

# 1.5 GHz to 2.5 GHz QUADRATURE MODULATOR

# FEATURES

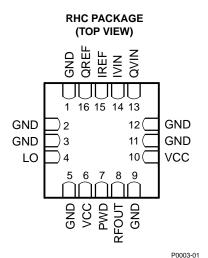
- 71 dBc Single-Carrier WCDMA ACPR at -14-dBm Channel Power
- P1dB of 7 dBm
- Typical Unadjusted Carrier Suppression 35 dBc at 2 GHz
- Typical Unadjusted Sideband Suppression 35 dBc at 2 GHz
- Very Low Noise Floor
- Differential or Single-Ended I, Q Inputs
- Convenient Single-Ended LO Input
- Silicon Germanium Technology

## **APPLICATIONS**

- Cellular Base Transceiver Station Transmit Channel
- IF Sampling Applications
- TDMA: GSM, IS-136, EDGE/UWC-136
- CDMA: IS-95, UMTS, CDMA2000
- Wireless Local Loop
- Wireless LAN IEEE 802.11
- LMDS, MMDS
- Wideband Transceivers

## DESCRIPTION

The TRF3702 is an ultralow-noise direct quadrature modulator that is capable of converting complex input signals from baseband or IF directly up to RF. An internal analog combiner sums the real and imaginary components of the RF outputs. This combined output can feed the RF preamp at frequencies of up to 2.5 GHz. The modulator is implemented as a double-balanced mixer. An internal local oscillator (LO) phase splitter accommodates a single-ended LO input, eliminating the need for a costly external balun.



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

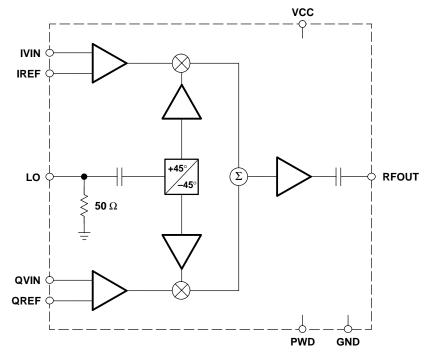


This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

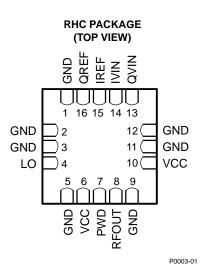
**AVAILABLE OPTIONS** 

T <sub>A</sub> 4-mm × 4-mm 16-Pin RHC (QFN) Package			
–40°C to 85°C	TRF3702IRHC		
	TRF3702IRHCR (Tape and reel)		



FUNCTIONAL BLOCK DIAGRAM

B0002-01



#### **TERMINAL FUNCTIONS**

TERMINAL		I/O	DESCRIPTION	
NAME	NO.	10	DESCRIPTION	
GND	1, 2, 3, 5, 9, 11, 12		Ground	
IREF	15	Ι	In-phase (I) reference voltage/differential input	
IVIN	14	Ι	In-phase (I) signal input	
LO	4	Ι	Local oscillator input	
PWD	7	Ι	Power down	
QREF	16	Ι	Quadrature (Q) reference voltage/differential input	
QVIN	13	Ι	Quadrature (Q) signal input	
RFOUT	8	0	RF output	
VCC	6, 10		Supply voltage	

#### **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)<sup>(1)(2)</sup>

V <sub>CC</sub>	Supply voltage range	–0.5 V to 6 V
	LO input power level	10 dBm
	Baseband input voltage level (single-ended)	3 Vp-р
T <sub>A</sub>	Operating free-air temperature range	–40°C to 85°C
	Lead temperature for 10 seconds	260°C

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Measured with respect to ground



## **RECOMMENDED OPERATING CONDITIONS**

		MIN	NOM	MAX	UNIT
Supp	lies and References				
$V_{CC}$	Analog supply voltage	4.5	5	5.5	V
	VCM (IVIN, QVIN, IREF, QREF input common-mode voltage)		3.7		V
	Local Oscillator (LO) Input	-	·		
	Input frequency	1500		2500	MHz
	Power level (measured into 50 $\Omega$ )	-6	0	6	dBm
	Signal Inputs (IVIN, QVIN)				
	Input bandwidth		700		MHz

# **ELECTRICAL CHARACTERISTICS**

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V,  $f_{LO}$  = 2140 MHz at 0 dBm,  $T_A$  = 25°C (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
Power Supply	·	•				
L Total averable average	V(PWD) = 5 V		145	170		
I <sub>CC</sub> Total supply current	V(PWD) = 0 V		13	30	mA	
Turnon time			120		ns	
Turnoff time			20		ns	
Power-down input impedance			11		kΩ	
Local Oscillator (LO) Input						
Input impedance <sup>(1)</sup>			27 + j8		Ω	
Signal Inputs (IVIN, QVIN, IREF, QRE	EF)	1 i				
Input bias current	I, Q = VCM = 3.7 V (all inputs tied to VCM)		16		μA	
	Single-ended input		260		kO	
Input impedance	Differential input		130		kΩ	

(1) For a listing of impedances at various frequencies, see Table 1.

# Table 1. RFOUT and LO Pin Impedance

Frequency (MHz)	Z (RFOUT Pin)	Z (LO Pin)
1500	31 – j 4.7	31.7 – j 8.8
1600	30.9 – j 0.3	29.3 – j 6.2
1700	29.3 + j 3.1	27.3 - j 3.1
1800	27.9 + j 7.2	26.5 – j 0.17
1900	27.6 + j 13	26.1+ – j 2.7
2000	29.4 +j 19.8	26.5 + j 5.4
2100	34.6 + j 27.2	27 + j 7.6
2200	44.2 + j 33	28 + j 9.5
2300	60 + j 33.6	29 + j 10.6
2400	78 + j 21	29.5 + j 11
2500	82 – j 5.8	29.8 + j 12.2



## **RF OUTPUT PERFORMANCE**

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V, f<sub>LO</sub> = 1842 MHz at 0 dBm (unless otherwise specified)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Single	e and Two-Tone Specificatio	ns	•			
	Output power		-5	-2.5		dBm
	Second baseband harmonic (USB or LSB) <sup>(2)</sup>	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz		-50	-42	dBc
	Third baseband harmonic (USB or LSB) <sup>(2)</sup>			-57	-50	dBc
	IMD <sub>3</sub>	I, $Q^{(1)} = 1$ Vp-p (two-tone signal, $f_{BB1} = 928$ kHz, $f_{BB2} = 992$ kHz)		-59	-53	dBc
	P1dB (output compression point)			7		dBm
NSD	Noise spectral density	I, Q = VCM = 3.7 VDC (all inputs tied to VCM), 6-MHz offset from carrier		-155		dBm/Hz
		6-MHz offset from carrier, P <sub>out</sub> = 0 dBm, over temperature		-148.5	-146.5 <sup>(3)</sup>	
	RFOUT pin impedance <sup>(4)</sup>			28 + j8		Ω
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted		30		
	Carrier suppression	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, optimized		55		dBc
		I, $Q^{(1)} = 1$ Vp-p, $f_{BB} = 928$ kHz, over temperature <sup>(5)</sup>		44		
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted		35		
	Sideband suppression	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, optimized		55		dBc
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, over temperature <sup>(5)</sup>	-	47		

(1) I, Q = 1 Vp-p implies that the magnitude of the signal at each input pin IVIN, IREF, QVIN, QREF is equal to 500 mVp-p.

(2) USB = upper sideband. LSB = lower sideband.

(3) Maximum noise values are assured by statistical characterization only, not production testing. The values specified are over the entire temperature range,  $T_A = -40^{\circ}$ C to 85°C.

(4) For a listing of impedances at various frequencies, see Table 1.

(5) After optimization at room temperature. See the Definitions of Selected Specifications section.

## **RF OUTPUT PERFORMANCE**

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V, f<sub>LO</sub> = 1960 MHz at 0 dBm (unless otherwise specified)

	PARAMETER	TEST CONDITIONS	MIN TYP	MAX	UNIT
Single	e and Two-Tone Specificatio	ns	-		
	Output power		-3		dBm
	Second baseband harmonic (USB or LSB) <sup>(2)</sup>	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz	-50		dBc
	Third baseband harmonic (USB or LSB) <sup>(2)</sup>		-60		dBc
	IMD <sub>3</sub>	I, $Q^{(1)} = 1$ Vp-p (two-tone signal, $f_{BB1} = 928$ kHz, $f_{BB2} = 992$ kHz)	-59	-53	dBc
	P1dB (output compression point)		7		dBm
NSD	Noise spectral density	6-MHz offset from carrier, P <sub>out</sub> = 0 dBm, over temperature	-148	-146.5 <sup>(3)</sup>	dBm/Hz
	RFOUT pin impedance <sup>(4)</sup>		28 + j15		Ω
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted	33		dDa
	Carrier suppression	I, $Q^{(1)} = 1$ Vp-p, $f_{BB} = 928$ kHz, optimized	55		dBc
	Sideband suppression	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted	35		dBc
	Sideband suppression	I, $Q^{(1)} = 1$ Vp-p, $f_{BB} = 928$ kHz, optimized	55		UDC

(1) I, Q = 1 Vp-p implies that the magnitude of the signal at each input pin IVIN, IREF, QVIN, QREF is equal to 500 mVp-p.

(2) USB = upper sideband. LSB = lower sideband.

(4) For a listing of impedances at various frequencies, see Table 1.

<sup>(3)</sup> Maximum noise values are assured by statistical characterization only, not production testing. The values specified are over the entire temperature range,  $T_A = -40^{\circ}$ C to 85°C.

#### **RF OUTPUT PERFORMANCE**

Over recommended operating conditions, VCC = 5 V, VCM = 3.7 V, f<sub>LO</sub> = 2.1 GHz at 0 dBm (unless otherwise specified)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
Single	e and Two-Tone Specificatio	ns					
	Output power		-5	-3		dBm	
	Second baseband harmonic (USB or LSB) <sup>(2)</sup>			-50	-42	dBc	
	Third baseband harmonic (USB or LSB) <sup>(2)</sup>			-60	-51	dBc	
	IMD <sub>3</sub>	I, Q <sup>(1)</sup> = 1 Vp-p, fBB = 928 kHz (two-tone signal, f <sub>BB1</sub> = 928 kHz, f <sub>BB2</sub> = 992 kHz)		-55	-47	dBc	
	P1dB (output compression point)			7		dBm	
NSD	Noise spectral density	60-MHz offset from carrier, P <sub>out</sub> = 0 dBm, over temperature		-151	-148.5 <sup>(3)</sup>	dBm/Hz	
	WCDMA ACPR	Single carrier, channel power = -14 dBm		71		dBc	
	RFOUT pin impedance <sup>(4)</sup>		3	65 + j27		Ω	
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted		30			
	Carrier suppression	I, $Q^{(1)} = 1$ Vp-p, $f_{BB} = 928$ kHz, optimized		55		dBc	
		I, $Q^{(1)} = 1$ Vp-p, $f_{BB} = 928$ kHz, over temperature <sup>(5)</sup>		47			
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, unadjusted		37			
	Sideband suppression	I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, optimized		55		dBc	
		I, Q <sup>(1)</sup> = 1 Vp-p, f <sub>BB</sub> = 928 kHz, over temperature <sup>(5)</sup>		47			

(1) I, Q = 1 Vp-p implies that the magnitude of the signal at each input pin IVIN, IREF, QVIN, QREF is equal to 500 mVp-p.

(2) USB = upper sideband. LSB = lower sideband.

(3) Maximum noise values are assured by statistical characterization only, not production testing. The values specified are over the entire temperature range,  $T_A = -40^{\circ}$ C to 85°C.

(4) For a listing of impedances at various frequencies, see Table 1.

(5) After optimization at room temperature. See the Definitions of Selected Specifications section.

## THERMAL CHARACTERISTICS

	PARAMETER	CONDITION	NOM	UNIT
$R_{\thetaJA}$	Thermal resistace, junction to ambient	Soldered pad using four-layer JEDEC board with four thermal vias	42.8	°C/W
$R_{\theta JM}$	Thermal resistace, junction to mounting surface		24.8	°C/W
$R_{\thetaJC}$	Thermal resistace, junction to case	Soldered pad using two-layer JEDEC board with four thermal vias	67.6	°C/W

## **DEFINITIONS OF SELECTED SPECIFICATIONS**

#### **Unadjusted Carrier Suppression**

This specification measures the amount by which the local oscillator component is attenuated in the output spectrum of the modulator relative to the carrier. It is assumed that the baseband inputs delivered to the pins of the TRF3702 are perfectly matched to have the same dc offset (VCM). This includes all four baseband inputs: IVIN, QVIN, IREF and QREF. Unadjusted carrier suppression is measured in dBc.

#### Adjusted (Optimized) Carrier Suppression

This differs from the unadjusted suppression number in that the dc offsets of the baseband inputs are iteratively adjusted around their theoretical value of VCM to yield the maximum suppression of the LO component in the output spectrum. Adjusted carrier suppression is measured in dBc.



## **DEFINITIONS OF SELECTED SPECIFICATIONS (continued)**

#### **Unadjusted Sideband Suppression**

This specification measures the amount by which the unwanted sideband of the input signal is attenuated in the output of the modulator, relative to the wanted sideband. It is assumed that the baseband inputs delivered to the modulator input pins are perfectly matched in amplitude and are exactly 90° out of phase. Unadjusted sideband suppression is measured in dBc.

#### Adjusted (Optimized) Sideband Suppression

This differs from the unadjusted sideband suppression in that the baseband inputs are iteratively adjusted around their theoretical values to maximize the amount of sideband suppression. Adjusted sideband suppression is measured in dBc.

#### **Suppressions Over Temperature**

This specification assumes that the user has gone through the optimization process for the suppression in question, and set the optimal settings for the I, Q inputs at  $T_A = 25$ °C. This specification then measures the suppression when temperature conditions change after the initial calibration is done.

Figure 1 shows a simulated output and illustrates the respective definitions of various terms used in this data sheet. The graph assumes a baseband input of 50 kHz.

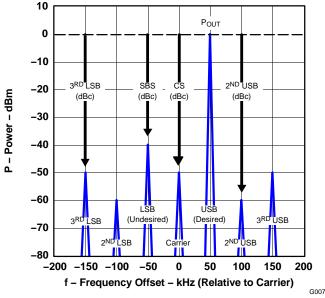
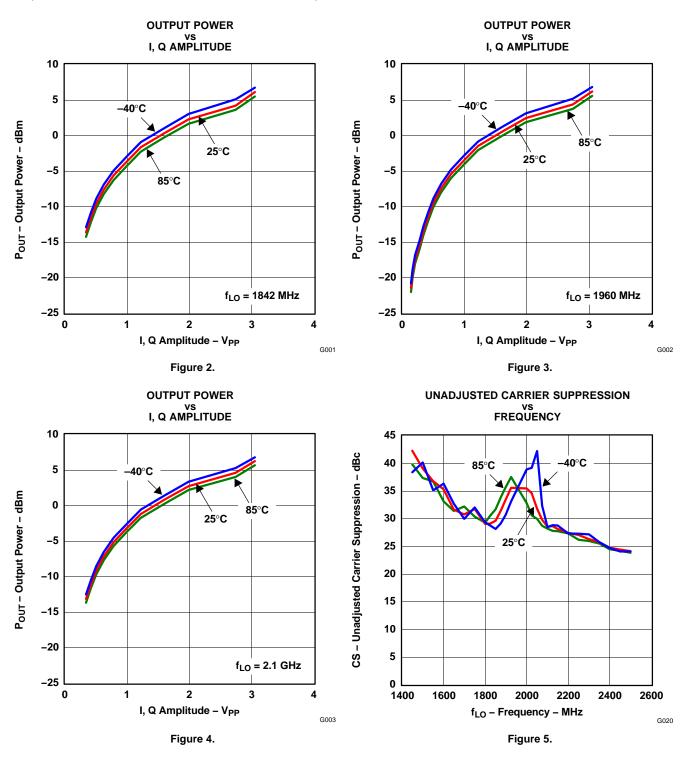
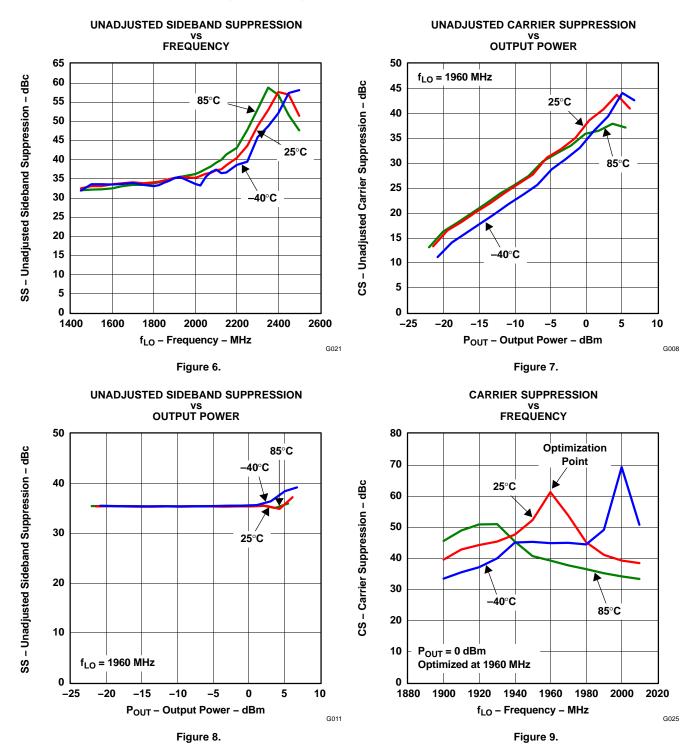


Figure 1. Graphical Illustration of Common Terms

## **TYPICAL CHARACTERISTICS**

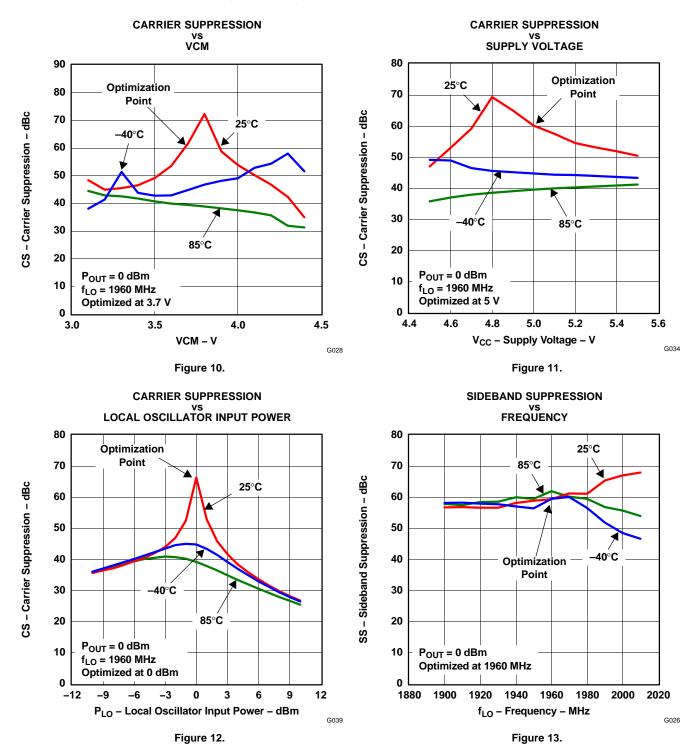
For all the performance plots in this section, the following conditions were used, unless otherwise noted: VCC = 5 V, VCM = 3.7 V, P<sub>LO</sub> = 0 dBm, I and Q inputs driven differentially at a frequency of 50 kHz. In the case of optimized suppressions, the point of optimization is noted and is always at nominal conditions and room temperature. A level of >50 dBc is assumed to be optimized.



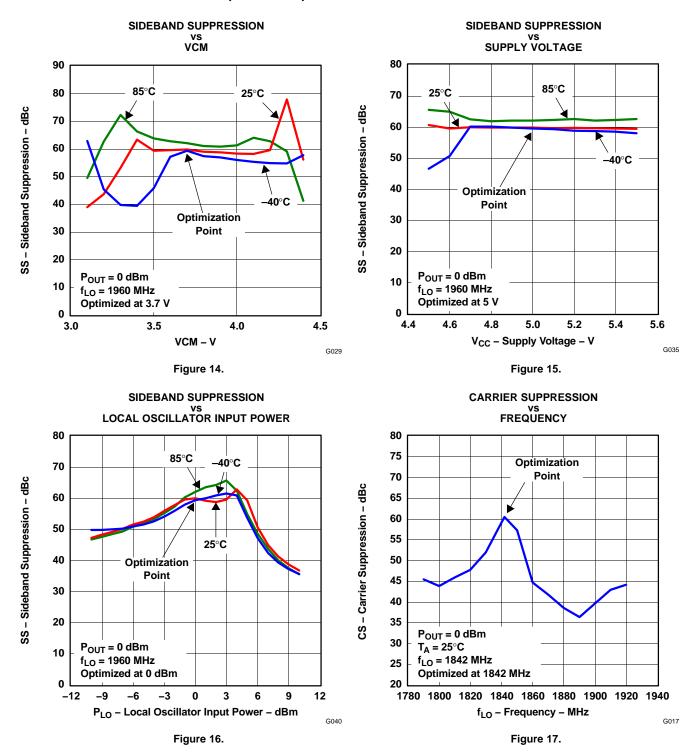






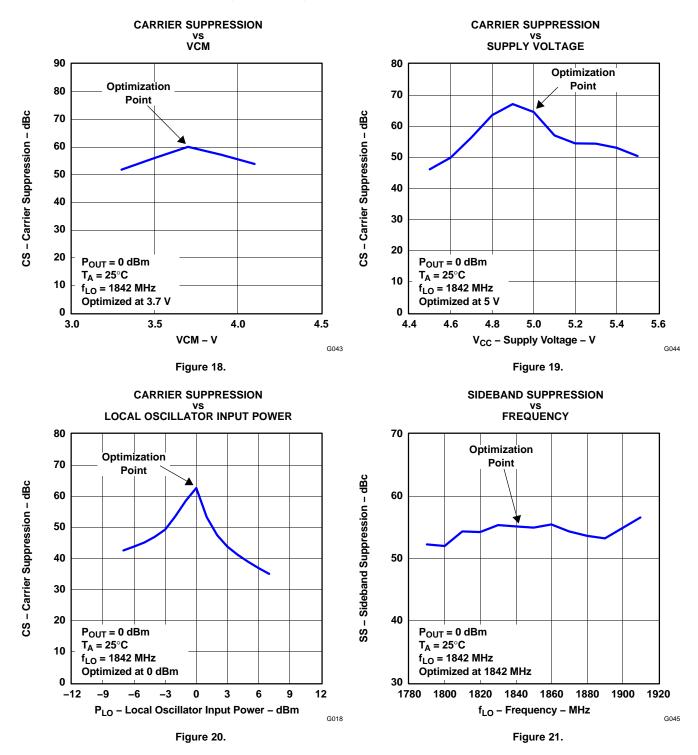




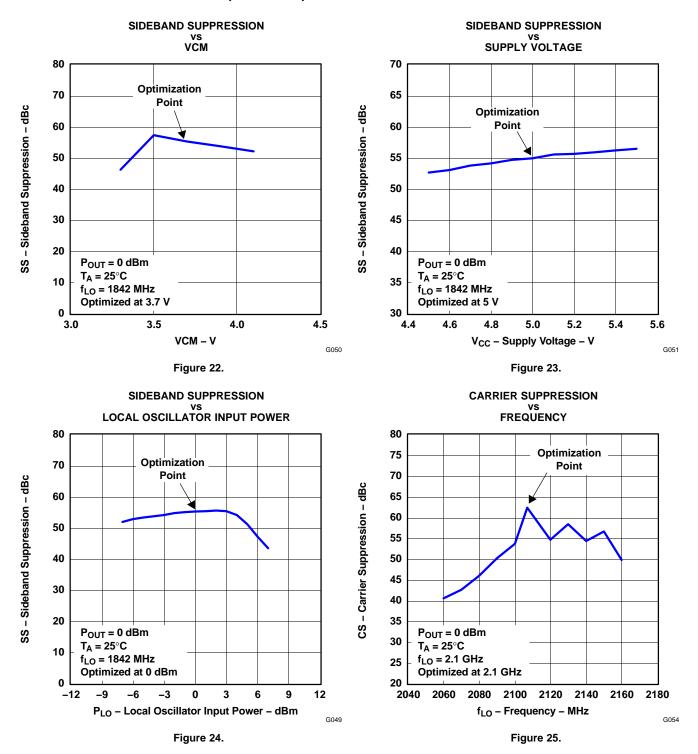






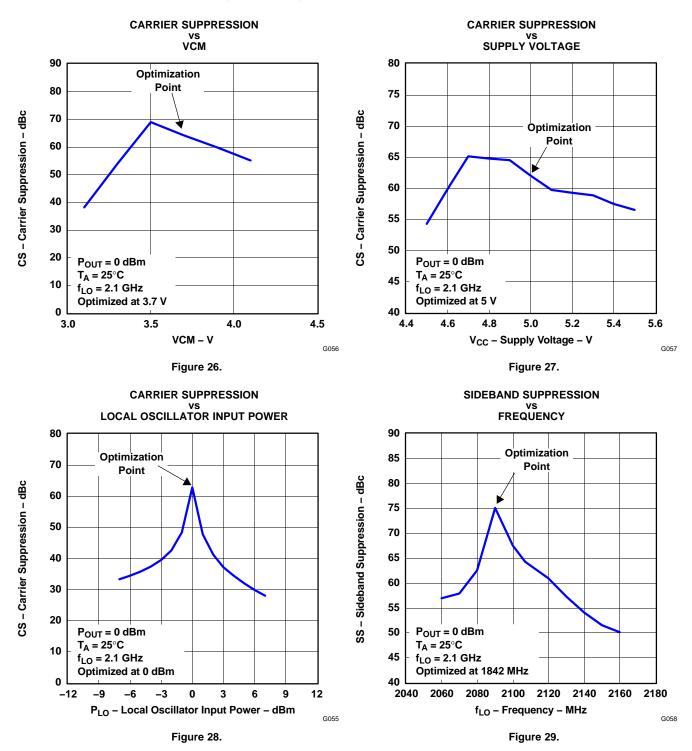






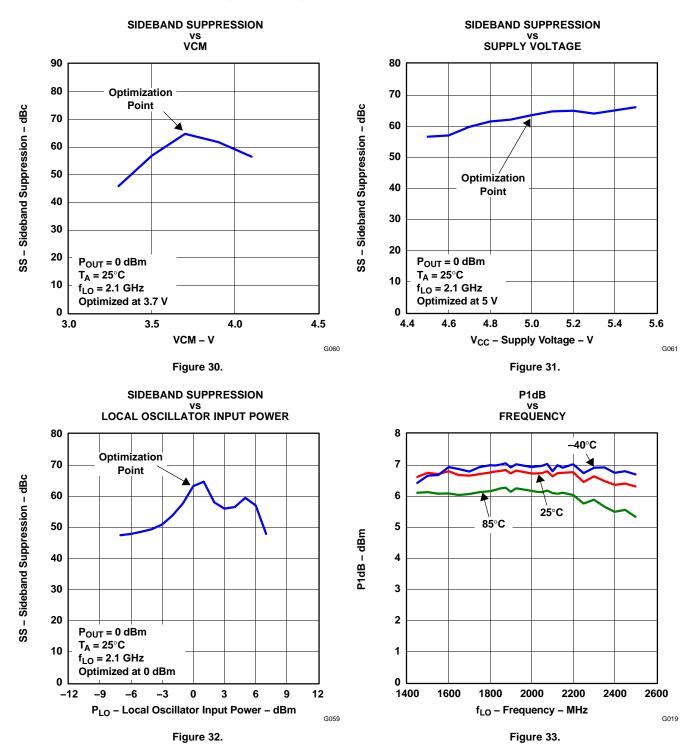




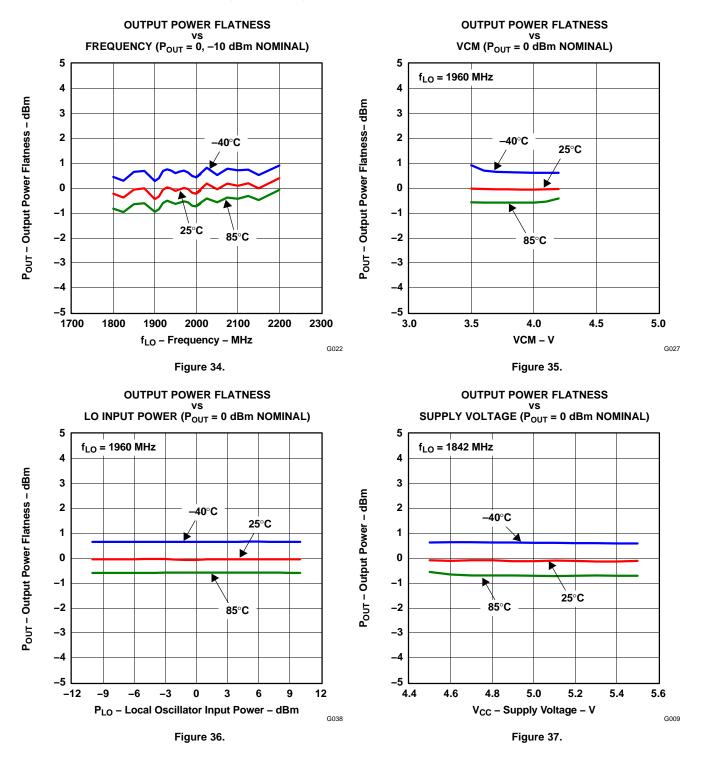


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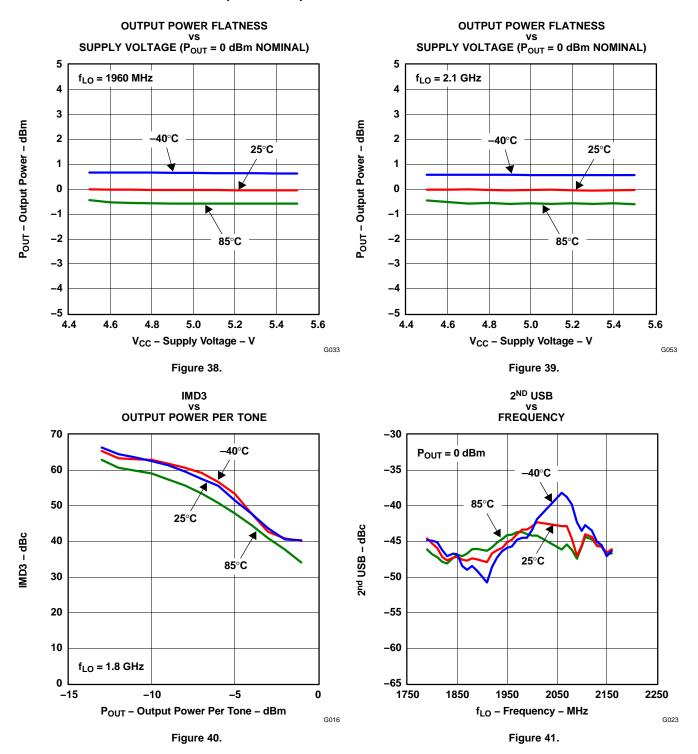




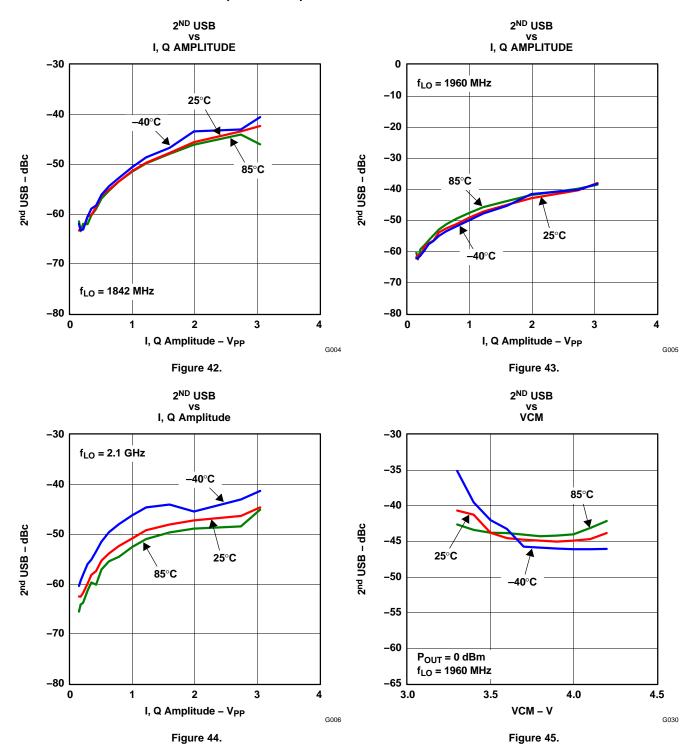
# TRF3702



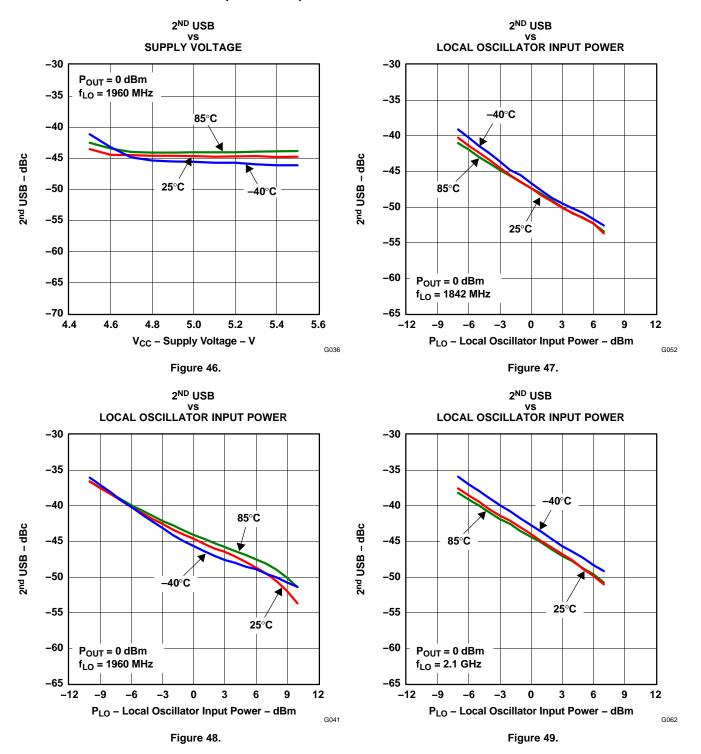
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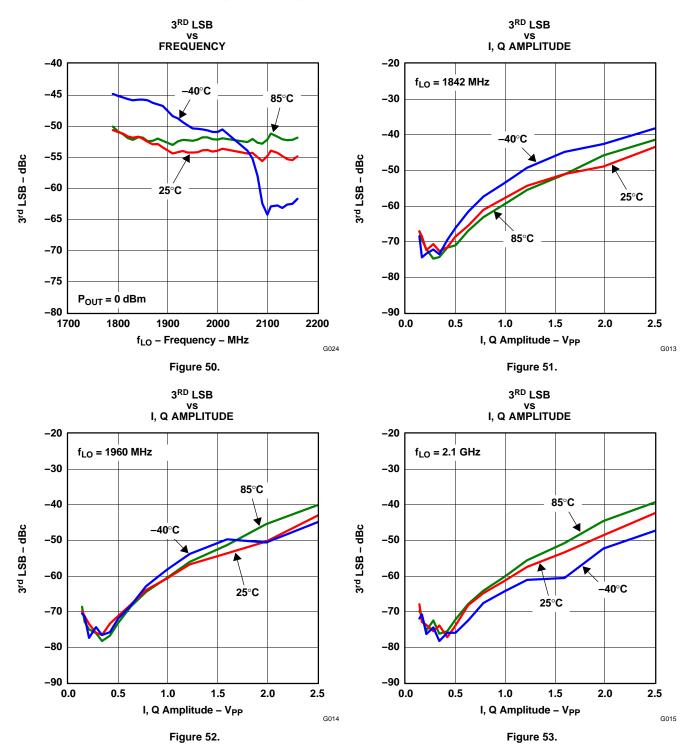






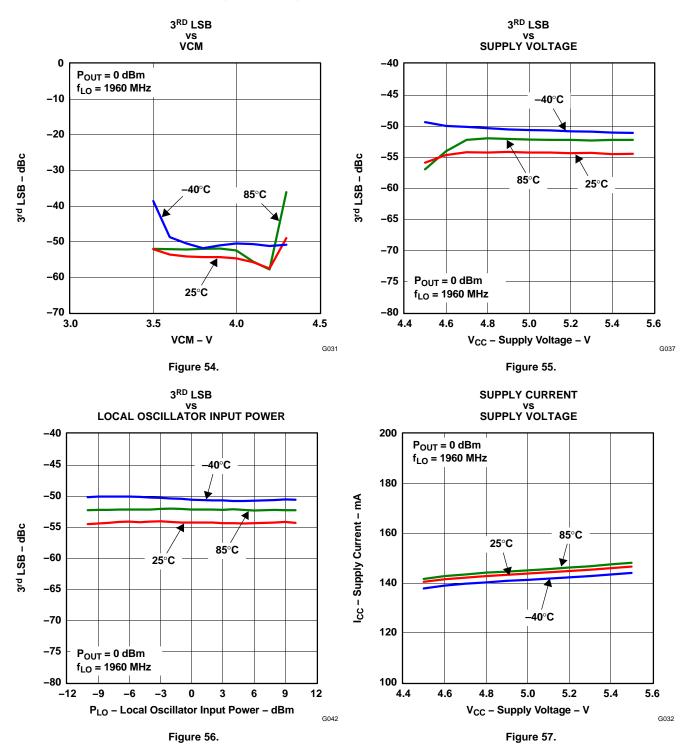




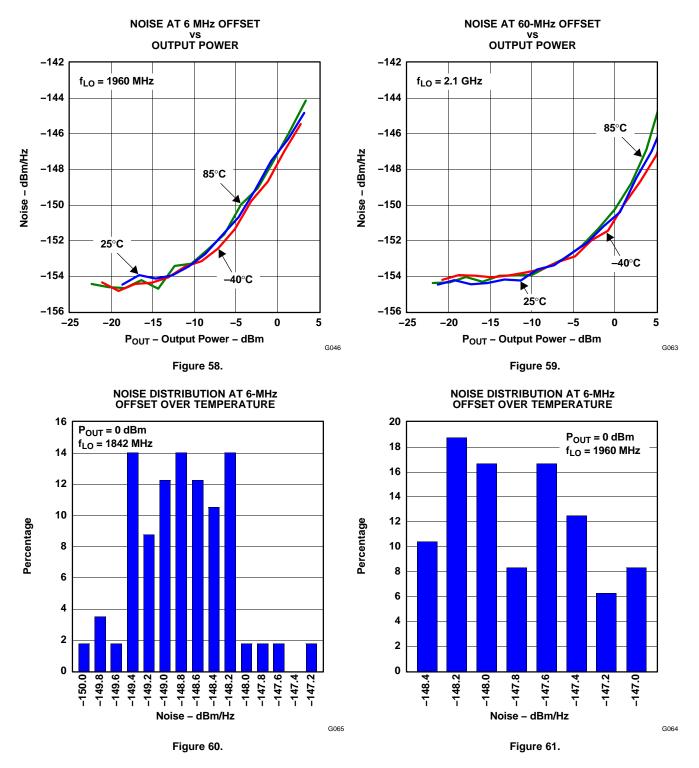


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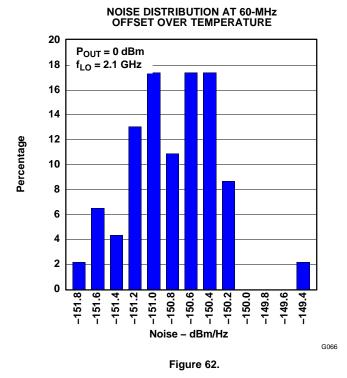
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## **TYPICAL CHARACTERISTICS (continued)**



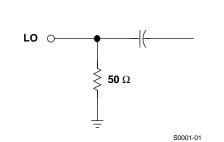
# THEORY OF OPERATION

The TRF3702 employs a double-balanced mixer architecture in implementing the direct I, Q upconversion. The I, Q inputs can be driven single-endedly or differentially, with comparable performance in both cases. The common mode level (VCM) of the four inputs (IVIN, IREF, QVIN, QREF) is typically set to 3.7 V and needs to be driven externally. These inputs go through a set of differential amplifiers and through a V-I converter to feed the double-balanced mixers. The AC-coupled LO input to the device goes through a phase splitter to provide the in-phase and quadrature signals that in turn drive the mixers. The outputs of the mixers are then summed, converted to single-ended signals, and amplified before they are fed to the output port RFOUT. The output of the TRF3702 is ac-coupled and can drive  $50-\Omega$  loads.

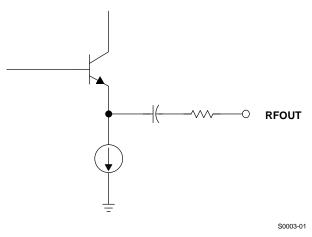


## **EQUIVALENT CIRCUITS**

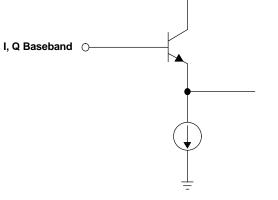
Figure 63 through Figure 66 show equivalent schematics for the main inputs and outputs of the device.



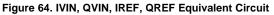


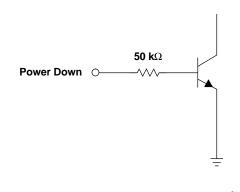






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S0004-01 Figure 66. Power-Down (PWD) Equivalent Circuit

# **APPLICATION INFORMATION**

#### DRIVING THE I, Q INPUTS

There are several ways to drive the four baseband inputs of the TRF3702 to the required amplitude and dc offset. The optimal configuration depends on the end application requirements and the signal levels desired by the designer.

The TRF3702 is by design a differential part, meaning that ideally the user should provide fully complementary signals. However, similar performance in every respect can be achieved if the user only has single-ended signals available. In this case, the IREF and QREF pins just need to have the VCM dc offset applied.

#### Implementing a Single-to-Differential Conversion for the I, Q inputs

In case differential I, Q signals are desired but not available, the THS4503 family of wideband, low-distortion, fully differential amplifiers can be used to provide a convenient way of performing this conversion. Even if differential signals are available, the THS4503 can provide gain in case a higher voltage swing is required. Besides featuring high bandwidth and high linearity, the THS4503 also provides a convenient way of applying the VCM to all four inputs to the modulator through the VOCM pin (pin 2). The user can further adjust the dc levels for optimum carrier suppression by injecting extra dc at the inputs to the operational amplifier, or by individually adding it to the four outputs. Figure 67 shows a typical implementation of the THS4503 as a driver for the TRF3702. Gain can be easily incorporated in the loop by adjusting the feedback resistors appropriately. For more details, see the THS4503 data sheet at www.ti.com.

# **APPLICATION INFORMATION (continued)**

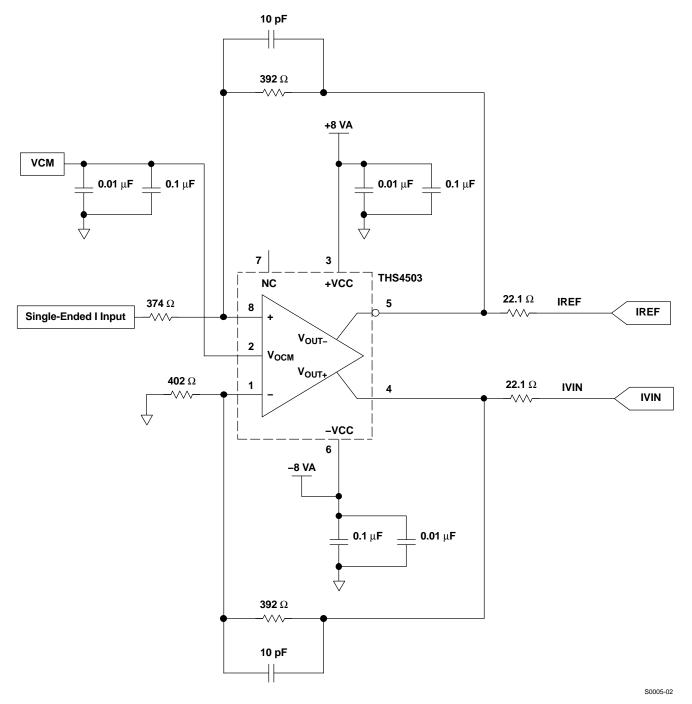


Figure 67. Using the THS4503 to Condition the Baseband Inputs to the TRF3702 (I Channel Shown)

TRF3702

#### **APPLICATION INFORMATION (continued)**

#### DRIVING THE LOCAL OSCILLATOR INPUT

The LO pin is internally terminated to 50  $\Omega$ , thus enabling easy interface to the LO source without the need for external impedance matching. The power level of the LO signal should be in the range of -6 to 6 dBm. For characterization purposes, a power level of 0 dBm was chosen. An ideal way of driving the LO input of the TRF3702 is by using the TRF3750, an ultralow-phase-noise integer-N PLL from Texas Instruments. Combining the TRF3750 with an external VCO can complete the loop and provide a flexible, convenient and cost-effective solution for the local oscillator of the transmitter. Figure 68 shows a typical application for the LO driver network that incorporates the TRF3750 integer-N PLL synthesizer into the design. Depending on the VCO output and the amount of signal loss, an optional gain stage may be added to the output of the VCO before it is applied to the TRF3702 LO input.

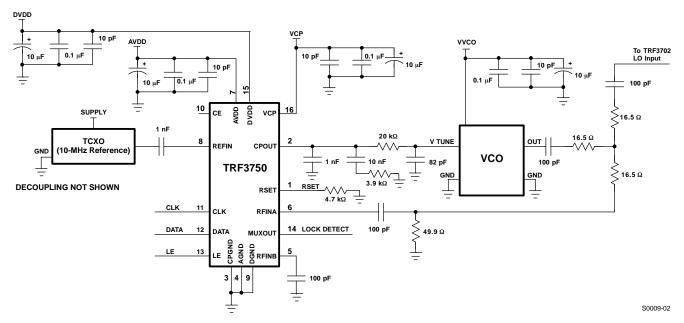


Figure 68. Typical Application Circuit for Generating the LO Signal for the TRF3702 Modulator

## PCB LAYOUT CONSIDERATIONS

The TRF3702 is a high-performance RF device; hence, care should be taken in the layout of the PCB in order to ensure optimum performance. Proper decoupling with low-ESR ceramic chip capacitors is needed for the VCC supplies (pins 6 and 10). Typical values used are in the order of 1 pF parallel to 0.1  $\mu$ F, with the lower-valued capacitors placed closer to the device pins. In addition, a larger tank capacitor in the order of 10  $\mu$ F should be placed on the supply line as layout permits. At least a 4-layer board is recommended for the PCB. If possible, a solid ground plane and a ground pour is also recommended, as is a power plane for the supplies. Because the balance of the four I, Q inputs to the modulator can be critical to device performance, care should be taken to ensure that the trace runs for all four inputs are equal in length. In the case of single-ended drive of the I, Q inputs, the two unused pins IREF and QREF are fed with the VCM dc voltage only, and should be decoupled with a 0.1- $\mu$ F capacitor (or smaller). The LO input trace should be minimized in length and have controlled impedance of 50  $\Omega$ . No external matching components are needed because there is an internal 50- $\Omega$  termination. The RFOUT pin should also have a relatively small trace to minimize parasitics and coupling, and should also be controlled to 50  $\Omega$ . An impedance-matching network can be used to optimize power transfer, but is not critical. All the results shown in the data sheet were taken with no impedance matching network used (RFOUT directly driving an external 50- $\Omega$  load).

The exposed thermal and ground pad on the bottom of the TRF3702 should be soldered to ground to ensure optimum electrical and thermal performance. The landing pattern on the PCB should include a solid pad and 4 thermal vias. These vias typically have 1,2-mm pitch and 0,3-mm diameter. The vias can be arranged in a 2×2 array. The thermal pad on the PCB should be at least 1,65×1,65 mm. A suggested layout is shown in Figure 69.

# **APPLICATION INFORMATION (continued)**

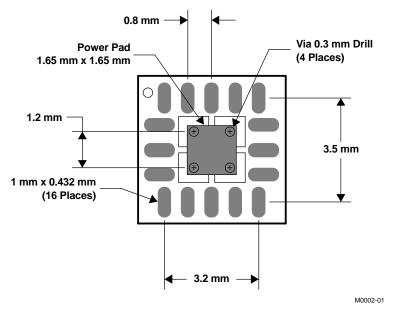


Figure 69. Board Layout for the TRF3702 Device

## IMPLEMENTING A DIRECT UPCONVERSION TRANSMITTER USING A TI DAC

The TRF3702 is ideal for implementing a direct upconversion transmitter, where the input I, Q data can originate from an ASIC or a DAC. Texas Instruments' line of digital-to-analog converters (DAC) is ideally suited for interfacing to the TRF3702. Such DACs include, among others, the DAC290x series, DAC5672, and DAC5686.

This section illustrates the use of the DAC5686, which offers a unique set of features that make interfacing to the TRF3702 easy and convenient. The DAC5686 is a 16-bit, 500 MSPS, 2×–16× interpolating dual-channel DAC, and it features I, Q adjustments for optimal interface to the TRF3702. User-selectable, 11-bit offset and 12-bit gain adjustments can optimize the carrier and sideband suppression of the modulator, resulting in enhanced performance and relaxed filtering requirements at RF. The preferred mode of operation of the DAC5686 for direct interface with the TRF3702 at baseband is the dual-DAC mode. The user also has the flexibility of selecting any one of the four possible complex spectral bands to be fed into the TRF3702. For details on the available modes and programming, see the DAC5686 data sheet available at www.ti.com.

Figure 70 shows the DAC5686 in dual-DAC mode, which is best-suited for zero-IF interface to the TRF3702. In this mode, a seamless, passive interface between the DAC output and the input to the modulator is used, so that no extra components are needed between the two devices. The optimum dc offset level for the inputs to the TRF3702 (VCM) is approximately 3.7 V. The output of the DAC should be centered around 3.3 V or less (depending on signal swing), in order to ensure that its output compliance limits are not exceeded. The resistive network shown in Figure 70 allows for this dc offset transition while still providing a dc path between the DAC output and the modulator. This ensures that the dc offset adjustments on the DAC5686 can still be applied to optimize the carrier suppression at the modulator output. The combination of the DAC5686 and the TRF3702 provides a unique signal-chain solution with state-of-the-art performance for wireless infrastructure applications.



#### **APPLICATION INFORMATION (continued)**

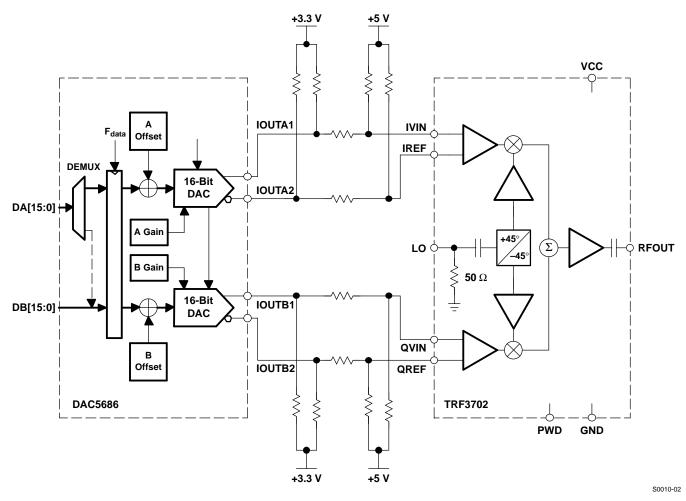
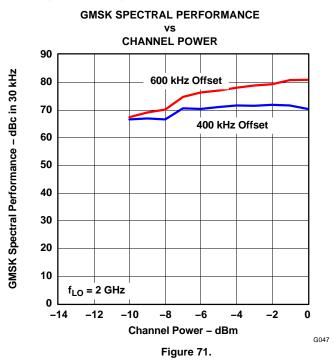


Figure 70. DAC5686 in Dual-DAC Mode With Quadrature Modulator

## **GSM** Applications

The TRF3702 is ideally suited for GSM applications, because it combines high linearity with very low noise levels. Figure 60 and Figure 61 show the distribution of noise vs output power for the TRF3702 over the entire recommended temperature range. The level of noise attained in combination with the superior IMD3 performance shown in Figure 40 means that the user can reach superior levels of C/N while maintaining high linearity. This combination offers the capability of delivering very low levels of EVM, meeting the stringent requirements imposed by the GSM/EDGE standards. Figure 71 shows the spectral mask compliance for the device versus channel power, for both 400-kHz and 600-kHz offsets.

# **APPLICATION INFORMATION (continued)**

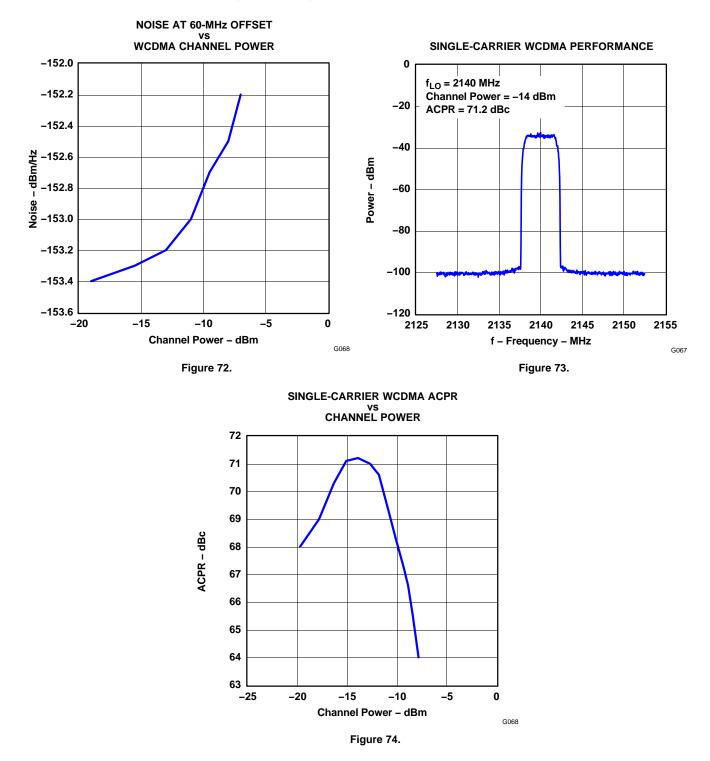


#### WCDMA Applications

The TRF3702 is also optimized for WCDMA applications, where both adjacent-channel power ratio (ACPR) and noise density are critically important. Figure 62 shows the noise performance of the modulator at a 60-MHz offset over temperature. In addition, Figure 72 shows the 60-MHz offset noise measured at the output of the TRF3702 versus WCDMA channel power. Using Texas Instruments' DAC568x series of high-performance digital-to-analog converters in the configuration depicted in Figure 70, state-of-the-art levels of ACPR have been measured. In each case, test model 1 was used with 64 active channels as the baseband input to the TRF3702. Figure 73 shows the performance attained for a single WCDMA carrier at 2.14 GHz, with a measured ACPR of 71.2 dBc for a channel power of -14 dBm. This unprecedented level of ACPR in conjunction with the very low levels of noise at 60-MHz offset make the TRF3702 an optimum choice for such applications. Figure 74 shows the single-carrier WCDMA ACPR performance versus channel power; it is important to note that even at very high output power levels, the TRF3702 maintains great linearity, offering 64 dBc of ACPR at an output-channel power of -8 dBm.

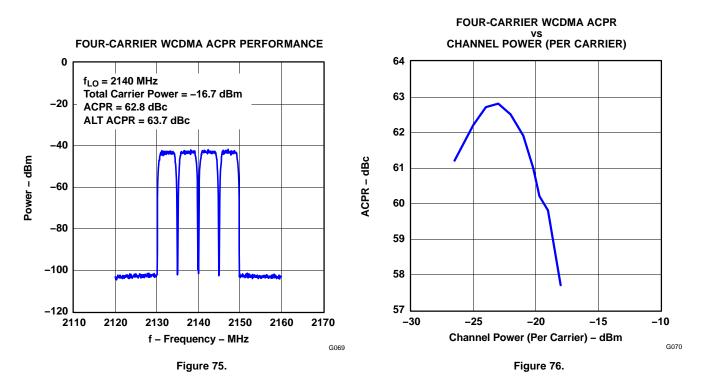


#### **APPLICATION INFORMATION (continued)**



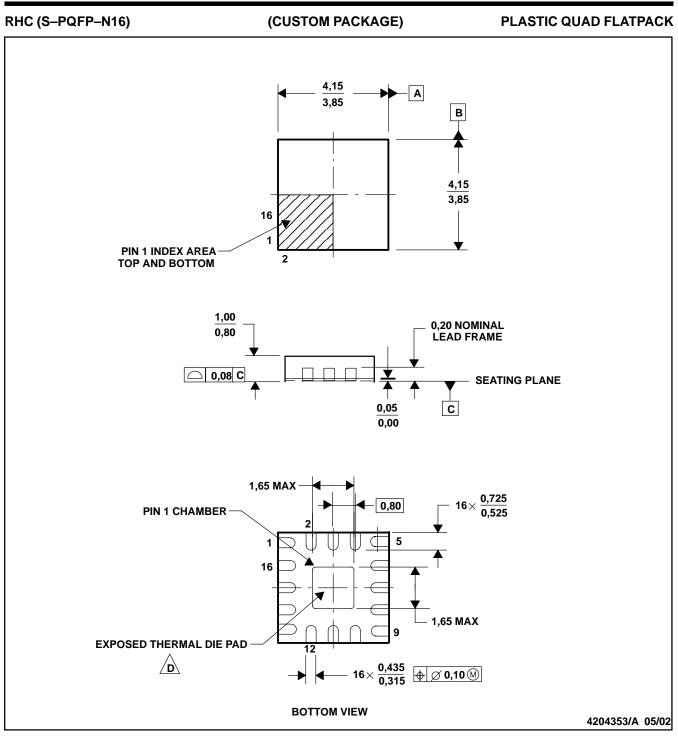
#### **APPLICATION INFORMATION (continued)**

The TRF3702 can also be used for multicarrier applications, as is illustrated in Figure 75. For a 4-carrier case at a total output power of –16.7 dBm, an ACPR of almost 63 dBc can be reached. Figure 76 shows the ACPR profile for a 4-carrier WCDMA application versus per-carrier channel power. Further improvements in performance can be achieved by including a low-pass filter between the output of the DAC and the input to the TRF3702, based upon the frequency planning and specific requirements of a given design. The combination of the TRF3702, the DAC568x, and the TRF3750 provides a unique signal-chain chipset capable of delivering state-of-the-art levels of performance for the most challenging WCDMA applications.



# **MECHANICAL DATA**

MPQF132 - JUNE 2002



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. QFN (Quad Flatpack No-Lead) Package configuration.
- b. The Package thermal performance may be enhanced by bonding the thermal die pad to an external thermal plane. This pad is electrically and thermally connected to the backside of the die and possibly selected ground leads.



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