

FEATURES

Large, triple 16 × 5 high speed, nonblocking switch array Pin compatible with th[e AD8175 a](http://www.analog.com/AD8175?doc=AD8178.pdf)nd [AD8176 \(](http://www.analog.com/AD8176?doc=AD8178.pdf)16 × 9 switch arrays) and th[e AD8177 \(](http://www.analog.com/AD8177?doc=AD8178.pdf)16 × 5 switch array) Differential or single-ended operation Supports sync-on common-mode and sync-on color operating modes RGB and HV outputs available for driving monitor directly G = +4 operation (differential input to differential output) Flexible power supplies: +5 V or ±2.5 V Logic ground for convenient control interface Serial or parallel programming of switch array High impedance output disable allows connection of multiple devices with minimal loading on output bus Adjustable output CM and black level through external pins Excellent ac performance Bandwidth: 450 MHz Slew rate: 1650 V/µs Settling time: 4 ns to 1% to support 1600 × 1200 at 85 Hz Low power of 2.3 W Low all hostile crosstalk −82 dB at 5 MHz −47 dB at 500 MHz Wide input common-mode range of 4 V Reset pin allows disabling of all outputs Fully populated 26 × 26 ball PBGA package (27 mm × 27 mm, 1 mm ball pitch) Convenient grouping of RGB signals for easy routing APPLICATIONS

RGB video switching KVM Professional video

GENERAL DESCRIPTION

The $AD8178$ is a high speed, triple 16×5 video crosspoint switch matrix. It supports 1600×1200 RGB displays at 85 Hz refresh rate, by offering a 450 MHz bandwidth and a slew rate of 1650 V/µs. With −82 dB of crosstalk and −84 dB isolation (at 5 MHz), the [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)s useful in many high speed video applications.

The [AD8178 s](http://www.analog.com/AD8178?doc=AD8178.pdf)upports two modes of operation: differential-in to differential-out mode with sync-on CM signaling passed through the switch and differential-in to differential-out mode with CM signaling removed through the switch. The output CM and black level can be conveniently set via external pins.

Rev. A [Document Feedback](https://form.analog.com/Form_Pages/feedback/documentfeedback.aspx?doc=AD8178.pdf&product=AD8178&rev=A)

Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties that may result from its use. Specifications subject to change without notice. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices. Trademarks and registered trademarks are the property of their respective owners.

450 MHz, Triple 16 \times 5 Video Crosspoint Switch

Data Sheet **[AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf)**

The outputs can be used single-ended in conjunction with decoded H and V outputs to drive a monitor directly.

The independent output buffers of the [AD8178 c](http://www.analog.com/AD8178?doc=AD8178.pdf)an be placed into a high impedance state to create larger arrays by paralleling crosspoint outputs. Inputs can be paralleled as well. Th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) offers both serial and a parallel programming modes.

The $AD8178$ is packaged in a fully populated 26×26 ball PBGA package and is available over the extended industrial temperature range of −40°C to +85°C.

One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A. ©2007-2016 Analog Devices, Inc. All rights reserved. **[Technical Support](http://www.analog.com/en/content/technical_support_page/fca.html) www.analog.com**

TABLE OF CONTENTS

REVISION HISTORY

5/16—Rev. 0 to Rev. A

SPECIFICATIONS

 $V_S = \pm 2.5$ V at T_A = 25°C, G = +4, R_L = 100 Ω (each output), VBLK = 0 V, output CM voltage = 0 V, differential I/O mode, unless otherwise noted.

Table 1.

Rev. A | Page 4 of 37

TIMING CHARACTERISTICS (SERIAL MODE)

Table 2.

Table 3. Logic Levels, $V_{DD} = 3.3 \text{ V}$

Table 4. H and V Logic Levels, $V_{DD} = 3.3$ V

Table 5. $\overline{\text{RST}}$ Logic Levels, $V_{\text{DD}} = 3.3 \text{ V}$

Table 6. $\overline{\text{CS}}$ Logic Levels, $V_{\text{DD}} = 3.3 \text{ V}$

TIMING CHARACTERISTICS (PARALLEL MODE)

Table 7.

Figure 3. Timing Diagram, Parallel Mode

Table 8. Logic Levels, $V_{DD} = 3.3 V$

Table 9. H and V Logic Levels, $V_{DD} = 3.3 V$

Table 10. $\overline{\text{RST}}$ Logic Levels, $V_{\text{DD}} = 3.3 \text{ V}$

Table 11. $\overline{\text{CS}}$ Logic Levels, $V_{\text{DD}} = 3.3 \text{ V}$

ABSOLUTE MAXIMUM RATINGS

Table 12.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

THERMAL RESISTANCE

 θ_{IA} is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

Table 13. Thermal Resistance

POWER DISSIPATION

The AD8178 is operated with ± 2.5 V or $+5$ V supplies and can drive loads down to 100 Ω , resulting in a large range of possible power dissipations. For this reason, extra care must be taken when derating the operating conditions based on ambient temperature.

Packaged in a 676-lead PBGA, the AD8178 junction-to-ambient thermal impedance (θ_{IA}) is 15°C/W. For long-term reliability, the maximum allowed junction temperature of the die must not exceed 150°C. Temporarily exceeding this limit may cause a shift in parametric performance due to a change in stresses exerted on the die by the package. Exceeding a junction temperature of 175°C for an extended period can result in device failure. The curve in Figure 4 shows the range of allowed internal die power dissipations that meet these conditions over the −40°C to +85°C ambient temperature range. When using Table 13, do not include external load power in the maximum power calculation, but do include load current dropped on the die output transistors. de Analog Input Voltage

Map (V_{tex +} 0.5 V) to

Ne ADS178 is operated with +2.5 V or +5 V supplies

(V_{tex} + 0.5 V) drive local down to 100 0, resulting the ange range

(V_{tex} - 1 V) to (V_{xtex} + 1 V) drive local dow

Figure 4. Maximum Die Power Dissipation vs. Ambient Temperature

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

Table 14. Pin Function Description

 $\overline{}$

 $\overline{}$

TRUTH TABLE AND LOGIC DIAGRAM

Table 15. Operation Truth Table

1 X = don't care.

Figure 7. Logic Diagram

EQUIVALENT CIRCUITS

Figure 8. Enabled Output (Also See ESD Protection Map, Figure 19)

Figure 9. Disabled Output (Also See ESD Protection Map, Figure 19)

Figure 10. Receiver Differential (Also See ESD Protection Map, Figure 19)

Figure 11. Receiver Simplified Equivalent Circuit When Driving Differentially

Figure 13. VBLK and VOCM_CMENCOFF Inputs (Also See ESD Protection Map, Figure 19)

Figure 14. VOCM_CMENCON Input (Also See ESD Protection Map[, Figure 19\)](#page-19-0)

Figure 15. RST Input (Also See ESD Protection Map[, Figure 19\)](#page-19-0)

Figure 16. Logic Input (Also See ESD Protection Map[, Figure 19\)](#page-19-0)

Figure 17. CS Input (Also See ESD Protection Map[, Figure 19\)](#page-19-0)

AD8178 Data Sheet

06608-032

06608-033

d −1.2
8

ñ0.9 ñ0.6 ñ0.3 0 0.3 0.6 0.9 1.2

VOUT, DIFF (V)

 V_{OUT} , I

DIFF (N)

06608-034

TYPICAL PERFORMANCE CHARACTERISTICS

 $V_S = \pm 2.5$ V at T_A = 25°C, G = +2, R_L = 100 Ω (each output), VBLK = 0 V, output CM voltage = 0 V, differential I/O mode, unless otherwise noted.

1.25 0.020 5 0.015 4 1.00 VOUT UPDATE NORMALIZED DC GAIN (dB) V_{OUT}, SINGLE-ENDED (V) **0.010 VOUT, SINGLE-ENDED (V) 0.75 3 0.005 UPDATE (V) UPDATE (V) 32ppm/°C 0.50 2 0 ñ0.005 0.25 1 ñ0.010** Figure 44. Enable Time

Figure 44. Enable Time

Figure 45. Norther Time

Figure 45. Norther Time

Figure 55. Normalized DC Gain y, Temperature

Figure 55. Normalized DC Gain y, Temperature **0 0** -0.015 -0.020 -40 -0.25 —1 └—
0 $\frac{4}{100}$ **0 20 40 60 80 100 120 140 160 180 200 220 240 260 280** 06608-053 **ñ40 ñ20 0 20 40 60 80 100 TEMPERATURE (°C) TIME (ns)** Figure 44. Enable Time

THEORY OF OPERATION

The [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) is a nonblocking crosspoint with 16 RGB input channels and 5 RGB output channels. Architecturally, the [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) is a differential-in, differential-out crosspoint suited for middle-of-Cat-5-run applications. Furthermore, its differentialin, differential-out gain of +4 and its decoded H and V sync outputs make it the ideal solution for driving a monitor directly. The ability to set the output common-mode (CM) and black level through external pins offers additional flexibility.

Processing of CM voltage levels is achieved by placing the AD8178 in either of its two operation modes. In the first operation mode (CMENC low), the input CM of each RGB differential pair (possibly present in the form of either sync-on CM signaling or noise) is removed through the switch, and the output CM is set to a global reference voltage via the VOCM_CMENCOFF analog input. In this mode, the AD8178 behaves as a traditional differential-in, differential-out switch. If sync-on CM signaling is present at the differential RGB inputs, then the H and V outputs represent decoded syncs. In the second operation mode (CMENC high), input sync-on CM signaling is propagated through the switch with unity gain. In this mode, the overall output CM is set to a global reference voltage via the VOCM_CMENCON analog input. Note that in both operation modes, the overall input CM is blocked through the switch.

Input Pin VBLK defines the black level of the positive output phase. The combination of VBLK and VOCM_CMENCOFF allows the user to position the positive and negative output phases anywhere in the allowable output voltage range, thus maximizing output headroom usage.

The switch is organized into five 16:1 RBG multiplexers, with each being responsible for connecting an RGB input channel to its respective RGB output channel. Decoding logic selects a single input (or none) in each multiplexer and connects it to its respective output. Feedback around each multiplexer realizes a closed-loop differential-in, differential-out gain of +2 in the core.

Each differential RGB input channel is buffered by a differential receiver that is capable of accepting input CM voltages extending all the way to either supply rail. Excess closed-loop receiver bandwidth reduces the effect of the receiver on the overall device bandwidth. Feedback around each differential receiver realizes a gain of +2 yielding an overall differential-in, differential-out crosspoint gain of +4. A separate loop realizes a closed-loop common-mode gain of +1.

The output stage is designed for fast slew rate and settling time, while driving a series-terminated Cat-5 cable. Unlike competing multiplexer designs, the small signal bandwidth closely approaches the large signal bandwidth.

The outputs of the [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) can be disabled to minimize on-chip power dissipation. When disabled, there is only a commonmode feedback network of 2.7 kΩ between the differential outputs. This high impedance allows multiple ICs to be bussed together without additional buffering. Care must be taken to reduce output capacitance, which can result in overshoot and frequencydomain peaking. A series of internal amplifiers drive internal nodes such that wideband high impedance is presented at the disabled output, even while the output bus experiences fast signal swings. When the outputs are disabled and driven externally, the voltage applied to them cannot exceed the valid output swing range for the AD8178 to keep these internal amplifiers in their linear range of operation. Applying excessive differential voltages to the disabled outputs can cause damage to th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) and must be avoided (see the Absolute Maximum Ratings section for guidelines).

The connectivity of the AD8178 is controlled by a flexible TTLcompatible logic interface. Either parallel or serial loading into a first rank of latches preprograms each output. A global update signal moves the programming data into the second rank of latches, simultaneously updating all outputs. In serial mode, a serial-out pin allows devices to be daisy-chained together for a single-pin programming of multiple ICs. A power-on reset pin is available to avoid bus conflicts by disabling all outputs. This power-on reset clears the second rank of latches but does not clear the first rank of latches. In serial mode, preprogramming individual inputs is not possible and the entire shift register needs to be flushed. A global chip-select pin gates the input clock and the global update signal to the second rank of buffers. diagle levels is achieved by placing the AD8178

similade output are othystane is signified to the first operation model

operation model is the first operation and the court of the output CM is experience in the first op

The AD8178 can operate on a single 5 V supply, powering both the signal path (with the VPOS/VNEG supply pins) and the control logic interface (with the VDD/DGND supply pins). Split supply operation is possible with ±2.5 V supplies that easily interface to ground-referenced video signals. In this case, a flexible logic interface allows the control logic supplies (VDD/DGND) to be run off 5 V/0 V to 3.3 V/0 V while the analog core remains on split supplies. Additional flexibility in the analog output commonmode level (VOCM_CMENCOFF) and output black level (VBLK) facilitates operation with unequally split supplies. If +3 V/−2 V still be set to 0 V for ground-referenced video signals.

APPLICATIONS INFORMATION **OPERATING MODES**

Depending on the state of the CMENC logic input, the [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) can be set in either of two differential-in, differential-out operating modes. In addition, monitors can be driven directly by tapping the outputs single-ended and making use of the decoded H and V sync outputs.

Middle of Cat-5 Run Application, CM Encoding Turned Off

In this application, the AD8178 is placed somewhere in the middle of a Cat-5 run. By tying CMENC low, the CM of each RGB differential pair is removed through the device (or turned off), and the overall CM at the output is defined by the reference value VOCM_CMENCOFF. In this mode of operation, CM noise is removed, while the intended differential RGB signals are buffered and passed to the outputs. The AD8178 is placed in this operation mode when used in a sync-on color scheme. Figure 46 shows the voltage levels and CM handling for a single input channel connected to a single output channel in a middle of Cat-5 run application with CM encoding turned off. Let the minimal technique of the middle of Cat-5 for and the middle of Cat-5 for an and technique of the extreme value of the control of the contr

Figure 46[. AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)n a Middle of Cat-5 Run Application, CM Encoding Off (Note that in this application, the H and V outputs, though asserted, are not used.)

Input VBLK and Input VOCM_CMENCOFF allow the user complete flexibility in defining the output CM level and the amount of overlap between the positive and negative phases, thus maximizing output headroom usage. Whenever VBLK differs from VOCM_CMENCOFF by more than ±100 mV, a differential voltage, Δ_{diff} , is added at the outputs according to the expression $\Delta_{diff} = 2 \times (VBLK - VOCM_CMENCOFF.)$ Conversely, whenever the difference between VBLK and VOCM_CMENCOFF is less than ±100 mV, no differential voltage is added at the outputs.

Middle of Cat-5 Run Application, CM Encoding Turned On

In this application, th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) is also placed somewhere in the middle of a Cat-5 run, although the common-mode handling is different. By tying CMENC high, the CM of each RGB input is passed through the part with a gain of +1, while at the same time, the overall output CM is stripped and set equal to the voltage applied at the VOCM_CMENCON pin. The [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)s placed in this operation mode when used with a sync-on CM scheme. Although asserted, the H and V outputs are not used in this application.

[Figure 47 s](#page-26-3)hows the voltage levels and CM handling for a single input channel connected to a single output channel in a middle of Cat-5 run application with CM encoding turned on.

Figure 47. AD8178 in Middle-of-Cat-5-Run Application, CM Encoding On (Note that in this application, the H and V outputs, though asserted, are not used.)

In this operation mode, the difference $\Delta_{\text{diff}} = 2 \times (\text{VBLK} - \text{C}^2)$ VOCM_CMENCOFF) still adds an output differential voltage, as described in th[e Middle of Cat-5 Run Application, CM](#page-26-4) Encoding Turned Off section.

End of Cat-5 Run Application, CM Encoding Turned Off— Driving a Monitor Directly

In this application, the AD8178 is placed at the end of a Cat-5 run to drive a monitor directly: the differential outputs are tapped single-ended to drive the monitor inputs, CMENC is tied to logic low to remove sync-on-CM information at the output of the part, and the decoded H and V sync outputs are tied to the sync inputs of the monitor.

The differential-in, differential-out gain of +4 provides a differential-in, single-ended out gain of +2 at the output pins of the AD8178. This yields the correct differential-in, single-ended out gain of +1 at the input of the monitor.

The relationship between the incoming sync-on CM signaling and the H and V syncs is defined according t[o Table 16.](#page-26-5)

Table 16. H and V Sync Truth Table ($V_{POS}/V_{NEG} = \pm 2.5 V$)

CM _R	CM_G	CMB	н	v
0.5	0		Low	High
0	0.5	-0.5	Low	Low
-0.5	0.5	0	High	Low
0	-0.5	0.5	High	High

The following two statements are equivalent to the truth table (see [Table 16\)](#page-26-5) in producing H and V for all allowable CM inputs:

- H sync is high when the CM of blue is larger than the CM of red.
- V sync is high when the combined CM of red and blue is larger than the CM of green.

For a practical example, refer t[o Figure 48.](#page-27-1) Note that the output pulses have been shifted slightly with respect to each other for clarity.

Figure 48. Output at the AD8178 Pins for 0 V to 0.7 V Input Differential Pulse, $VBLK = 0 V$, VOCM CMENCOFF = 0.7 V

The input to the AD8178 is a differential pulse with a low level of 0 V and a high level of 0.7 V. VBLK is set to 0 V, and VOCM_ CMENCOFF is set to 0.7 V. With this choice of values, the positive and negative output phases are overlapped, with the positive phase ranging from 0 V to 1.4 V, and the negative phase ranging from 1.4 V to 0 V, respectively. The supplies are set to +3 V/−2 V to be in compliance with output headroom requirements.

The voltage on the positive output phase for a 0 V differential input is equal to the voltage on VBLK, for all cases when VBLK and VOCM_CMENCOFF differ by more than ±100 mV.

PROGRAMMING

The [AD8178 h](http://www.analog.com/AD8178?doc=AD8178.pdf)as two options for changing the programming of the crosspoint matrix. In the first option, a serial word of 45 bits can be provided that updates the entire matrix each time. The second option allows for changing the programming of a single output using a parallel interface. The serial option requires fewer signals, but more time (clock cycles), for changing the programming; the parallel programming technique requires more signals, but it allows for changing a single output at a time, therefore requiring fewer clock cycles.

Serial Programming Description

The serial programming mode uses the device pins $\overline{\text{CS}}, \overline{\text{CLK}},$ SERIN, UPDATE, and SER/PAR. The first step is to enable the $\overline{\text{CLK}}$ on by pulling $\overline{\text{CS}}$ low. Next, $\overline{\text{SER}}$ /PAR is pulled low to enable the serial programming mode. Hold the parallel clock WE high during the entire serial programming operation.

Ensure that the UPDATE signal is high during the time that data is shifted into the serial port of the device. Although the data still shifts in when UPDATE is low, the transparent, asynchronous latches allow the shifting data to reach the matrix. This causes the matrix to try to update to every intermediate state as defined by the shifting data.

The data at SERIN is clocked in at every falling edge of CLK. A total of 45 bits must be shifted in to complete the programming. A total of five bits must be supplied for each of the five RGB output channels: an output enable bit (D4) and four bits (D3 to D0) that determine the input channel.

If D4 is low (output disabled), the four associated bits (D3 to D0) do not matter because no input is switched to that output. A sequence of five bits at Logic 0 must be supplied in between each D4 to D0 group of bits for padding purposes. There is a total of four such sequences of zeros.

The most significant output address data is shifted in first, with the enable bit (D4) shifted in first, followed by the input address (D3 to D0) entered sequentially with D3 first and D0 last. The first sequence of five bits at Logic 0 is shifted in next. Each remaining output is programmed sequentially in a similar fashion, until the least significant output address data is shifted in. Note that the last D4 to D0 group is not followed by a corresponding group of five zeros. At this point, UPDATE can be taken low, which causes the programming of the device according to the data that was just shifted in. The UPDATE latches are asynchronous; and when UPDATE is low, they are transparent.

If more than one AD8178 device is to be serially programmed in a system, the SEROUT signal from one device can be connected to the SERIN of the next device to form a serial chain. Connect all of the CLK, UPDATE, and SER/PAR pins in parallel and operate as described previously. The serial data is input to the SERIN pin of the first device of the chain, and it ripples through to the last. Therefore, the data for the last device in the chain must come at the beginning of the programming sequence. The length of the programming sequence is 45 bits times the number of devices in the chain. CS gates the CLK and UPDATE signals; therefore, when $\overline{\text{CS}}$ is held high, both $\overline{\text{CLK}}$ and $\overline{\text{UPDATE}}$ are held in their inactive high state., and when $\overline{\text{CS}}$ is held low, both $\overline{\text{CLK}}$ and $\overline{\text{UPDATE}}$ function normally. **EVALUATE: The state of the CIF and The CONCILE STATE of the state of the CONCILE AND THE STATE AND THE STATE**

Parallel Programming Description

When using the parallel programming mode, it is not necessary to reprogram the entire device when making changes to the matrix. In fact, parallel programming allows the modification of a single output or more at a time. Because this modification takes only one WE/UPDATE cycle, significant time savings can be realized by using parallel programming.

One important consideration in using parallel programming is that the RST signal does not reset all registers in the [AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf) When taken low, the $\overline{\text{RST}}$ signal only sets each output to the disabled state. This is helpful during power-up to ensure that two parallel outputs are not active at the same time.

After initial power-up, the internal registers in the device generally have random data, even though the RST signal is asserted. If parallel programming is used to program one output, then that output is properly programmed, but the rest of the device has a random program state, depending on the internal register content at power-up. Therefore, when using parallel programming, it is essential that all outputs be programmed to a desired state after power-up. This ensures that the programming matrix is always in a known state. From then on, parallel programming can be used to modify a single output or more at a time.

In similar fashion, if UPDATE is taken low after initial power-up, the random power-up data in the shift register is programmed into the matrix. Therefore, to prevent the crosspoint from being programmed into an unknown state, do not apply a logic level to UPDATE after power is initially applied. Programming the device into a known state after reset or power-up is a one-time event that is accomplished by the following two steps:

- 1. Output 4 to Output 0 are programmed to the off state while holding the CLR input at a logic high.
- 2. Each output (Output 4 to Output 0) is programmed to its desired state while holding the CLR input at a logic low.

CLR is held at logic low thereafter.

To change the programming of an output via parallel programming, take $\overline{\text{CS}}$ low, and take $\overline{\text{SER}}$ /PAR and $\overline{\text{UPDATE}}$ high. Leave the serial programming clock, $\overline{\text{CLK}}$, high during parallel programming. Start the parallel clock, \overline{WE} , in the high state. Put the 3-bit address of the output to be programmed on A2 to A0. Data Bit D3 to Data Bit D0 must contain the information that identifies the input that is programmed to the output that is addressed. Data Bit D4 determines the enabled state of the output. If D4 is low (output disabled), the data on D3 to D0 does not matter. put (Output 18 to Output 18 is programmed to the Sole of the Coupling of the contract in single-ended fashion. Si

tate while holding the CLR imput at a logic low

tate while holding the CLR imput via parallel

sections, a

After the desired address and data signals have been established, they can be latched into the shift register by a high-to-low transition of the WE signal. The matrix is not programmed, however, until the UPDATE signal is taken low. It is thus possible to latch in new data for several or all of the outputs first via successive negative transitions of WE while UPDATE is held high, and then have all the new data take effect when UPDATE goes low. Use this technique to program the device for the first time after powerup when using parallel programming.

Programming the device to a known state can be accomplished in serial programming mode by clocking in the entire 45-bit sequence immediately after reset or power-up.

Reset

When powering up the AD8178, it is usually desirable to have the outputs come up in the disabled state. The RST pin, when taken low, causes all outputs to be in the disabled state. However, the RST signal does not reset all registers in the AD8178. This is important when operating in the parallel programming mode. See th[e Parallel Programming Description s](#page-27-2)ection for information about programming internal registers after power-up. Serial programming programs the entire matrix each time, so no special considerations apply.

Because the data in the shift register is random after power-up, do not use it to program the matrix, or the matrix can enter unknown states. To prevent this, do not apply a logic low signal to UPDATE initially after power-up. First load the shift register with the desired data, and only then can the UPDATE be taken low to program the device.

The RST pin has a 20 k Ω pull-up resistor to VDD that can be used to create a simple power-up reset circuit. A capacitor from $\overline{\text{RST}}$ to ground holds $\overline{\text{RST}}$ low for some time, while the rest of the device stabilizes. The low condition causes all the outputs to be disabled. The capacitor then charges through the pull-up resistor to the high state, thus allowing full programming capability of the device.

DIFFERENTIAL AND SINGLE-ENDED OPERATION

Although th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) has fully differential inputs and outputs, it can also operate in single-ended fashion. Single-ended and differential configurations are discussed in the following sections, along with implications on gain, impedances, and terminations.

Differential Input

Each differential input to the AD8178 is applied to a differential receiver. These receivers allow the user to drive the inputs with an uncertain common-mode voltage, such as from a remote source over twisted pair. The receivers respond only to the differences in input voltages and restore an internal common mode suitable for the internal signal path. Noise or crosstalk, which affect each the inputs of each receiver equally, are rejected by the input stage, as specified by its common-mode rejection ratio (CMRR).

Furthermore, the overall common-mode voltage of all three differential pairs comprising an RGB channel is processed and rejected by a separate circuit block. For example, a static discharge or a resistive voltage drop in a middle-of-Cat-5-run application with sync-on CM signaling coupling into all three pairs in an RGB channel are rejected at the output of th[e AD8178,](http://www.analog.com/AD8178?doc=AD8178.pdf) while the sync-on CM signals are allowed through the switch.

The circuit configuration used by the differential input receivers is similar to that of several Analog Devices, Inc. general-purpose differential amplifiers, such as the AD8131. The topology is that of a voltage-feedback amplifier with internal gain resistors. The input differential impedance for each receiver is 5 kΩ in parallel with 10 kΩ or 3.33 kΩ, as shown in Figure 49.

Figure 49. Input Receiver Equivalent Circuit

This impedance creates a small differential termination error if the user does not account for the 3.33 k Ω parallel element. However, this error is less than 1% in most cases. Additionally, the source impedance driving the [AD8178 a](http://www.analog.com/AD8178?doc=AD8178.pdf)ppears in parallel with the internal gain-setting resistors, such that there may be a gain error for some values of source resistance.

The [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)s adjusted such that its gain is correct when driven by a back terminated Cat-5 cable (25 Ω effective impedance to ground at each input pin, or 100 Ω differential source impedance across pairs of input pins). If a different source impedance is presented, calculate the differential gain of the [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)nput receiver by

$$
G_{DM} = \frac{5.05 \,\text{k}\Omega}{2.5 \,\text{k}\Omega + R_S}
$$

where R_s is the effective impedance to ground at each input pin.

When operating with a differential input, care must be taken to keep the common mode, or average, of the input voltages within the linear operating range of the AD8178 receiver. For the AD8178 receiver, this common-mode range can extend rail-to-rail, provided the differential signal swing is small enough to avoid forward biasing the ESD diodes (it is safest to keep the common mode plus differential signal excursions within the supply voltages of the part).

The input voltage of the AD8178 is linear for ± 0.5 V of differential input voltage difference (this limitation is primarily due to the ability of the output to swing close to the rails because the differential gain through the part is +4). Beyond this level, the signal path saturates and limits the signal swing. This is not a desired operation because the supply current increases and the signal path is slow to recover from clipping. The absolute maximum allowed differential input signal is limited by longterm reliability of the input stage. Observe the limits in the [Absolute Maximum Ratings s](#page-6-0)ection to avoid degrading device performance permanently.

AC Coupling of Inputs

It is possible to ac-couple the inputs of the AD8178 receiver so that bias current does not need to be supplied externally. A capacitor in series with the inputs to the AD8178 creates a highpass filter with the input impedance of the device. This capacitor needs to be large enough that the corner frequency includes all frequencies of interest.

Single-Ended Input

The [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)nput receiver can be driven single-ended (unbalanced). Single-ended inputs apply a component of common-mode signal to the receiver inputs, which is then rejected by the receiver (see the Specifications section for common-mode-to-differential-mode ratio of the part).

The single-ended input resistance, R_{IN} , differs from the differential input impedance, and is equal to

$$
R_{IN} = \frac{R_G}{1 - \frac{R_F}{2 \times (R_G + R_F)}}
$$

with R_G and R_F , as shown in Figure 49.

Note that this value is smaller than the differential input resistance, but it is larger than RG. The difference is due to the component of common-mode level applied to the receiver by single-ended inputs. A second, smaller component of input

resistance (R_{CM} , also shown i[n Figure 49\)](#page-28-1) is present across the inputs in both single-ended and differential operation.

In single-ended operation, an input is driven, and the undriven input is often tied to midsupply or ground. Because signal frequency current flows at the undriven input, treat such an input as a signal line in the board design.

For example, to achieve best dynamic performance, terminate the undriven input with an impedance matching that is seen by the device at the driven input.

Differential Output

Benefits of Differential Operation

The AD8178 has a fully differential switch core with differential outputs. The two output voltages move in opposite directions, with a differential feedback loop maintaining a fixed output stage differential gain of +2 through the core. This differential output stage provides improved crosstalk cancellation due to parasitic coupling from one output to another being equal and out of phase. Additionally, if the output of the device is used in a differential design, then noise, crosstalk, and offset voltages generated on-chip that are coupled equally into both outputs are cancelled by the common-mode rejection ratio of the next device in the signal chain. By utilizing the AD8178 outputs in a differential application, the best possible noise and offset specifications can be realized. 2000 the converge of the input vto the state in the state of the input vto the state in the state of the input vector of t

Differential Gain

The specified signal path gain of the AD8178 refers to its differential gain. For the AD8178, the gain of +4 means that the difference in voltage between the two output terminals is equal to four times the difference between the two input terminals.

Common-Mode Gain

The common-mode, or average voltage pairs of output signals is set by the voltage on the VOCM_CMENCOFF pin when common-mode encoding is off (CMENC is a logic low), or by the voltage on the VOCM_CMENCON pin when common-mode encoding is on (CMENC is a logic high). Note that in the latter case, VCOM_CMENCON sets the overall common mode of RGB triplets of differential outputs, and the individual common mode of each RGB output is free to change. VCOM_CMENCON and VCOM_CMENCOFF are typically set to midsupply (often ground) but can be moved approximately ±0.5 V to accommodate cases where the desired output common-mode voltage may not be midsupply (as in the case of unequal split supplies). Adjusting the output common-mode voltage beyond ±0.5 V can limit differential swing internally below the specifications on the data sheet. The overall common mode of the output voltages follow the voltage applied to VOCM_CMENCON or VCOM_CMENCOFF, implying a gain of +1. Likewise, sync-on common-mode signaling is carried through th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) (CMENC must be in its high state), implying a gain of +1 for this path as well.

The common-mode reference pins are analog signal inputs, common to all output stages on the device. They require only

small amounts of bias current, but noise appearing on these pins is buffered to all the output stages. As such, connect them to low noise, low impedance voltage references to avoid being sources of noise, offset, and crosstalk in the signal path.

Termination

The [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) is designed to drive 100 Ω terminated to ground on each output (or an effective 200 Ω differential) while meeting data sheet specifications over the specified operating temperature range, if care is taken to observe the maximum power derating curves.

Termination at the load end is recommended to shorten settling time and provide for best signal integrity. In differential signal paths, it is often desirable to series-terminate the outputs, with a resistor in series with each output. A side effect of termination is an attenuation of the output signal by a factor of two. In this case, gain is usually necessary somewhere else in the signal path to restore the signal level.

Whenever a differential output is used single-ended, it is desirable to terminate the used single-ended output with a series resistor, as well as to place a resistor on the unused output to match the load seen by the used output.

When disabled, the outputs float to midsupply. A small current is required to drive the outputs away from their midsupply state. This current is easily provided by an AD8178 output (in its enabled state) bussed together with the disabled output. Exceeding the allowed output voltage range may saturate internal nodes in the disabled output, and consequently, an increase in disabled output current may be observed.

Single-Ended Output

Usage

The [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) output pairs can be used single-ended, taking only one output and not using the second. This is often desired to reduce the routing complexity in the design or because a singleended load is being driven directly. This mode of operation produces good results but has some shortcomings when compared to taking the output differentially. When observing the single-ended output, noise that is common to both outputs appears in the output signal.

When observing the output single-ended, the distribution of offset voltages appears greater. In the differential case, the difference between the outputs, when the difference between the inputs is zero, is a small differential offset. This offset is created from mismatches in devices in the signal path. In the single-ended case, this differential offset is still observed, but an additional offset component is also relevant. This additional component is the common-mode offset, which is the difference between the average of the outputs and the output common-mode reference. This offset is created by mismatches that affect the signal path in a common-mode manner. A differential receiver rejects this common-mode offset voltage, but in the single-ended case, this offset is observed with respect to the signal ground. The singleended output sums half the differential offset voltage and all of

the common-mode offset voltage for a net increase in observed offset.

Single-Ended Gain

The [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) operates as a closed-loop differential amplifier. The primary control loop forces the difference between the output terminals to be a ratio of the difference between the input terminals. One output increases in voltage, while the other decreases an equal amount to make the total output voltage difference correct. The average of these output voltages is forced to the voltage on the common-mode reference terminal (VOCM_CMENCOFF or VOCM_CMENCON) by a second control loop. If only one output terminal is observed with respect to the common-mode reference terminal, only half of the difference voltage is observed. This implies that when using only one output of the device, half of the differential gain is observed. An AD8178 taken with single-ended output appears to have a gain of +2.

It is important to note that all considerations that apply to the used output phase regarding output voltage headroom apply unchanged to the complement output phase, even if this is not actually used.

Termination

When operating the AD8178 with a single-ended output, the preferred output termination scheme is to refer the load to the output common mode. A series termination can be used, at an additional cost of one half the signal gain.

In single-ended output operation, the complementary phase of the output is not used and may or may not be terminated locally. Although the unused output can be floated to reduce power dissipation, there are several reasons for terminating the unused output with a load resistance matched to the load on the signal output.

One component of crosstalk is magnetic coupling by mutual inductance between output package traces and bond wires that carry load current. In a differential design, there is coupling from one pair of outputs to other adjacent pairs of outputs. The differential nature of the output signal simultaneously drives the coupling field in one direction for one phase of the output and in an opposite direction for the other phase of the output. These magnetic fields do not couple equally into adjacent output pairs, due to different proximities; but they do destructively cancel the crosstalk to some extent. If the load current in each output is equal, this cancellation is greater and less adjacent crosstalk is observed (regardless of whether the second output is actually being used). is forced to the voltaing on the complementation and the signal integrals and the velocity of the complementation and the complementation of the complementation of the complementation of the complementation of the compleme

> A second benefit of balancing the output loads in a differential pair is to reduce fluctuations in current requirements from the power supply. In single-ended loads, the load currents alternate from the positive supply to the negative supply. This creates a parasitic signal voltage in the supply pins due to the finite resistance and inductance of the supplies. This supply fluctuation appears as crosstalk in all outputs, attenuated by the power supply rejection ratio (PSRR) of the device.

At low frequencies, this is a negligible component of crosstalk, but PSRR falls off as frequency increases. With differential, balanced loads, as one output draws current from the positive supply, the other output draws current from the negative supply. When the phase alternates, the first output draws current from the negative supply and the second draws from the positive supply. The effect is that a more constant current is drawn from each supply, such that the crosstalk-inducing supply fluctuation is minimized.

A third benefit of driving balanced loads is that the output pulse response changes as the load changes. The differential signal control loop in the AD8178 forces the difference of the outputs to be a fixed ratio to the difference of the inputs. If the two output responses are different due to loading, this creates a difference that the control loop sees as signal response error, and it attempts to correct this error. This distorts the output signal from the ideal response compared to the case when the two outputs are balanced.

Decoupling

The signal path of the AD8178 is based on high open-loop gain amplifiers with negative feedback. Dominant-pole compensation is used on-chip to stabilize these amplifiers over the range of expected applied swing and load conditions. To guarantee this designed stability, proper supply decoupling is necessary with respect to both the differential control loops and the commonmode control loops of the signal path. Signal-generated currents must return to their sources through low impedance paths at all frequencies in which there is still loop gain (up to 700 MHz at a minimum). The matter of the distribution of the distribution of the coupling of the control of the state of the difference of the inputs of the two control loop sees as signal response error, and

and the difference of the inputs o

The signal path compensation capacitors in the AD8178 are connected to the VNEG supply. At high frequencies, this limits the power supply rejection ratio (PSRR) from the VNEG supply to a lower value than that from the VPOS supply. If given a choice, design the application board such that the VNEG power is supplied from a low inductance plane, subject to a least amount of noise.

VOCM_CMENCON and VOCM_CMENCOFF are high speed common-mode control loops of all output drivers. In the singleended output sense, there is no rejection from noise on these inputs to the outputs. For this reason, care must be taken to produce low noise sources over the entire range of frequencies of interest. This is important not only to single-ended operation, but to differential operation, because there is a common-modeto-differential gain conversion that becomes greater at higher frequencies.

VOCM_CMENCON and VOCM_CMENCOFF are internally buffered to prevent transients flowing into or out of these inputs from acting on the source impedance and becoming sources of crosstalk.

Power Dissipation

Calculation of Power Dissipation

Figure 50. Maximum Die Power Dissipation vs. Ambient Temperature

The curve in Figure 50 was calculated from

$$
P_{D,MAX} = \frac{T_{JUNCTION, MAX} - T_{AMBLEM}}{\theta_{JA}} \tag{1}
$$

As an example, if the AD8178 is enclosed in an environment at 45°C (TA), the total on-chip dissipation under all load and supply conditions must not be allowed to exceed 7.0 W.

When calculating on-chip power dissipation, it is necessary to include the power dissipated in the output devices due to current flowing in the loads. For a sinusoidal output about ground and symmetrical split supplies, the on-chip power dissipation due to the load can be approximated by

$$
P_{D,OUTPUT} = (V_{POS} - V_{OUTPUT,RMS}) \times I_{OUTPUT,RMS}
$$
 (2)

For nonsinusoidal output, calculate the power dissipation by integrating the on-chip voltage drop across the output devices multiplied by the load current over one period.

The user can subtract the quiescent current for the Class AB output stage when calculating the loaded power dissipation. For each output stage driving a load, subtract a quiescent power, according to

$$
P_{DQ,OUTPUT} = (V_{POS} - V_{NEG}) \times I_{OUTPUT,QUIESCENT}
$$
 (3)

where $I_{\text{OUTPUT, QUIESCENT}} = 1.65 \text{ mA}$ for each single-ended output pin of th[e AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf)

For each disabled RGB output channel, the quiescent power supply current in V_{POS} and V_{NEG} drops by approximately 34 mA.

Figure 51. Simplified Output Stage

Example

With an ambient temperature of 85°C, all nine RGB output channels driving 1 V rms into 100 Ω loads, and power supplies at ±2.5 V, follow these steps:

1. Calculate the power dissipation of the AD8178 using data sheet quiescent currents, neglecting the V_{DD} current because it is insignificant.

$$
P_{D,QUIESCENT} = (V_{POS} \times I_{VPOS}) + (V_{NEG} \times I_{VNEG}) \tag{4}
$$

 $P_{D,OUTSCENT} = (2.5 \text{ V} \times 460 \text{ mA}) + (2.5 \text{ V} \times 460 \text{ mA}) = 2.3 \text{ W}$

2. Calculate power dissipation from loads. For a differential output and ground-referenced load, the output power is symmetrical in each output phase.

 $P_{D,OUTPUT} = (V_{POS} - V_{OUTPUT,RMS}) \times I_{OUTPUT,RMS}$ (5)

 $P_{D,OUTPUT} = (2.5 V - 1 V) \times (1 V/100 \Omega) = 15 mW$

There are 15 output pairs, or 30 output currents.

 $nP_{D,OUTPUT} = 30 \times 15$ mW = 0.45 W

3. Subtract quiescent output stage current for the number of loads (30 in this example). The output stage is either standing or driving a load, but the current needs to be counted only once (valid for output voltages > 0.5 V).

$$
P_{DQ,OUTPUT} = (V_{POS} - V_{NEG}) \times I_{OUTPUT,QUIESCENT}
$$
 (6)

$$
P_{DQ,OUTPUT} = (2.5 \text{ V} - (-2.5 \text{ V})) \times 1.65 \text{ mA} = 8.25 \text{ mW}
$$

There are 15 output pairs, or 30 output currents.

 $nP_{D,OUTPUT} = 30 \times 8.25$ mW = 0.25 W

4. Verify that the power dissipation does not exceed the maximum allowed value.

$$
P_{D,ON\text{-}CHIP} = P_{D,QUIES\text{-}ENT} + n P_{D,OUTPUT} - n P_{DQ,OUTPUT}
$$
\n
$$
P_{D,ON\text{-}CHIP} = 2.3 \text{ W} + 0.45 \text{ W} - 0.25 \text{ W} = 2.5 \text{ W}
$$
\n
$$
(7)
$$

From [Figure 50 o](#page-31-0)r Equation 1, this power dissipation is below the maximum allowed dissipation for all ambient temperatures up to and including 85°C.

In a general case, the power delivered by the digital supply and dissipated into the digital output devices has to be taken into account following a similar derivation. However, because the loads driven by the H and V outputs are high and because the voltage at these outputs typically sits close to either rail, the

correction to the on-chip power estimate is small. Furthermore, the H and V outputs are active only briefly during sync generation and returned to digital ground thereafter.

Short-Circuit Output Conditions

Although there is short-circuit current protection on th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) outputs, the output current can reach values of 80 mA into a grounded output. Any sustained operation with too many shorted outputs can exceed the maximum die temperature and can result in device failure (see th[e Absolute Maximum Ratings](#page-6-0) section).

Crosstalk

Many systems (such as KVM switches) that handle numerous analog signal channels have strict requirements for keeping the various signals from influencing any of the other signals in the system. Crosstalk is the term used to describe the coupling of the signals of other nearby channels to a given channel.

When there are many signals in close proximity in a system, as is undoubtedly the case in a system that uses th[e AD8178,](http://www.analog.com/AD8178?doc=AD8178.pdf) the crosstalk issues can be quite complex. A good understanding of the nature of crosstalk and some definition of terms is required to specify a system that uses one or more crosspoint devices.

Types of Crosstalk

Crosstalk can be propagated by means of any of three methods. These fall into the categories of electric field, magnetic field, and the sharing of common impedances. This section explains these effects.

Every conductor can be both a radiator of electric fields and a receiver of electric fields. The electric field crosstalk mechanism occurs when the electric field created by the transmitter propagates across a stray capacitance (for example, free space) and couples with the receiver and induces a voltage. This voltage is an unwanted crosstalk signal in any channel that receives it.

Currents flowing in conductors create magnetic fields that circulate around the currents. These magnetic fields then generate voltages in any other conductors whose paths they link. The undesired induced voltages in these other channels are crosstalk signals. The channels that crosstalk can be said to have a mutual inductance that couples signals from one channel to another. Figure 51. Simplified Output Stope

ection).
 OBSOLUT CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT (SECT) TO DISPUTE THE RELATION OF DRAMAL CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT CONSTANT

Various channels generally share the power supplies, grounds, and other signal return paths of a multichannel system. When a current from one channel flows in one of these paths, a voltage that is developed across the impedance becomes an input crosstalk signal for other channels that share the common impedance.

All these sources of crosstalk are vector quantities, so the magnitudes cannot simply be added together to obtain the total crosstalk. In fact, there are conditions where driving additional circuits in parallel in a given configuration can actually reduce the crosstalk. The fact that th[e AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)s a fully differential design means that many sources of crosstalk either destructively cancel, or are common mode to, the signal and can be rejected by a differential receiver.

Areas of Crosstalk

A practica[l AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) circuit must be mounted to an actual circuit board to connect it to power supplies and measurement equipment. This, however, raises the issue that system crosstalk is a combination of the intrinsic crosstalk of the devices, in addition to the circuit board to which they are mounted. It is important to try to separate these two areas when attempting to minimize the effect of crosstalk.

In addition, crosstalk can occur among the inputs to a crosspoint and among the outputs. It can also occur from input to output. In the following sections, techniques are discussed for diagnosing which part of a system is contributing to crosstalk.

Measuring Crosstalk

Crosstalk is measured by applying a signal to one or more channels and measuring the relative strength of that signal on a desired selected channel. The measurement is usually expressed as decibels (dB) down from the magnitude of the test signal. The crosstalk is expressed by

$$
|XT| = 20 \log_{10} \left(\frac{A_{SEL}(s)}{A_{TEST}(s)} \right)
$$
 (8)

where:

 $s = j\omega$ is the Laplace transform variable.

 $A_{SEL}(s)$ is the amplitude of the crosstalk induced signal in the selected channel.

 $A_{TEST}(s)$ is the amplitude of the test signal.

It can be seen that crosstalk is a function of frequency but not a function of the magnitude of the test signal (to first order). In addition, the crosstalk signal has a phase relative to the test signal associated with it.

A network analyzer is most commonly used to measure crosstalk over a frequency range of interest. It can provide both magnitude and phase information about the crosstalk signal.

As a crosspoint system or device grows larger, the number of theoretical crosstalk combinations and permutations can become extremely large. For example, in the case of the triple 16×5 matrix of the [AD8178,](http://www.analog.com/AD8178?doc=AD8178.pdf) note the number of crosstalk terms that can be considered for a single channel, for example, Input Channel INPUT0. INPUT0 is programmed to connect to one of the [AD8178 o](http://www.analog.com/AD8178?doc=AD8178.pdf)utputs where the measurement can be made.

First, the crosstalk terms associated with driving a test signal into each of the other 15 input channels can be measured one at a time, while applying no signal to INPUT0. Next, the crosstalk terms associated with driving a parallel test signal into all 15 other inputs can be measured two at a time in all possible combinations; then three at a time; and so on, until, finally, there is only one way to drive a test signal into all 15 other input channels in parallel.

Each of these cases is legitimately different from the others and can yield a unique value, depending on the resolution of the measurement system, but it is hardly practical to measure all these terms and then specify them. In addition, this measurement describes the crosstalk matrix for just one input channel. A similar crosstalk matrix can be proposed for every other input. In addition, if the possible combinations and permutations for connecting inputs to the other outputs (not used for measurement) are taken into consideration, the numbers rather quickly grow to astronomical proportions. If a larger crosspoint array of multiple AD8178 devices is constructed, the numbers grow larger still.

Obviously, some subset of all these cases must be selected to be used as a guide for a practical measure of crosstalk. One common method is to measure all hostile crosstalk; this means that the crosstalk to the selected channel is measured while all other system channels are driven in parallel. In general, this yields the worst crosstalk number; but this is not always the case, due to the vector nature of the crosstalk signal.

Other useful crosstalk measurements are those created by one nearest neighbor or by the two nearest neighbors on either side. These crosstalk measurements are generally higher than those of more distant channels, so they can serve as a worst-case measure for any other one-channel or two-channel crosstalk measurements.

Input and Output Crosstalk

Capacitive coupling is voltage-driven (dV/dt), but it is generally a constant ratio. Capacitive crosstalk is proportional to input or output voltage, but this ratio is not reduced by simply reducing signal swings. Attenuation factors must be changed by changing impedances (lowering mutual capacitance), or destructive canceling must be utilized by summing equal and out-of-phase components. For high input impedance devices such as the AD8178, capacitances generally dominate input-generated crosstalk. Figures It can also occur from input to output.

The structure is the minimizary and the structure of t

Inductive coupling is proportional to current (dI/dt) and often scales as a constant ratio with signal voltage, but it also shows a dependence on impedances (load current). Inductive coupling can also be reduced by constructive canceling of equal and outof-phase fields. In the case of driving low impedance video loads, output inductances contribute highly to output crosstalk.

The flexible programming capability of th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) can diagnose whether crosstalk is occurring more on the input side or the output side. Some examples are illustrative. A given input channel (INPUT7 roughly in the middle for this example) can drive OUTPUT2 (exactly in the middle). The inputs to INPUT7 are terminated to ground (via 50 Ω or 75 Ω), and no signal is applied.

All the other inputs are driven in parallel with the same test signal (practically provided by a distribution amplifier), with all other outputs except OUTPUT2 disabled. Because grounded INPUT7 is programmed to drive OUTPUT2, no signal should be present. Any signal that is present can be attributed to the other 15 hostile

input signals because no other outputs are driven (they are all disabled). Thus, this method measures the all hostile input contribution to crosstalk into INPUT7. Of course, the method can be used for other input channels and combinations of hostile inputs.

For output crosstalk measurement, a single input channel is driven (INPUT0, for example) and all outputs other than a given output (OUTPUT2 in the middle) are programmed to connect to INPUT0. OUTPUT2 is programmed to connect to INPUT15 (far away from INPUT0), which is terminated to ground. Thus, OUTPUT2 should not have a signal present because it is listening to a quiet input. Any signal measured at OUTPUT2 can be attributed to the output crosstalk of the other eight hostile outputs. Again, this method can be modified to measure other channels and other crosspoint matrix combinations.

Effect of Impedances on Crosstalk

The input side crosstalk can be influenced by the output impedance of the sources that drive the inputs. The lower the impedance of the drive source, the lower the magnitude of the crosstalk. The dominant crosstalk mechanism on the input side is capacitive coupling. The high impedance inputs do not have significant current flow to create magnetically induced crosstalk. However, significant current can flow through the input termination resistors and the loops that drive them. Thus, the PC board on the input side can contribute to magnetically coupled crosstalk. **[E](http://www.analog.com/AD8178?doc=AD8178.pdf)VANY INTO IN (WE ART IS the ROST CONDUCT AND A CHOUNAL CONDUCT AND A CHOUNAL CONDUCT AND A CHOUNAL CONDUCT AND A CHOUNAL CHO**

From a circuit standpoint, the input crosstalk mechanism looks like a capacitor coupling to a resistive load. For low frequencies, the magnitude of the crosstalk is given by

 $|XT| = 20 \log_{10} [(R_sC_M) \times s]$ (9)

where:

R_s is the source resistance.

 C_M is the mutual capacitance between the test signal circuit and the selected circuit.

s is the Laplace transform variable.

Equation 9 illustrates that this crosstalk mechanism has a highpass nature; it can also be minimized by reducing the coupling capacitance of the input circuits and lowering the output impedance of the drivers. If the input is driven from a 75 $Ω$ terminated cable, the input crosstalk can be reduced by buffering this signal with a low output impedance buffer.

On the output side, the crosstalk can be reduced by driving a lighter load. Although the [AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) is specified with excellent settling time when driving a properly terminated Cat-5, the crosstalk is higher than the minimum obtainable due to the high output currents. These currents induce crosstalk via the mutual inductance of the output pins and the bond wires of the [AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf)

From a circuit standpoint, this output crosstalk mechanism looks like a transformer with a mutual inductance between the windings that drives a load resistor. For low frequencies, the magnitude of the crosstalk is given by

$$
|XT| = 20 \log_{10} \left(M_{XY} \times \frac{s}{R_L} \right) \tag{10}
$$

where:

 M_{XY} is the mutual inductance of output X to output Y. R_L is the load resistance on the measured output.

This crosstalk mechanism can be minimized by keeping the mutual inductance low and increasing RL. The mutual inductance can be kept low by increasing the spacing of the conductors and minimizing their parallel length.

PCB Layout

Extreme care must be exercised to minimize additional crosstalk generated by the system circuit board(s). The areas that must be carefully detailed are grounding, shielding, signal routing, and supply bypassing.

The packaging of the AD8178 is designed to help keep crosstalk to a minimum. On the PBGA substrate, each pair is carefully routed to predominately couple to each other, with shielding traces separating adjacent signal pairs. The ball grid array is arranged such that similar board routing can be achieved. Input and output differential pairs are grouped by channel rather than by color to allow for easy, convenient board routing.

The input and output signals have minimum crosstalk if they are located between ground planes on layers above and below, and are separated by ground in between. Locate vias as close to the IC as possible to carry the inputs and outputs to the inner layer. The input and output signals surface at the input termination resistors and the output series back termination resistors. To the extent possible, also separate these signals as soon as they emerge from the IC package.

PCB Termination Layout

As frequencies of operation increase, the importance of proper transmission line signal routing becomes more important. The bandwidth of the AD8178 is large enough that using high impedance routing does not provide a flat in-band frequency response for practical signal trace lengths. It is necessary for the user to choose a characteristic impedance suitable for the application and properly terminate the input and output signals of th[e AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf) Traditionally, video applications have used 75 Ω single-ended environments. RF applications are generally 50 Ω single-ended (and board manufacturers have the most experience with this application). Cat-5 cabling is usually driven as differential pairs of 100 $Ω$ differential impedance.

For flexibility, the [AD8178 d](http://www.analog.com/AD8178?doc=AD8178.pdf)oes not contain on-chip termination resistors. This flexibility in application comes with some board layout challenges. The distance between the termination of the input transmission line and the [AD8178 d](http://www.analog.com/AD8178?doc=AD8178.pdf)ie is a high impedance stub and causes reflections of the input signal.

With some simplification, it can be shown that these reflections cause peaking of the input at regular intervals in frequency, dependent on the propagation speed (V_P) of the signal in the chosen board material and the distance (d) between the termination resistor and th[e AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf) If the distance is great enough, these peaks can occur in-band. In fact, practical experience shows that these peaks are not high-Q and must be pushed out to three or four times the desired bandwidth to not have an effect on the signal. For a board designer using FR4 ($V_P = 144 \times 10^6$ m/sec), this means th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) must be no more than 1.5 cm after the termination resistors and preferably placed even closer. The PBGA substrate routing inside the [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)s approximately 1 cm in length and adds to the stub length, so 1.5 cm PCB routing equates to $d = 2.5 \times 10^{-2}$ m in the calculations.

$$
f_{PEAK} = \frac{(2n+1)V_p}{4d} \tag{11}
$$

where $n = \{0, 1, 2, 3, ...\}$.

In some cases, it is difficult to place the termination close to the [AD8178 d](http://www.analog.com/AD8178?doc=AD8178.pdf)ue to space constraints, differential routing, and large resistor footprints. A preferable solution in this case is to maintain a controlled transmission line past the AD8178 inputs and terminate the end of the line. This is known as fly-by termination. The input impedance of the AD8178 is large enough, and stub length inside the package is small enough, that this works well in practice. Implementation of fly-by input termination often includes bringing the signal in on one routing layer, then passing through a filled via under the AD8178 input ball, then back out to termination on another signal layer. In this case, care must be taken to tie the reference ground planes together near the signal via if the signal layers are referenced to different ground planes.

Figure 52. Fly-By Input Termination (Grounds for the two transmission lines shown must be tied together close to the INn pin.)

If multiple [AD8178s](http://www.analog.com/AD8178?doc=AD8178.pdf) are to be driven in parallel, a fly-by input termination scheme is very useful, but the distance from each [AD8178 i](http://www.analog.com/AD8178?doc=AD8178.pdf)nput to the driven input transmission line is a stub that must be minimized in length and parasitics by using the discussed guidelines.

When driving th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) single-ended, the undriven input is often terminated with a resistance to balance the input stage. By terminating the undriven input with a resistor of one-half the characteristic impedance, the input stage is perfectly balanced (25 Ω, for example, to balance the two parallel 50 Ω terminations on the driven input). However, due to the feedback in the input receiver, there is high speed signal current leaving the undriven input. To terminate this high speed signal, use proper transmission line techniques. One solution is to adjust the trace width to create a transmission line of half the characteristic impedance and terminate the far end with this resistance (25 Ω in a 50 Ω) system). This is not often practical because trace widths become large. In most cases, the best practical solution is to place the halfcharacteristic impedance resistor as close as possible (preferably less than 1.5 cm away) and reduce the parasitics of the stub (by removing the ground plane under the stub, for example). In either case, the designer must decide if the layout complexity created by a balanced, terminated solution is preferable to simply grounding the undriven input at the ball with no trace. signal in the termination resistors and preferably

the driven input). However, due to the freeBook

The PBGA substrate routing inside the

receiver, there is high speed signal curver and the receiver.

The signal curver

While the examples discussed so far are for input termination, the theory is similar for output back termination. Taking the AD8178 as an ideal voltage source, any distance of routing between the AD8178 and a back termination resistor is an impedance mismatch that potentially creates reflections. For this reason, also place back termination resistors close to th[e AD8178.](http://www.analog.com/AD8178?doc=AD8178.pdf) In practice, because back termination resistors are series elements, they can be placed close to the AD8178 outputs.

Finally, the AD8178 pinout allows the user to bring the outputs out as surface traces to the back termination resistors. The designer can avoid creating stubs and reflections by keeping th[e AD8178](http://www.analog.com/AD8178?doc=AD8178.pdf) output signal path on the surface of the board. A stub is created when a top-to-bottom via connection is made on the output

COMPLIANT TO JEDEC STANDARDS MS-034-AAL-1

Figure 53. 676-Ball Plastic Ball Grid Array [PBGA]

(B-676) Dimensions shown in millimeters

ORDERING GUIDE

www.analog.com

©2007–2016 Analog Devices, Inc. All rights reserved. Trademarks and registered trademarks are the property of their respective owners. D06608-0-5/16(A)

Rev. A | Page 37 of 37