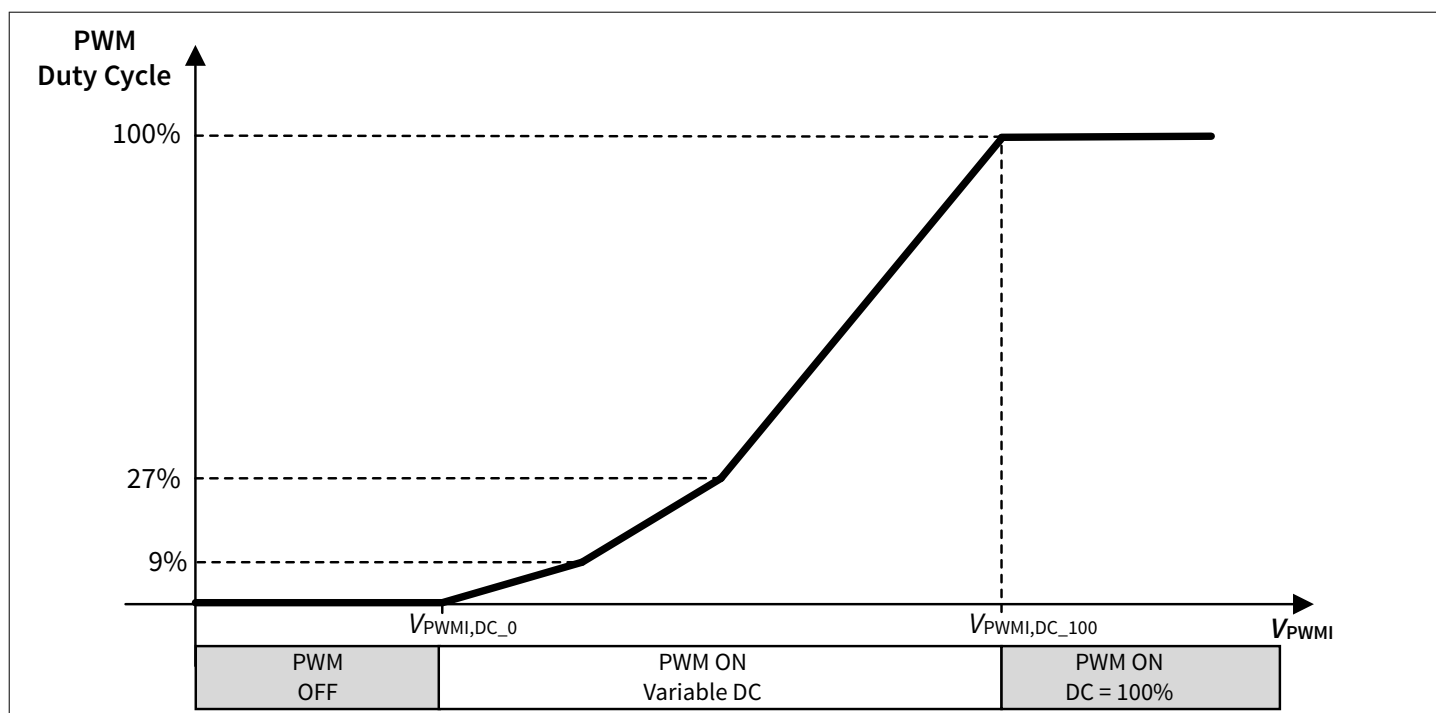


Figure 20 Analog PWM DC curve

6.2 Electrical characteristics

Table 8 Electrical characteristics

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
PWMI Turn on threshold	$V_{PWMI,ON}$	–	–	2	V	–	PRQ-100
PWMI Turn off threshold	$V_{PWMI,OFF}$	0.8	–	–	V	–	PRQ-101
PWMI Off time threshold	$t_{PWMI,OFF}$	–	–	25	ms	1)	PRQ-199
PWMI Minimum frequency	$f_{PWM,min}$	75	–	–	Hz	1)	PRQ-202
PWM Engine minimum voltage	V_{PWMI,DC_0}	0.176* V_{IVCC}	0.18* V_{IVCC}	–	V	–	PRQ-102
PWM Engine maximum voltage	V_{PWMI,DC_100}	–	0.38* V_{IVCC}	0.387* V_{IVCC}	V	–	PRQ-103
PWM Engine DC	$PWM_{DC_15\%}$	14.25	15	15.75	%	$V_{PWMI} = 0.246 * V_{IVCC}$	PRQ-104
PWM Engine frequency	f_{PWM}	220	275	330	Hz	–	PRQ-105
PWMI Internal pull down current	I_{PWMI_INT}	1.5	–	3.5	uA	1) $V_{PWMI} = 0.2 * V_{IVCC}$	PRQ-106
PWMO Gate driver sourcing current	I_{PWMO_SRC}	-40	-22	-10	mA	1) $V_{PWMO} = 2.5\text{ V}; V_{IVCC} = 5\text{ V}$	PRQ-109

(table continues...)

Table 8 (continued) Electrical characteristics

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
PWMO Gate driver sinking current	I_{PWMO_SNK}	10	25	40	mA	¹⁾ $V_{PWMO} = 2.5\text{ V}$; $V_{VCC} = 5\text{ V}$	PRQ-110
PWMO Gate driver rise time	$t_{R,PWMO}$	200	450	700	ns	¹⁾ $C_{gate} = 2.2\text{ nF}$; $V_{PWMO} = 1\text{ V to }4\text{ V}$	PRQ-111
PWMO Gate driver fall time	$t_{F,PWMO}$	150	375	600	ns	¹⁾ $C_{gate} = 2.2\text{ nF}$; $V_{PWMO} = 4\text{ V to }1\text{ V}$	PRQ-112
PWMO Gate driver supply voltage	V_{PWMO}	4.8	5	5.2	V	–	PRQ-113

¹⁾ Not subject to production test, specified by design

7 Analog dimming

The analog dimming feature allows further control of the output current. This approach is used to:

- Reduce the default current in a narrow range to adjust to different binning classes of the used LEDs
- Adjust the load current to enable the usage of one hardware for several LED types where different current levels are required
- Reduce the current at high temperatures (protect LEDs from overtemperature)
- Reduce the current at low input voltages (for example, cranking-pulse breakdown of the supply or power derating)

7.1 Description

The analog dimming feature is adjusting the average load current level via the control of the feedback error amplifier voltage ($V_{FBH-FBL}$).

The SET pin is used to adjust the mean output current/voltage. The V_{SET} range where analog dimming is enabled is from 200 mV to 1.5 V.

Different application scenarios are described in [Figure 22](#).

Using the SET pin to adjust the output current:

For the calculation of the output current I_{OUT} the following equation is used:

$$I_{OUT} = \frac{V_{FBH-FBL}}{R_{FB}} \quad (8)$$

A decrease of the average output current can be achieved by controlling the voltage at the SET pin (V_{SET}) between 0.2 V and 1.4 V. The mathematical relation is given in the formula below:

$$I_{OUT} = \frac{V_{SET} - 200mV}{R_{FB} \cdot 8} \quad (9)$$

If V_{SET} is 200 mV (typ.) the LED current is only determined by the internal offset voltages of the comparators. To assure the switching activity is stopped and $I_{OUT} = 0$, V_{SET} has to be < 100 mV.

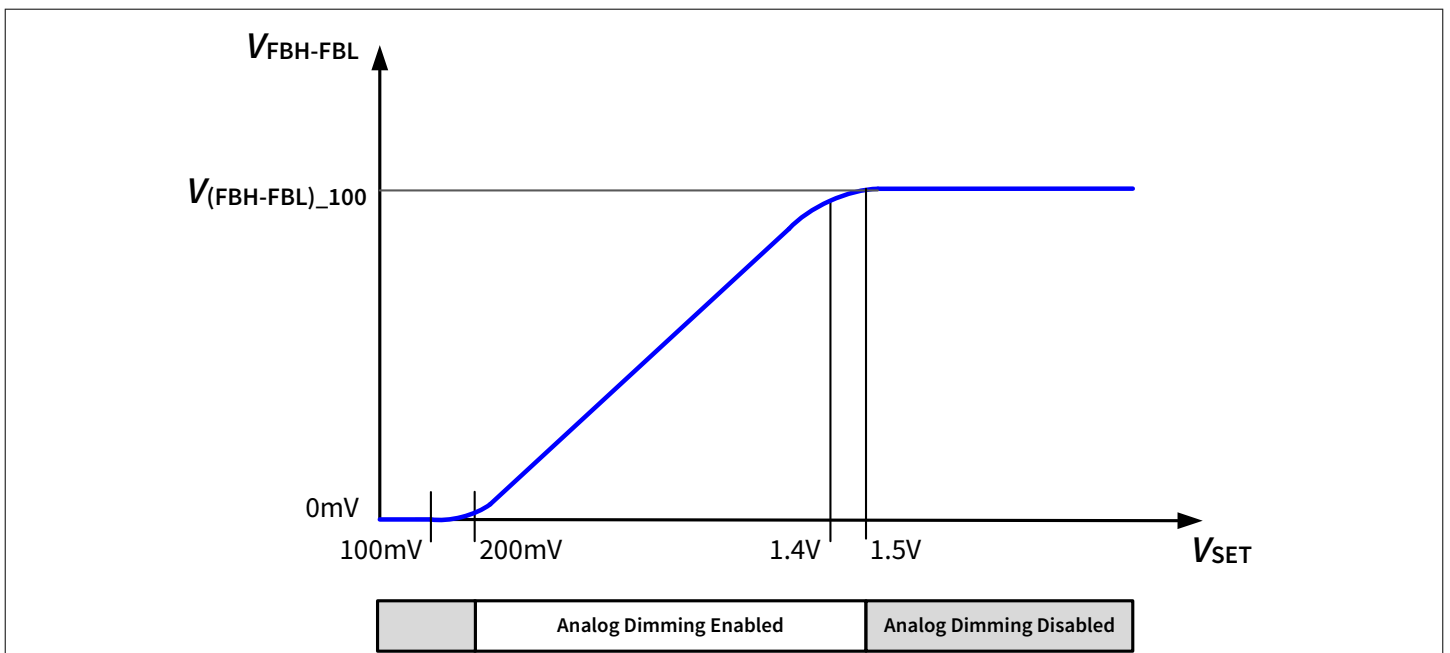


Figure 21 Analog dimming overview

Multi-purpose usage of the analog dimming feature

1. A μC integrated digital analog converter (DAC) output or a stand alone DAC can be used to supply the SET pin of the TLD5191ES.
2. The usage of an external resistor divider connected between IVCC, SET and GND can be chosen for systems without μC on board. The concept allows control of the LED current by placing low power resistors.
3. Furthermore a temperature sensitive resistor (thermistor) to protect the LED loads from thermal destruction can be connected.
4. If the analog dimming feature is not needed, the SET pin should be connected to the IVCC pin.
5. Instead of a DAC, the μC can provide a PWM signal and an external R-C filter to produce a constant voltage for the analog dimming. The voltage level depends on the duty cycle which can be controlled by the μC software after reading the coding resistor placed on the LED module.

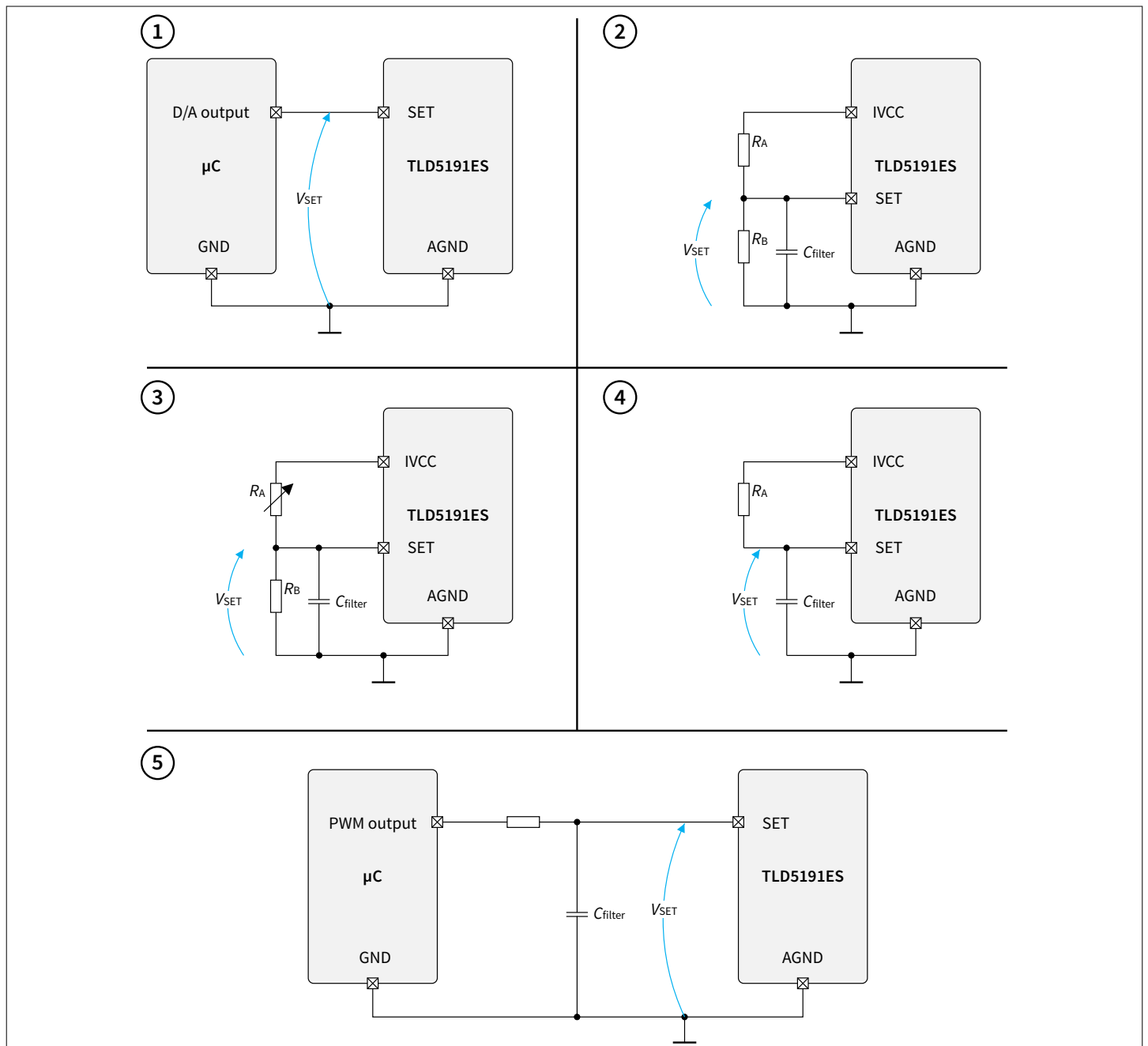


Figure 22 Different use cases for analog dimming pin SET

7.2 Electrical characteristics

Table 9 Electrical characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Source current on SET pin	I_{SET_source}	–	–	1	μA	¹⁾ $V_{SET} = 0.2 V$ to $1.4 V$	PRQ-114

¹⁾ Not subject to production test, specified by design

8 Linear regulator

The TLD5191ES features an integrated voltage regulator for the supply of the internal gate driver stages.

8.1 IVCC description

Internal linear voltage regulator supplies the internal gate drivers with a typical voltage of 5 V and current up to I_{LIM} . An external output capacitor with low ESR is required on pin IVCC for stability and buffering transient load currents. During normal operation the external MOSFET switches will draw transient currents from the linear regulator and its output capacitor. Proper sizing of the output capacitor must be considered to supply sufficient peak current to the gate of the external MOSFET switches. A minimum capacitance value is given in parameter C_{IVCC} .

Integrated undervoltage protection for the external switching MOSFET

An integrated undervoltage reset threshold circuit monitors the linear regulator output voltage. If the voltage on IVCC pin falls below $V_{IVCC_RTH,d}$ the gate drivers are turned OFF.

The undervoltage reset threshold for the IVCC pin helps to protect the external switches from excessive power dissipation by ensuring the gate drive voltage is sufficient to enhance the gate of the external logic level n-channel MOSFETs.

8.2 Electrical characteristics

Table 10 Electrical characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Output voltage	V_{IVCC}	4.8	5	5.2	V	$V_{VIN} = 13.5 V$; $0.1 mA \leq I_{IVCC} \leq 50 mA$	PRQ-134
Output current limitation	I_{LIM}	70	90	110	mA	¹⁾ $V_{IVCC} = 4 V$	PRQ-135
Drop out voltage	V_{DR}	–	200	350	mV	$V_{VIN} = 5 V$; $I_{IVCC} = 10 mA$	PRQ-136
IVCC buffer capacitor	C_{IVCC}	10	–	–	μF	^{1) 2)}	PRQ-137
IVCC undervoltage reset switch OFF threshold	$V_{IVCC_RTH,d}$	3.7	3.9	4.1	V	³⁾ V_{IVCC} decreasing	PRQ-138
IVCC undervoltage hysteresis	V_{IVCC_HYST}	0.31	0.34	0.37	V	V_{IVCC} increasing;	PRQ-139

¹⁾ not subject to production test, specified by design

²⁾ minimum value given is needed for regulator stability; application might need higher capacitance than the minimum. Use capacitors with LOW ESR

³⁾ selection of external switching MOSFET is crucial and the $V_{IVCC_RTH,d}$ min, as worst case the threshold voltage of MOSFET must be considered

9 Protection and diagnostic functions

9.1 Description

The TLD5191ES has integrated circuits to diagnose and protect against overvoltage, short circuits of the load and overtemperature faults.

In IDLE state only the overtemperature shut-down is reported according to specifications.

In [Figure 23](#) a summary of the protection, diagnostic and monitor functions is displayed.

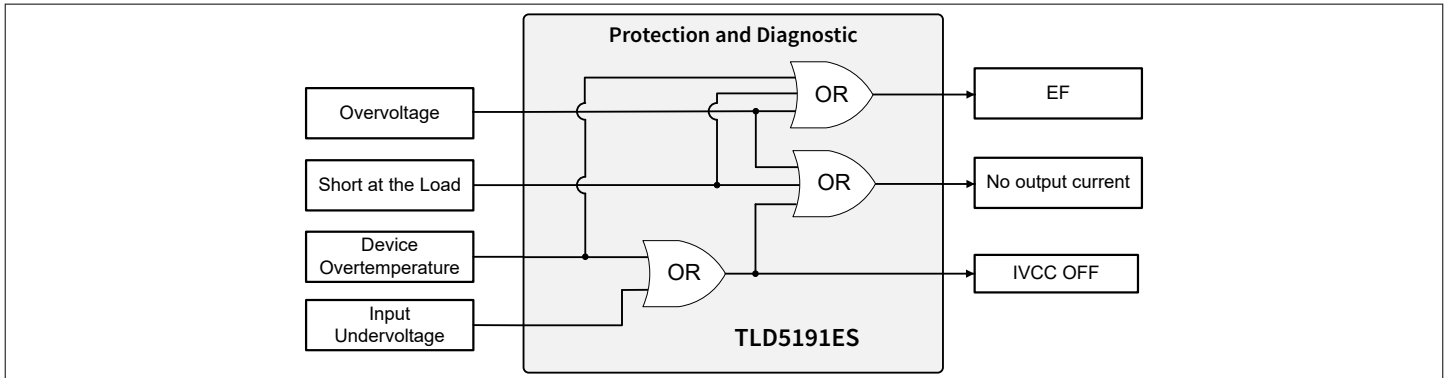


Figure 23 Protection and diagnostic overview - TLD5191ES

9.2 Output overvoltage, short circuit protection

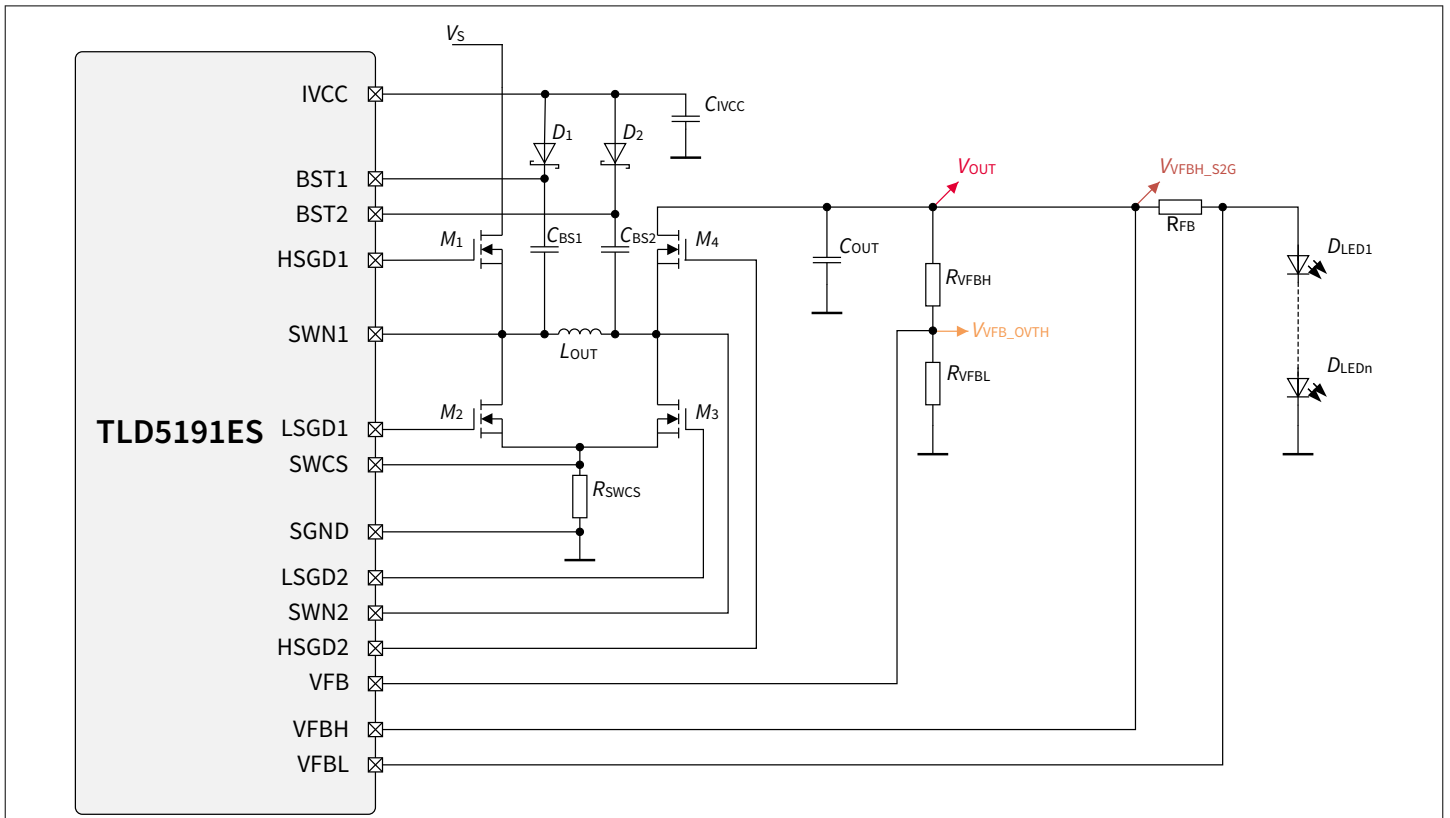


Figure 24 Protections pins - overview

9.2.1 Short circuit protection

The device detects a short circuit at the output if this condition is verified:

- The pin V_{FBH} falls below the threshold voltage $V_{VFBH_S2G_dec}$ for at least t_{S2G_mask} .

During the rising edge of the soft-start the short circuit detection is ignored until $V_{SOFT_START_LOFF}$.

The TLD5191ES provides an open-drain status pin, EF, which pulls low when the short circuit is detected.

In case of short circuit detection, the SOFT START pin is used to implement a fault mask and wait-before-retry time, on rising and falling edge respectively. See [Figure 8](#) for more details.

Note: If the short circuit condition disappears, the device will re-start with the soft start routine as described in [Chapter 5.2](#).

9.2.2 Overvoltage protection

TLD5191ES integrates an output overvoltage protection by monitoring the voltage on the VFB pin.

A voltage divider between VOUT, VFB pin and AGND is used to adjust the overvoltage protection threshold.

To fix the overvoltage protection threshold the following equation is used:

$$V_{OUT_OV_protected} = V_{VFB_OVTH} \cdot \frac{R_{VFBH} + R_{VFB L}}{R_{VFB L}} \quad (10)$$

An overvoltage event is detected when $V_{VFB} > V_{VFB_OVTH}$ and the device reacts as described below:

- Switching activity is disabled
- Mosfet M_1 , M_3 and M_4 are kept OFF while mosfet M_2 is kept ON to discharge the inductor current to the output

Once the voltage $V_{VFB} < V_{VFB_OVTH} - V_{VFB_OVTH,HYS}$ the switching activity is resumed.

In case of overvoltage event at the output, the open-drain status pin EF will toggle to LOW. After the overvoltage event disappeared the device will auto restart and the status pin EF will toggle to HIGH.

Note: During the overvoltage event the inductor current is discharged to the output, thus an output voltage increase may be observed based on the L_{OUT} and C_{OUT} design. The overvoltage threshold must be designed to avoid to exceed the device maximum absolute ratings.

9.3 Device temperature monitoring

A temperature sensor is integrated on the chip. The temperature monitoring circuit compares the measured temperature to the shutdown threshold.

If the internal temperature sensor reaches the shut-down temperature $T_{J,SD}$, the IVCC regulator is shut down and the gate driver outputs are set to LOW.

The device exits from thermal shutdown condition with a soft start routine after the temperature measured by the integrated sensor decreases below $T_{J,SD} - T_{J,SD,hyst}$.

The TLD5191ES provides an open-drain status pin, EF, which pulls low when the shut-down temperature is reached.

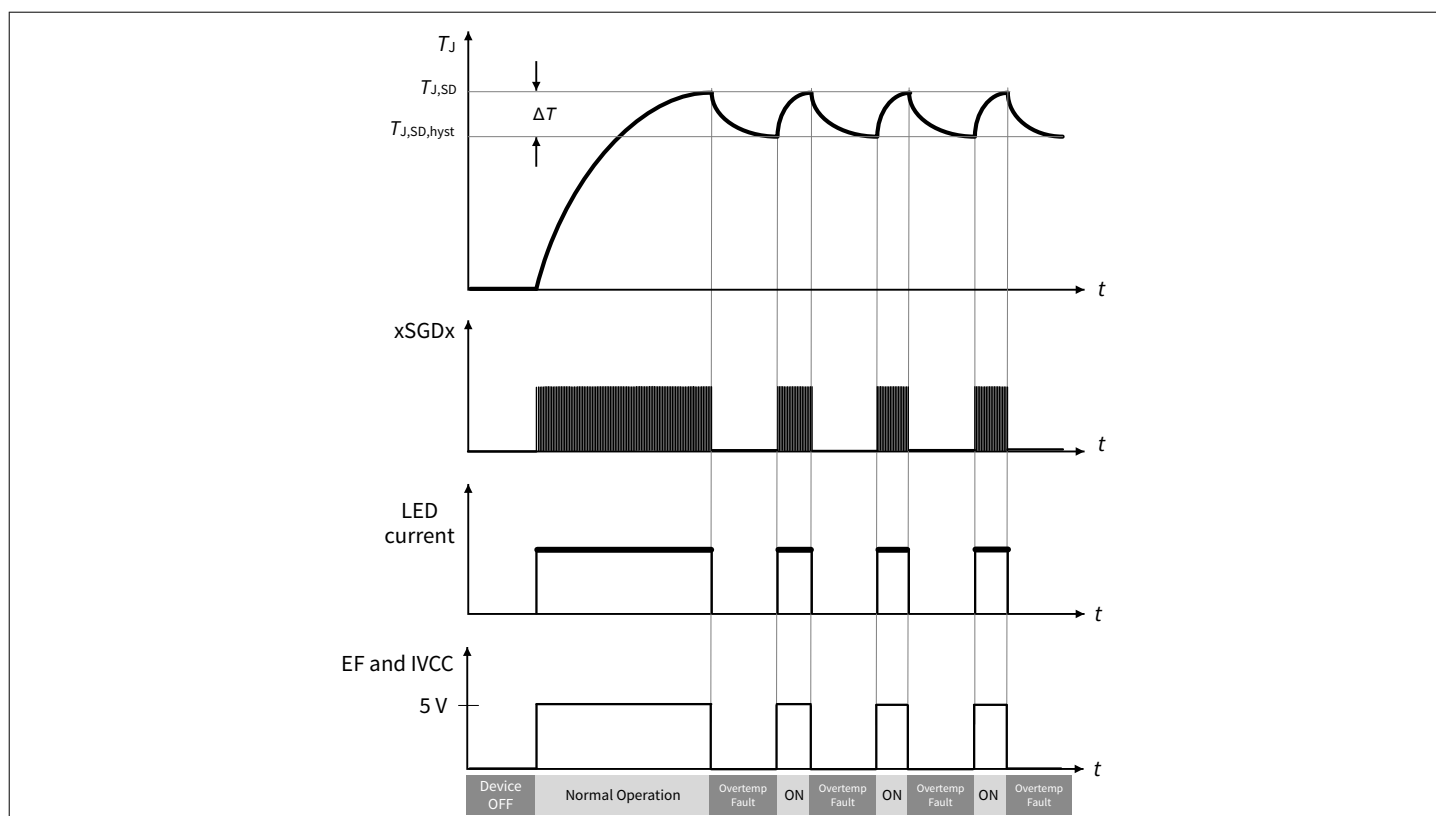


Figure 25 Device overtemperature protection behavior

9.4 Electrical characteristics

Table 11 Electrical characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Short to GND exit threshold	$V_{FBH_S2G_inc}$	1.9	2	2.15	V	V_{FBH} increasing	PRQ-127
Short to GND entry threshold	$V_{FBH_S2G_dec}$	1.65	1.75	1.85	V	V_{FBH} decreasing	PRQ-128
Short to GND masking time	t_{S2G_mask}	–	42	50	μs	1)	PRQ-203
Over temperature shutdown	$T_{J,SD}$	160	175	190	$^{\circ}C$	1)	PRQ-129
Over temperature shutdown hysteresis	$T_{J,SD,hyst}$	–	10	–	$^{\circ}C$	1)	PRQ-130
VFB over voltage feedback threshold	V_{VFB_OVTH}	1.42	1.46	1.50	V	–	PRQ-131
Output over voltage feedback hysteresis	$V_{VFB_OVTH,HYS}$	25	40	58	mV	Output Voltage decreasing	PRQ-132

(table continues...)

Table 11 (continued) Electrical characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
EF pin output impedance	R_{EF}	–	2.1	–	k Ω	¹⁾ Fault Condition $I = 100 \mu A$	PRQ-133

¹⁾ specified by design; not subject to production test

Note: Integrated protection functions are designed to prevent IC destruction under fault conditions described in the datasheet. Fault conditions are considered as “outside” normal operating range. Protection functions are not designed for continuous repetitive operation.

10 Infineon FLAT SPECTRUM feature

10.1 Description

The Infineon FLAT SPECTRUM feature has the target to minimize external additional filter circuits.

10.2 Spread spectrum

The spread spectrum modulation technique significantly improves the lower frequency range of the spectrum ($f < 30$ MHz).

By using the spread spectrum technique, it is possible to optimize the input filter only for the peak limits, and also pass the average limits (average emission limits are -20 dB lower than the peak emission limits). By using spread spectrum, the need for low ESR input capacitors is relaxed because the input capacitor series resistor is important for the low frequency filter characteristic. This can be an economic benefit if there is a strong requirement for average limits.

The TLD5191ES features a built in spread spectrum function always activated with modulation frequency f_{FM} and a frequency deviation f_{dev} .

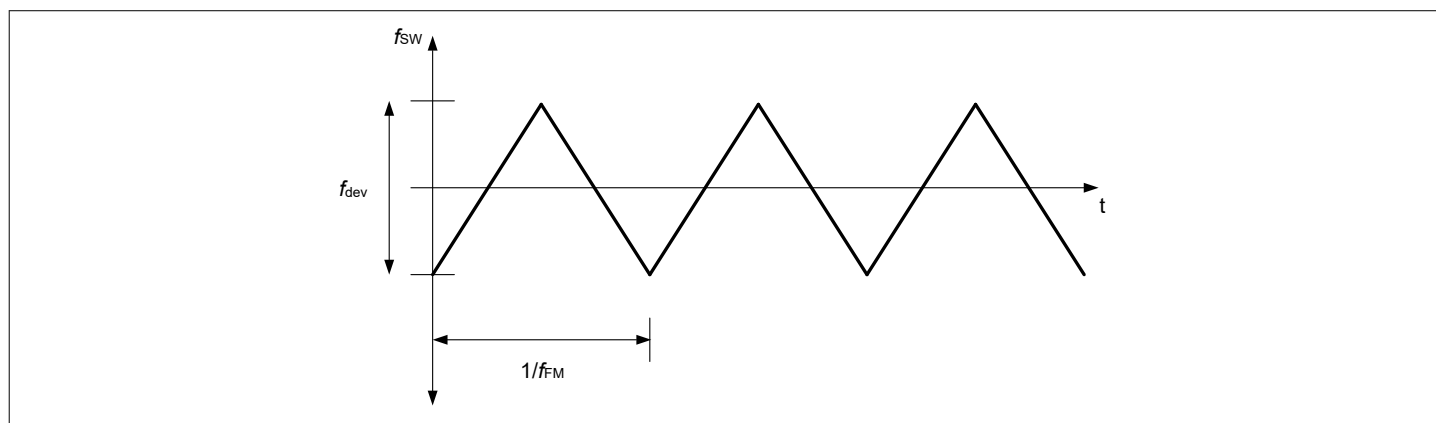


Figure 26 Spread spectrum overview

10.3 Electrical characteristics

Table 12 Electrical Characteristics

$V_{IN} = 8V$ to $36V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$, all voltages with respect to ground, positive current flowing into pin; (unless otherwise specified)

Parameter	Symbol	Values			Unit	Note or condition	P-Number
		Min.	Typ.	Max.			
Frequency deviation	f_{dev}	-	± 20	-	%	1)	PRQ-140
Frequency modulation	f_{FM}	-	12	-	kHz	1)	PRQ-141

1) specified by design; not subject to production test

11 Application information

Note: The following information is given as a hint for the implementation of the device only and shall not be regarded as a description or warranty of a certain functionality, condition or quality of the device.

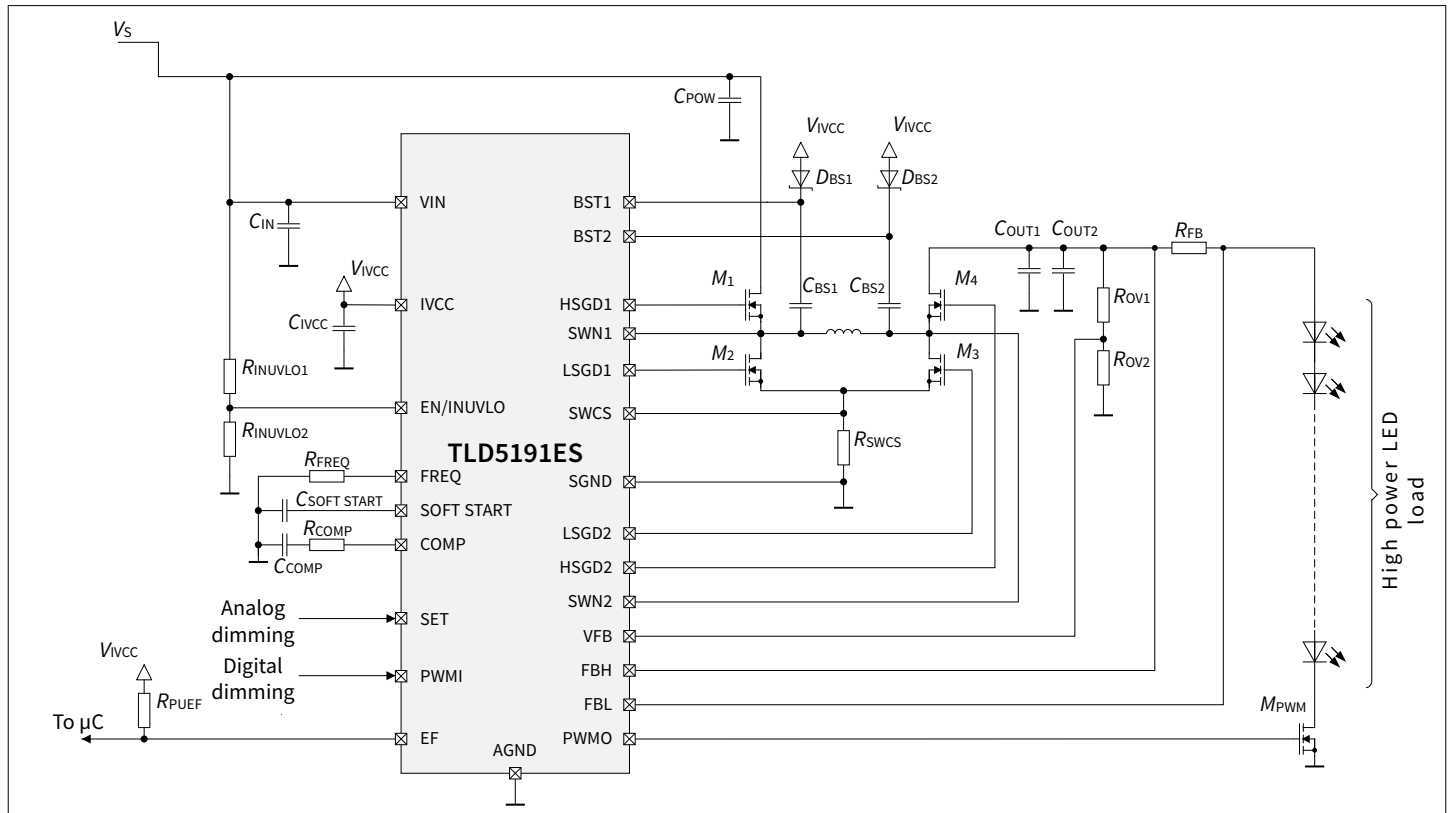


Figure 27 Application drawing - TLD5191ES as current regulator

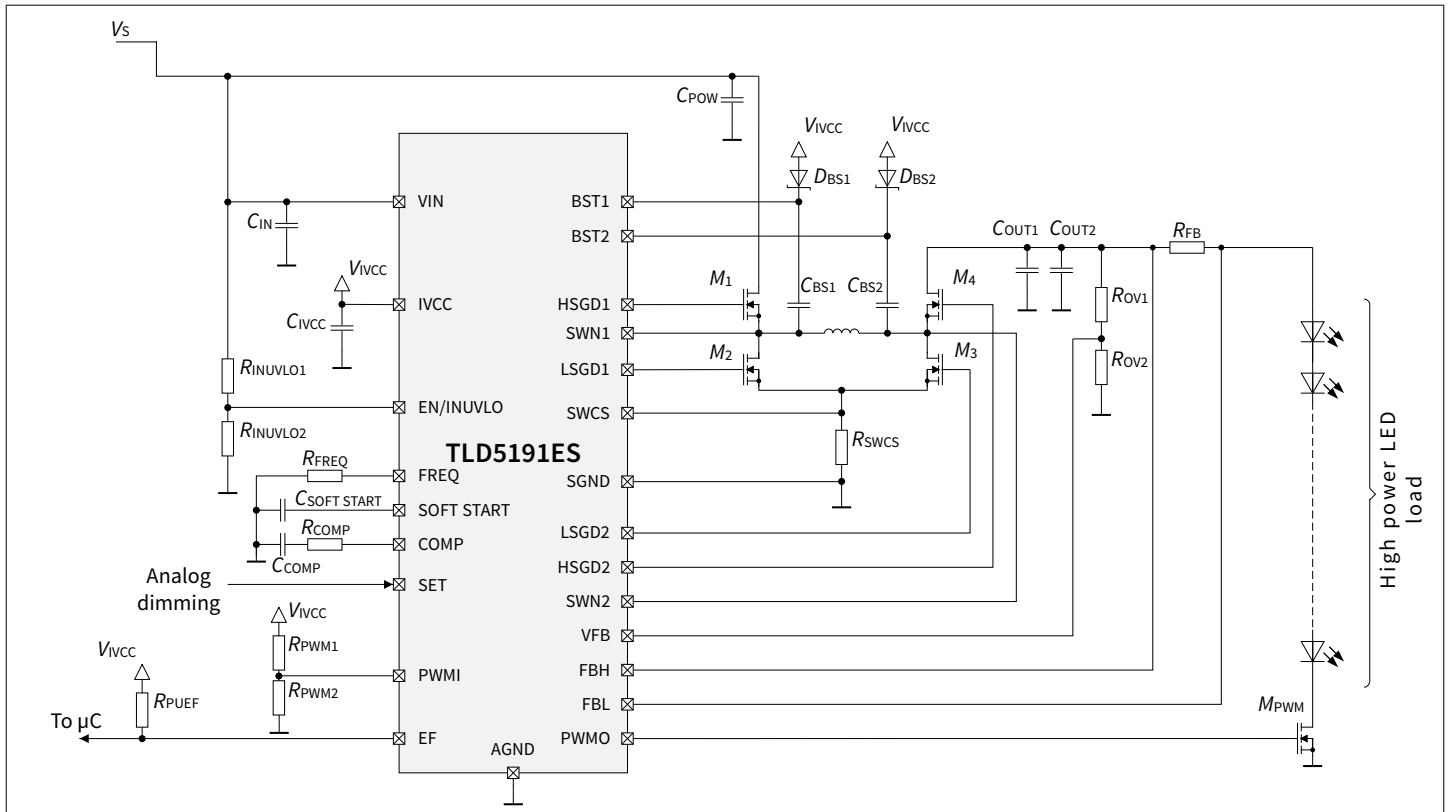


Figure 28 Application drawing - TLD5191ES as current regulator with PWM engine

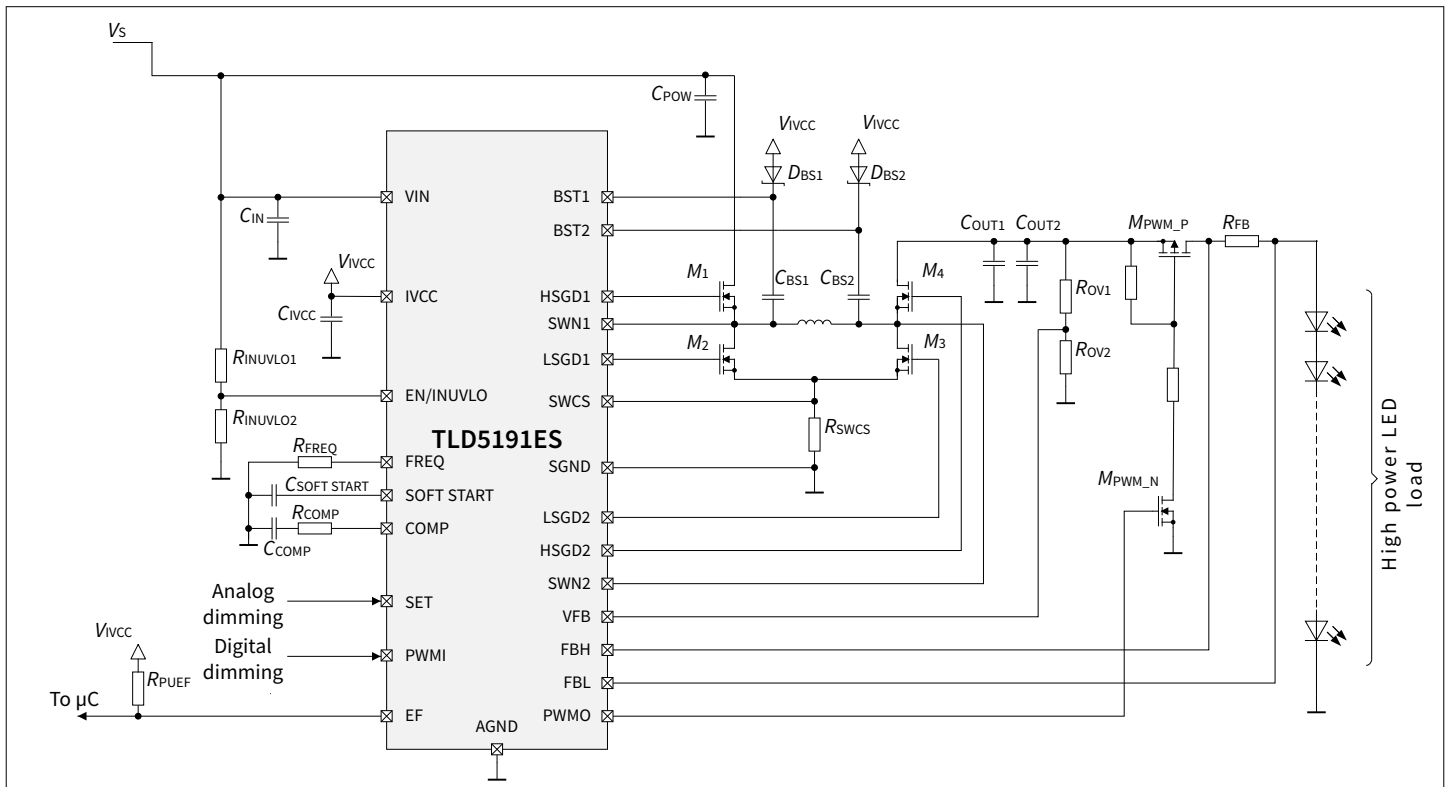


Figure 29 Application drawing - TLD5191ES as current regulator with dimming PMOS

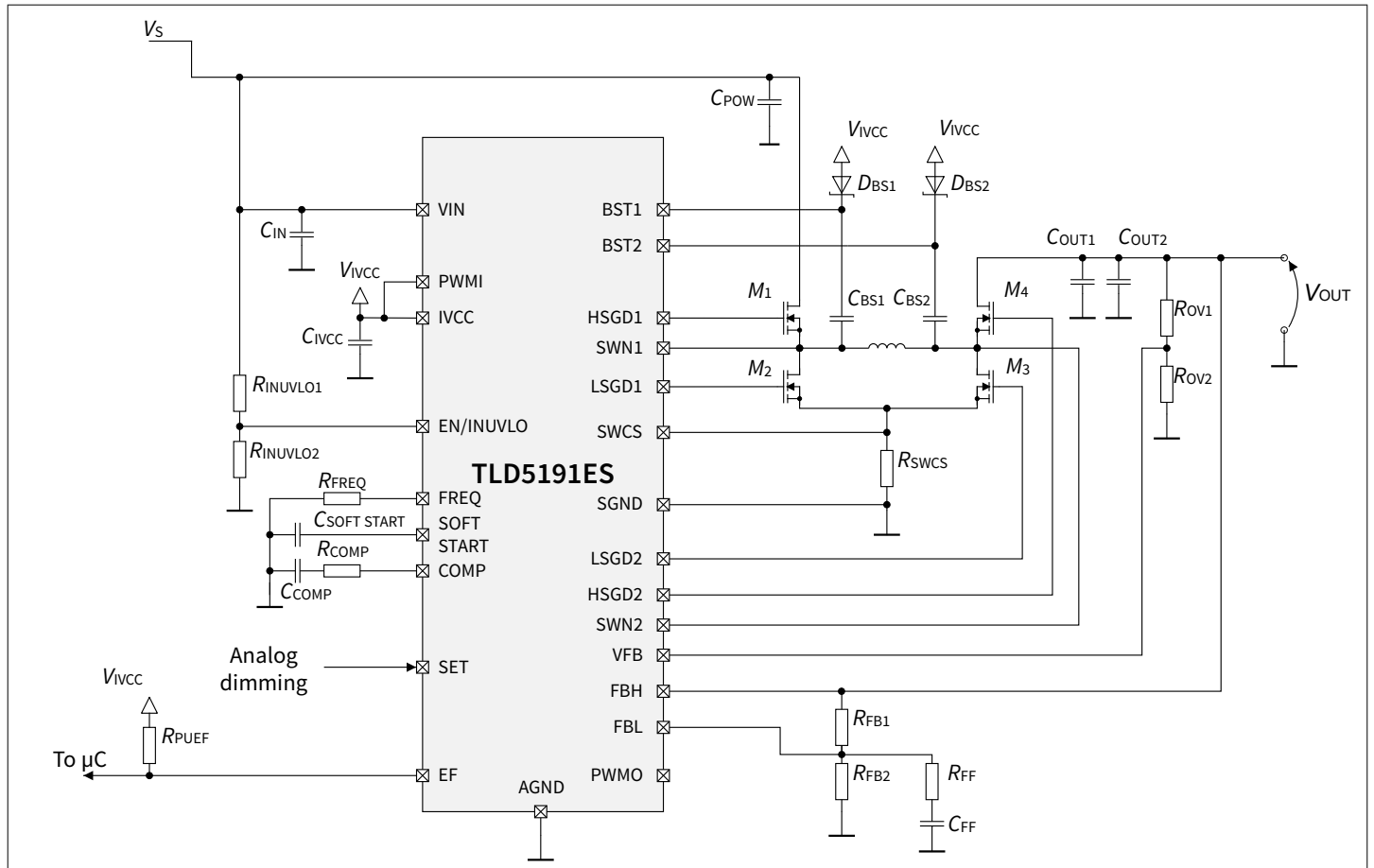


Figure 30 Application drawing - TLD5191ES voltage mode

Revision history

Document version	Date of release	Description of changes
Rev.1.00	2022-02-18	Datasheet release

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