

### **Normally – OFF Silicon Carbide Junction Transistor**

#### **Features Package**

- 175 °C Maximum Operating Temperature
- Gate Oxide Free SiC Switch
- Optional Gate Return Pin
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Temperature Independent Switching Performance
- Low Output Capacitance
- $\bullet$  Positive Temperature Coefficient of  $R_{DS,ON}$
- Suitable for Connecting an Anti-parallel Diode

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20 µs Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- Minimal Input Signal Distortion
- High Amplifier Bandwidth





 $V_{DS}$  = 1200 V







#### pins are not exchangeable. Their exchange might lead to malfunction.

Source

Drain (TAB)

#### Advantages **Advantages Applications Applications**

- Down Hole Oil Drilling, Geothermal Instrumentation
- Hybrid Electric Vehicles (HEV)
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)
- Induction Heating
- Uninterruptible Power Supply (UPS)
- Motor Drives

### **Table of Contents**



#### <span id="page-0-0"></span>**Section I: Absolute Maximum Ratings**



### **GA10JT12-263**



### <span id="page-1-0"></span>**Section II: Static Electrical Characteristics**



### <span id="page-1-1"></span>**Section III: Dynamic Electrical Characteristics**





 $1 -$  All times are relative to the Drain-Source Voltage V<sub>DS</sub>

# **GeneSiC**

## **GA10JT12-263**

<span id="page-2-0"></span>**Section IV: Figures**







**Figure 3: Typical Output Characteristics at 175 °C Figure 4: DC Current Gain vs. Drain Current** 



<span id="page-2-1"></span>Figure 5: On-Resistance vs. Gate Current **Figure 6: On-Resistance vs. Temperature Figure 6: On-Resistance vs.** Temperature



**Figure 1: Typical Output Characteristics at 25 °C Figure 2: Typical Output Characteristics at 150 °C**



<span id="page-2-2"></span>





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<span id="page-3-0"></span>



<span id="page-3-2"></span>



<span id="page-3-4"></span>**Figure 12: Typical Switching Times and Turn Off Energy Losses vs. Temperature** 

<span id="page-3-5"></span>**B: Dynamic Characteristics** 



<span id="page-3-1"></span>**Figure 9: Input, Output, and Reverse Transfer Capacitance Figure 10: Energy Stored in Output Capacitance**



<span id="page-3-3"></span>**Figure 11: Typical Switching Times and Turn On Energy Losses vs. Temperature** 





<span id="page-4-2"></span>**Figure 13: Typical Switching Times and Turn On Energy Losses vs. Drain Current**





Figure 15: Typical Hard Switched Device Power Loss vs.<br>Switching Frequency<sup>2</sup>



<span id="page-4-0"></span>

 **GA10JT12-263**



<span id="page-4-3"></span>**Figure 14: Typical Switching Times and Turn Off Energy Losses vs. Drain Current**



<span id="page-4-1"></span>



 $^2$  – Representative values based on device conduction and switching loss. Actual losses will depend on gate drive conditions, device load, and circuit topology.

#### Genes  $\mathsf{C}$  $\Omega$

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### **GA10JT12-263**

<span id="page-5-0"></span>

<span id="page-5-1"></span>



#### <span id="page-6-0"></span>**Section V: Driving the GA10JT12-263**



#### **A: Static TTL Logic Driving**

The GA10JT12-263 may be driven with direct (5 V) TTL logic and current amplification. The amplified current level of the supply must meet or exceed the steady state gate current ( $I_{G,steady}$ ) required to operate the GA10JT12-263. Minimum  $I_{G,steady}$  is dependent on the anticipated drain current I<sub>D</sub> through the SJT and the DC current gain h<sub>FE</sub>, it may be calculated from the following equation. An accurate value of the h<sub>FE</sub> may be read from [Figure 4.](#page-2-2) An optional resistor R<sub>G</sub> may be used in series with the gate pin to trim  $I_{G,steady}$  also an optional capacitor C<sub>G</sub> may be added in parallel with  $R<sub>G</sub>$  to facilitate faster SJT switching if desired, further details on these options are given in the following section.



**Figure 21: TTL Gate Drive Schematic**

#### **B: High Speed Driving**

The SJT is a current controlled transistor which requires a positive gate current for turn-on and to remain in on-state. An idealized gate current waveform for ultra-fast switching of the SJT while maintaining low gate drive losses is shown in [Figure 22,](#page-6-1) it features a positive current peak during turn-on, a negative current peak during turn-off, and continuous gate current during on-state.



**Figure 22: An idealized gate current waveform for fast switching of an SJT.**

<span id="page-6-1"></span>An SJT is rapidly switched from its blocking state to on-state when the necessary gate charge,  $Q<sub>G</sub>$ , for turn-on is supplied by a burst of high gate current,  $I_{G,on}$ , until the SJT gate-source capacitance,  $C_{GS}$ , and gate-drain capacitance,  $C_{GD}$ , are fully charged.

$$
Q_{on} = I_{G,on} * t_1
$$

$$
Q_{on} \ge Q_{gs} + Q_{gd}
$$



Ideally, I<sub>G, on</sub> should terminate when the drain voltage falls to its on-state value in order to avoid unnecessary drive losses during the steady onstate. In practice, the rise time of the I<sub>G,on</sub> pulse is affected by the parasitic inductances, L<sub>par</sub> in the device package and drive circuit. A voltage developed across the parasitic inductance in the source path, Ls, can de-bias the gate-source junction, when high drain currents begin to flow through the device. The voltage applied to the gate pin should be maintained high enough, above the  $V_{GS, sat}$  (see [Figure 7\)](#page-3-5) level to counter these effects.

A high negative peak current, -I<sub>G,off</sub> is recommended at the start of the turn-off transition, in order to rapidly sweep out the injected carriers from the gate, and achieve rapid turn-off. Turn off can be achieved with  $V_{GS} = 0$  V, however a negative gate voltage  $V_{GS}$  may be used in order to speed up the turn-off transition.

#### **Gate Return Pin**

The optional gate return (GR) pin allows for a reduction of source path inductive and resistive coupling in the gate driver connection to the GA10JT12-263. Drain currents through the source pin during transient and steady state operation induce an undesirable source voltage in all power transistors due to unavoidable source pin inductance and resistance. This voltage can negatively affect gate driving performance, however the gate return pin allows for decoupling from these source current path effects which results in faster switching and higher efficiency gate driving.

#### **B:1: High Speed, Low Loss Drive with Boost Capacitor, GA03IDDJT30-FR4**

The GA10JT12-263 may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide fast switching current peaks at turn-on and turn-off and a continuous gate current while in on-state. A 3 kV isolated evaluation gate drive board [\(GA03IDDJT30-FR4\)](http://www.genesicsemi.com/images/products_sic/sjt/GA03IDDJT30-FR4.pdf) utilizing this topology is commercially available for high and lowside driving, its datasheet provides additional details about this drive topology.



**Figure 23: Topology of the GA03IDDJT30-FR4 Two Voltage Source gate driver.** 

The GA03IDDJT30-FR4 evaluation board comes equipped with two on board gate drive resistors (RG1, RG2) pre-installed for an effective gate resistance $^3$  of R $_\mathrm{G}$  = 3.75 $\Omega$ . It may be necessary for the user to reduce RG1 and RG2 under high drain current conditions for safe operation of the GA10JT12-263. The steady state current supplied to the gate pin of the GA10JT12-263 with on-board R<sub>G</sub> = 3.75 Ω, is shown i[n Figure 24.](#page-8-0) The maximum allowable safe value of RG for the user's required drain current can be read from [Figure 25.](#page-8-1) 

#### For the GA10JT12-263,  $R_G$  must be reduced for  $I_D \geq -11$  A for safe operation with the GA03IDDJT30-FR4.

For operation at  $I_D \geq$  ~11 A, R<sub>G</sub> may be calculated from the following equation, which contains the DC current gain h<sub>FE</sub> [\(Figure 4\)](#page-2-2) and the gatesource saturation voltage  $V_{GS,sat}$  [\(Figure 7\)](#page-3-5).

$$
R_{G,max} = \frac{(4.7V - V_{GS,sat}) * h_{FE}(T, I_D)}{I_D * 1.5} - 0.6\Omega
$$



<span id="page-8-0"></span>**GA03IDDJT30-FR4 board for the GA10JT12-263 with the on board resistance of 3.75 Ω**

<span id="page-8-1"></span>

#### **B:2: High Speed, Low Loss Drive with Boost Inductor**

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the GA10JT12-263 at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses  $I_{G,on}$  and  $I_{G,off}$ . During operation, inductor L is charged to a specified  $I_{G,on}$ current value then made to discharge I<sub>L</sub> into the SJT gate pin using logic control of  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$ , as shown in [Figure 26.](#page-8-2) After turn on, while the device remains on the necessary steady state gate current *I<sub>G,steady*</sub> is supplied from source V<sub>CC</sub> through R<sub>G</sub>. Please refer to the article "A current-source concept for fast and efficient driving of silicon carbide transistors" by Dr. Jacek Rąbkowski for additional information on this driving topology.<sup>4</sup>



**Figure 26: Simplified Inductive Pulsed Drive Topology** 

<span id="page-8-2"></span> $^3$  – R<sub>G</sub> = (1/RG1 +1/RG2)<sup>-1</sup>. Driver is pre-installed with RG1 = RG2 = 7.5 Ω

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#### **C: Proportional Gate Current Driving**

For applications in which the GA10JT12-263 will operate over a wide range of drain current conditions, it may be beneficial to drive the device using a proportional gate drive topology to optimize gate drive power consumption. A proportional gate driver relies on instantaneous drain current  $I_D$  feedback to vary the steady state gate current  $I_{G, steady}$  supplied to the GA10JT12-263

#### **C:1: Voltage Controlled Proportional Driver**

The voltage controlled proportional driver relies on a gate drive IC to detect the GA10JT12-263 drain-source voltage  $V_{DS}$  during on-state to sense I<sub>D</sub>. The gate drive IC will then increase or decrease I<sub>G,steady</sub> in response to I<sub>D</sub>. This allows I<sub>G,steady</sub>, and thus the gate drive power consumption, to be reduced while  $I_D$  is relatively low or for  $I_{G,steady}$  to increase when is  $I_D$  higher. A high voltage diode connected between the drain and sense protects the IC from high-voltage when the driver and GA10JT12-263 are in off-state. A simplified version of this topology is shown in [Figure 27,](#page-9-0) additional information will be available in the future at<http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/>



**Figure 27: Simplified Voltage Controlled Proportional Driver**

#### <span id="page-9-0"></span>**C:2: Current Controlled Proportional Driver**

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback  $I<sub>D</sub>$  of the GA10JT12-263 during on-state to supply  $I_{G,steady}$  into the device gate.  $I_{G,steady}$  will then increase or decrease in response to  $I_D$  at a fixed forced current gain which is set be the turns ratio of the transformer,  $h_{\text{force}} = I_D / I_G = N_2 / N_1$ . GA10JT12-263 is initially turned-on using a gate current pulse supplied into an RC drive circuit to allow I<sub>D</sub> current to begin flowing. This topology allows I<sub>G,steady</sub>, and thus the gate drive power consumption, to be reduced while I<sub>D</sub> is relatively low or for I<sub>G,steady</sub> to increase when is I<sub>D</sub> higher. A simplified version of this topology is shown in Figure 28, additional information will be available in the future at [http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/.](http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/) 



<span id="page-9-1"></span>**Figure 28: Simplified Current Controlled Proportional Driver** 



### **Section VI: Package Dimensions**

#### <span id="page-10-0"></span> **TO-263-7L PACKAGE OUTLINE**





#### **NOTE**

1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.

2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS



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### GeneSiC SEMICONDUCTOR

#### <span id="page-11-0"></span>**Section VII: SPICE Model Parameters**

This is a secure document. Please copy this code from the SPICE model PDF file on our website [\(http://www.genesicsemi.com/images/products\\_sic/sjt/GA10JT12-263\\_SPICE.pdf\)](http://www.genesicsemi.com/images/products_sic/sjt/GA10JT12-263_SPICE.pdf) into LTSPICE (version 4) software for simulation of the GA10JT12-263.

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* MODEL OF GeneSiC Semiconductor Inc. 
* 
* $Revision: 2.0 $ 
* $Date: 20-NOV-2015 $ 
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* Models accurate up to 2 times rated drain current. 
* 
.model GA10JT12 NPN 
+ IS 9.833E-48
+ ISE 1.073E-26
+ EG 3.23
+ BF 87
+ BR 0.55
+ IKF 5000
+ NF 1 
+ NE 2 
+ RB 4.67
+ IRB 0.001
+ RBM 0.16
+ RE 0.005
+ RC 0.08
+ CJC 229.9E-12
+ VJC 3.22
+ MJC 0.492
+ CJE 1244E-9 
+ VJE 2.86
+ MJE 0.465
+ XTI 3 
+ XTB -1.35+ TRC1 7E-3 
+ VCEO 1200
+ ICRATING 10
+ MFG GeneSiC_Semiconductor
* 
* End of GA10JT12 SPICE Model
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