

[SN888C](http://www.ti.com/product/sn888c?qgpn=sn888c)

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Bus-Polarity Correcting RS-485 Transceiver for E-Meters

Check for Samples: [SN888C](http://www.ti.com/product/sn888c#samples)

- **Exceeds Requirements of EIA-485 Standard E-meters**
- **Bus-Polarity Correction within 76 ms**
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- -
	-
-
- **SOIC-8 Package for Backward Compatibility**
- - **±16 kV HBM protection**
	- **±12 kV IEC61000-4-2 Contact Discharge**
	- **+4 kV IEC61000-4-4 Fast Transient Burst**

¹FEATURES APPLICATIONS

DESCRIPTION
 DESCRIPTION

The SN888C is a low-power RS-485 transceiver with
 Werke with Type Configurations: The SN888C is a low-power RS-485 transceiver with **• Works with Two Configurations:** bus-polarity correction and transient protection. Upon hot plug-in the device detects and corrects the bus **– Failsafe and Termination Resistors** polarity within the first 76 ms of bus idling. On-chip transient protection protects the device against **• Up to 256 Nodes on a Bus** IEC61000 ESD and EFT transients.

The SN888C is available in an SOIC-8 package. The **Bus-Pin Protection:** The **example in an SOIC-8** package. The device is characterized from –40°C to 85°C.

Figure 1. Typical Network Application With Polarity Correction (POLCOR)

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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

DRIVER PIN FUNCTIONS

(1) The polarity-correcting mode is entered when $V_{1D} < V_{1T-}$ and t > t_{FS} and DE = low. This state is latched when /RE turns from low to high.

RECEIVER PIN FUNCTIONS

(1) The polarity-correcting mode is entered when $V_{1D} < V_{1T-}$ and t > t_{FS} and DE = low. This state is latched when /RE turns from low to high.

ABSOLUTE MAXIMUM RATINGS(1)

(1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

THERMAL INFORMATION

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](http://www.ti.com/lit/pdf/spra953). (2) The junction-to-board thermal resistance is obtained by simulating in an environment with a ring cold plate fixture to control the PCB temperature, as described in JESD51-8.

POWER DISSIPATION

RECOMMENDED OPERATING CONDITIONS

(1) The algebraic convention in which the least positive (most negative) limit is designated as minimum is used in this data sheet. (2) Operation is specified for internal (junction) temperatures up to 150°C. Self-heating due to internal power dissipation should be considered for each application. Maximum junction temperature is internally limited by the thermal shut-down (TSD) circuit which disables the driver outputs when the junction temperature reaches 170°C.

ELECTRICAL CHARACTERISTICS

over operating free-air temperature range (unless otherwise noted)

(1) Under any specific conditions, V_{IT+} is ensured to be at least V_{HYS} higher than V_{IT-} .

ELECTRICAL CHARACTERISTICS (continued)

over operating free-air temperature range (unless otherwise noted)

SWITCHING CHARACTERISTICS

3.3 ms $>$ bit time $>$ 4 µs (unless otherwise noted)

XAS STRUMENTS

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PARAMETER MEASUREMENT INFORMATION

Figure 2. Measurement of Driver Differential-Output Voltage With Common-Mode Load

Figure 3. Measurement of Driver Differential and Common-Mode Output With RS-485 Load

Figure 4. Measurement of Driver Differential-Output Rise and Fall Times and Propagation Delays

Figure 5. Measurement of Driver Enable and Disable Times With Active-High Output and Pull-Down Load

Figure 6. Measurement of Driver Enable and Disable Times With Active-Low Output and Pull-Up Load

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PARAMETER MEASUREMENT INFORMATION (continued)

RECEIVER

Figure 7. Measurement of Receiver Output Rise and Fall Times and Propagation Delays

Figure 8. Measurement of Receiver Enable and Disable Times With Driver Enabled

Figure 9. Measurement of Receiver Enable Times With Driver Disabled

Figure 10. Measurement of Receiver Polarity-Correction Time With Driver Disabled

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DEVICE INFORMATION

Low-Power Standby Mode

When the driver and the receiver are both disabled ($DE = low$ and $RE = high$) the device enters standby mode. If the enable inputs are in the disabled state for only a brief time (for example: less than 100 ns), the device does not enter standby mode, preventing the SN888C device from entering standby mode during driver or receiver enabling. Only when the enable inputs are held in the disabled state for a duration of 300 ns or more does the device enter low-power standby mode. In this mode most internal circuitry is powered down, and the steady-state supply current is typically less than 400 nA. When either the driver or the receiver is re-enabled, the internal circuitry becomes active. During V_{CC} power-up, when the device is set for both driver and receiver disabled mode, the device may consume more than 5-µA of ICC disabled current because of capacitance charging effects. This condition occurs only during V_{CC} power-up.

Bus Polarity Correction

The SN888C device automatically corrects a wrong bus-signal polarity caused by a cross-wire fault. In order to detect the bus polarity, all three of the following conditions must be met:

- A failsafe-biasing network (commonly at the master node) must define the signal polarity of the bus.
- A slave node must enable the receiver and disable the driver ($/RE = DE = low$).
- The bus must idle for the failsafe time, t_{FS-max} .

After the failsafe time has passed, the polarity correction is complete and applied to both the receive and transmit channels. The status of the bus polarity latches within the transceiver and maintains for subsequent data transmissions.

NOTE

Avoid data string durations of consecutive 0s or 1s exceeding t_{FS-min} , which can accidently trigger a wrong polarity correction.

[Figure 11](#page-8-0) shows a simple point-to-point data link between a master node and a slave node. Because the master node with the failsafe biasing network determines the signal polarity on the bus, an RS-485 transceiver without polarity correction, such as SN65HVD82, suffices. All other bus nodes, typically performing as slaves, require the SN888C transceiver with polarity correction.

Figure 11. Point-To-Point Data Link With Cross-Wire Fault

Prior to initiating data transmission the master transceiver must idle for a time span that exceeds the maximum failsafe time, t_{FS-max} , of a slave transceiver. To accomplish this idle time, drive the direction control line, DIR, low. After a time, $t > t_{FS-max}$, the master begins transmitting data.

Because of the indicated cross-wire fault between master and slave, the slave node receives bus signals with reversed polarity. Assuming the slave node has just been connected to the bus, the direction-control pin is pulled-down during power-up, and then is actively driven low by the slave MCU. The polarity correction begins as soon as the slave supply is established and ends after approximately 44 to 76 ms.

EXAS **STRUMENTS**

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Figure 12. Polarity Correction Timing Prior to a Data Transmission

Initially the slave receiver assumes that the correct bus polarity is applied to the inputs and performs no polarity reversal. Because of the reversed polarity of the bus-failsafe voltage, the output of the slave receiver, R_S , turns low. After t_{FS} has passed and the receiver has detected the wrong bus polarity, the internal POLCOR logic reverses the input signal and R_S turns high.

At this point, all incoming bus data with reversed polarity are polarity-corrected within the transceiver. Because polarity correction is also applied to the transmit path, the data sent by the slave MCU are reversed by the POLCOR logic, then fed into the driver.

The reversed data from the slave MCU are reversed again by the cross-wire fault in the bus, and the correct bus polarity is reestablished at the master end.

This process repeats each time the device powers up and detects an incorrect bus polarity.

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APPLICATION INFORMATION

Device Configuration

The SN888C device is a half-duplex RS-485 transceiver operating from a single 5-V ±10% supply. The driver and receiver enable pins that allow for the configuration of different operating modes.

Figure 13. Transceiver Configurations

Using independent enable lines provides the most flexible control as the lines allow for the driver and the receiver to be turned on and off individually. While this configuration requires two control lines, it allows for selective listening to the bus traffic, whether the driver is transmitting data or not. Only this configuration allows the SN888C device to enter low-power standby mode because it allows both the driver and receiver to be disabled simultaneously.

Combining the enable signals simplifies the interface to the controller by forming a single direction-control signal. Thus, when the direction-control line is high, the transceiver is configured as a driver, while when low, the device operates as a receiver.

Tying the receiver enable to ground and controlling only the driver-enable input also uses only one control line. In this configuration, a node not only receives the data on the bus sent by other nodes, but also receives the data sent on the bus, enabling the node to verify the correct data has been transmitted.

Bus Design

An RS-485 bus consists of multiple transceivers connected in parallel to a bus cable. To eliminate line reflections, each cable end is terminated with a termination resistor, RT, whose value matches the characteristic impedance, Z0, of the cable. This method, known as parallel termination, allows for relatively high data rates over long cable length.

Common cables used are unshielded twisted pair (UTP), such as low-cost CAT-5 cable with $Z0 = 100 \Omega$, and RS-485 cable with $Z0 = 120 \Omega$. Typical cable sizes are AWG 22 and AWG 24.

The maximum bus length is typically given as 4000 ft or 1200 m, and represents the length of an AWG 24 cable whose cable resistance approaches the value of the termination resistance, thus reducing the bus signal by half or 6 dB. Actual maximum usable cable length depends on the signaling rate, cable characteristics, and environmental conditions.

v_{cc}	R _I Differential Termination	R_{FS} Pull-Up	R_{FS} Pull-Down	V _{ID}
5 V	54 Ω	560 Ω	560 Ω	230 mV
		1 $K\Omega$	1 KΩ	131 mV
		4.7 K Ω	4.7 K Ω	29 mV
		10 K Ω	10 $K\Omega$	13 mV

Table 1. VID With a Failsafe Network and Bus Termination

An external failsafe-resistor network must be used to ensure failsafe operation during an idle bus state. When the bus is not actively driven, the differential receiver inputs could float allowing the receiver output to assume a random output. A proper failsafe network forces the receiver inputs to exceed the VIT threshold, thus forcing the SN888C receiver output into the failsafe (high) state. [Table 1](#page-10-0) shows the differential input voltage (V_{ID}) for various failsafe networks with a 54- Ω differential bus termination.

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Cable Length Versus Data Rate

There is an inverse relationship between data rate and cable length, which means the higher the data rate, the shorter the cable length; and conversely, the lower the data rate, the longer the cable length. While most RS-485 systems use data rates between 10 kbps and 100 kbps, applications such as e-metering often operate at rates of up to 250 kbps even at distances of 4000 ft and longer. Longer distances are possible by allowing for small signal jitter of up to 5 or 10%.

Stub Length

When connecting a node to the bus, the distance between the transceiver inputs and the cable trunk, known as the stub, should be as short as possible. The reason for the short distance is because a stub presents a nonterminated piece of bus line, which can introduce reflections if the distance is too long. As a general guideline, the electrical length or round-trip delay of a stub should be less than one-tenth of the rise time of the driver, thus leading to a maximum physical stub length as shown in [Equation 1.](#page-11-0)

 $L_{\text{Stub}} \leq 0.1 \times t_r \times v \times c$

where

- t_r is the 10 / 90 rise time of the driver
- c is the speed of light (3 \times 10⁸ m/s or 9.8 \times 10⁸ ft/s)
- v is the signal velocity of the cable $(v = 78%)$ or trace $(v = 45%)$ as a factor of c (1)

Based on [Equation 1,](#page-11-0) with a minimum rise time of 400 ns, [Equation 2](#page-11-1) shows the maximum cable-stub length of the SN888C device.

 L_{Stub} ≤ 0.1 × 400 × 10⁻⁹ × 3 × 10⁸ × 0.78 = 9,4 m (or 30.6 ft) (2)

Figure 14. Stub Length

3-V to 5-V Interface

Interfacing the SN888C device to a 3-V controller is easy. Because the 5-V logic inputs of the transceiver accept 3-V input signals, they can be directly connected to the controller I/O. The 5-V receiver output, R, however, must be level-shifted by a Schottky diode and a 10-k resistor to connect to the controller input (see [Figure 15](#page-12-0)). When R is high, the diode is reverse biased and the controller supply potential lies at the controller RxD input. When R is low, the diode is forward biased and conducts. Only in this case, the diode forward voltage of 0.2 V lies at the controller RxD input.

Figure 15. 3-V to 5-V Interface

Noise Immunity

The input sensitivity of a standard RS-485 transceiver is ± 200 mV. When the differential input voltage, V_{ID}, is greater than +200 mV, the receiver output turns high, for $V_{ID} < -200$ mV the receiver outputs low.

The SN888C transceiver implements high receiver noise-immunity by providing a typical positive-going input threshold of 35 mV and a minimum hysteresis of 40 mV. In the case of a noisy input condition, a differential noise voltage of up to 40 mV_{PP} can be present without causing the receiver output to change states from high to low.

Transient Protection

The bus terminals of the SN888C transceiver family possess on-chip ESD protection against ±16 kV HBM and ±12 kV IEC61000-4-2 contact discharge. The International Electrotechnical Commision (IEC) ESD test is far more severe than the HBM ESD test. The 50% higher charge capacitance, $C_{\rm S}$, and 78% lower discharge resistance, R_D of the IEC model produce significantly higher discharge currents than the HBM model.

As stated in the IEC 61000-4-2 standard, contact discharge is the preferred transient protection test method. Although IEC air-gap testing is less repeatable than contact testing, air discharge protection levels are inferred from the contact discharge test results.

Figure 16. HBM and IEC-ESD Models and Currents in Comparison (HBM Values in Parenthesis)

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The on-chip implementation of IEC ESD protection significantly increases the robustness of equipment. Common discharge events occur because of human contact with connectors and cables. Designers may choose to implement protection against longer duration transients, typically referred to as surge transients. [Figure 10](#page-6-3) suggests two circuit designs providing protection against short and long-duration surge transients, in addition to ESD and Electrical Fast Transients (EFT) transients. [Table 2](#page-14-0) lists the bill of materials for the external protection devices.

EFTs are generally caused by relay-contact bounce, or the interruption of inductive loads. Surge transients often result from lightning strikes (direct strike or an indirect strike which induces voltages and currents), or the switching of power systems, including load changes and short circuits switching. These transients are often encountered in industrial environments, such as in factory automation and power-grid systems.

[Figure 17](#page-13-0) compares the pulse-power of the EFT and surge transients with the power caused by an IEC ESD transient. In the diagram on the left of [Figure 17](#page-13-0), the tiny blue blip in the bottom left corner represents the power of a 10-kV ESD transient, which is low compared to the significantly higher EFT power spike, and certainly lower than the 500-V surge transient. This type of transient power is well representative of factory environments in industrial and process automation. The diagram on the right of [Figure 17](#page-13-0) compares the enormous power of a 6 kV surge transient, most likely occurring in e-metering applications of power generating and power grid systems, with the aforementioned 500-V surge transient.

NOTE

The unit of the pulse-power changes from kW to MW, thus making the power of the 500-V surge transient almost disappear from the scale.

Figure 17. Power Comparison of ESD, EFT, and Surge Transients

In the case of surge transients, hgih-energy content is signified by long pulse duration and slow-decaying pulse power

The electrical energy of a transient that is dumped into the internal protection cells of the transceiver is converted into thermal energy. This thermal energy heats the protection cells and literally destroys them, thus destroying the transceiver. [Figure 18](#page-14-1) shows the large differences in transient energies for single ESD, EFT, and surge transients as well as for an EFT pulse train, commonly applied during compliance testing.

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Figure 18. Comparison of Transient Energies

Figure 19. Transient Protections Against ESD, EFT, and Surge Transients

The left circuit shown in [Figure 19](#page-14-2) provides surge protection of ≥ 500-V transients, while the right protection circuits can withstand surge transients of 5 kV.

Design and Layout Considerations for Transient Protection

Because ESD and EFT transients have a wide frequency bandwidth from approximately 3 MHz to 3 GHz, highfrequency layout techniques must be applied during PCB design.

In order for PCB design to be successful, begin with the design of the protection circuit in mind.

- 1. Place the protection circuitry close to the bus connector to prevent noise transients from penetrating your board.
- 2. Use V_{cc} and ground planes to provide low-inductance. Note that high-frequency currents follow the path of least inductance, not the path of least impedance.
- 3. Design the protection components into the direction of the signal path. Do not force the transients currents to divert from the signal path to reach the protection device.
- 4. Apply 100-NF to 220-nF bypass capacitors as close as possible to the V_{CC} -pins of transceiver, UART, controller ICs on the board.
- 5. Use at least two vias for V_{CC} and ground connections of bypass capacitors and protection devices to minimize effective via-inductance.
- 6. Use 1-k to 10-k pull-up or pull-down resistors for enable lines to limit noise currents in these lines during transient events.
- 7. Insert pulse-proof resistors into the A and B bus lines, if the TVS clamping voltage is higher than the specified maximum voltage of the transceiver bus terminals. These resistors limit the residual clamping current into the transceiver and prevent it from latching up.
	- While pure TVS protection is sufficient for surge transients up to 1 kV, higher transients require metaloxide varistors (MOVs), which reduce the transients to a few-hundred volts of clamping voltage, and transient blocking units (TBUs) that limit transient current to 200 mA.

Isolated Bus Node Design

Many RS-485 networks use isolated bus nodes to prevent the creation of unintended ground loops and their disruptive impact on signal integrity. An isolated bus node typically includes a micro controller that connects to the bus transceiver through a multi-channel, digital isolator [\(Figure 20\)](#page-16-0).

Figure 20. Isolated Bus Node With Transient Protection

Power isolation is accomplished using the push-pull transformer driver SN6501 and a low-cost LDO, TLV70733.

Signal isolation uses the quadruple digital isolator ISO7241. Notice that both enable inputs, EN1 and EN2, are pulled-up via 4.7-k resistors to limit input currents during transient events.

While the transient protection is similar to the one in [Figure 19](#page-14-2) (left circuit), an additional high-voltage capacitor diverts transient energy from the floating RS-485 common further towards protective earth (PE) ground. This diversion is necessary as noise transients on the bus are usually referred to earth potential.

 R_{VH} refers to a high-voltage resistor, and in some applications, even a varistor. This resistance is applied to prevent charging of the floating ground to dangerous potentials during normal operation.

Occasionally varistors are used instead of resistors in order to rapidly discharge C_{HV} , if expecting that fast transients might charge C_{HV} to high-potentials.

Note that the PE island represents a copper island on the PCB for the provision of a short, thick earth wire connecting this island to PE ground at the entrance of the power supply unit (PSU).

In equipment designs using a chassis, the PE connection is usually provided through the chassis itself. Typically the PE conductor is tied to the chassis at one end, while the high-voltage components, C_{HV} and R_{HV} , connect to the chassis at the other end.

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PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

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(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE OPTION ADDENDUM

PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

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PACKAGE MATERIALS INFORMATION

*All dimensions are nominal

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TUBE

*All dimensions are nominal

PACKAGE OUTLINE

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.

EXAMPLE BOARD LAYOUT

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.

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