

# 2.7V to 5.5V Input, 3A Integrated MOSFET Single Synchronous Buck DC/DC Converter BD9A301MUV-LB

#### **General Description**

This is the product guarantees long time support in Industrial market. BD9A301MUV-LB is a synchronous buck switching regulator with built-in low on-resistance power MOSFETs. It is capable of providing current up to 3A.The SLLM<sup>TM</sup> control provides excellent efficiency characteristics in light-load conditions which make the product ideal for equipment and devices that demand minimal standby power consumption. The oscillating frequency is high at 1MHz using a small value of inductance. It is a current mode control DC/DC converter and features high-speed transient response. Phase compensation can also be set easily.

#### **Features**

- Long Time Support Product for Industrial Application
- Synchronous Single DC/DC Converter.
- SLLM<sup>™</sup> (Simple Light Load Mode) Control.
- Over Current Protection.
- Short Circuit Protection.
- Thermal Shutdown Protection.
- Under Voltage Lockout Protection.
- Adjustable Soft start Function.
- Power Good Output.
- VQFN016V3030 Package (Backside Heat Dissipation)

#### **Applications**

- Industrial Equipment,
- Step-Down Power Supply for DSPs, FPGAs, Microprocessors, etc.
- Storage Devices (HDDs/SSDs).
- Printers, OA Equipment.
- Distributed Power Supply, Secondary Power Supply.

# **Typical Application Circuit**

#### BD9A301MUV-LB PGD VIN **PVIN** PGD BOOT AVIN MODE MODE 0.1µF 10µF 0.1µF VOUT \_ Enable SW ΕN 1.5µH SS ITH 22µF × 2 $\leq R_1$ PGND $\leq$ R<sub>ith</sub> FB AGND Сттн R<sub>2</sub>

Figure 1. Application Circuit

OProduct structure : Silicon monolithic integrated circuit OThis product has no designed protection against radioactive rays

# **Key Specifications**

- Input Voltage Range:
- Output Voltage Range: -
- Average Output Current:
  - Switching Frequency: 1MHz(Typ)
- High-Side MOSFET On-Resistance: 60mΩ (Typ)
- Low-Side MOSFET On-Resistance: 60mΩ (Typ)
  - Standby Current: 0µA (Typ)

#### Package

VQFN016V3030

W(Typ) x D(Typ) x H(Max) 3.00mm x 3.00mm x 1.00mm

2.7V to 5.5V

3A(Max)

0.8V to V<sub>PVIN</sub>×0.7V



# **Pin Configuration**

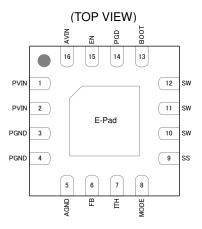
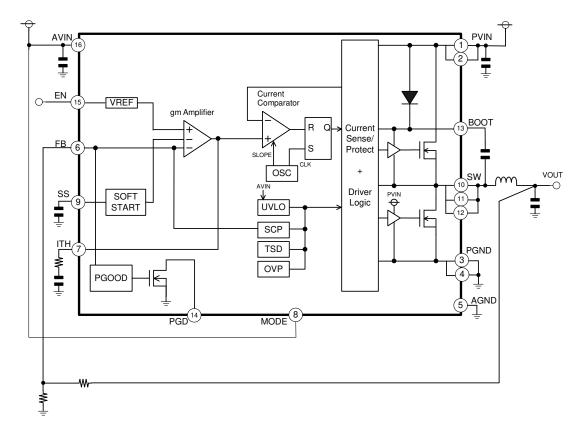


Figure 2. Pin Configuration

# **Pin Descriptions**

Pin No.	Pin Name	Function				
1, 2	PVIN	Power supply terminals for the switching regulator. These terminals supply power to the output stage of the switching regulator. Connecting a $10\mu$ F ceramic capacitor is recommended.				
3, 4	PGND	Ground terminals for the output stage of the switching regulator.				
5	AGND	Ground terminal for the control circuit.				
6	FB	An inverting input node for the gm error amplifier. See page 23 for how to calculate the resistance of the output voltage setting.				
7	ITH	An input terminal for the gm error amplifier output and the output switch current comparator. Connect a frequency phase compensation component to this terminal. See page 24 for how to calculate the resistance and capacitance for phase compensation.				
8	MODE	Turning this terminal signal Low (0.2V or lower) forces the device to operate in the fixed frequency PWM mode. Turning this terminal signal High (0.8V or higher) enables the SLLM control and the mode is automatically switched between the SLLM control and fixed frequency PWM mode.				
9	SS	Terminal for setting the soft start time. The rise time of the output voltage can be specified by connecting a capacitor to this terminal. See page 23 for how to calculate the capacitance.				
10, 11, 12	SW	Switch nodes. These terminals are connected to the source of the high-side MOSFET and drain of the low-side MOSFET. Connect a bootstrap capacitor of $0.1\mu$ F between these terminals and BOOT terminals. In addition, connect an inductor of $1.5\mu$ H considering the direct current superimposition characteristic.				
13	BOOT	Connect a bootstrap capacitor of $0.1\mu$ F between this terminal and SW terminals. The voltage of this capacitor is the gate drive voltage of the high-side MOSFET.				
14	PGD	A "Power Good" terminal, an open drain output. Use of pull up resistor is needed. See page 18 for how to specify the resistance. When the FB terminal voltage reaches within ±7% of 0.8V (Typ), the internal Nch MOSFET turns off and the output turns High.				
15	EN	Turning this terminal signal low (0.8V or lower) forces the device to enter the shutdown mode. Turning this terminal signal high (2.0V or higher) enables the device. This terminal must be terminated.				
16	AVIN	Supplies power to the control circuit of the switching regulator. Connecting a $0.1\mu$ F ceramic capacitor is recommended.				
-	E-Pad	A backside heat dissipation pad. Connecting to the internal PCB ground plane by using multiple vias provides excellent heat dissipation characteristics.				

# **Block Diagram**





# **Description of Blocks**

1. VREF

The VREF block generates the internal reference voltage.

2. UVLO

The UVLO block is for under voltage lockout protection. It will shut down the IC when the VIN falls to 2.45V (Typ) or lower. The threshold voltage has a hysteresis of 100mV (Typ).

# 3. SCP

After the soft start is completed and when the feedback voltage of the output voltage has fallen below 0.4V (Typ) for 1msec (Typ), the SCP stops the operation for 16msec (Typ) and subsequently initiates restart.

# 4. OVP

Over voltage protection function (OVP) compares FB terminal voltage with the internal standard voltage VREF. When the FB terminal voltage exceeds 0.88V (Typ) it turns MOSFET of output part MOSFET off. After output voltage drop it returns with hysteresis.

# 5. TSD

The TSD block is for thermal protection. The thermal protection circuit shuts down the device when the internal temperature of IC rises to 175°C (Typ) or higher. Thermal protection circuit resets when the temperature falls. The circuit has a hysteresis of 25°C (Typ).

# 6. SOFT START

The Soft Start circuit slows down the rise of output voltage during start-up and controls the current, which allows the prevention of output voltage overshoot and inrush current. A built-in soft start function is provided and a soft start is initiated in 1msec (Typ) when the SS terminal is open.

# 7. gm Amplifier

The gm Amplifier block compares the reference voltage with the feedback voltage of the output voltage. The error and the ITH terminal voltage determine the switching duty. A soft start is applied at startup. The ITH terminal voltage is limited by the internal slope voltage.

#### 8. Current Comparator

The Current Comparator block compares the output ITH terminal voltage of the error amplifier and the slope block signal to determine the switching duty. In the event of over current, the current that flows through the high-side MOSFET is limited at each cycle of the switching frequency.

# 9. OSC

This block generates the oscillating frequency.

#### 10.DRIVER LOGIC

This block is a DC/DC driver. A signal from current comparator is applied to drive the MOSFETs.

11.PGOOD

When the FB terminal voltage reaches 0.8V (Typ) within ±7%, the Nch MOSFET of the built-in open drain output turns off and the output turns high.

# Absolute Maximum Ratings (Ta = 25°C)

Parameter	Symbol	Rating	Unit
Supply Voltage	VPVIN, VAVIN	-0.3 to +7	V
EN Voltage	V <sub>EN</sub>	-0.3 to +7	V
MODE Voltage	VMODE	-0.3 to +7	V
PGD Voltage	VPGD	-0.3 to +7	V
Voltage from GND to BOOT	V <sub>BOOT</sub>	-0.3 to +14	V
Voltage from SW to BOOT	⊿∨воот	-0.3 to +7	V
FB Voltage	V <sub>FB</sub>	-0.3 to +7	V
ITH Voltage	VITH	-0.3 to +7	V
SW Voltage	Vsw	-0.3 to V <sub>PVIN</sub> + 0.3	V
Allowable Power Dissipation <sup>(Note 1)</sup>	Pd	2.66	W
Maximum Junction Temperature	Tjmax	150	S°
Storage Temperature Range	Tstg	-55 to 150	°C

(Note 1) When mounted on a 70mm x 70mm x 1.6mm 4-layer glass epoxy board (copper foil area: 70 mm x 70 mm)

Derate by 21.3mW when operating above 25°C.

Caution1: Operating the IC over the absolute maximum ratings may damage the IC. The damage can either be a short circuit between pins or an open circuit between pins and the internal circuitry. Therefore, it is important to consider circuit protection measures, such as adding a fuse, in case the IC is operated over the absolute maximum ratings.

Caution2: Long-term reliability may be influenced when operated at or near the absolute maximum rating.

# **Recommended Operating Conditions**

Parameter	Symbol	Min	Тур	Max	Unit
Supply Voltage	VPVIN, VAVIN	2.7	-	5.5	V
Output Current <sup>(Note 2)</sup>	Іоит	-	-	3	А
Output Voltage Range	VRANGE	0.8	-	V <sub>PVIN</sub> × 0.7	V
Operating Junction Temperature Range	Tj	-40	-	+125	°C

(Note 2) Pd,ASO should not be exceeded.

# **Electrical Characteristics** (Unless otherwise specified Ta = 25°C, V<sub>AVIN</sub> = V<sub>PVIN</sub> = 5V, V<sub>EN</sub> = 5V)

Parameter	Symbol	Min	Тур	Max	Unit	Conditions
AVIN PIN						
Standby Supply Current	I <sub>STB</sub>	-	0	10	μA	EN= GND
Operating Supply Current	lcc	-	350	500	μA	I <sub>OUT</sub> = 0mA Non-switching
UVLO Detection Voltage	V <sub>UVLO1</sub>	2.35	2.45	2.55	V	V <sub>IN</sub> falling
UVLO Release Voltage	VUVLO2	2.425	2.55	2.7	V	V <sub>IN</sub> rising
ENABLE						
EN Input High Level Voltage	VENH	2.0	-	VAVIN	V	
EN Input Low Level Voltage	VENL	AGND	-	0.8	V	
EN Input Current	IEN	-	5	10	μA	EN= 5V
MODE	1	1		J I		
MODE Threshold Voltage	VMODEH	0.2	0.4	0.8	V	
MODE Input Current	IMODE	-	10	20	μA	MODE= 5V
Reference Voltage, Error Amplifier	1	1		J I		
FB Terminal Voltage	VFB	0.792	0.8	0.808	V	
FB Input Current	I <sub>FB</sub>	-	0	1	μA	FB= 0.8V
ITH Sink Current	ITHSI	10	20	40	μA	FB= 0.9V
ITH Source Current	I <sub>THSO</sub>	10	20	40	μA	FB= 0.7V
Soft Start Time	Tss	0.5	1.0	2.0	ms	With internal constant
Soft Start Current	lss	0.9	1.8	3.6	μA	
SWITCHING FREQUENCY	1	1		J I		
Switching Frequency	Fosc	800	1000	1200	kHz	
POWER GOOD	1	1		J I		
Falling (Fault) Voltage	VPGDFF	87	90	93	%	OUTPUT voltage falling
Rising (Good) Voltage	VPGDRG	90	93	96	%	OUTPUT voltage rising
Rising (Fault) Voltage	VPGDRF	107	110	113	%	OUTPUT voltage rising
Falling (Good) Voltage	VPGDFG	104	107	110	%	OUTPUT voltage falling
PGD Output Leakage Current	I <sub>LKPGD</sub>	-	0	5	μA	PGD= 5V
Power Good ON Resistance	Rpgd	-	100	200	Ω	
Power Good Low Level Voltage	P <sub>GDVL</sub>	-	0.1	0.2	V	I <sub>PGD</sub> = 1mA
SWITCH MOSFET	I			1		
High Side FET ON Resistance	Ronh	-	60	120	mΩ	BOOT – SW= 5V
Low Side FET ON Resistance	Ronl	-	60	120	mΩ	
High Side Output Leakage Current	RILH	-	0	10	μA	Non-switching
Low Side Output Leakage Current	R <sub>ILL</sub>	-	0	10	μΑ	Non-switching
SCP						-
Short Circuit Protection Detection Voltage	V <sub>SCP</sub>	0.28	0.4	0.52	V	

# **Typical Performance Curves**

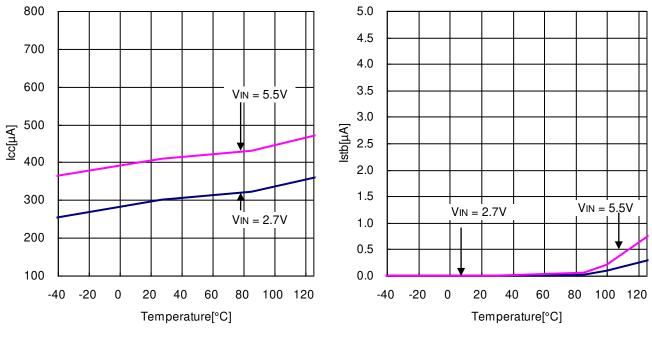


Figure 4. Operating Current vs Temperature

Figure 5. Stand-by Current vs Temperature

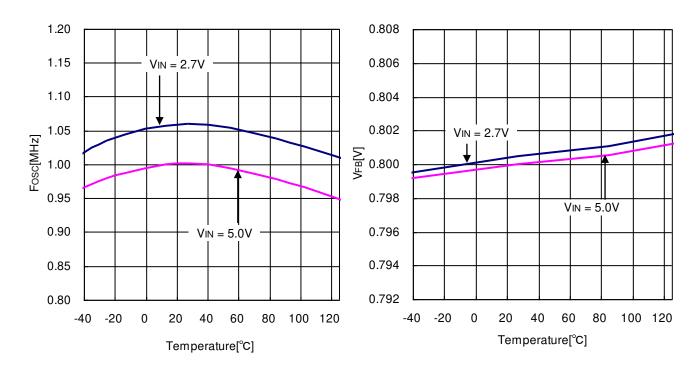


Figure 6. Switching Frequency vs Temperature

Figure 7. FB Voltage vs Temperature

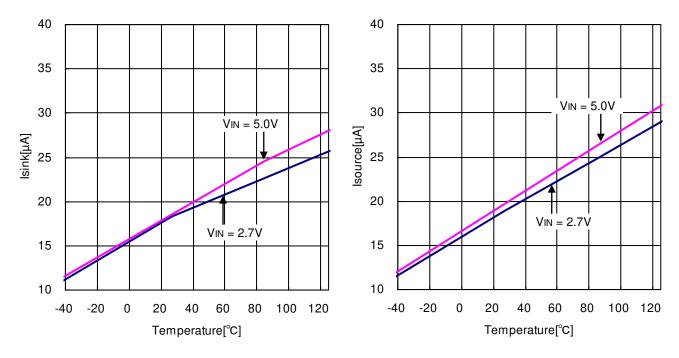


Figure 8. ITH Sink Current vs Temperature

Figure 9. ITH Source Current vs Temperature

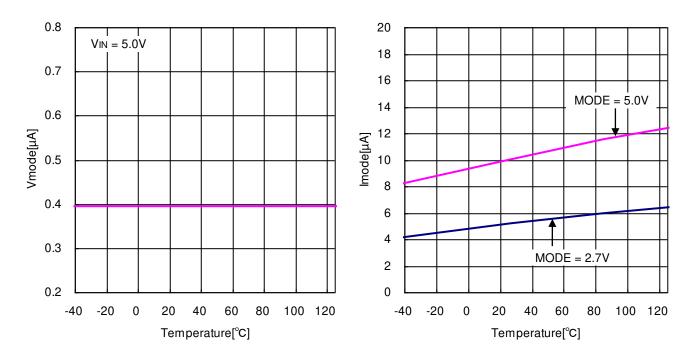


Figure 10. Mode Threshold vs Temperature

Figure 11. Mode Input Current vs Temperature

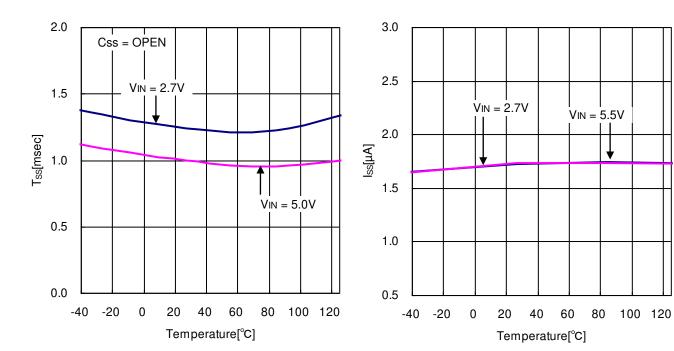
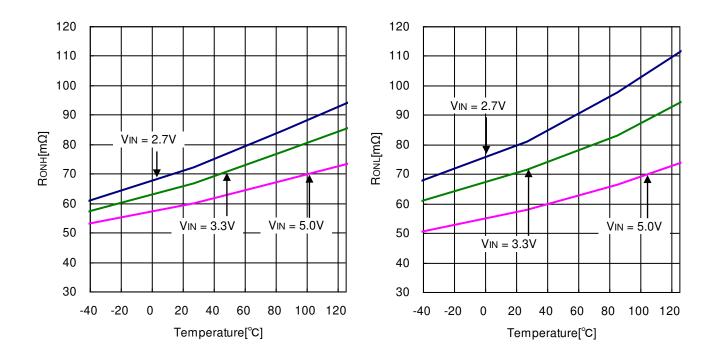


Figure 12. Soft Start Time vs Temperature

Figure 13. Soft Start Terminal Current vs Temperature



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Figure 14. High side FET ON-Resistance vs Temperature

Figure 15. Low side FET ON-Resistance vs Temperature

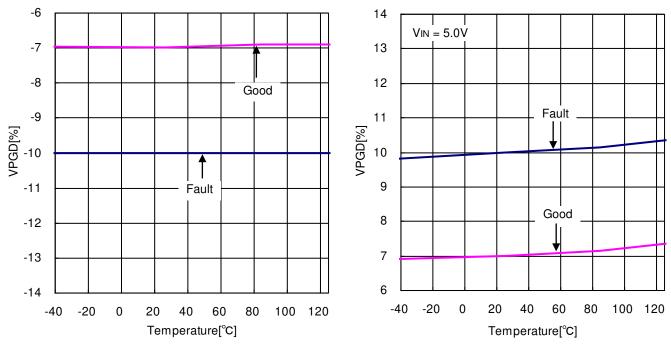
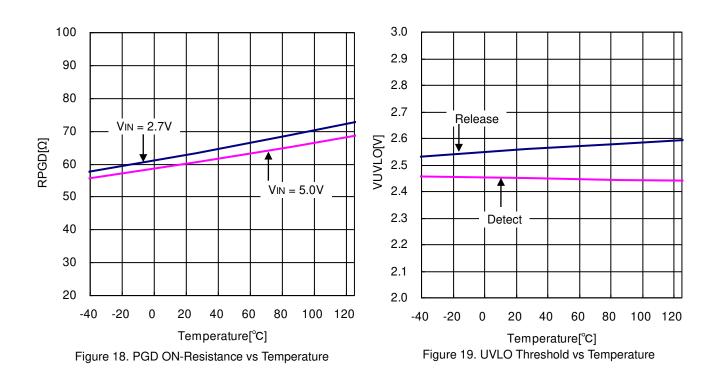
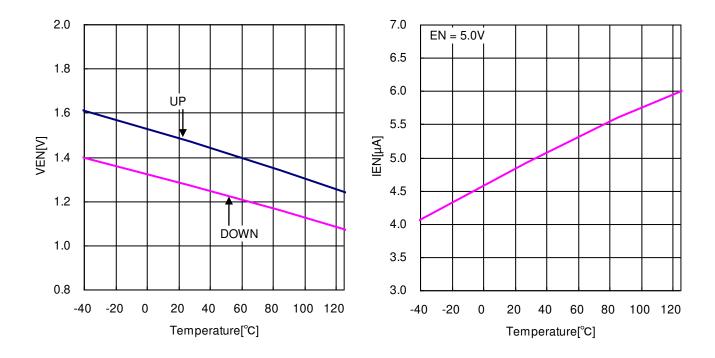


Figure 16. PGD Voltage vs Temperature

Figure 17. PGD Voltage vs Temperature





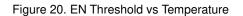


Figure 21. EN Input Current vs Temperature

# **Typical Performance Curves (Application)**

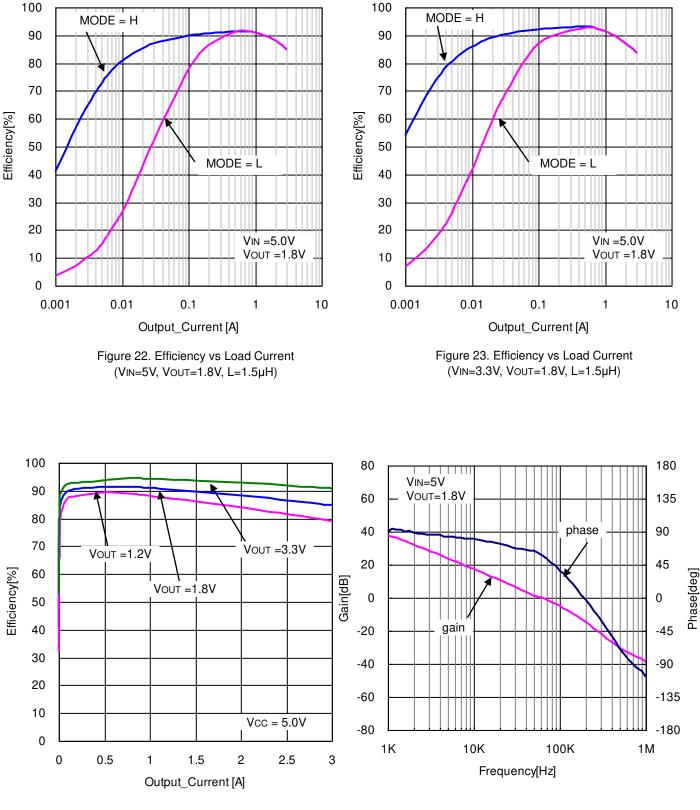


Figure 24. Efficiency vs Load Current (VIN = 5.0V, MODE = 5.0V, L= $1.5\mu$ H)

Figure 25. Closed Loop Response (VIN=5V, VOUT=1.8V, IOUT=1A, L=1.5  $\mu H,$  Cout=Ceramic 44  $\mu F)$ 

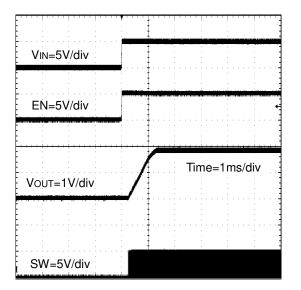


Figure 26. Power Up (VIN = EN)

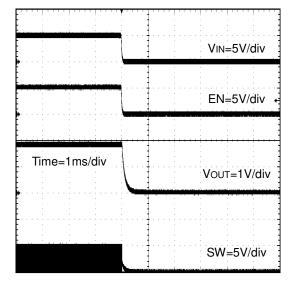


Figure 27. Power Down (VIN = EN)

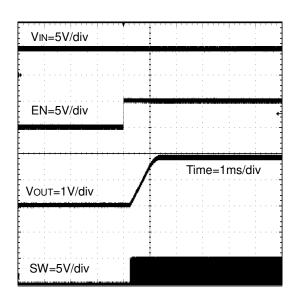


Figure 28. Power Up (EN =  $0V \rightarrow 5V$ )

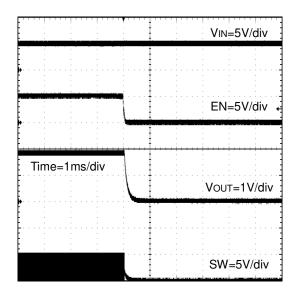


Figure 29. Power Down (EN =  $5V \rightarrow 0V$ )



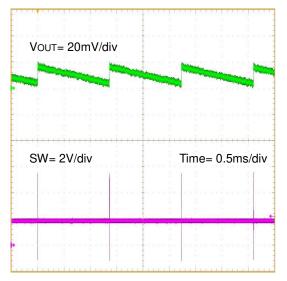


Figure 30. Output Ripple ( $V_{IN} = 5V$ ,  $V_{OUT} = 1.8V$ ,  $I_{OUT} = 0A$ )

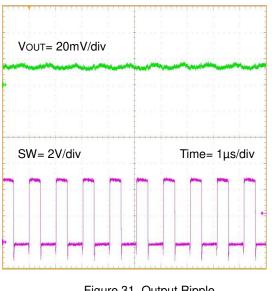
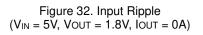


Figure 31. Output Ripple ( $V_{IN} = 5V$ , VOUT = 1.8V, IOUT = 3A)

VIN=50mV/div	
SW=2V/div	Time=20ms/div



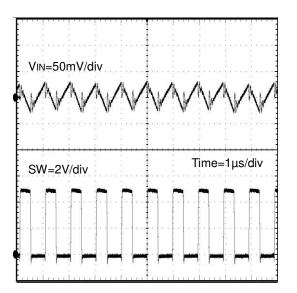


Figure 33. Input Ripple (V\_{IN} = 5V, VOUT = 1.8V, IOUT = 3A)

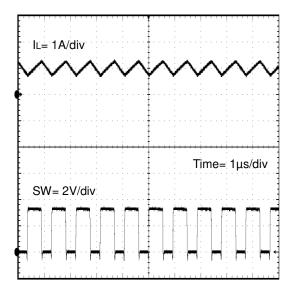


Figure 34. Switching Waveform (VIN = 3.3V, VOUT = 1.8V, IOUT = 1A, L=1.5  $\mu H)$ 

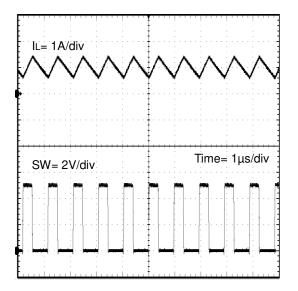


Figure 35. Switching Waveform (VIN = 5.0V, VOUT = 1.8V, IOUT = 1A, L=1.5 $\mu$ H)

I∟= 500mA/div	
	Time= 10µs/div
SW= 2V/div	SLLM <sup>™</sup> Control
	ļ

Figure 36. Switching Waveform with SLLM<sup>TM</sup> (VIN = 3.3V, VOUT = 1.8V, IOUT = 30mA, L=1.5 $\mu$ H)

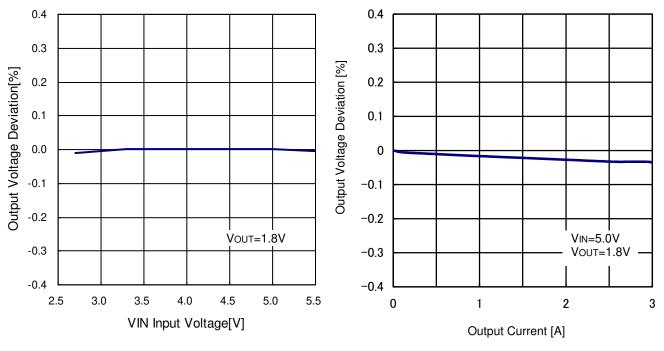


Figure 37. Line Regulation vs Input Voltage

Figure 38. Load Regulation vs Load Current

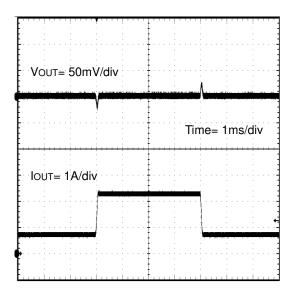


Figure 39. Load Transient Response IOUT= 0.75A to 2.25A load step (VIN= 5V, VOUT= 1.8V, COUT= Ceramic 44µF)

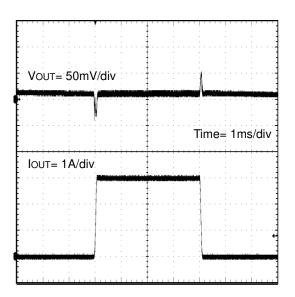


Figure 40. Load Transient Response IOUT=0A to 3A load step (VIN= 5V, VOUT= 1.8V, COUT= Ceramic  $44\mu$ F)

- 1. Function Explanations
  - (1) DC/DC converter operation

BD9A301MUV-LB is a synchronous rectifying step-down switching regulator that achieves faster transient response by employing current mode PWM control system. It utilizes switching operation in PWM (Pulse Width Modulation) mode for heavier load, while it utilizes SLLM (Simple Light Load Mode) control for lighter load to improve efficiency.

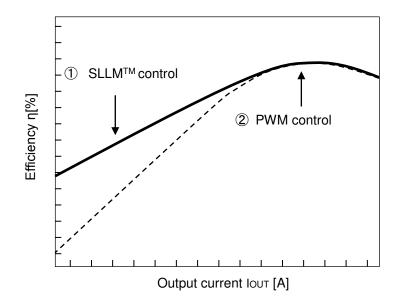
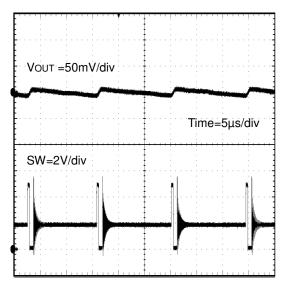
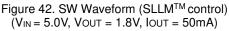


Figure 41. Efficiency (SLLM<sup>TM</sup> control and PWM control)

# SLLM<sup>™</sup> control





2 PWM control

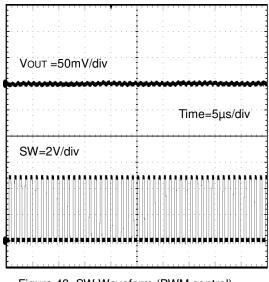
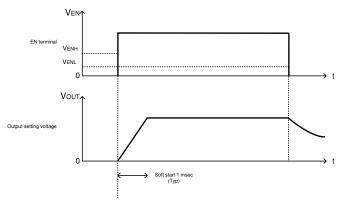
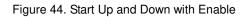


Figure 43. SW Waveform (PWM control)  $(V_{IN} = 5.0V, VOUT = 1.8V, IOUT = 1A)$ 

# (2) Enable Control

The IC shutdown can be controlled by the voltage applied to the EN terminal. When VEN reaches 1.5V (Typ), the internal circuit is activated and the IC starts up. To enable shutdown control with the EN terminal, the shutdown interval (Low level interval of EN) must be set to 100µs or longer.





# (3) Power Good

When the output voltage reaches outside  $\pm 10\%$  of the voltage setting, the open drain N-ch MOSFET internally connected to the PGD terminal turns on and the PGD terminal is pulled down with an impedance of  $100\Omega$  (Typ). A hysteresis of 3% applies to resetting. Connecting a pull up resistor ( $10k\Omega$  to  $100k\Omega$ ) is recommended.

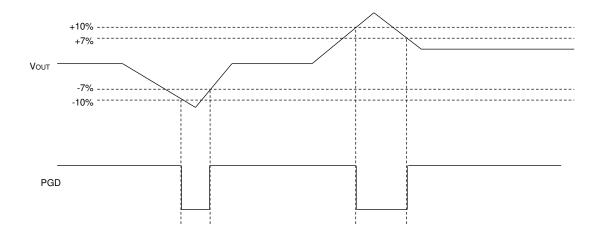


Figure 45. PGD Timing Chart

# 2. Protection

# The protective circuits are intended for prevention of damage caused by unexpected accidents. Do not use them for continuous protective operation.

(1) Short Circuit Protection (SCP)

The short circuit protection block compares the FB terminal voltage with the internal reference voltage VREF. When the FB terminal voltage has fallen below 0.4V (Typ) and remained there for 1msec (Typ), SCP stops the operation for 16msec (Typ) and subsequently initiates a restart.

EN Terminal	FB Terminal	Short Circuit Protection	Short Circuit Protection Operation
2.0V or higher	<0.4V(Typ)	Enabled	ON
2.0V OF Higher	>0.4V(Typ)	Enabled	OFF
0.8V or lower	-	Disabled	OFF

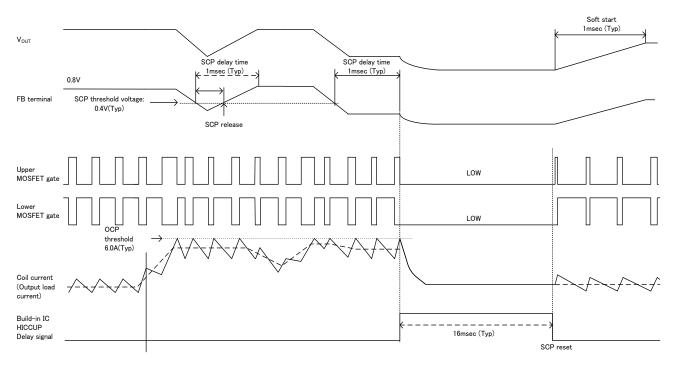


Figure 46. Short Circuit Protection (SCP) timing chart

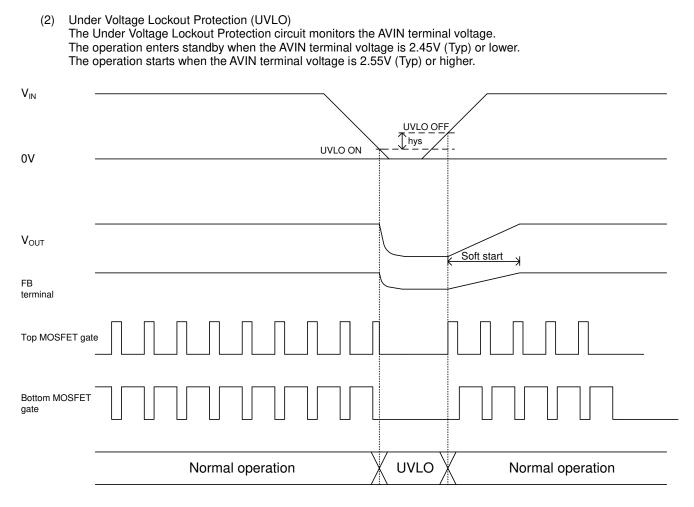


Figure 47. UVLO Timing Chart

(3) Thermal Shutdown

When the chip temperature exceeds  $Tj = 175^{\circ}C$ , the DC/DC converter output is stopped. The thermal shutdown circuit is intended for shutting down the IC from thermal runaway in an abnormal state with the temperature exceeding Tjmax =  $150^{\circ}C$ . It is not meant to protect or guarantee the soundness of the application. Do not use the function of this circuit for application protection design.

(4) Over Current Protection

The Over Current Protection function operates by using the current mode control to limit the current that flows through the high-side MOSFET at each cycle of the switching frequency. The designed over current limit value is 6.0A (Typ).

(5) Over Voltage Protection (OVP)

Over voltage protection function (OVP) compares FB terminal voltage with internal standard voltage VREF and when FB terminal voltage exceeds 0.88V (Typ) it turns MOSFET of output part MOSFET off. After output voltage drop it returns with hysteresis.

# **Application Example**

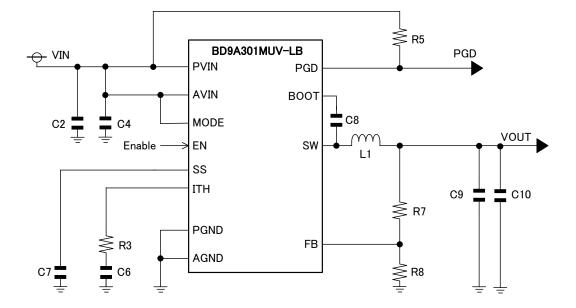


Figure 48. Application Circuit

Reference	Output Voltage					Description
Designator	1.1V	1.2V	1.5V	1.8V	3.3V	Description
R3	8.2kΩ	8.2kΩ	9.1kΩ	9.1kΩ	18kΩ	-
R5	100kΩ	100kΩ	100kΩ	100kΩ	100kΩ	-
R7	10kΩ	10kΩ	16kΩ	30kΩ	75kΩ	-
R8	27kΩ	20kΩ	18kΩ	24kΩ	24kΩ	-
C2	10µF	10µF	10µF	10µF	10µF	10V, X5R, 3216
C4	0.1µF	0.1µF	0.1µF	0.1µF	0.1µF	25V, X5R, 1608
C6	2700pF	2700pF	2700pF	2700pF	2700pF	-
C7	0.01µF	0.01µF	0.01µF	0.01µF	0.01µF	-
C8	0.1µF	0.1µF	0.1µF	0.1µF	0.1µF	-
C9	22µF	22µF	22µF	22µF	22µF	10V, X5R, 3225
C10	22µF	22µF	22µF	22µF	22µF	10V, X5R, 3225
L1	1.5µH	1.5µH	1.5µH	1.5µH	1.5µH	TOKO, FDSD0630

# Selection of Components Externally Connected

# 1. Output LC Filter Constant

The DC/DC converter requires an LC filter for smoothing the output voltage in order to supply a continuous current to the load. BD9A301MUV-LB is returned to the IC and IL ripple current flowing through the inductor for SLLM<sup>™</sup> control. This feedback current, Inductance value is the behavior of the best when the 1.5µH. Therefore, the inductor to use is recommended 1.5µH.

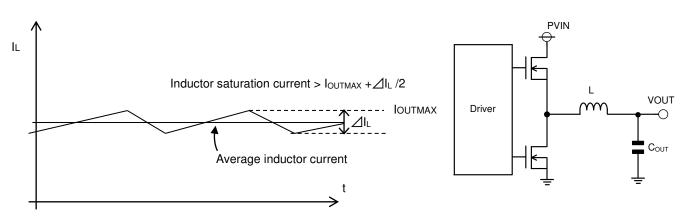


Figure 49. Waveform of current through inductor

Figure 50. Output LC filter circuit

Computation with VIN = 5V, VOUT = 1.8V, L=1.5µH, and the switching frequency Fosc = 1MHz, the method is as below.

Inductor ripple current  $\Delta IL$ 

$$\Delta I_{L} = V_{OUT} \times (V_{IN} - V_{OUT}) \times \frac{1}{V_{IN} \times F_{OSC} \times L} = 768 [\text{mA}]$$

The saturation current of the inductor must be larger than the sum of the maximum output current and 1/2 of the inductor ripple current  $\Delta IL$ .

The output capacitor  $C_{OUT}$  affects the output ripple voltage characteristics. The output capacitor  $C_{OUT}$  must satisfy the required ripple voltage characteristics.

The output ripple voltage can be represented by the following equation.

$$\Delta V_{RPL} = \Delta I_L \times (R_{ESR} + \frac{1}{8 \times C_{OUT} \times F_{OSC}}) [V]$$

 $R_{ESR}$  is the Equivalent Series Resistance (ESR) of the output capacitor. With Cout =  $44\mu F,$  ResR =  $10m\Omega$  the output ripple voltage is calculated as

$$\Delta V_{RPL} = 0.768 \times (10m + \frac{1}{(8 \times 44\mu \times 1MHz)}) = 9.8 [\text{mV}]$$

\*Be careful of total capacitance value, when additional capacitor CLOAD is connected in addition to output capacitor COUT. Use maximum additional capacitor CLOAD(max.) condition which satisfies the following method.

Maximum starting inductor ripple current  $IL_{START}$  < Over Current limit 3.8A(min)

Maximum starting inductor ripple current ILSTART can be expressed in the following method.

$$IL_{START} = Maximum \ starting \ output \ current(I_{OMAX}) + Charge \ current \ to \ output \ capacitor(I_{CAP}) + \frac{\Delta I_L}{2}$$

Charge current to output capacitor  $I_{CAP}$  can be expressed in the following method.

$$I_{CAP} = \frac{(C_{OUT} + C_{LOAD}) \times V_{OUT}}{T_{SS}} [A]$$

Computation with VIN= 5V, VOUT= 3.3V, L= 1.5 $\mu$ H, switching frequency F<sub>OSC</sub>= 800kHz(Min), Output capacitor COUT= 44 $\mu$ F, Soft Start time Tss= 0.5ms(Min), load current during soft start loss= 2A the method is as below.

$$C_{LOAD}(max) < \frac{(3.8 - I_{OSS} - \Delta I_{L}/2) \times T_{SS}}{V_{OUT}} - C_{OUT} = 157.9 [\mu F]$$

If the value of C<sub>LOAD</sub> is large, and cannot meet the above equation,

$$C_{LOAD}(max) < \frac{(1.5 - I_{OSS} - \Delta I_L/2) \times V_{FB}}{V_{OUT} \times I_{SS}} \times C_{SS} - C_{OUT}$$

Adjust the value of the capacitor Css to meet the above formula.

(Refer to the following items (3) Soft Start Setting equation of time T<sub>SS</sub> and soft-start value of the capacitor to be connected to the C<sub>SS</sub>.)

Computation with VIN = 5V, VOUT = 3.3V, L =  $1.5\mu$ H, load current during soft start Ioss = 2A, switching frequency Fosc= 800kHz (Min), Output capacitor COUT =  $44\mu$ F, VFB = 0.792V(Max), Iss =  $3.6\mu$ A(Max), A capacitor connected to the Css if you want to connect the CLOAD = 220uF is the following equation.

$$C_{SS} > \frac{V_{OUT} \times I_{SS}}{(3.8 - I_{OSS} - \Delta I_L/2) \times V_{FB}} \times (C_{LOAD} + C_{OUT}) = 2.97 [\text{nF}]$$

2. Output Voltage Setting

The output voltage value can be set by the feedback resistance ratio.

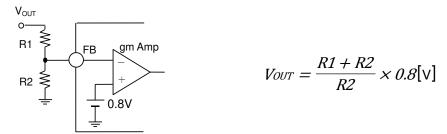


Figure 51. Feedback Resistor Circuit

3. Soft Start Setting

Turning the EN terminal signal high activates the soft start function. This causes the output voltage to rise gradually while the current at startup is placed under control. This allows the prevention of output voltage overshoot and inrush current. The rise time depends on the value of the capacitor connected to the SS terminal.

$$T_{SS} = (C_{SS} \times V_{FB}) / I_{SS}$$

 $T_{SS}$  : Soft Start Time

 $C_{SS}$  : Capacitor connected to Soft Start Time Termind

V<sub>FB</sub> : FB TerminalVoltage(0.8V (Typ))

 $I_{SS}$  : Soft Start TerminalSource Current (1.8µA(Typ))

with 
$$C_{SS} = 0.01 \mu F$$
,  
 $T_{SS} = (0.010 [\mu F] \times 0.8 [V]) / 1.8 [\mu A]$   
 $= 4.44 [msec]$ 

Turning the EN terminal signal high with the SS terminal open (no capacitor connected) or with the terminal signal high causes the output voltage to rise in 1msec (Typ).

# BD9A301MUV-LB

# 4. Phase Compensation Component

A current mode control buck DC/DC converter is a one-pole, one-zero system. One poles are formed by an error amplifier and load and the one zero point is added by phase compensation. The phase compensation resistor  $R_{ITH}$  determines the crossover frequency  $F_{CRS}$  where the total loop gain of the DC/DC converter is 0dB. A high value crossover frequency  $F_{CRS}$  provides a good load transient response characteristic but inferior stability. Conversely, a low value crossover frequency  $F_{CRS}$  greatly stabilizes the characteristics but the load transient response characteristic is impaired.

(1) Selection of Phase Compensation Resistor R<sub>ITH</sub> The Phase Compensation Resistance R<sub>ITH</sub> can be determined by using the following equation.

$$R_{ITH} = \frac{2\pi \times V_{OUT} \times F_{CRS} \times C_{OUT}}{V_{FB} \times G_{MP} \times G_{MA}} [\Omega]$$

V<sub>OUT</sub> : Output Voltage[V]

 $F_{CRS}$ : Crossover Frequency[Hz]

 $C_{OUT}$ : Output Capacitan@[F]

 $V_{FB}$  : Feedback Reference Voltage(0.8V (Typ))

G<sub>MP</sub> : Current Sense Gain (13A/V (Typ))

 $G_{MA}$  : Error AmplifierTrans conductance (260µA /V(Typ))

(2) Selection of Phase Compensation Capacitance CITH For stable operation of the DC/DC converter, zero for compensation cancels the phase delay due to the pole formed by the load.

The phase compensation capacitance  $C_{\text{ITH}}$  can be determined by using the following equation.

$$C_{ITH} = \frac{C_{OUT} \times V_{OUT}}{R_{ITH} \times I_{OUT}} [F]$$

(3) Loop stability

To ensure the stability of the DC/DC converter, make sure that a sufficient phase margin is provided. A phase margin of at least 45° in the worst conditions is recommended.

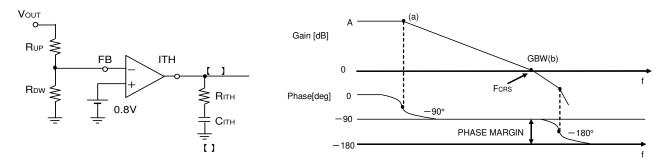


Figure 52. Phase Compensation Circuit

Figure 53. Bode Plot

# **PCB Layout Design**

In the buck DC/DC converter, a large pulse current flows into two loops. The first loop is the one into which the current flows when the high-side FET is turned on. The flow starts from the input capacitor  $C_{IN}$ , runs through the FET, inductor L and output capacitor  $C_{OUT}$  and back to GND of  $C_{IN}$  via GND of  $C_{OUT}$ . The second loop is the one into which the current flows when the low-side FET is turned on. The flow starts from the low-side FET, runs through the inductor L and output capacitor  $C_{OUT}$  and back to GND of the low-side FET via GND of  $C_{OUT}$ . Route these two loops as thick and as short as possible to allow noise to be reduced for improved efficiency. It is recommended to connect the input and output capacitors directly to the GND plane. The PCB layout has a great influence on the DC/DC converter in terms of all of the heat generation, noise and efficiency characteristics.

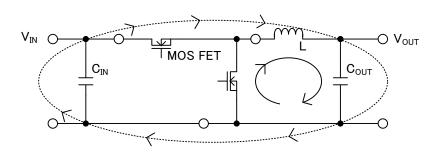
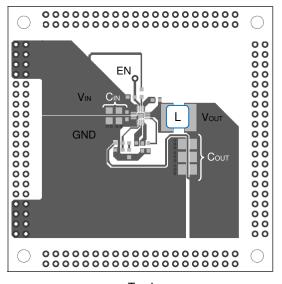
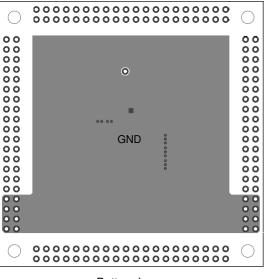


Figure 54. Current Loop of Buck DC/DC Converter

Accordingly, design the PCB layout considering the following points.

- Connect an input capacitor as close as possible to the IC PVIN terminal on the same plane as the IC.
- If there is any unused area on the PCB, provide a copper foil plane for the GND node to assist heat dissipation from the IC and the surrounding components.
- Switching nodes such as SW are susceptible to noise due to AC coupling with other nodes. Route the coil pattern as thick and as short as possible.
- Provide lines connected to FB and ITH far from the SW nodes.
- · Place the output capacitor away from the input capacitor in order to avoid the effect of harmonic noise from the input.





Top Layer

Bottom Layer

Figure 55. Example of evaluation board layout

# **Power Dissipation**

When designing the PCB layout and peripheral circuitry, sufficient consideration must be given to ensure that the power dissipation is within the allowable dissipation curve.

This package incorporates an exposed thermal pad. Solder directly to the PCB ground plane. After soldering, the PCB can be used as a heatsink.

The exposed thermal pad dimensions for this package are shown in page 31.

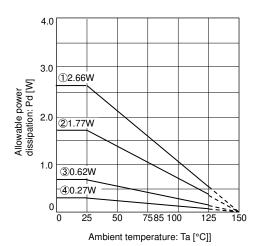
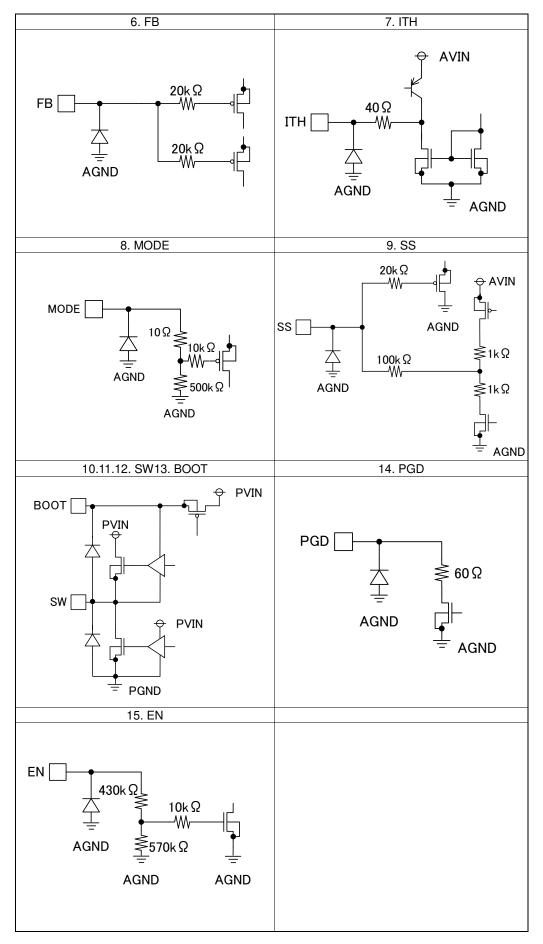


Figure 56. Thermal Derating Characteristics (VQFN016V3030)

- (1)4-layer board (surface heat dissipation copper foil 5505mm2) (copper foil laminated on each layer)  $\theta_{JA}=47.0^{\circ}C/W$
- (2) 4-layer board (surface heat dissipation copper foil 6.28mm<sup>2</sup>) (copper foil laminated on each layer)  $\theta_{JA}=70.62^{\circ}C/W$
- (3) 1-layer board (surface heat dissipation copper foil 6.28mm<sup>2</sup>)  $\theta_{JA}=201.6^{\circ}C/W$
- (4) IC only
- θ <sub>JA</sub>=462.9°C/W

# I/O equivalence circuits



# **Operational Notes**

# 1. Reverse Connection of Power Supply

Connecting the power supply in reverse polarity can damage the IC. Take precautions against reverse polarity when connecting the power supply, such as mounting an external diode between the power supply and the IC's power supply pins.

# 2. Power Supply Lines

Design the PCB layout pattern to provide low impedance supply lines. Separate the ground and supply lines of the digital and analog blocks to prevent noise in the ground and supply lines of the digital block from affecting the analog block. Furthermore, connect a capacitor to ground at all power supply pins. Consider the effect of temperature and aging on the capacitance value when using electrolytic capacitors.

# 3. Ground Voltage

Ensure that no pins are at a voltage below that of the ground pin at any time, even during transient condition.

# 4. Ground Wiring Pattern

When using both small-signal and large-current ground traces, the two ground traces should be routed separately but connected to a single ground at the reference point of the application board to avoid fluctuations in the small-signal ground caused by large currents. Also ensure that the ground traces of external components do not cause variations on the ground voltage. The ground lines must be as short and thick as possible to reduce line impedance.

# 5. Thermal Consideration

Should by any chance the power dissipation rating be exceeded the rise in temperature of the chip may result in deterioration of the properties of the chip. The absolute maximum rating of the Pd stated in this specification is when the IC is mounted on a 70mm x 70mm x 1.6mm 4-layer glass epoxy board. In case of exceeding this absolute maximum rating increase the board size and copper area to prevent exceeding the Pd rating.

# 6. Recommended Operating Conditions

These conditions represent a range within which the expected characteristics of the IC can be approximately obtained. The electrical characteristics are guaranteed under the conditions of each parameter.

# 7. Inrush Current

When power is first supplied to the IC, it is possible that the internal logic may be unstable and inrush current may flow instantaneously due to the internal powering sequence and delays, especially if the IC has more than one power supply. Therefore, give special consideration to power coupling capacitance, power wiring, width of ground wiring, and routing of connections.

#### 8. Operation Under Strong Electromagnetic Field

Operating the IC in the presence of a strong electromagnetic field may cause the IC to malfunction.

# 9. Testing on Application Boards

When testing the IC on an application board, connecting a capacitor directly to a low-impedance output pin may subject the IC to stress. Always discharge capacitors completely after each process or step. The IC's power supply should always be turned off completely before connecting or removing it from the test setup during the inspection process. To prevent damage from static discharge, ground the IC during assembly and use similar precautions during transport and storage.

#### 10. Inter-pin Short and Mounting Errors

Ensure that the direction and position are correct when mounting the IC on the PCB. Incorrect mounting may result in damaging the IC. Avoid nearby pins being shorted to each other especially to ground, power supply and output pin. Inter-pin shorts could be due to many reasons such as metal particles, water droplets (in very humid environment) and unintentional solder bridge deposited in between pins during assembly to name a few.

# **Operational Notes – continued**

#### **Unused Input Pins** 11.

Input pins of an IC are often connected to the gate of a MOS transistor. The gate has extremely high impedance and extremely low capacitance. If left unconnected, the electric field from the outside can easily charge it. The small charge acquired in this way is enough to produce a significant effect on the conduction through the transistor and cause unexpected operation of the IC. So unless otherwise specified, unused input pins should be connected to the power supply or ground line.

#### 12. **Regarding the Input Pin of the IC**

This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated. P-N junctions are formed at the intersection of the P layers with the N layers of other elements, creating a parasitic diode or transistor. For example (refer to figure below):

When GND > Pin A and GND > Pin B, the P-N junction operates as a parasitic diode. When GND > Pin B, the P-N junction operates as a parasitic transistor.

Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, operational faults, or physical damage. Therefore, conditions that cause these diodes to operate, such as applying a voltage lower than the GND voltage to an input pin (and thus to the P substrate) should be avoided.

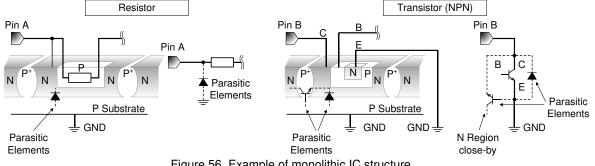


Figure 56. Example of monolithic IC structure

#### 13. **Ceramic Capacitor**

When using a ceramic capacitor, determine the dielectric constant considering the change of capacitance with temperature and the decrease in nominal capacitance due to DC bias and others.

#### 14. Area of Safe Operation (ASO)

Operate the IC such that the output voltage, output current, and power dissipation are all within the Area of Safe Operation (ASO).

#### 15. Thermal Shutdown Circuit(TSD)

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. Normal operation should always be within the IC's power dissipation rating. If however the rating is exceeded for a continued period, the junction temperature (Tj) will rise which will activate the TSD circuit that will turn OFF all output pins. When the Tj falls below the TSD threshold, the circuits are automatically restored to normal operation.

Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.

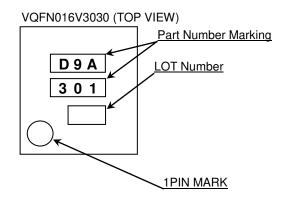
#### 16. Over Current Protection Circuit (OCP)

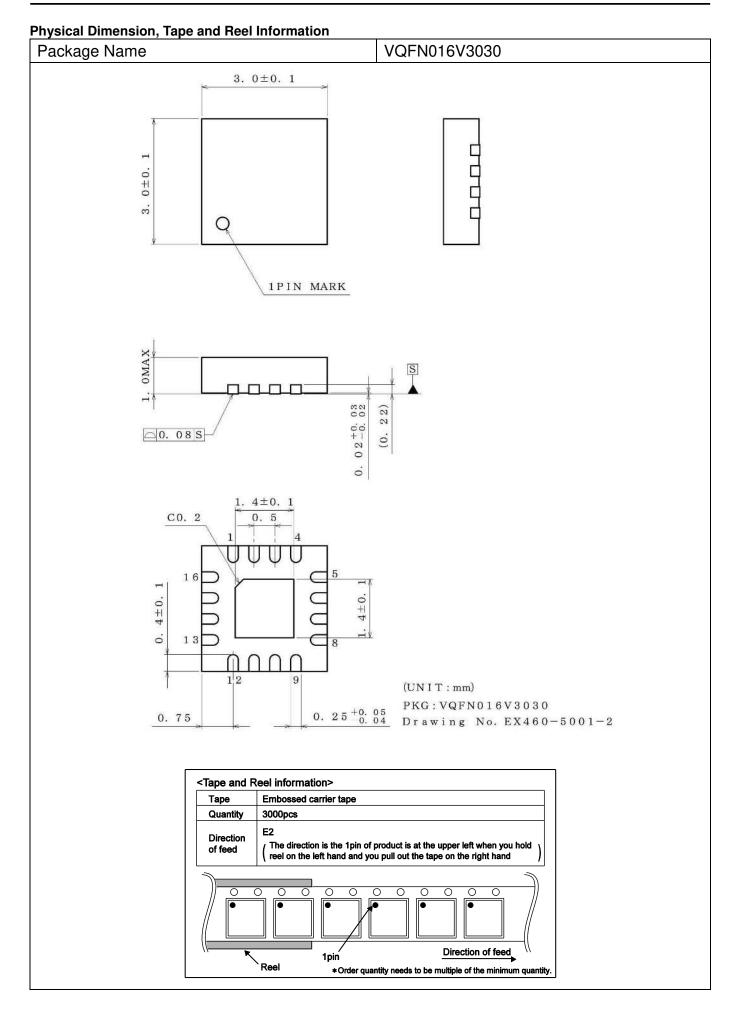
This IC incorporates an integrated overcurrent protection circuit that is activated when the load is shorted. This protection circuit is effective in preventing damage due to sudden and unexpected incidents. However, the IC should not be used in applications characterized by continuous operation or transitioning of the protection circuit.

# **Ordering Information**



# **Marking Diagrams**





# **Revision History**

Date	Revision	Changes
20.Aug.2014	001	New Release
20.Jul.2017	002	Modified EN electrical Characteristics

# Notice

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- 4. The Products are not subject to radiation-proof design.
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- 6. In particular, if a transient load (a large amount of load applied in a short period of time, such as pulse. is applied, confirmation of performance characteristics after on-board mounting is strongly recommended. Avoid applying power exceeding normal rated power; exceeding the power rating under steady-state loading condition may negatively affect product performance and reliability.
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For details, please refer to ROHM Mounting specification

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