

FAN4146 — Ground Fault Interrupter

Features

- For Two-Wire ALCI and RCD Applications
- Precision Sense Amplifier and Bandgap Reference
- Built-in AC Rectifier

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- Direct DC Coupled to Sense Coil
- Built-in Noise Filter
- Low-Voltage SCR Disable
- SCR Gate Driver
- Adjustable Sensitivity
- Minimum External Components
- Meets UL 943B Requirements
- Ideal for 120 V or 220 V Systems
- Space-Saving SuperSOT[™] 6-Pin Package

Applications

- Personal Care Products
- Two-Wire Electrical Outlets, Circuit Breakers, and Power Cords Requiring GFI Safety Features
- ALCI and RCCB Circuits

Description

The FAN4146 is a low-power controller for AC outlet Appliance Leakage Circuit Interrupters (ALCI) and twowire Residual Current Devices (RCD). The FAN4146 detects hazardous grounding conditions and open circuits the line before a harmful shock occurs.

Internally, the FAN4146 contains a diode rectifier, precision bandgap 12 V shunt regulator, precision low V_{OS} offset-sense amplifier, time delay noise filter, window-detection comparators, and a SCR driver. With the addition of a minimum number of external components, the FAN4146 detects and protects against a hot-wire-to-ground fault. The minimum number of components and the small SuperSOTTM package allow for a small-form-factor, low-cost application solution.

The FAN4146 circuitry has a built-in rectifier and shunt regulator that operates with a low quiescent current. This allows for a high-value, low-wattage-series supply resistor. The internal temperature compensated shunt regulator, sense amplifier, and bias circuitry provide for precision ground-fault detection. The low V_{OS} offset-sense amplifier allows direct coupling of the sense coil to the amplifier's feedback signal. This eliminates the large 50/60 Hz AC-coupling capacitor. The internal delay filter rejects high-frequency noise spikes common with inductive loads. This decreases false nuisance tripping. The internal SCR driver is temperature compensated and designed to satisfy the current requirements for a wide selection of external SCRs.

The minimum number of external components and the 6-pin SuperSOT[™] package enable for a low-cost, compact design and layout. The FAN4146ESX is an enhanced temperature range device.

Ordering Information

Part Number	Operating Temperature Range	Package	Packing Method	
FAN4146SX	0°C to +70°C	6 Lood SUDEDSOTE JEDEC MO 102 16 mm	Tapa and Baal	
FAN4146ESX	-35°C to +85°C	6-Lead SUPERSON, JEDEC MO-193, 1.8 mm	Tape and Reel	





Note:

Value depends on sense-coil characteristics and application (value chosen for 10 mA trip threshold).
Contact Fairchild for best application practices for nuisance tripping rejection.



AmpOut

6

External resistor connected to VFB sets the Ifault sensitivity threshold

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Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol	Parameter		Condition	Min.	Max.	Unit
Icc	Supply Current		Continuous Current, Line to Neutral		15	mA
V	V _{CC} Supply Voltage		Continuous Voltage, Line to Neutral	-1.5	16.0	V
Vcc		All other pins	Continuous Voltage to Neutral	-0.8	15.0	V
T _{STG}	Storage Temperature Range			-65	+150	°C
			Human Body Model, JESD22-A114		2500	
ESD	ESD Electrostatic Discharge Capability		Charged Device Model, JESD22-C101		1000	V
			Machine Model, JESD22-A115		200	

DC Electrical Characteristics

Unless otherwise specified, T_A=25°C, I_{shunt}=1 mA.

Symbol	Parameter	Conditions	Min.	Тур.	Max.	Units	
M	Power Supply Shunt Regulator	Line to Neutral	12.2	12.7	13.2	V	
VREG	Voltage	Line to Neutral, I _{shunt} =- 2mA	-0.9 -0.7			V	
lq	Quiescent Current	Line to Neutral=10 V	350	400	450	μA	
V_{REF}	Reference Voltage	V _{REF} to Neutral	5.8	6.0	6.2	V	
V_{TH}	Trip Threshold	AmpOut to V _{REF}	3.4	3.5	3.6	V	
V _{OS}	Amplifier Offset	R _{SET} =511 KΩ, R _{IN} =500 Ω	-450	0	450	μV	
los	Amplifier Input Offset ⁽⁵⁾	Design Value	-50	0	50	nA	
G	Amplifier DC Gain ⁽⁵⁾	Design Value		100		dB	
f _{GBW}	Amplifier Gain Bandwidth ⁽⁵⁾	Design Value		1.5		MHz	
V _{SW+}	Amplifier Positive Voltage Swing	AmpOut to V _{REF} , I _{FAULT} =10 µA	4.0			V	
V _{SW-}	Amplifier Negative Voltage Swing	V _{REF} to AmpOut, I _{FAULT} =-10 µA	4.0			V	
I _{SINK}	Amplifier Current Sink	AmpOut=V _{REF} + 3 V, V _{FB} =V _{REF} + 100 mV	400			μA	
I _{SRL}	Amplifier Current Source	AmpOut=V _{REF} – 3 V, V _{FB} =V _{REF} - 100 mV	400			μA	
t _d	Delay Filter	Delay from C₁ Trip to SCR, LOW to HIGH	0.75	1.00	1.25	ms	
R _{OUT}	SCR Output Resistance	SCR to Neutral=250 mV, AmpOut=V _{REF}		0.5	1.0	KΩ	
		SCR to Neutral, AmpOut=V _{REF}		1	10	mV	
V _{OUT}	SCR Output Voltage	SCR to Neutral, AmpOut =V _{REF} +4 V	2.5			V	
I _{OUT}	SCR Output Current	SCR to Neutral=1 V AmpOut=V _{REF} + 4 V	350	500		μA	

Note:

5. Guaranteed by design; not tested in production.

Functional Description

Refer to Figure 1 and Figure 3.

The FAN4146 is a two-wire GFCI controller for AC ground-fault-circuit interrupters. The internal rectifier circuit is biased by the AC line during the positive half cycle of the AC line voltage. The internal 12 V shunt regulator uses a precision temperature-compensated bandgap reference. The combination of precision reference circuitry and precision sense amplifier provides for an accurate ground-fault tolerance. This allows for selection of external components with wider and lower-cost parameter variation. Due to the low quiescent current, a high value external series resistor (R1) can be used which reduces the maximum power wattage required for this resistor. The 12 V shunt regulator generates the reference voltage V_{REF} for the sense amplifier's (A1) non-inverting input (AC ground reference) and supplies the bias for the delay timer (t_1) . comparators ($C_1 \& C_2$), and the SCR driver.

The secondary winding of the sense transformer is directly DC coupled to the inverting input of the sense amplifier at pin 5 (VFB). The RSET resistor converts the sense transformer's secondary current to a voltage at pin 6 (AmpOut). This voltage is compared to the internal window comparator (C1 & C2) and, when the AmpOut voltage exceeds the $\pm V_{TH}$ threshold voltage, the window comparator triggers the internal delay timer. The output of the window comparator must stay HIGH for the duration of the t₁ timer. If the window comparator's output momentarily goes LOW, the t₁ timer resets. If the window comparator's output is still HIGH at the end of the t₁ pulse, the SCR driver enables the current source I_1 and disables Q_1 . The current source I_1 then enables the external SCR, which energizes the solenoid, opens the contact switches to the load, and removes the hazardous ground fault. The window comparator allows detection of a positive or negative IFAULT signal independent from the phase of the line voltage. An internal under-voltage lockout circuit disables the SCR driver if the voltage at pin 3 (LINE) is below 7.5 V. This prevents the SCR from energizing the solenoid when the SCR's anode voltage is below 65 V.

The sense transformer typically has a toroidal core made of laminated steel rings or solid ferrite material. The secondary of the transformer is typically 1000 turns of #40 wire wound through the toroid. The primary is typically one turn made by passing the AC hot and neutral wires through the center of the toroid. When a ground fault exists, a difference exists between the current flowing in hot and neutral wires. The primary difference current divided by the primary-to-secondary turns ratio is the current that flows through the secondary wire of the transformer.

Calculation of R_{SET} Resistor

The AmpOut signal must exceed the window comparator's V_{TH} threshold voltage for longer than the delay timer and calculated by:

 $V_{TH} = I_{FAULT} \times 1.41 \times R_{SET} \times C_{OS}(2\pi \times (t/2P)) / N$ (1)

 $R_{SET} = (V_{TH} \times N) / (1.41 \times I_{FAULT} \times C_{OS}(\pi \times t/P))$ (2)

where:

 V_{TH} = 3.5 V I_{FAULT} = 5 mA (UL943B)

- t = 1 ms (timer delay)
- P = Period of the AC Line (1/60 Hz)
- N = Ratio of secondary to primary turns (1000:1)

 $R_{SET} = 505 \text{ K}\Omega \text{ (511 K}\Omega \text{ standard 1\% value)}$

In practice, the transformer is non-ideal, so R_{SET} may need to be adjusted by up to 30% to obtain the desired I_{fault} trip threshold.

Calculation of Vos Trip Threshold Error

Since the sense coil is directly connected to the feedback of the sense amplifier, the V_{OS} offset introduces an I_{fault} threshold error. This error can be calculated as follows:

%Error=100 x (V_{OS} x R_{SET}) / (R_{IN} + RL_{DC} + RL_{AC}) / V_{TH} (3)

where:

,	_	±450 µV (worst case)
/OS	-	±150 µV (typical)

- $R_{SET} = 511 \text{ K}\Omega$
- $R_{IN} = 470 \Omega$ (typical value)
- $RL_{DC} = 75 \Omega$ (sense coil secondary DC resistance)
- $RL_{AC} = \begin{cases} 1.5 \text{ K}\Omega (AC_{(j\omega L)} \text{ impedance of sense coil}), \\ L = 4 \text{ H}, \text{ f} = 60 \text{ Hz}) \end{cases}$

%Error= ± 3.2% (worst case) ± 1.1% (typical)









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