# **HFA3726**



### **Data Sheet November 1999 File Number 4310.3**

## **400MHz Quadrature IF Modulator/Demodulator**



The HFA3726 is a highly integrated baseband converter for quadrature modulation applications. It features all the necessary functionality for baseband modulation and

demodulation of I and Q signals. It has a two stage integrated limiting IF amplifier with 84dB of gain and a built in Receive Signal Strength Indicator (RSSI). "I" and "Q" Baseband antialiasing and shaping filters are integrated in this design. In addition, these filters are continuously tunable over a ±10% frequency range via one external resistor. The modulator channel receives digital I and Q data for processing. To achieve broadband operation, the Local Oscillator frequency input is required to be twice the desired frequency of modulation/demodulation. A selectable buffered divide by 2 LO output and a stable reference voltage is provided for convenience of the user. The device is housed in a thin 80 lead TQFP package well suited for PCMCIA board applications.

## **Ordering Information**



## **Simplified Block Diagram**

#### **Features**

- Integrates all IF Transmit and Receive Functions
- Broad Frequency Range . . . . . . . . . . . 10MHz to 400MHz
- 5th Order Low Pass Filter. . . . . . . . . . . . . . . . . . . .7.7MHz
- 400MHz Limiting IF Gain Strip with RSSI. . . . . . . . . . 84dB
- Low LO Drive Level . -15dBm
- Fast Transmit-Receive Switching . . . . . . . . . . . . . . . . . 1µs
- Power Management/Standby Mode
- Single Supply 2.7V to 5.5V Operation

#### **Applications**

- Systems Targeting IEEE 802.11 Standard
- TDD Quadrature-Modulated Communication Systems
- Wireless Local Area Networks
- PCMCIA Wireless Transceivers
- ISM Systems
- TDMA Packet Protocol Radios
- PCS/Wireless PBX
- Wireless Local Loop



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**Pinout**

**80 LEAD TQFP** TOP VIEW



## **Block Diagram**



NOTE:  $V_{CC}$ , GND and Bypass capacitors not shown.

## **Pin Descriptions**



## **Pin Descriptions (Continued)**



## **Pin Descriptions (Continued)**



NOTES:

1. The HFA3726 generates a lower side band signal when the "I" input leads the "Q" input by 90 degrees.

2. For a reference LO frequency higher than a CW IF signal input, the "I" channel leads the "Q" channel by 90 degrees.

3. The in-phase reference LO transitions occur at the rising edges of the 2XLO signal. Quadrature LO transitions occur at the falling edges. 180 degrees phase ambiguity is expected for carrier locked systems without differential encoding.

#### **TABLE 1. POWER MANAGEMENT**



#### Absolute Maximum Ratings **Thermal Information**

#### Supply Voltage . -0.3V to +6.0V Voltage on Any Other Pin. . . . . . . . . . . . . . . . . . -0.3V to VCC +0.3V

#### **Operating Conditions**





CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

#### NOTE:

4.  $θ<sub>JA</sub>$  is measured with the component mounted on an low effective thermal conductivity test board in free air. See Technical Brief 379 for details.





NOTE:

5.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design.

# **AC Electrical Specifications, Demodulator Performance** Application Targeting IEEE 802.11, V<sub>CC</sub> = 3V, Figure 22

Unless Otherwise Specified





#### **AC Electrical Specifications, Demodulator Performance** Application Targeting IEEE 802.11, V<sub>CC</sub> = 3V, Figure 22 Unless Otherwise Specified **(Continued)**



NOTES:

6.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design

7. 2XLO input = 572MHz, measure IF input level required to drop the I and Q output at 6MHz by 3dB from a reference output generated at IF input = -30dBm (hard limiting). This is a noise limited case with a BW of 47MHz. Please refer to the Overall Device Description, IF limiter.

8. The residual DC voltage generated by the RSSI circuit due to a noise limited stage at the end of the chain with no IF input. IF port terminated into 50Ω. Please referred to the Overall Device Description, IF limiter.

9. Both limiter RSSI current outputs are summed by 2 on chip 6kΩ resistors in parallel.

10. Range is defined where the indicated received input strength by the RSSI is ±3dBm accurate.

#### **AC Electrical Specifications, Modulator Performance** Application Targeting IEEE 802.11, V<sub>CC</sub> = 3V, Figure 22

Unless Otherwise Specified



NOTES:

11.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design

12. Data is characterized by DC levels applied to MOD TXI and Q pins for 4 quadrants with LO output as reference or indirectly by the SSB characteristics.

13. Power at the fundamental SSB frequency of two 6MHz, 90 degrees apart square waves applied at TXI and TXQ inputs. Levels are 3.4V<sub>P-P</sub> 1.7V offset.

14. Cutoff frequency is specified for both modulator and demodulator as the filter bank is shared and multiplexed for Transmit and Receive. Data is characterized by observing the attenuation of the fundamental of a square wave digital input swept at each channel separately. The IF output is down converted by an external wideband mixer with a coherent LO input for each of quadrature signals separately.

15. Typical ratio characterization with R<sub>TUNE</sub> set to 7.7MHz. TXI and TXQ analog Inputs at two independent and aligned 11M chip/s, 2<sup>23</sup>-1 sequence code signals.

## **Typical Performance Curves, Demodulator** (Figure 22 Test Diagram)







**FIGURE 3. DEMOD I/Q OUTPUT SWING vs V<sub>CC</sub> AND TEMPERATURE**



FIGURE 5. DEMOD I/Q PHASE BALANCE VARIATION vs V<sub>CC</sub> FIGURE 6. DEMOD I/Q AMPLITUDE BALANCE VARIATION vs



**FIGURE 2. DEMODULATOR I/Q OUTPUT SWING vs INPUT POWER**



**FIGURE 4. CASCADED LIMITER -3dB INPUT SENSITIVITY RESPONSE vs V<sub>CC</sub> AND TEMPERATURE** 



**VCC**

## **Typical Performance Curves, Demodulator** (Figure 22 Test Diagram) **(Continued)**











**FIGURE 8. DEMOD I/Q AMPLITUDE BALANCE VARIATION vs TEMPERATURE**







**FIGURE 11. DEMODULATOR RSSI DC OFFSET vs VCC AND TEMPERATURE**

## **Typical Performance Curves, Modulator** (Figure 23 Test Diagram)







FIGURE 14. MODULATOR SSB OUTPUT POWER vs V<sub>CC</sub> AND **TEMPERATURE**







**FIGURE 13. TYPICAL SSB MODULATOR RESPONSE (NOTE 13 ON AC ELECTRICAL SPECS, MODULATOR PERFORMANCE TABLE, LO BUFFER ENABLED)**



**FIGURE 15. MODULATOR SSB SIDE BAND SUPPRESSION VARIATION vs V<sub>CC</sub> AND TEMPERATURE** 





## **Typical Performance Curves, Modulator** (Figure 23 Test Diagram) **(Continued)**











**FIGURE 19. LPF CUTOFF FREQUENCY vs RTUNE,**  $V_{CC}$  = 3V,  $T_A$  = 25<sup>o</sup>C



**FIGURE 21. TYPICAL MODULATOR SPREAD SPECTRUM OUTPUT 11M CHIPS/s, QPSK. RTUNE = 900**Ω

### **Test Diagram** (280MHz IF)



NOTES:

16. Input termination used to provide a 50Ω impedance. Limiter Noise Figure ≅ 9dB for this configuration.

17. Bandpass filter for 280MHz, BW =  $47$ MHz, Q = 6.

18. Network shown for a typical -10dBm input at 50Ω.

19. Matching network from 250Ω to 50Ω at 280MHz.

#### **FIGURE 22. TEST DIAGRAM (280MHz IF)**



## **Typical Application Diagram** (Targeting IEEE 802.11 Standard)

#### NOTES:

20. Input termination used to match a SAW filter.

21. Typical bandpass filter for 280MHz, BW = 47MHz,  $Q = 6$ . Can also be used if desired after the second stage.

22. Network shown for a typical -10dBm input at  $50\Omega$ .

23. Output termination used to match a SAW filter.

24. R<sub>TUNE</sub> value for a 7.7 MHz cutoff frequency setting.

#### **FIGURE 23. TYPICAL APPLICATION DIAGRAM (TARGETING IEEE 802.11 STANDARD)**

## **Overall Device Description**

The HFA3726 is a highly integrated baseband converter for half duplex wireless data applications. It features all the necessary blocks for baseband modulation and demodulation of "I" and "Q" quadrature multiplexing signals. It targets applications using all phase shift types of modulation (PSK) due to its hard limiting receiving front end. Four fully independent blocks adds flexibility for numerous applications covering a wide range of IF frequencies. A differential design architecture, device pin out and layout have been chosen to improve system RF properties such as common mode signal immunity (noise, crosstalk), reduce relevant parasitics, settling times and optimize dynamic range for low power requirements. Single power supply requirements from  $2.7V_{DC}$  to  $5.5V_{DC}$  makes the HFA3726 a good choice for portable transceiver designs.

The HFA3726 has a two stage integrated limiting IF amplifier with frequency response to 400MHz. These amplifiers exhibit a -84dBm, -3dB cascaded limiting sensitivity with a built in Receive Signal Strength Indicator (RSSI) covering 60dB of dynamic range with excellent linearity. An up conversion and down conversion pair of quadrature doubly balanced mixers are available for "I" and "Q" baseband IF processing. These converters are driven by an internal quadrature LO generator which has a broadband response with excellent quadrature properties. To achieve broadband operation, the Local Oscillator frequency input is required to be twice the desired frequency for modulation/demodulation. Duty cycle and signal purity requirements for the 2X LO input using this type of quadrature architecture are less restrictive

for the HFA3726. Ground reference input signals as low as - 15dBm and frequencies up to 900MHz (2XLO) can be used and tailored by the user. A buffered, divide by 2, LO single ended 50Ω selectable output is provided for convenience of PLL designs. The receive channel mixers "I" and "Q" quadrature outputs have a frequency response up to 30MHz for baseband signals and the transmit mixers are summed and amplified to a single ended open collector output with frequency response up to 400MHz.

Multiplexed or half duplex baseband 5th order Butterworth low pass filters are also included in the design. The "I" and "Q" filters address applications requiring low pass and antialiasing filtering for external baseband threshold comparison or simple analog to digital conversion in the receive channel. During transmission, the filter is used for pulse shaping and control of spectral mask.

These cut off frequency is selected for optimization of spectrum output responses for 11Mchips/s for spread spectrum applications (This rate can also be interpreted as symbol rates for conventional data transmission). External processing correlators in the receive channel as in the Intersil HSP3824 baseband converter, will bring the demodulation to lower effective data rates. As an example, the use of 11M chips/s, 11 chip Barker code using the 7.7MHz low pass filter in a QPSK type of modulation scheme will bring a post processed effective data rate to 1M symbol/s or 2Mbits/s. In addition, these filters are continuously tunable over a  $\pm$ 10% frequency range via one external resistor. This feature gives the user the ability to reshape the spectrum of a transmitted signal at the antenna port which takes into account any spectral regrowth along the transmitter chain. The modulator "I" and "Q" filter inputs accept digital signal level data for modulation and their phase and gain characteristics, including I/Q matching and group delay are well suitable for reliable data transmission. In the Receive mode and over the full input limiting dynamic range, both low pass filters outputs swing a  $500 \text{mV}_{\text{P-P}}$ baseband signal.

Each block has its own independent power enable control for power management and half duplex transmit/receive operation. A stable  $2V_{DC}$  output and a buffered band gap reference voltage are also provided for an external analog to digital conversion reference.

## **Detailed Description** (Refer to Block Diagram)

#### **IF Limiter**

Two independent limiting amplifiers are available in the HFA3726. Each one has a broadband response to 400MHz with 45dB of gain. The low frequency response is limited by external components because the device has no internal coupling capacitors. The differential limiting output swing with a 500Ω load is typically 200mV<sub>P-P</sub> at the fundamental frequency and is temperature stable.

Both amplifiers are very stable within their passband and the cascaded performance also exhibits very good stability for any input source impedance. Wide bandwidth SAW filters for spread spectrum applications or any desired source impedance filter implementation can be used for IF filtering before the cascaded amplifiers. The stability is remarkable for such an integrated solution. In fact, in many applications it is possible to remove the bypass pin capacitors with no degradation in stability. The cascaded -1dB and -3dB input limiting sensitivity have been characterized as -79dBm and 84dBm respectively, for a 50Ω single ended input at 280MHz and with a 47MHz bandwidth interstage bandpass LC filter (refer to Figure 22, Test Diagram). The input sensitivity is determined to a large extent by the bandwidth of the interstage filter and input source impedance.

The noise figure for each stage has been characterized at 6dB for a 250 $\Omega$  single end input impedance and 9dB for a 50Ω input impedance. These low noise figures combined with their high gain, eliminate the need for additional IF gain components. The use of interstage bandpass filtering is suggested to decrease the noise bandwidth of the signal driving the second stage. Excessive broadband noise energy amplified by the first stage will force the last limiting stage to lose some of its effective gain or "limit on the noise". The use of interstage filters with narrower bandwidths will further improve the sensitivity of the cascaded limiter chain.

The amplifier differential output impedance is 140 $\Omega$  (70 $\Omega$ ) single ended) which gives the user, the ability to design simple wide or narrow LC bandwidth interstage filters, or tailor a desired cascaded gain by using differential attenuators. The filter can be designed with a desired "Q" by using the following relationship:  $Q = Rp/X$ ; where Rp is the parallel combination of 140Ω source resistance and the load (approximately 500Ω when using 560Ω termination as in Figure 22, Test Diagram), and X is the reactance of either L or C at the desired center frequency.

Another independent feature of the limiting amplifier is its Receive Signal Strength Indicator (RSSI). A Log-Amp design was developed which resulted in a current output proportional to the input power. The RSSI output voltage is set by summing the two stages output currents, which are full wave rectified signals, to a common resistor to ground. This full wave rectified voltage can then be converted to DC by the use of a filter capacitor in parallel with the resistor (The larger the capacitor value, the less the AC ripple with the expense of longer RSSI settling times). This arrangement gives the user the flexibility to set the dynamic voltage swing to any desired level by an appropriate resistance choice. Each stage has an available on chip 6kΩ low temperature coefficient resistor to ground for current output termination that can be used for convenience. The RSSI gives a ±3dBm accurate indication of the receive input power. This accuracy is across a 60dB input dynamic range. The cascaded HFA3726 RSSI slope is of 5.0µa/dB.

## **Quadrature Down Converter**

The quadrature down converter mixers are based in a Gilbert cell design. The input signal is routed to both mixers in parallel. With full balanced differential architecture, these mixers are driven by an accurate internal Local Oscillator (LO) chain as described later. Phase and gain accuracy of the output baseband signals are excellent and are a function of the combination of LO accuracy, balanced device design and layout characteristics. Mainly used for down conversion, its input frequency response exceeds 400MHz with a differential voltage gain of 2.5. With a differential input impedance of 1kΩ, the input compression point exceeds  $2V_{P-P}$ , which makes it suitable for use with the hard limiting output from the limiter amplifier chain or any low power external AGC application. The output frequency response is limited to 30MHz for "I" and "Q" baseband signals driving a 4kW differential load.

The HFA3726 down conversion mixers can generate two 10MHz, 90<sup>o</sup> apart signals, with the use of proper low pass filtering, and exhibits  $\pm 4^{\circ}$  and  $\pm 0.5$ dB of phase and amplitude match for a input CW IF signal of 400MHz and a 2XLO input of 780MHz.

## **LO Quadrature Generator**

The In Phase and Quadrature reference signals are generated by a divide by two chain internal to the device which drives both the up and down conversion mixers. With a fully balanced approach, the phase relationship between the two quadrature signals is within  $90^{\sf o}$   $\pm4^{\sf o}$  for a wide 20 to 400MHz frequency range. The reference signal input frequency needs to be twice the desired internal reference frequency. The ground referenced 2XLO input is current driven, which makes the input power requirement a function of external components that can be calculated assuming the input impedance of 130Ω. A typical input current value of 200µARMS is the only requirement for reliable LO generation. Figure 24 shows a typical 2XLO input network.

Divide by two flip flop architectures for LO generation often require tight control of signal purity or duty cycles. The HFA3726 has an internal duty cycle compensation scheme which eases the requirements of tight controlled duty cycles.

In addition, a 50 $\Omega$  LO buffer is available to the user for PLL's design reference. It substitutes a divide by two prescaler needed to bring the 2X LO frequency reference down. It is capable to drive 100mV<sub>P-P</sub> into 50 $\Omega$  and its frequency response is from 20MHz to 400MHz corresponding to a 2XLO input frequency response of 40MHz to 800MHz. The LO buffer can be disabled by removing the ground connection to the pin LO GND. The quadrature generator is always enabled for either transmit or receive modes.



**FIGURE 24. MOD LO IN (2XLO) EQUIVALENT CIRCUIT**

## **Quadrature Up Converter**

The Quadrature up converter mixers are also based on a doubly balanced Gilbert Cell design. "I" and "Q" Up converter signals are summed and buffered together through a single end open collector stage. As with the demodulators, both modulator mixers are driven from the same quadrature LO generator. It features a  $\pm4^{\sf o}$  and 0.5dB of phase and amplitude balance up to 400MHz which are reflected into its SSB characteristics. For "I" and "Q" differential inputs of  $500$ m $V_{P,P}$ ,  $90^{\circ}$  apart, the carrier feedthrough or LO leakage is typical -30dBc into 250 $\Omega$  with a sideband suppression of minimum 26dBc at 400MHz. Carrier feedthrough can be further improved by disabling the LO output port (please refer to pin #50 description) or using a DC bias network as in Figure 25. Featuring an output compression level of  $1V_{\text{P-P}}$ , the modulator output can generate a CW signal of typical -10dBm into 250Ω (158mV<sub>RMS</sub>) when differential DC inputs of 500mV<sub>P-P</sub> (equivalent to applying  $\pm$ 125mV ground referenced levels from the DC bias quiescent point of the device input) are applied to both "I" and "Q" inputs. Four quadrant phase shifts of the carrier output, like in Vector Modulator applications, can be set by proper choice of "I" and "Q" DC differential inputs, such that the square root of the sum of the squares of I and Q is constant.

Although specified to drive a 250 $\Omega$  load, the HFA3726 modulator open collector output enables user designed output matching networks to suit any application interface. The nominal AC current capability of this port is of 1.3mA<sub>RMS</sub>, which is shared between the termination resistor and the load for I and Q differential DC inputs of  $500$ m $V_{P-P}$  as explained above. (Use 70.7% of this AC capability for I and Q quadrature signals in case of SSB generation).

## **Low Pass Filters**

These filters are implemented using a 5th order Butterworth architecture. They are multiplexed, i.e., the same filter bank is used for both transmit and receive modes.

The filter block, in the transmit mode is set to accept digital (TTL threshold) levels inputs for "I" and "Q" signals with a frequency cutoff of 7.7MHz. An external resistor is used to fine tune the cut off frequencies for each setting within  $\pm 10\%$ of the nominal value. This feature is often needed to fulfill requirements of spectral mask compliance at the antenna output.

The "I" and "Q" filter matching is within 2<sup>0</sup> for phase and 0.5dB for amplitude at the passband. Group delay characteristics follow closely a theoretical 5th order Butterworth design.

When in the receive mode, the filters exhibit a 0dB of gain with differential inputs and single ended outputs.

In the transmit mode, the digital ground referenced "I" and "Q" input signals are level shifted, shaped and buffered with constant driving differential outputs of  $550 \text{mVp.p.}$ 

## **Coupling Capacitors**

Capacitor coupling is used to tie all HFA3726 blocks together. Special bias is used to maintain the DC levels on both ends of coupling pins (capacitors) when the device is changes from Transmitter to a Receiver and vice versa. The capacitance values must be chosen as a compromise to maintain proper frequency response and settling times (when the device is brought up from sleep mode or power down).



**FIGURE 25. CARRIER NULL BIASING**





NOTE:

25. A = Production Tested, B = Based on Characterization, C = By Design

**TABLE 3. IF LIMITER S11, S22 PARAMETER**

<b>FREQUENCY</b>	<b>S11 (SINGLE ENDED)</b>		<b>S22 (DIFFERENTIAL)</b>	
50MHz	0.96	$-4.0^{o}$	0.45	$0.0^{\circ}$
100MHz	0.95	$-8.0^{o}$	0.45	$3.0^\circ$
200MHz	0.91	$-17.0^{o}$	0.47	7.0 <sup>o</sup>
300MHz	0.84	$-26.0^{\circ}$	0.50	$9.0^{\circ}$
400MHz	0.80	$-33.0^{0}$	0.53	$10.0^{o}$



## AC Electrical Specifications, I/Q Down Converter Individual Performance Full Supply Range, TA = 25<sup>o</sup>C

NOTE:

26.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design

# AC Electrical Specifications, I/Q Up Converter and LO Individual Performance Full Supply Range, T<sub>A</sub> = 25<sup>o</sup>C



NOTE:

27.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design

#### **TABLE 4. QUADRATURE MODULATOR S22 PARAMETER**



#### **AC Electrical Specifications, TX Buffer Individual Performance** Full Supply Range, T<sub>A</sub> = 25<sup>o</sup>C



NOTE:

28.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design

## AC Electrical Specifications, RX/TX 5TH Order LPF Individual Performance Full Supply Range, T<sub>A</sub> = 25<sup>o</sup>C



NOTE:

29.  $A =$  Production Tested,  $B =$  Based on Characterization,  $C =$  By Design



#### **TABLE 5. TYPICAL LPF TUNE RESISTANCE**

NOTE:

30. Do not use an R<sub>TUNE</sub> value of less than 775 $\Omega$ .

## **Typical Performance Curves, Individual Blocks**







**FIGURE 27. SINGLE STAGE LIMITER NOISE FIGURE vs V<sub>CC</sub> AND TEMPERATURE, RS = 250**Ω**, FREQUENCY = 400MHz**

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