# <span id="page-0-0"></span>**Description**

The 8V41N012A is a PLL-based clock generator specifically designed for Cavium Networks Octeon II processors. This high-performance device is optimized to generate the processor core reference clock, the PCI-Express, sRIO, XAUI, SerDes reference clocks, and the clocks for both the Gigabit Ethernet MAC and PHY. The output frequencies are generated from a 25MHz external input source or an external 25MHz parallel resonant crystal.

The industrial temperature range of the 8V41N012A supports telecommunication, networking, and storage requirements.

### <span id="page-0-1"></span>Features

- Ten selectable 100MHz, 125MHz, 156.25MHz and 312.5MHz clocks for PCI Express, sRIO, and GbE, HCSL interface levels
- One single-ended QG LVCMOS/LVTTL clock output at 125MHz
- One single-ended QF LVCMOS/LVTTL clock output at 50MHz
- Two single-ended QREFx LVCMOS/LVTTL outputs at 25MHz
- Selectable external crystal or differential (single-ended) input source
- Crystal oscillator interface designed for 25MHz, parallel resonant crystal
- Differential CLK, nCLK input pair that can accept: LVPECL, LVDS, LVHSTL, and HCSL input levels
- Internal resistor bias on nCLK pin allows the user to drive CLK input with external single-ended (LVCMOS/ LVTTL) input levels
- Supply Modes, (125MHz QG output and 25MHz QREFx outputs):
	- Core / Output
	- 3.3V / 3.3V
	- 3.3V / 2.5V
- Supply Modes, (HCSL outputs, and 50MHz QF output):
	- Core / Output
	- 3.3V / 3.3V
- -40°C to 85°C ambient operating temperature
- 10 x 10 mm 72-VFQFPN, lead-free (RoHS 6) packaging

### <span id="page-1-0"></span>Block Diagram



# **Contents**



## <span id="page-3-0"></span>Pin Assignments



10 x 10 mm 72-VFQFPN

Note: Exposed pad must always be connected to GND. Note: Pin 1 is located at bottom left corner as shown.

### <span id="page-3-1"></span>Pin Descriptions





### Table 1. Pin Descriptions (Continued)



#### Table 1. Pin Descriptions (Continued)



Table 1. Pin Descriptions (Continued)

<b>Number</b>	<b>Name</b>	Type		<b>Description</b>
70	QG.	Output		Bank G single-ended output. 3.3V or 2.5V LVCMOS/LVTTL interface levels.
72	OE G	Input	Pullup	Active HIGH output enable for Bank G output. LVCMOS/LVTTL interface levels. $0 =$ Bank G outputs disabled/high impedance I = Bank G outputs enabled (default)
	EPAD			Connect to GND.

# <span id="page-6-0"></span>Pin Characteristics

<span id="page-6-2"></span>Table 2. Pin Characteristics<sup>[a]</sup>

Symbol	<b>Parameter</b>		<b>Test Conditions</b>	<b>Minimum</b>	<b>Typical</b>	<b>Maximum</b>	<b>Units</b>
$C_{\text{IN}}$	Input	CLK, nCLK			2.5		pF
	Capacitance	<b>Control Pins</b>			6		pF
R <sub>PULLUP</sub>	Input Pullup Resistor				50		$k\Omega$
R <sub>PULLDOWN</sub>	Input Pulldown Resistor				50		$k\Omega$
$R_{OUT}$	Output Impedance	QF, QG, QREF[1:0]	$V_{DDO_QF}$ = $V_{DDO_QG}$ = $V_{DDO_QREF}$ $= 3.\overline{4}65V$		15		W
		QG, QREF[1:0]	$V_{DDO QREF}$ , $V_{DDO QG}$ = 2.625V		19		W

[a] *Pullup* and *Pulldown* refer to internal input resistors. For typical values, see [Table 2.](#page-6-2)

# <span id="page-6-1"></span>Function Tables





[a] FSEL\_X denotes FSEL\_A, \_B, \_C, \_D, \_E.

[b] Any two outputs operated at the same frequency will be synchronous.



#### Table 4. PLL\_SEL Control Input Function Table

#### Table 5. REF\_SEL Control Input Function Table



#### Table 6. OE\_[A:E] Control Input Function Table



#### Table 7. OE\_G Control Input Function Table



#### Table 8. OE\_REF Control Input Function Table



# <span id="page-8-0"></span>Absolute Maximum Ratings

Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These ratings are stress specifications only. Functional operation of product at these conditions or any conditions beyond those listed in the *DC Characteristics or AC Characteristics* is not implied. Exposure to absolute maximum rating conditions for extended periods may affect product reliability.

#### Table 9. Absolute Maximum Ratings



# <span id="page-8-1"></span>DC Electrical Characteristics

Table 10. Power Supply DC Characteristics (V<sub>DD</sub> = 3.3V ±5%, V<sub>DDO Q[A:E]</sub> = V<sub>DDO Q[F:G]</sub> = V<sub>DDO QREF</sub> = 3.3V  $\pm$ 5%, T<sub>A</sub> = -40°C to 85°C)<sup>[a] [b]</sup>



[a] V<sub>DDO\_QX</sub> denotes V<sub>DDO\_Q[A:E],</sub> V<sub>DDO\_Q[F:G],</sub> V<sub>DDO\_QREF.</sub>

 $[b]$   $I_{DDO_QX}$  denotes  $I_{DDO_Q[A:E]+}$   $I_{DDO_Q[FE:G]+}$   $I_{DDO_QREF}$ .

#### Table 11. Power Supply DC Characteristics (V<sub>DD</sub> = VDDO\_Q[A:E] = VDDO\_QF = 3.3V ±5%, V<sub>DDO</sub>  $_{\text{QG}}$  = V<sub>DDO</sub>  $_{\text{QREF}}$  = 2.5V ± 5%, T<sub>A</sub> = -40°C to 85°C)



#### Table 12. LVCMOS/LVTTL DC Characteristics (V<sub>DD</sub> = V<sub>DDO\_Q[A:E]</sub> = V<sub>DDO\_QF</sub> = 3.3V ± 5%; V<sub>DDO\_QG</sub> = V<sub>DDO\_QREF</sub> = 3.3V ± 5% or 2.5V ± 5%, T<sub>A</sub> = -40°C to 85°C)



# Table 13. Differential DC Characteristics,  $V_{DD}$  = 3.3V  $\pm$  5%, T<sub>A</sub> = -40°C to 85°C<sup>[a][b]</sup>



[a]  $V_{\parallel}$  should not be less than -0.3V.

[b] Common mode voltage is defined as  $V_{\text{IH}}$ .

#### Table 14. Crystal Characteristics

Parameter	<b>Test Conditions</b>	<b>Minimum</b>	<b>Typical</b>	<b>Maximum</b>	<b>Units</b>
Mode of Oscillation Fundamental					
Frequency			25		MHz
Equivalent Series Resistance (ESR)				50	W
Load Capacitance (CL)			12		pF
Shunt Capacitance					pF

Table 15. Input Frequency Characteristics (V<sub>DD</sub> = V<sub>DDO\_Q[A:E]</sub> = V<sub>DDO\_QF</sub> = 3.3V ± 5%; V<sub>DDO\_QG</sub> = V<sub>DDO</sub> QREF = 3.3V ± 5% or 2.5V ± 5%, T<sub>A</sub> = -40°C to 85°C)



# <span id="page-10-0"></span>AC Electrical Characteristics

#### Table 16. PCI Express Jitter Specifications (V<sub>DD</sub> = V<sub>DDO\_Q[A:E]</sub> = 3.3V ± 5%, T<sub>A</sub> = -40°C to 85°C)



NOTE: Electrical parameters are guaranteed over the specified ambient operating temperature range, which is established when the device is mounted in a test socket with maintained transverse airflow greater than 500 lfpm. The device will meet specifications after thermal equilibrium has been reached under these conditions. For additional information, refer to the *PCI Express Application Note section* in the datasheet. NOTE 1: Peak-to-Peak jitter after applying system transfer function for the Common Clock Architecture. Maximum limit for PCI Express Gen 1 is 86ps peak-to-peak for a sample size of  $10^6$  clock periods.

NOTE 2: RMS jitter after applying the two evaluation bands to the two transfer functions defined in the Common Clock Architecture and reporting the worst case results for each evaluation band. Maximum limit for PCI Express Generation 2 is 3.1ps RMS for tREFCLK HF RMS (High Band) and 3.0ps RMS for t<sub>REFCLK</sub> LF RMS (Low Band).

NOTE 3: RMS jitter after applying system transfer function for the common clock architecture. This specification is based on the PCI Express Base Specification *Revision 0.7, October 200*9 and is subject to change pending the final release version of the specification. NOTE 4: This parameter is guaranteed by characterization. Not tested in production.

#### Table 17. HCSL AC Characteristics (V<sub>DD</sub> = V<sub>DDO\_Q[A:E]</sub> = V<sub>DDO\_QF</sub> = 3.3V ± 5%; V<sub>DDO\_QG</sub> = V<sub>DDO\_QREF</sub> = 3.3V  $\pm$  5% or 2.5V  $\pm$  5%, T<sub>A</sub> = -40°C to 85°C)



NOTE: Electrical parameters are guaranteed over the specified ambient operating temperature range, which is established when the device is mounted in a test socket with maintained transverse airflow greater than 500 lfpm. The device will meet specifications after thermal equilibrium has been reached under these conditions.

NOTE: All parameters measured at  $f_{\text{OUT}}$  and in PLL mode unless noted otherwise.

NOTE 1: Measurement taken from differential waveform.

NOTE 2: t<sub>STABLE</sub> is the time the differential clock must maintain a minimum  $\pm 150$ mV differential voltage after rising/falling edges before it is allowed to drop back into the  $V_{RB} \pm 100$ mV range. See Parameter Measurement Information Section.

NOTE 3: Measurement taken from single-ended waveform.

NOTE 4: Defined as the maximum instantaneous voltage including overshoot. See Parameter Measurement Information Section.

NOTE 5: Defined as the minimum instantaneous voltage including undershoot. See Parameter Measurement Information Section.

NOTE 6: Measured at the crossing point where the instantaneous voltage value of the rising edge of Q[Ax:Ex] equals the falling edge of nQ[Ax:Ex].

NOTE 7: Refers to the total variation from the lowest crossing point to the highest, regardless of which edge is crossing. Refers to all crossing points for this measurement.

NOTE 8: Defined as the total variation of all crossing voltages of rising Q[Ax:Ex] and falling nQ[Ax:Ex]. This is the maximum allowed variance in Vcross for any particular system.

NOTE 9: Measured from -150mV to +150mV on the differential waveform (derived from Q[Ax:Ex] minus nQ[Ax:Ex]). The signal must be monotonic through the measurement region for rise and fall time. The 300mV measurement window is centered on the differential zero crossing. NOTE 10: Measurements taken with 25MHz XTAL as input source and spur off.

#### Table 18. LVCMOS AC Characteristics (V<sub>DD</sub> = V<sub>DDO\_Q[A:E]</sub> = V<sub>DDO\_QF</sub> = 3.3V ± 5%; V<sub>DDO\_QG</sub> = V<sub>DDO\_QREF</sub> = 3.3V  $\pm$  5% or 2.5V  $\pm$  5%, T<sub>A</sub> = -40°C to 85°C)



NOTE: Electrical parameters are guaranteed over the specified ambient operating temperature range, which is established when the device is mounted in a test socket with maintained transverse airflow greater than 500 lfpm. The device will meet specifications after thermal equilibrium has been reached under these conditions.

NOTE: All parameters measured at  $f_{\text{OUT}}$  and in PLL mode unless noted otherwise.

NOTE 1: Measurements taken with 25MHz XTAL as input source and spur off.

### <span id="page-13-0"></span>Typical Phase Noise at 156.25MHz



**Offset Frequency (Hz)**

### <span id="page-14-0"></span>Parameter Measurement Information

<span id="page-14-1"></span>







This load condition is used for  $V_{MAX}$ ,  $V_{MIN}$ ,  $V_{RB}$ ,  $t_{STABLE}$ ,  $V_{CROSS,} \Delta V_{CROSS}$  and  $t_{SLEW\pm}$  measurements.

#### Figure 3. Differential Input Level



#### Figure 4. 3.3V Core/2.5V LVCMOS Output Load Test Circuit







This load condition is used for tjit and odc measurements.

#### Figure 6. RMS Phase Jitter











Figure 9. Single-ended Measurement Points for Delta Cross Point



Figure 10. LVCMOS Output Rise/Fall Time



#### Figure 11. Single-ended Measurement Points for Absolute Cross Point/Swing



#### Figure 12. Differential Measurement Points for Ringback







# <span id="page-17-0"></span>Application Information

### <span id="page-17-1"></span>Wiring the Differential Input to Accept Single-Ended Levels

[Figure 1](#page-14-1) shows how a differential input can be wired to accept single ended levels. The reference voltage  $V_1$ =  $V_{DD}/2$  is generated by the bias resistors R1 and R2. The bypass capacitor (C1) is used to help filter noise on the DC bias. This bias circuit should be located as close to the input pin as possible. The ratio of R1 and R2 might need to be adjusted to position the V<sub>1</sub>in the center of the input voltage swing. For example, if the input clock is driven from a single-ended 2.5V LVCMOS driver and the DC offset (or swing center) of this signal is 1.25V, the R1 and R2 values should be adjusted to set the V1 at 1.25V. The values below are for when both the single ended swing and  $V_{DD}$  are at the same voltage.





This configuration requires that the sum of the output impedance of the driver (Ro) and the series resistance (Rs) equals the transmission line impedance. In addition, matched termination at the input will attenuate the signal in half. This can be done in one of two ways. First, R3 and R4 in parallel should equal the transmission line impedance. For most 50 $\Omega$  applications, R3 and R4 can be 100 $\Omega$ . The values of the resistors can be increased to reduce the loading for slower and weaker LVCMOS driver. When using single-ended signaling, the noise rejection benefits of differential signaling are reduced. Even though the differential input can handle full rail LVCMOS signaling, it is recommended that the amplitude be reduced while maintaining an edge rate faster than 1V/ns. The datasheet specifies a lower differential amplitude, however this only applies to differential signals. For single-ended applications, the swing can be larger, however  $V_{II}$  cannot be less than -0.3V and  $V_{III}$  cannot be more than  $V_{DD}$  + 0.3V. Though some of the recommended components might not be used, the pads should be placed in the layout. They can be utilized for debugging purposes. The datasheet specifications are characterized and guaranteed by using a differential signal.

### <span id="page-18-0"></span>Differential Clock Input Interface

The CLK /nCLK accepts LVDS, LVPECL, LVHSTL, HCSL and other differential signals. Both  $V_{SWING}$  and  $V_{OH}$  must meet the V<sub>PP</sub> and V<sub>CMR</sub> input requirements. [Figure 15](#page-18-1) to [Figure 19](#page-19-1) show interface examples for the CLK/nCLK input driven by the most common driver types. The input interfaces suggested here are examples only. Please consult with the vendor of the driver component to confirm the driver termination requirements. For example, in [Figure 15,](#page-18-1) the input termination applies for IDT open emitter LVHSTL drivers. If you are using an LVHSTL driver from another vendor, use their termination recommendation.

<span id="page-18-1"></span>



Figure 16. CLK/nCLK Input Driven by a 3.3V LVPECL Driver



Figure 17. CLK/nCLK Input Driven by a 3.3V LVDS Driver



#### Figure 18. CLK/nCLK Input Driven by a 3.3V LVPECL Driver



#### <span id="page-19-1"></span>Figure 19. CLK/nCLK Input Driven by a 3.3V HCSL Driver



### <span id="page-19-0"></span>Overdriving the XTAL Interface

The XTAL\_IN input can be overdriven by an LVCMOS driver or by one side of a differential driver through an AC coupling capacitor. The XTAL\_OUT pin can be left floating. The amplitude of the input signal should be between 500mV and 1.8V and the slew rate should not be less than 0.2V/nS. For 3.3V LVCMOS inputs, the amplitude must be reduced from full swing to at least half the swing in order to prevent signal interference with the power rail and to reduce internal noise. [Figure 20](#page-19-2) shows an example of the interface diagram for a high speed 3.3V LVCMOS driver. This configuration requires that the sum of the output impedance of the driver (Ro) and the series resistance (Rs) equals the transmission line impedance. In addition, matched termination at the crystal input will attenuate the signal in half. This can be done in one of two ways.

First, R1 and R2 in parallel should equal the transmission line impedance. For most 50 $\Omega$  applications, R1 and R2 can be 100 $\Omega$ . This can also be accomplished by removing R1 and changing R2 to  $50\Omega$ . The values of the resistors can be increased to reduce the loading for a slower and weaker LVCMOS driver. [Figure 21](#page-20-1) shows an example of the interface diagram for an LVPECL driver. This is a standard LVPECL termination with one side of the driver feeding the XTAL\_IN input. It is recommended that all components in the schematics be placed in the layout. Though some components might not be used, they can be utilized for debugging purposes. The datasheet specifications are characterized and guaranteed by using a quartz crystal as the input.

#### <span id="page-19-2"></span>Figure 20. General Diagram for LVCMOS Driver to XTAL Input Interface





#### <span id="page-20-1"></span>Figure 21. General Diagram for LVPECL Driver to XTAL Input Interface

### <span id="page-20-0"></span>Recommended Termination

[Figure 22](#page-20-2) is the recommended source termination for applications where the driver and receiver will be on a separate PCBs. This termination is the standard for PCI Express™ and HCSL output types. All traces should be 50Ω impedance single-ended or 100Ω differential.

#### <span id="page-20-2"></span>Figure 22. Recommended Source Termination (where the driver and receiver will be on separate PCBs)



[Figure 23](#page-21-1) is the recommended termination for applications where a point-to-point connection can be used. A point-to-point connection contains both the driver and the receiver on the same PCB. With a matched termination at the receiver, transmission-line reflections will be minimized. In addition, a series resistor (Rs) at the driver offers flexibility and can help dampen unwanted reflections. The optional resistor can range from 0Ω to 33Ω. All traces should be 50Ω impedance single-ended or 100Ω differential.



#### <span id="page-21-1"></span>Figure 23. Recommended Termination (where a point-to-point connection can be used)

### <span id="page-21-0"></span>VFQFPN EPAD Thermal Release Path

In order to maximize both the removal of heat from the package and the electrical performance, a land pattern must be incorporated on the Printed Circuit Board (PCB) within the footprint of the package corresponding to the exposed metal pad or exposed heat slug on the package, as shown in [Figure 24](#page-21-2)*.* The solderable area on the PCB, as defined by the solder mask, should be at least the same size/shape as the exposed pad/slug area on the package to maximize the thermal/electrical performance. Sufficient clearance should be designed on the PCB between the outer edges of the land pattern and the inner edges of pad pattern for the leads to avoid any shorts.

While the land pattern on the PCB provides a means of heat transfer and electrical grounding from the package to the board through a solder joint, thermal vias are necessary to effectively conduct from the surface of the PCB to the ground plane(s). The land pattern must be connected to ground through these vias. The vias act as "heat pipes". The number of vias (i.e. "heat pipes") are application specific and dependent upon the package power dissipation as well as electrical conductivity requirements. Thus, thermal and electrical analysis and/or testing are recommended to determine the minimum number needed. Maximum thermal and electrical performance is achieved when an array of vias is incorporated in the land pattern. It is recommended to use as many vias connected to ground as possible. It is also recommended that the via diameter should be 12 to 13mils (0.30 to 0.33mm) with 1oz copper via barrel plating. This is desirable to avoid any solder wicking inside the via during the soldering process which may result in voids in solder between the exposed pad/slug and the thermal land. Precautions should be taken to eliminate any solder voids between the exposed heat slug and the land pattern. Note: These recommendations are to be used as a guideline only. For further information, please refer to the Application Note on the Surface Mount Assembly of Amkor's Thermally/ Electrically Enhance Leadframe Base Package, Amkor Technology.



<span id="page-21-2"></span>Figure 24. P.C. Assembly for Exposed Pad Thermal Release Path – Side View (drawing not to scale)

### <span id="page-22-0"></span>Recommendations for Unused Input and Output Pins

#### <span id="page-22-1"></span>Inputs

#### *LVCMOS Control Pins*

All control pins have internal pullups or pulldowns; additional resistance is not required but can be added for additional protection. A 1k $\Omega$ resistor can be used.

#### *Crystal Inputs*

For applications not requiring the use of the crystal oscillator input, both XTAL\_IN and XTAL\_OUT can be left floating. Though not required, but for additional protection, a  $1k\Omega$  resistor can be tied from XTAL IN to ground.

#### *CLK/nCLK Inputs*

For applications not requiring the use of the differential input, both CLK and nCLK can be left floating. Though not required, but for additional protection, a  $1k\Omega$  resistor can be tied from CLK to ground.

#### <span id="page-22-2"></span>**Outputs**

#### *LVCMOS Outputs*

All unused LVCMOS outputs can be left floating. There should be no trace attached.

#### *Differential Outputs*

All unused differential outputs can be left floating. We recommend that there is no trace attached. Both sides of the differential output pair should either be left floating or terminated.

### <span id="page-22-3"></span>PCI Express Application Information

PCI Express jitter analysis methodology models the system response to reference clock jitter. The block diagram below shows the most frequently used *Common Clock Architecture* in which a copy of the reference clock is provided to both ends of the PCI Express Link.

In the jitter analysis, the transmit (Tx) and receive (Rx) serdes PLLs are modeled as well as the phase interpolator in the receiver. These transfer functions are called H1, H2, and H3 respectively. The overall system transfer function at the receiver is:  $Ht(s) = H3(s) \times [H1(s) - H2(s)]$ 

The jitter spectrum seen by the receiver is the result of applying this system transfer function to the clock spectrum X(s) and is:

 $Y(s) = X(s) \times H3(s) \times [H1(s) - H2(s)]$ 

In order to generate time domain jitter numbers, an inverse Fourier Transform is performed on X(s)\*H3(s) \* [H1(s) - H2(s)].

#### Figure 25. PCI Express Common Clock Architecture



For **PCI Express Gen 1**, one transfer function is defined and the evaluation is performed over the entire spectrum: DC to Nyquist (e.g for a 100MHz reference clock: 0Hz – 50MHz) and the jitter result is reported in peak-peak.

Figure 26. PCIe Gen 1 Magnitude of Transfer Function



For **PCI Express Gen 2**, two transfer functions are defined with 2 evaluation ranges and the final jitter number is reported in RMS. The two evaluation ranges for PCI Express Gen 2 are 10kHz – 1.5MHz (Low Band) and 1.5MHz – Nyquist (High Band). The plots show the individual transfer functions as well as the overall transfer function Ht.





#### Figure 28. PCIe Gen 2B Magnitude of Transfer Function



For **PCI Express Gen 3**, one transfer function is defined and the evaluation is performed over the entire spectrum. The transfer function parameters are different from Gen 1 and the jitter result is reported in RMS.

Figure 29. PCIe Gen 3 Magnitude of Transfer Function



For a more thorough overview of PCI Express jitter analysis methodology, please refer to IDT Application Note *PCI Express Reference Clock Requirements.* 



### <span id="page-25-0"></span>Schematic Example

[Figure 30](#page-26-0) shows an example of 8V41N012A application schematic. In this example, the device is operated at V<sub>DD</sub> = V<sub>DDA</sub> = V<sub>DDO Qx</sub> = 3.3V. The schematic example focuses on functional connections and is not configuration specific. Refer to the pin description and functional tables in the datasheet to ensure that the logic control inputs are properly set.

A 12pF parallel resonant 25MHz crystal is used. For this device, the crystal load capacitors are required for proper operation. The load capacitance, C1 = C2 = 2pF, are recommended for frequency accuracy. Depending on the variation of the parasitic stray capacity of the printed circuit board traces between the crystal and the Xtal\_In and Xtal\_Out pins, the values of C1 and C2 might require a slight adjustment to optimize the frequency accuracy. Crystals with other load capacitance specifications can be used, but this will require adjusting C1 and C2. When designing the circuit board, return the capacitors to ground though a single point contact close to the package. Two Fox crystal options are shown in the schematic for design flexibility.

The ePAD provides a low thermal impedance connection between the internal device and the PCB. It also provides an electrical connection to the die and must be connected to ground.

As with any high speed analog circuitry, the power supply pins are vulnerable to random noise. To achieve optimum jitter performance, power supply isolation is required. The 8V41N012A provides separate power supplies to isolate any high switching noise from coupling into the internal PLL.

In order to achieve the best possible filtering, it is recommended that the placement of the filter components be on the device side of the PCB as close to the power pins as possible. If space is limited, the 0.1µF capacitor in each power pin filter should be placed on the device side. The other components can be on the opposite side of the PCB.

Power supply filter recommendations are a general guideline to be used for reducing external noise from coupling into the devices. The filter performance is designed for a wide range of noise frequencies. This low-pass filter starts to attenuate noise at approximately 10kHz. If a specific frequency noise component is known, such as switching power supplies frequencies, it is recommended that component values be adjusted and if required, additional filtering be added. Additionally, good general design practices for power plane voltage stability suggests adding bulk capacitance in the local area of all devices.

<span id="page-26-0"></span>Figure 30. 8V41N012A Schematic Example



### <span id="page-27-0"></span>Power Considerations

This section provides information on power dissipation and junction temperature for the 8V41N012A. Equations and example calculations are also provided.

#### **1. Power Dissipation.**

The total power dissipation for the 8V41N012A is the sum of the core power plus the analog power plus the power dissipated due to loading.

The following is the power dissipation for  $V_{DD} = 3.3V + 5\% = 3.465V$ , which gives worst case results.

NOTE: Please refer to Section 3 for details on calculating power dissipated due to loading.

- Power (core)<sub>MAX</sub> = V<sub>DD\_MAX</sub> \* (I<sub>DD</sub> + I<sub>DDA</sub>)= 3.465V \* (235mA + 45mA) = 970.2mW
- Power  $(HCSL)_{MAX} = (3.465V 17mA * 50) 17mA = 44.5mW per output$
- $\blacksquare$  Total Power (HCSL)<sub>MAX</sub> = 44.5mW \* 10 = 445mW

#### **LVCMOS Driver Power Dissipation**

- **•** Output Impedance R<sub>OUT</sub> Power Dissipation due to Loading 50 $\Omega$  to V<sub>DDO\_Qx</sub> / 2 Output Current  $I_{\text{OUT}} = V_{\text{DD}}$  <sub>MAX</sub> / [2 \* (50 $\Omega$  + R<sub>OUT</sub>)] = 3.465V / [2 \* (50 $\Omega$  + 15 $\Omega$ )] = **26.65mA**
- **Power Dissipation on the R<sub>OUT</sub> per LVCMOS output** Power (LVCMOS) =  $R_{OUT} * (1_{OUT})^2 = 15\Omega * (26.65mA)^2 = 10.65mW$  per output
- **•** Total Power Dissipation on the  $R_{\text{OUT}}$ Total Power  $(R_{\text{OUT}}) = 10.65 \text{mW}$  \* 4 = 42.6mW
- Total Power Dissipation
- **Total Powe**r
	- = Power (core) + Total Power (HCSL) + Total Power ( $R_{OUT}$ )
	- = 970.2mW + 445mW + 42.6mW
	- **= 1457.8mW**

#### **2. Junction Temperature.**

Junction temperature, Tj, is the temperature at the junction of the bond wire and bond pad directly affects the reliability of the device. The maximum recommended junction temperature is 125°C. Limiting the internal transistor junction temperature, Tj, to 125°C ensures that the bond wire and bond pad temperature remains below 125°C.

The equation for Tj is as follows: Tj =  $\theta_{JA}$  \* Pd\_total + T<sub>A</sub>

Tj = Junction Temperature

 $\theta_{JA}$  = Junction-to-Ambient Thermal Resistance

Pd\_total = Total Device Power Dissipation (example calculation is in section 1 above)

T<sub>A</sub> = Ambient Temperature

In order to calculate junction temperature, the appropriate junction-to-ambient thermal resistance  $\theta_{JA}$  must be used. Assuming no air flow and a multi-layer board, the appropriate value is 26.6°C/W per [Table 19](#page-28-0).

Therefore, Tj for an ambient temperature of 85°C with all outputs switching is:

85 °C + 1.458W  $*$  26.6 °C/W = 123.8 °C. This is below the limit of 125 °C.

This calculation is only an example. Tj will obviously vary depending on the number of loaded outputs, supply voltage, air flow and the type of board (multi-layer).

#### <span id="page-28-0"></span>Table 19. Thermal Resistance  $\theta_{JA}$  for 72 Lead VFQFPN, Forced Convection



#### **3. Calculations and Equations.**

The purpose of this section is to calculate power dissipation on the IC per HCSL output pair.

HCSL output driver circuit and termination are shown in [Figure 31](#page-28-1)*.* 

#### <span id="page-28-1"></span>Figure 31. HCSL Driver Circuit and Termination



HCSL is a current steering output which sources a maximum of 17mA of current per output. To calculate worst case on-chip power dissipation, use the following equations which assume a  $50\Omega$  load to ground.

The highest power dissipation occurs when  $V_{DD-MAX}$ .

Power=  $(V_{DD\_MAX} - V_{OUT})$  \*  $I_{OUT}$ since  $V_{\text{OUT}} = I_{\text{OUT}} * R_1$ Power= (V<sub>DD\_MAX</sub> – I<sub>OUT</sub> \* R<sub>L</sub>) \* I<sub>OUT</sub>

 $= (3.465V - 17mA * 50<sub>\Omega</sub>) * 17mA$ 

Total Power Dissipation per output pair = **44.5mW**

### <span id="page-29-0"></span>Reliability Information

#### Table 20.  $\theta_{JA}$  vs. Air Flow Table for a 72 Lead VFQFPN



### <span id="page-29-1"></span>Transistor Count

The transistor count for 8V41N012A is: 176,555.

## <span id="page-29-2"></span>Package Outline Drawings

The package outline drawings are appended at the end of this document and are accessible from the link below. The package information is the most current data available.

www.idt.com/document/psc/72-vfqfpn-package-outline-drawing-100-x-100-x-090-mm-body-epad-590-x-590-mm-punch-050mm-pitch

### <span id="page-29-3"></span>Marking Diagram



• "\$" denotes the mark code.

### <span id="page-29-4"></span>Ordering Information





# <span id="page-30-0"></span>Revision History





## 72-VFQFPN, Package Outline Drawing

10.0 x 10.0 x 0.90 mm Body, Epad 5.90 x 5.90 mm Punch 0.50mm Pitch NLG72D1, PSC-4208-05, Rev 01, Page 1





### 72-VFQFPN, Package Outline Drawing

10.0 x 10.0 x 0.90 mm Body, Epad 5.90 x 5.90 mm Punch 0.50mm Pitch NLG72D1, PSC-4208-05, Rev 01, Page 2





### 72-VFQFPN, Package Outline Drawing

10.0 x 10.0 x 0.90 mm Body, Epad 5.90 x 5.90 mm Punch 0.50mm Pitch NLG72D1, PSC-4208-05 Rev 01, Page 3



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