

[TPS51123A](http://www.ti.com/product/tps51123a?qgpn=tps51123a)

Dual-Synchronous, Step-Down Controller with Out-of-Audio™ Operation and 100-mA LDOs for Notebook System Power

Check for Samples: [TPS51123A](http://www.ti.com/product/tps51123a#samples)

- **² Wide-Input Voltage Range: 5.5 V to 28 V Notebook Computers**
- **Output Voltage Range: 2 V to 5.5 V I/O Supplies**
- **Built-in 100-mA 5-V/3.3-V LDO with Switches System Power Supplies**
- **Built-in 1% 2-V Reference Output**
- **DESCRIPTION With/Without Out-of-Audio™ Mode Selectable**
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-

¹FEATURES APPLICATIONS

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-
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The TPS51123A is a cost effective, dual-synchronous **Light-Load and PWM-Only Operation** buck controller targeted for notebook system power **• Internal 1.6-ms Voltage Servo Soft-Start** supply solutions. It provides 5-V and 3.3-V LDOs and **• Adaptive On-Time Control Architecture with** requires few external components. The TPS51123A **Four Selectable Frequency Setting The Supports high-efficiency, fast transient responses and 4500 ppm/°C R_{DS(on)} Current Sensing • Provides a combined power-good signal.** Out-of-**Audio™** mode light-load operation enables low
 • Built-In Output Discharge accustic noise at much higher efficiency than **• Power Good Output** conventional forced PWM operation. Adaptive on-**Built-in OVP/UVP/OCP**
 • time D-CAP™ control provides convenient and efficient operation. The part operates with supply efficient operation. The part operates with supply **• Thermal Shutdown (Non-latch)** input voltages ranging from 5.5 V to 28 V and supports output voltages from 2 V to 5.5 V. The TPS51123A is available in a 24-pin QFN package and is specified from -40°C to 85°C ambient temperature range.

Table 1. Differences Between the TPS51123 and TPS51123A

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Æ Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. Out-of-Audio, D-CAP are trademarks of Texas Instruments.

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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

ORDERING INFORMATION(1)

(1) For the most current spcifications and package information, see the Package Option Addendum located at the end of this data sheet or refer to our web site at [http://www.ti.com.](http://www.ti.com)

ABSOLUTE MAXIMUM RATINGS(1)

over operating free-air temperature range (unless otherwise noted)

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Voltage values are with respect to the corresponding LLx terminal.

DISSIPATION RATINGS

2-oz. trace and copper pad with solder.

(1) Enhanced thermal conductance by 3 x 3 thermal vias beneath thermal pad.

RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

ELECTRICAL CHARACTERISTICS

over operating free-air temperature range, VIN = 12 V (unless otherwise noted)

(1) Ensured by design. Not production tested.

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ELECTRICAL CHARACTERISTICS (continued)

over operating free-air temperature range, VIN = 12 V (unless otherwise noted)

ELECTRICAL CHARACTERISTICS (continued)

over operating free-air temperature range, VIN = 12 V (unless otherwise noted)

(2) Ensured by design. Not production tested.

DEVICE INFORMATION

Table 2.

Functional Block Diagram

EXAS STRUMENTS

TYPICAL CHARACTERISTICS

Figure 3. Figure 4.

. TYPICAL CHARACTERISTICS (continued)

Figure 5. Figure 6.

Figure 7. Figure 8.

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TYPICAL CHARACTERISTICS (continued)

Figure 9. Figure 10.

Figure 11. Figure 12.

Figure 15. Figure 16.

Figure 13. Figure 14.

Texas

NSTRUMENTS

TYPICAL CHARACTERISTICS (continued)

Figure 19. Figure 20.

TYPICAL CHARACTERISTICS (continued)

Figure 21. Figure 22.

TYPICAL CHARACTERISTICS (continued)

Figure 25. Figure 26.

6 8 10 12 14 16 18 20 22 24 26 VIN - Input Voltage - V

Figure 27.

Texas **NSTRUMENTS**

Figure 30. Figure 31.

Figure 34. Figure 35.

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APPLICATION INFORMATION

PWM Operations

The main control loop of the switch mode power supply (SMPS) is designed as an adaptive on-time pulse width modulation (PWM) controller. It supports a proprietary D-CAP™ mode. D-CAP™ mode does not require external compensation circuit and is suitable for low external component count configuration when used with appropriate amount of ESR at the output capacitor(s).

At the beginning of each cycle, the synchronous top MOSFET is turned on, or becomes 'ON' state. This MOSFET is turned off, or becomes OFF state, after internal one shot timer expires. This one shot is determined by V_{IN} and V_{OUT} to keep frequency fairly constant over input voltage range, hence it is called adaptive on-time control. The MOSFET is turned on again when the feedback point voltage, V_{VFBx} , decreased to match with internal 2-V reference. The inductor current information is also monitored and should be below the over current threshold to initiate this new cycle. Repeating operation in this manner, the controller regulates the output voltage. The synchronous bottom or the rectifying MOSFET is turned on at the beginning of each OFF state to keep the conduction loss minimum.The rectifying MOSFET is turned off before the top MOSFET turns on at next switching cycle or when inductor current information detects zero level. In the auto-skip mode or the OOA skip mode, this enables seamless transition to the reduced frequency operation at light load condition so that highefficiency is kept over broad range of load current.

Adaptive On-Time Control and PWM Frequency

TPS51123A does not have a dedicated oscillator on board. However, the part runs with pseudo-constant frequency by feed-forwarding the input and output voltage into the on-time, one-shot timer. The on-time is controlled inverse proportional to the input voltage and proportional to the output voltage so that the duty ratio is kept as $V_{\text{OUT}}/V_{\text{IN}}$ technically with the same cycle time. The frequencies are set by the TONSEL pin as shown in [Table 3.](#page-19-0)

Table 3. TONSEL Connection and Switching Frequency

Loop Compensation

From small-signal loop analysis, a buck converter using D-CAPTM mode can be simplified as below.

Figure 36. Simplifying the Modulator

The output voltage is compared with internal reference voltage after divider resistors, R1 and R2. The PWM comparator determines the timing to turn on high-side MOSFET. The gain and speed of the comparator is high enough to keep the voltage at the beginning of each on cycle substantially constant. For the loop stability, the 0dB frequency, f_0 , defined below need to be lower than 1/4 of the switching frequency.

$$
f_0 = \frac{1}{2\pi \times \text{ESR} \times C_O} \le \frac{f_{SW}}{4}
$$
\n⁽¹⁾

As f₀ is determined solely by the output capacitor's characteristics, loop stability of D-CAPTM mode is determined by the capacitor's chemistry. For example, specialty polymer capacitors (SP-CAP) have Co in the order of several 100 μF and ESR in range of 10 m Ω . These make f₀ on the order of 100 kHz or less and the loop will be stable. However, ceramic capacitors have f_0 at more than 700 kHz, which is not suitable for this operational mode.

Ramp Signal

The TPS51123A adds a ramp signal to the 2-V reference in order to improve its jitter performance. As described in the previous section, the feedback voltage is compared with the reference information to keep the output voltage in regulation. By adding a small ramp signal to the reference, the dignal-to-noise ratio at the onset of a new switching cycle is improved. Therefore the operation becomes less jitter and stable. The ramp signal is controlled to start with -20 mV at the beginning of ON-cycle and to become 0 mV at the end of OFF-cycle in steady state. By using this scheme, the TPS51123A improve jitter performance without sacrificing the reference accuracy.

Light Load Condition in Auto-Skip Operation

The TPS51123A automatically reduces switching frequency at light load conditions to maintain high-efficiency. This reduction of frequency is achieved smoothly and without increase of V_{OUT} ripple. Detail operation is described as follows. As the output current decreases from heavy load condition, the inductor current is also reduced and eventually comes to the point that its valley touches zero current, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when this zero inductor current is detected. As the load current further decreased, the converter runs in discontinuous conduction mode and it takes longer and longer to discharge the output capacitor to the level that requires next ON cycle. The ON time is kept the same as that in the heavy load condition. In reverse, when the output current increase from light load to heavy load, switching frequency increases to the preset value as the inductor current reaches to the continuous conduction. The transition load point to the light load operation $I_{\text{OUT}(L)}$ (i.e. the threshold between continuous and discontinuous conduction mode) can be calculated as follows;

$$
I_{\text{OUT}}(LL) = \frac{1}{2 \times L \times f} \times \frac{(V_{\text{IN}} - V_{\text{OUT}}) \times V_{\text{OUT}}}{V_{\text{IN}}}
$$
(2)

where f is the PWM switching frequency.

Switching frequency versus output current in the light load condition is a function of L, V_{IN} and V_{OUT}, but it decreases almost proportional to the output current from the $I_{\text{OUT(LL)}}$ shown in [Equation 2](#page-21-0). For example, it ise 60 kHz at $I_{\text{OUT}}/5$ if the frequency setting is 300 kHz.

Out-of-Audio™ Light-Load Operation

Out-of-Audio™ (OOA) light-load mode is a unique control feature that keeps the switching frequency above acoustic audible frequencies toward virtually no load condition while maintaining best of the art high conversion efficiency. When the Out-of-Audio™ operation is selected, OOA control circuit monitors the states of both MOSFET and force to change into the ON state if both of MOSFETs are off for more than 32 μs. This means that the top MOSFET is turned on even if the output voltage is higher than the target value so that the output capacitor is tends to be overcharged.

The OOA control circuit detects the over-voltage condition and begins to modulate the on time to keep the output voltage regulated. As a result, the output voltage becomes 0.5% higher than normal light-load operation.

Enable and Soft Start

EN0 is the control pin of VREG5, VREG3 and VREF regulators. Bring this node down to GND disables those three regulators and minimize the shutdown supply current to 10 μA. Pulling this node up to 3.3 V or 5 V will turn the three regulators on to standby mode. The two switch mode power supplies (channel-1, channel-2) become ready to enable at this standby mode. The TPS51123A has an internal, 1.6 ms, voltage servo soft-start for each channel.

Both channel 1 and channel 2 can be enabled simultaneously with the ENC pin when only the OCL trip setting resistance is connected to TRIPx pin. Channel 1 and channel 2 can be disabled independently by shorting the TRIPx pin to ground when the ENC pin voltage is higher than its enable threshold, which is typically 1.26 V. After enabling channel 1 and/or channel 2, an internal DAC begins ramping up the reference voltage of the PWM comparator. Smooth control of the output voltage is maintained during start up. As TPS51123A shares one DAC with both channels, if TRIPx pin becomes higher than the enable threshold voltage while another channel is starting up, soft-start is postponed until another channel soft-start has completed. If both of TRIP1 and TRIP2 become higher than the enable threshold voltage at the same time (within 60 µs), both channels start up simultaneously.

Table 4. Enabling State

(1) Either high or low, does no affect the enable state.

VREG5/VREG3 Linear Regulators

There are two sets of 100-mA standby linear regulators which outputs 5 V and 3.3 V, respectively. The VREG5 serves as the main power supply for the analog circuitry of the device and provides the current for gate drivers. The VREG3 is intended mainly for auxiliary 3.3-V supply for the notebook system during standby mode.

Add a high-quality X5R or X7R ceramic capacitor with a value of 10-µF or larger placed close to the VREG5 and VREG3 pins to stabilize LDOs. For VREG3, a 1-µF ceramic capacitor is acceptable when not loaded.

VREG5 Switch Over

When the VO1 voltage becomes higher than 4.7 V AND channel-1 internal powergood flag is generated, internal 5-V LDO regulator is shut off and the VREG5 output is connected to VO1 by internal switch over MOSFET. The 510-μs powergood delay helps a switch over without glitch.

VREG3 Switch Over

When the VO2 voltage becomes higher than 3.15 V AND channel-2 internal powergood flag is generated, internal 3.3-V LDO regulator is shut off and the VREG3 output is connected to VO2 by internal switch over MOSFET. The 510-μs powergood delay helps a switch over without glitch.

Powergood

The TPS51123A has one powergood output that indicates a high state when both switcher outputs are within the targets (AND gated). The powergood function is activated with 2-ms internal delay after ENC goes high. If the output voltage becomes within ±5% of the target value, internal comparators detect power good state and the powergood signal becomes high after 510-μs internal delay. Therefore PGOOD goes high around 2.5 ms after ENC goes high. If the output voltage goes outside of ±10% of the target value, the powergood signal becomes low after 2-μs internal delay. The powergood output is an open drain output and is needed to be pulled up outside.

Also note that, in the case of Auto-skip or Out-of-Audio™ mode, if the output voltage goes +10% above the target value and the power-good signal flags low, then the loop attempts to correct the output by turning on the low-side driver (forced PWM mode). After the feedback voltage returns to be within +5% of the target value and the power-good signal goes high, the controller returns back to auto-skip mode or Out-of-Audio™ mode.

Output Discharge Control

When ENC is low, the TPS51123A discharges outputs using internal MOSFET which is connected to VOx and GND. The current capability of these MOSFETs is limited to discharge slowly.

Low-Side Driver

The low-side driver is designed to drive high current low $R_{DS(on)}$ N-channel MOSFET(s). The drive capability is represented by its internal resistance, which are 4 $Ω$ for VREG5 to DRVLx and 1.5 $Ω$ for DRVLx to GND. A dead time to prevent shoot through is internally generated between top MOSFET off to bottom MOSFET on, and bottom MOSFET off to top MOSFET on. 5-V bias voltage is delivered from VREG5 supply. The instantaneous drive current is supplied by an input capacitor connected between VREG5 and GND. The average drive current is equal to the gate charge at $Vgs = 5$ V times switching frequency. This gate drive current as well as the highside gate drive current times 5 V makes the driving power which need to be dissipated from TPS51123A package.

High-Side Driver

The high-side driver is designed to drive high current, low $R_{DS(on)}$ N-channel MOSFET(s). When configured as a floating driver, 5-V bias voltage is delivered from VREG5 supply. The average drive current is also calculated by the gate charge at Vgs = 5 V times switching frequency. The instantaneous drive current is supplied by the flying capacitor between VBSTx and LLx pins. The drive capability is represented by its internal resistance, which are 4 Ω for VBSTx to DRVHx and 1.5Ω for DRVHx to LLx.

Current Protection

TPS51123A has cycle-by-cycle over current limiting control. The inductor current is monitored during the 'OFF' state and the controller keeps the 'OFF' state during the inductor current is larger than the over current trip level. In order to provide both good accuracy and cost effective solution, TPS51123A supports temperature compensated MOSFET $R_{DS(on)}$ sensing. The TRIPx pin should be connected to GND through the trip voltage setting resistor, R_{TRIP} . TRIPx terminal sources I_{TRIP} current, which is 10 µA typically at room temperature, and the trip level is set to the OCL trip voltage V_{TRIP} as below. Note that the V_{TRIP} is limited up to about 205 mV internally.

$$
V_{TRIP}(mV) = \frac{R_{TRIP}(k\Omega) \times I_{TRIP}(\mu A)}{9} - 24(mV)
$$
\n(3)

Note that when TRIPx voltage is under a certain thershould (typically 0.4V), the switcher channel concerned is shut down. The inductor current is monitored by the voltage between GND pin and LLx pin so that LLx pin should be connected to the drain terminal of the bottom MOSFET properly. Itrip has 4500 ppm/°C temperature slope to compensate the temperature dependency of the $R_{DS(on)}$. GND is used as the positive current sensing node so that GND should be connected to the proper current sensing device, i.e. the source terminal of the bottom MOSFET.

As the comparison is done during the OFF state, V_{TRIP} sets valley level of the inductor current. Thus, the load current at over current threshold, I_{OCP} , can be calculated in [Equation 4.](#page-23-0)

$$
I_{OCP} = \frac{V_{TRIP}}{R_{DS(on)}} + \frac{I_{RIPPLE}}{2} = \frac{V_{TRIP}}{R_{DS(on)}} + \frac{1}{2 \times L \times f} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}}
$$
(4)

In an overcurrent condition, the current to the load exceeds the current to the output capacitor thus the output voltage tends to fall down. Eventually, it ends up with crossing the under voltage protection threshold and shutdown both channels.

Overvoltage and Undervoltage Protection

TPS51123A monitors a resistor divided feedback voltage to detect over and under voltage. When the feedback voltage becomes higher than 115% of the target voltage, the OVP comparator output goes high and the circuit latches as the top MOSFET driver OFF and the bottom MOSFET driver ON.

Also, TPS51123A monitors VOx voltage directly and if it becomes greater than 5.75 V the TPS51123A turns off the top MOSFET driver.

When the feedback voltage becomes lower than 60% of the target voltage, the UVP comparator output goes high and an internal UVP delay counter begins counting. After 32 μs, TPS51123A latches OFF both top and bottom MOSFETs drivers, and shut off both drivers of another channel. This function is enabled after 2 ms following ENC has become high.

UVLO Protection

TPS51123A has VREG5 under voltage lock out protection (UVLO). When the VREG5 voltage is lower than UVLO threshold voltage both switch mode power supplies are shut off. This is non-latch protection. When the VREG3 voltage is lower than (V_{OUT2} - 1 V), both switch mode power supplies are also shut off

Thermal Shutdown

TPS51123A monitors the temperature of itself. If the temperature exceeds the threshold value (typically 150°C), TPS51123A is shut off including LDOs. This is non-latch protection.

External Parts Selection

The external components selection is much simple in D-CAP™ Mode.

1. Determine output voltage

The output voltage is programmed by the voltage-divider resistor, R1 and R2, as shown in [Figure 36.](#page-20-0) R1 is connected between VFBx pin and the output, and R2 is connected betwen the VFBx pin and GND.

Recommended R2 value is from 10 k Ω to 20 k Ω . Determine R1 using equation as below.

$$
R1 = \frac{(V_{OUT} - 2.0)}{2.0} \times R2
$$
 (5)

2. Choose the Inductor

The inductance value should be determined to give the ripple current of approximately 1/4 to 1/2 of maximum output current. Larger ripple current increases output ripple voltage and improves S/N ratio and helps stable operation.

$$
L = \frac{1}{I_{\text{IND}(ripple)} \times f} \times \frac{V_{\text{IN}(max)} - V_{\text{OUT}}V_{\text{OUT}}}{V_{\text{IN}(max)}} = \frac{3}{I_{\text{OUT}(max)} \times f} \times \frac{V_{\text{IN}(max)} - V_{\text{OUT}}V_{\text{NOT}}}{V_{\text{IN}(max)}}
$$
(6)

The inductor also needs to have low DCR to achieve good efficiency, as well as enough room above peak inductor current before saturation. The peak inductor current can be estimated as follows.

$$
I_{IND(peak)} = \frac{V_{TRIP}}{R_{DS(on)}} + \frac{1}{L \times f} \times \frac{(V_{IN(max)} - V_{OUT}) \times V_{OUT}}{V_{IN(max)}}
$$
(7)

3. Choose the Output Capacitor(s)

Organic semiconductor capacitor(s) or specialty polymer capacitor(s) are recommended. Determine ESR to meet required ripple voltage. A quick approximation is as shown in [Equation 8.](#page-25-0) This equation is based on that required output ripple slope is approximately 20 mV per T_{SW} (switching period) in terms of VFB terminal voltage.

$$
ESR = \frac{V_{OUT} \times 20 \, (mV) \times (1-D)}{2(V) \times I_{RIPPLE}} - \frac{20 \, (mV) \times L \times f}{2(V)}
$$

where

- D is the duty cycle
- the required output ripple slope is approximately 20 mV per t_{SW} (switching period) in terms of VFB terminal voltage voltage (8)

4. Choose the Low-Side MOSFET

It is highly recommended that the low-side MOSFET should have an integrated Schottky barrier diode, or an external Schottky barrier diode in parallel to achieve stable operation.

Layout Considerations

Certain points must be considered before starting a layout work using the TPS51123A.

- TPS51123A has only one GND pin and special care of GND trace design makes operation stable, especially when both channels operate. Group GND terminals of output voltage divider of both channels and the VREF capacitor as close as possible, and connect them to an inner GND plane with PowerPad and the overcurrent setting resistor, as shown in the thin GND line of [Figure 37](#page-27-0). This trace is named Signal Ground (SGND). Group ground terminals of VIN capacitor(s), VOUT capacitor(s) and source of low-side MOSFETs as close as possible, and connect them to another inner GND plane with GND pin of the device and the GND terminal of VREG3 and VREG5 capacitors, as shown in the bold GND line of [Figure 37.](#page-27-0) This trace is named Power Ground (PGND). SGND should be connected to PGND at the middle point between ground terminal of V_{OUT} capacitors.
- Inductor, V_{OUT} capacitor(s), V_{IN} capacitor(s) and MOSFETs are the power components and should be placed on one side of the PCB (solder side). Power components of each channel should be at the same distance from the TPS51123A. Other small signal parts should be placed on another side (component side). Inner GND planes should shield and isolate the small signal traces from noisy power lines.
- PCB trace defined as LLx node, which connects to source of high-side MOSFET, drain of low-side MOSFET and high-voltage side of the inductor, should be as short and wide as possible.
- A high-quality X5R or X7R ceramic bypass capacitor should be placed close to the device and traces should be no longer than 10 mm. Use the following capacitance values.
	- VREG5: 10 µF or larger
	- $-$ VREG3: 10 µF or larger (1 µF is acceptable when not loaded)
	- VREF: between 220 nF and 1 µF
- Connect the overcurrent setting resistors from TRIPx to SGND and close to the device, right next to the device if possible.
- The discharge path (VOx) should have a dedicated trace to the output capacitor; separate from the output voltage sensing trace. When LDO5 is switched over Vo1 trace should be 1.5 mm with no loops. When LDO3 is switched over and loaded VO2 trace should also be 1.5 mm with no loops. There is no restriction for just monitoring Vox. Make the feedback current setting resistor (the resistor between VFBx to SGND) close to the device. Place on the component side and avoid vias between this resistor and the device.
- Connections from the drivers to the respective gate of the high-side or the low-side MOSFET should be as short as possible to reduce stray inductance. Use 0.65-mm (25 mils) or wider trace and via(s) of at least 0.5 mm (20 mils) diameter along this trace.
- All sensitive analog traces and components such as VOx, VFBx, VREF, GND, EN0, TRIPx, PGOOD, TONSEL and SKIPSEL should be placed away from high-voltage switching nodes such as LLx, DRVLx, and DRVHx nodes to avoid coupling.
- Traces for VFB1 and VFB2 should be short and laid apart each other to avoid channel to channel interference.
- In order to effectively remove heat from the package, prepare thermal land and solder to the package's thermal pad. Three by three or more vias with a 0.33-mm (13 mils) diameter connected from the thermal land to the internal ground plane should be used to help dissipation. This thermal land underneath the package should be connected to SGND, and should NOT be connected to PGND.

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* Driver and switch node traces are shown for CH1 only.

Application Circuit

Figure 39. 5-V/8-A, 3.3-V/8-A Application Circuit (245-kHz/305-kHz Setting)

Table 5. List of Materials for 5-V/8-A, 3.3-V/8-A Application Circuit

(1) Use a MOSFET with an integrated Schottky barrier diode (SBD) for the low-side, or add an SBD in parallel with a normal MOSFET.

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REVISION HISTORY

www.ti.com 10-Dec-2020

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE OPTION ADDENDUM

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TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

Pack Materials-Page 1

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PACKAGE MATERIALS INFORMATION

www.ti.com 20-Apr-2023

*All dimensions are nominal

GENERIC PACKAGE VIEW

RGE 24 VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

RGE0024B VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

EXAMPLE BOARD LAYOUT

RGE0024B VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RGE0024B VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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