

LM6172QML Dual High Speed, Low Power, Low Distortion, Voltage Feedback Amplifiers

Check for Samples: [LM6172QML](http://www.ti.com/product/lm6172qml#samples)

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- **Wide Unity-Gain Bandwidth 100MHz**
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- **ADSL/HDSL Drivers**
- **Multimedia Broadcast Systems**
- **Video Amplifiers**
- **NTSC, PAL® and SECAM Systems**
- **ADC/DAC Buffers**
- **Pulse Amplifiers and Peak Detectors**

Connection Diagram

¹FEATURES DESCRIPTION

²³⁴ The LM6172 is a dual high speed voltage feedback **• Available with Radiation Specification** amplifier. It is unity-gain stable and provides excellent **– High Dose Rate 300 krad(Si)** DC and AC performance. With 100MHz unity-gain **– ELDRS Free 100 krad(Si)** bandwidth, 3000V/μs slew rate and 50mA of output **Easy to Use Voltage Feedback Topology be a current per channel, the LM6172 offers high** performance in dual amplifiers; yet it only consumes **• High Slew Rate 3000V/μ^s** 2.3mA of supply current each channel.

The LM6172 operates on ±15V power supply for
 • Low Supply Current 2.3mA / Amplifier systems requiring large voltage swings, such as
 • High Output Current 50mA / Amplifier ADSL, scanners and ultrasound equipment. It i ADSL, scanners and ultrasound equipment. It is also • **Specified for ±15V and ±5V Operation specified at ±5V power supply for low voltage** applications such as portable video systems.

APPLICATIONS The LM6172 is built with TI's advanced VIP™ III (Vertically Integrated PNP) complementary bipolar **• Scanner I- to -V Converters**

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EXAS NSTRUMENTS

LM6172 Driving Capacitive Load

 $1 k\Omega$

LM6172 Simplified Schematic (Each Amplifier)

SALL

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ABSOLUTE MAXIMUM RATINGS (1)

(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

(3) The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{Jmax} (maximum junction temperature), $\theta_{\sf JA}$ (package junction to ambient thermal resistance), and T_A (ambient temperature). The maximum allowable power dissipation at any temperature is P_{Dmax} = (Τ_{Jmax} - Τ_Α)/θ_{JA} or the number given in the Absolute Maximum Ratings, whichever is lower.

- (4) The package material for these devices allows much improved heat transfer over our standard ceramic packages. In order to take full advantage of this improved heat transfer, heat sinking must be provided between the package base (directly beneath the die), and either metal traces on, or thermal vias through, the printed circuit board. Without this additional heat sinking, device power dissipation must be calculated using θ_{JA} , rather than θ_{JC} , thermal resistance. It must not be assumed that the device leads will provide substantial heat transfer out the package, since the thermal resistance of the leadframe material is very poor, relative to the material of the package base. The stated θ_{JC} thermal resistance is for the package material only, and does not account for the additional thermal resistance between the package base and the printed circuit board. The user must determine the value of the additional thermal resistance and must combine this with the stated value for the package, to calculate the total allowed power dissipation for the device.
- (5) Continuous short circuit operation can result in exceeding the maximum allowed junction temperature of 150°C
- (6) All numbers apply for packages soldered directly into a PC board.
- (7) Human body model, 1.5 k Ω in series with 100 pF.

RECOMMENDED OPERATING CONDITIONS (1)

(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

⁽²⁾ Differential Input Voltage is measured at $V_S = \pm 15V$.

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QUALITY CONFORMANCE INSPECTION

Mil-Std-883, Method 5005 - Group A

LM6172 (±5V) ELECTRICAL CHARACTERISTICS (1) DC PARAMETERS

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +5V, V⁻ = -5V, V_{CM} = 0V & R_L > 1MΩ

⁽¹⁾ Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are specified only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

⁽²⁾ Large signal voltage gain is the total output swing divided by the input signal required to produce that swing. For $V_S = \pm 15V$, $V_{\text{OUT}} =$ $\pm 5V$. For $V_S = \pm 5V$, $V_{OUT} = \pm 1V$.

LM6172 (±5V) ELECTRICAL CHARACTERISTICS [\(1\)](#page-4-0) DC PARAMETERS (continued)

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +5V, V⁻ = -5V, V_{CM} = 0V & R_L > 1MΩ

(3) The open loop output current is specified by measurement of the open loop output voltage swing using 100Ω output load.

DC DRIFT PARAMETERS(1)

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +5V, V⁻ = -5V, V_{CM} = 0V & R_L > 1MΩ Delta calculations performed on QMLV devices at group B , subgroup 5.

(1) Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are specified only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

LM6172 (±15V) ELECTRICAL CHARACTERISTICS DC PARAMETERS (1)

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +15V, V⁻ = −15V, V_{CM} = 0V, & R_L = 1MΩ

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⁽¹⁾ Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are specified only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

⁽²⁾ Large signal voltage gain is the total output swing divided by the input signal required to produce that swing. For $V_S = \pm 15V$, $V_{\text{OUT}} =$ \pm 5V. For V_S = \pm 5V, V_{OUT} = \pm 1V.

RUMENTS

LM6172 (±15V) ELECTRICAL CHARACTERISTICS DC PARAMETERS [\(1\)](#page-4-0) (continued)

The following conditions apply, unless otherwise specified. $T_J = 25$ °C, V⁺ = +15V, V⁻ = −15V, V_{CM} = 0V, & R_L = 1MΩ

(3) The open loop output current is specified by measurement of the open loop output voltage swing using 100Ω output load.

AC PARAMETERS (1)

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +15V, V[−] = −15V, V_{CM} = 0V

(1) Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are specified only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

See AN0009 for SR test circuit.

(3) Slew Rate measured between ±4V.

(4) See AN0009 for GBW test circuit.

DC DRIFT PARAMETERS (1)

The following conditions apply, unless otherwise specified. $T_J = 25^{\circ}C$, V⁺ = +15V, V⁻ = −15V, V_{CM} = 0V Delta calculations performed on QMLV devices at group B , subgroup 5.

(1) Pre and post irradiation limits are identical to those listed under AC and DC electrical characteristics. These parts may be dose rate sensitive in a space environment and demonstrate enhanced low dose rate effect. Radiation end point limits for the noted parameters are specified only for the conditions as specified in Mil-Std-883, Method 1019.5, Condition A.

TYPICAL PERFORMANCE CHARACTERISTICS

Unless otherwise noted, $T_A = 25^{\circ}C$

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Texas **ISTRUMENTS**

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

10M

100k

 $1M$

100M

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

Unless otherwise noted, $T_A = 25^{\circ}C$

vs. vs. Load Load 82.00 Open Loop Gain (dB) 80.00 +125°C 78.00 25° C 76.00 -55° C $-$ 74.00 $V_S = \pm 5V$ 72.00 500 1000 1500 2000 $\mathbf 0$ Load Resistor (Ω)

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ISTRUMENTS

Texas

 $100k$

 $9 - 10$

73 TEXAS **INSTRUMENTS**

SNOSAR4A –DECEMBER 2010–REVISED OCTOBER 2011 **www.ti.com TYPICAL PERFORMANCE CHARACTERISTICS (continued)** Unless otherwise noted, $T_A = 25^{\circ}C$
Large Signal Pulse Response
 $\begin{array}{r} 4y = -1, V_S = \pm 15V \end{array}$ **Large Signal Pulse Response Small Signal Pulse Response A^V = −1, V^S = ±15V A^V = −1, V^S = ±15V** (100 mV/div) V_{IN}
(5V/div) \bar{z} (100 mV/div) V_{OUT}
(5V/div) V_{OUT} Time $(50 \text{ ns}/\text{div})$ Time $(50 \text{ ns}/\text{div})$ **Figure 33.** Figure 34. **Large Signal Pulse Response Small Signal Pulse Response A^V = −1, V^S = ±5V A^V = −1, V^S = ±5V** (100 mV/div) $(2V/div)$ $\sum_{i=1}^{n}$ $\sum_{i=1}^{n}$ (100 mV/div) $\frac{V_{\text{OUT}}}{(2V/div)}$ V_{OUT} Time (50 ns/div) Time $(50 \text{ ns}/\text{div})$ **Figure 35. Figure 36. Closed Loop Frequency Response**

vs.
 vs.
 v= +2)
 v= +2) $V_S = 115$ $V_S = 15$ 10 GAIN (dB) GAIN (dB) $\overline{0}$ $\overline{0}$ $V_S = \pm 2.75$ $V_S = \frac{1}{2}$ 2.75 $V_S = \pm 10$ $V_S = \pm 10$ -10 -10 $V_S = \pm 5$ $V_S = \pm 5$ -20 -20 $1M$ 10M 100M 1_N 10M 100M FREQUENCY (Hz) FREQUENCY (Hz) **Figure 37. Figure 38.**

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

Figure 41. Figure 42.

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APPLICATION NOTES

LM6172 PERFORMANCE DISCUSSION

The LM6172 is a dual high-speed, low power, voltage feedback amplifier. It is unity-gain stable and offers outstanding performance with only 2.3mA of supply current per channel. The combination of 100MHz unity-gain bandwidth, 3000V/μs slew rate, 50mA per channel output current and other attractive features makes it easy to implement the LM6172 in various applications. Quiescent power of the LM6172 is 138mW operating at \pm 15V supply and 46mW at ±5V supply.

LM6172 CIRCUIT OPERATION

The class AB input stage in LM6172 is fully symmetrical and has a similar slewing characteristic to the current feedback amplifiers. In the LM6172 Simplified Schematic (Page 2), Q1 through Q4 form the equivalent of the current feedback input buffer, R_F the equivalent of the feedback resistor, and stage A buffers the inverting input. The triple-buffered output stage isolates the gain stage from the load to provide low output impedance.

LM6172 SLEW RATE CHARACTERISTIC

The slew rate of LM6172 is determined by the current available to charge and discharge an internal high impedance node capacitor. This current is the differential input voltage divided by the total degeneration resistor RE. Therefore, the slew rate is proportional to the input voltage level, and the higher slew rates are achievable in the lower gain configurations.

When a very fast large signal pulse is applied to the input of an amplifier, some overshoot or undershoot occurs. By placing an external series resistor such as 1kΩ to the input of LM6172, the slew rate is reduced to help lower the overshoot, which reduces settling time.

REDUCING SETTLING TIME

The LM6172 has a very fast slew rate that causes overshoot and undershoot. To reduce settling time on LM6172, a 1kΩ resistor can be placed in series with the input signal to decrease slew rate. A feedback capacitor can also be used to reduce overshoot and undershoot. This feedback capacitor serves as a zero to increase the stability of the amplifier circuit. A 2pF feedback capacitor is recommended for initial evaluation. When the LM6172 is configured as a buffer, a feedback resistor of 1kΩ must be added in parallel to the feedback capacitor.

Another possible source of overshoot and undershoot comes from capacitive load at the output. Please see the section " [Driving Capacitive Loads](#page-13-0)" for more detail.

DRIVING CAPACITIVE LOADS

Amplifiers driving capacitive loads can oscillate or have ringing at the output. To eliminate oscillation or reduce ringing, an isolation resistor can be placed as shown in [Figure 43](#page-13-1). The combination of the isolation resistor and the load capacitor forms a pole to increase stability by adding more phase margin to the overall system. The desired performance depends upon the value of the isolation resistor; the bigger the isolation resistor, the more damped (slow) the pulse response becomes. For LM6172, a 50Ω isolation resistor is recommended for initial evaluation.

Figure 43. Isolation Resistor Used to Drive Capacitive Load

NSTRUMENTS

Figure 44. The LM6172 Driving a 510pF Load with a 30Ω Isolation Resistor

Figure 45. The LM6172 Driving a 220 pF Load with a 50Ω Isolation Resistor

LAYOUT CONSIDERATION

Printed Circuit Boards And High Speed Op Amps

There are many things to consider when designing PC boards for high speed op amps. Without proper caution, it is very easy to have excessive ringing, oscillation and other degraded AC performance in high speed circuits. As a rule, the signal traces should be short and wide to provide low inductance and low impedance paths. Any unused board space needs to be grounded to reduce stray signal pickup. Critical components should also be grounded at a common point to eliminate voltage drop. Sockets add capacitance to the board and can affect frequency performance. It is better to solder the amplifier directly into the PC board without using any socket.

Using Probes

Active (FET) probes are ideal for taking high frequency measurements because they have wide bandwidth, high input impedance and low input capacitance. However, the probe ground leads provide a long ground loop that will produce errors in measurement. Instead, the probes can be grounded directly by removing the ground leads and probe jackets and using scope probe jacks.

Components Selection And Feedback Resistor

It is important in high speed applications to keep all component leads short because wires are inductive at high frequency. For discrete components, choose carbon composition-type resistors and mica-type capacitors. Surface mount components are preferred over discrete components for minimum inductive effect.

Large values of feedback resistors can couple with parasitic capacitance and cause undesirable effects such as ringing or oscillation in high speed amplifiers. For LM6172, a feedback resistor less than 1kΩ gives optimal performance.

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COMPENSATION FOR INPUT CAPACITANCE

The combination of an amplifier's input capacitance with the gain setting resistors adds a pole that can cause peaking or oscillation. To solve this problem, a feedback capacitor with a value

 $C_F > (R_G \times C_{IN})/R_F$

can be used to cancel that pole. For LM6172, a feedback capacitor of 2pF is recommended. [Figure 46](#page-15-0) illustrates the compensation circuit.

Figure 46. Compensating for Input Capacitance

POWER SUPPLY BYPASSING

Bypassing the power supply is necessary to maintain low power supply impedance across frequency. Both positive and negative power supplies should be bypassed individually by placing 0.01μF ceramic capacitors directly to power supply pins and 2.2μF tantalum capacitors close to the power supply pins.

Figure 47. Power Supply Bypassing

TERMINATION

In high frequency applications, reflections occur if signals are not properly terminated. [Figure 48](#page-16-0) shows a properly terminated signal while [Figure 49](#page-16-1) shows an improperly terminated signal.

Figure 48. Properly Terminated Signal

Figure 49. Improperly Terminated Signal

To minimize reflection, coaxial cable with matching characteristic impedance to the signal source should be used. The other end of the cable should be terminated with the same value terminator or resistor. For the commonly used cables, RG59 has 75Ω characteristic impedance, and RG58 has 50Ω characteristic impedance.

POWER DISSIPATION

The maximum power allowed to dissipate in a device is defined as:

$$
P_D = (T_{J(max)} - T_A)/\theta_{JA}
$$

Where

- P_D is the power dissipation in a device
- $T_{J(max)}$ is the maximum junction temperature
- T_A is the ambient temperature
- \cdot θ_{JA} is the thermal resistance of a particular package

For example, for the LM6172 in a SOIC-16 package, the maximum power dissipation at 25°C ambient temperature is 1000mW.

Thermal resistance, θ_{JA} , depends on parameters such as die size, package size and package material. The smaller the die size and package, the higher θ_{JA} becomes. The 8-pin CDIP package has a lower thermal resistance (95°C/W) than that of 8-pin SOIC (160°C/W). Therefore, for higher dissipation capability, use an 8-pin CDIP package.

The total power dissipated in a device can be calculated as:

 $P_D = P_Q + P_L$

- \bullet P_{O} is the quiescent power dissipated in a device with no load connected at the output.
- \bullet P_L is the power dissipated in the device with a load connected at the output; it is not the power dissipated by

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the load.

Furthermore,

- P_Q : = supply current x total supply voltage with no load
- P_L : = output current x (voltage difference between supply voltage and output voltage of the same supply)

For example, the total power dissipated by the LM6172 with $V_S = \pm 15V$ and both channels swinging output voltage of 10V into 1kΩ is

$$
P_D: = P_Q + P_L
$$

- : = $2[(2.3mA)(30V)] + 2[(10mA)(15V 10V)]$
- $= 138$ mW + 100mW
- : $= 238$ mW

Application Circuits

Figure 50. I- to -V Converters

Figure 51. Differential Line Driver

REVISION HISTORY

PACKAGING INFORMATION

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(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the \leq =1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

PACKAGE OPTION ADDENDUM

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(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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OTHER QUALIFIED VERSIONS OF LM6172QML, LM6172QML-SP :

- Military : [LM6172QML](http://focus.ti.com/docs/prod/folders/print/lm6172qml.html)
- _● Space : <mark>[LM6172QML-SP](http://focus.ti.com/docs/prod/folders/print/lm6172qml-sp.html)</mark>

NOTE: Qualified Version Definitions:

- Military QML certified for Military and Defense Applications
- Space Radiation tolerant, ceramic packaging and qualified for use in Space-based application

TEXAS INSTRUMENTS

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TUBE

B - Alignment groove width

*All dimensions are nominal

NAB0008A

PACKAGE OUTLINE

NAC0016A CFP - 2.33mm max height

CERAMIC FLATPACK

- 1. Controlling dimension is Inch. Values in [] are milimeters. Dimensions in () for reference only.
- 2. For solder thickness and composition, see the "Lead Finish Composition/Thickness" link in the packaging section of the
- Texas Instruments website 3. Lead 1 identification shall be:
- a) A notch or other mark within this area
- b) A tab on lead 1, either side
- 4. No JEDEC registration as of December 2021

EXAMPLE BOARD LAYOUT

NAC0016A CFP - 2.33mm max height

CERAMIC FLATPACK

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