

# <span id="page-0-0"></span>**XDPL8220 Digital PFC+Flyback Controller IC**

# **XDP™ Digital Power**

**Data Sheet Revision 1.0 Quality Requirement Category: Industrial**

# **Features**

- Universal AC input (90 305 VAC) or DC input (90 305 VDC)
- Applicable power range of 20 W to 150 W
- Small number of external parts optimizes **[Bill of Materials \(BOM\)](#page-55-0)** and form factor
- High efficiency  $(> 90\%)$
- Multicontrol mode (**[Constant Current \(CC\)](#page-55-0)**/**[Constant Voltage \(CV\)](#page-55-0)**/**[Limited Power \(LP\)](#page-56-0)**) reduces required product variety
- Important parameters can be configured after manufacturing
- Low harmonic distortion (**[Total Harmonic Distortion \(THD\)](#page-57-0)** < 15%)
- Low output ripple current
- Integrated startup cell ensures fast time to light (< 250 ms)
- Adaptive Temperature Protection
- Ambient operating temperature -40 °C to 85 °C
- Automatic switching between **[Quasi-Resonant Mode \(QRM\)](#page-57-0)** and **[Discontinuous Conduction Mode \(DCM\)](#page-56-0)**
- Wide output voltage range
- **[Pulse Width Modulation \(PWM\)](#page-57-0)** dimming control
- Output dimming by analog reduction of driving current down to 5%

For safe operation, the XDPL8220 contains a comprehensive set of protection features:

- Output overvoltage protection (open load)
- Output undervoltage protection (output short)
- VCC over- and undervoltage lockout
- Input over- and undervoltage protection
- Bus over- and undervoltage protection
- Overcurrent protection for **[Power Factor Correction \(PFC\)](#page-57-0)** and **[Flyback \(FB\)](#page-56-0)** stage

# **Applications**

• Integrated **[Electronic Control Gear \(ECG\)](#page-56-0)** for **[Light Emitting Diode \(LED\)](#page-56-0)** luminaires



#### <span id="page-1-0"></span>**Description**



**Figure 1 Typical Application for XDPL8220**



# **Description**

XDPL8220 is a highly integrated next-generation device combining a boundary mode **[PFC](#page-57-0)** plus a quasi-resonant **[FB](#page-56-0)** controller with primary-side regulation. The integration of these functions enables saving of external parts and optimizes performance by harmonized operation of the two stages.

XDPL8220 uses a constant on-time scheme with a **[THD](#page-57-0)** improvement algorithm to provide a high power factor and excellent **[THD](#page-57-0)** performance.

With its unique control scheme of **[CV](#page-55-0)**, **[CC](#page-55-0)** and **[LP](#page-56-0)**, the **[LED](#page-56-0)** driver designer is provided with a large degree of flexibility and can utilize the system hardware to its limits.

The on-chip **[One Time Programmable Memory \(OTP\)](#page-57-0)** memory has an area for parameters that control the behavior of the circuit, e. g. the output current or the maximum output power. This enables the user of the device to create a platform concept with significantly fewer different hardware versions while still covering the same application range.

The two-stage approach reduces any variation in the output current (flicker) to a non-visible level. By separating the **[PFC](#page-57-0)** from the power conversion part (**[FB](#page-56-0)**), both stages operate in a more stable manner and require fewer margins, which has a positive influence on the cost.

Lighting requires more and more 24/7 operation, making it necessary to have a stand-by mode with short wakeup times and low power consumption. The power consumption of less than 100 mW of the XDPL8220-based systems defines the new standard for stand-by power in lighting **[ECG](#page-56-0)**s.

XDPL8220 enables adaptive temperature protection using either the internal sensor or an external **[Negative](#page-56-0) Temperature Coefficient [Thermistor \(NTC\)](#page-56-0)**, or both.

Futureproof flexibility with application-oriented programmable operating windows enables management of **[LED](#page-56-0)** generations and portfolio complexity .



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### <span id="page-4-0"></span>**Functional Block Diagram**

# **1 Functional Block Diagram**

The functional block diagram shows the basic data flow from input pins via signal processing to the output pins.



**Figure 2 XDPL8220 Simplified Functional Block Diagram**



# <span id="page-5-0"></span>**Pin Configuration**

# **2 Pin Configuration**

Pin assignments and basic pin description information are shown below.





### **Table 1 Pin Definitions and Functions**





# **Pin Configuration**



### **Table 1 Pin Definitions and Functions (continued)**



# <span id="page-7-0"></span>**3 Functional Description**

This chapter provides a summary of the integrated functions and features, and describes the relationships between them. The parameters and equations are based on typical values at  $T_A = 25 \degree C$ .

XDPL8220 is a digital dual-stage **[PFC](#page-57-0)** and **[FB](#page-56-0)** controller IC supporting **[PWM](#page-57-0)** dimming functionality. Both stages use configurable multimode operation to select the best mode of operation for every operation condition. Multimode operation automatically switches between **[Quasi-Resonant Mode, switching in valley n \(QRMn\)](#page-57-0)** and **[DCM](#page-56-0)**.

XDPL8220 features a comprehensive set of configurable protection modes to detect fault conditions.

XDPL8220 provides a high degree of flexibility in design-in of the application. A **[Graphic User Interface \(GUI\)](#page-56-0)** tool supports users in the configuration of the operational and protection parameters.



# <span id="page-8-0"></span>**3.1 PFC Controller Features**

The **[PFC](#page-57-0)** stage ensures high power quality by maximizing the power factor and minimizing harmonic distortion.

The **[PFC](#page-57-0)** stage operates in **[Quasi-Resonant Mode, switching in valley 1 \(QRM1\)](#page-57-0)** and **[QRMn](#page-57-0)**, to support low load conditions and ensure efficient operation.

The **[PFC](#page-57-0)** stage is implemented as a boost converter. It drains a sinusoidal current from the single-phase line supply and provides stabilized **[Direct Current \(DC\)](#page-55-0)** voltage at the internal bus voltage rail. The power factor of the single-phase line supply is almost one. Fluctuations in line voltage as well as voltage drops of short duration are compensated.

# **3.1.1 Shared CS/ZCD Function**

The **[PFC](#page-57-0)** stage makes use of combined CS/ZCD functionality at the CSPFC pin.

During the gate driver on-time the pin acts as a current sense (CS), while during the gate driver off-time the pin acts as a zero-crossing-detector (ZCD). The CS senses the on-time current and implements overcurrent limitation; the ZCD exploits the quasi-resonant function to minimize conduction losses.

The CSPFC pin is connected via a resistor divider composed of R<sub>ZCD,1,PFC</sub> and R<sub>ZCD,2,PFC</sub> and a set of diodes to an auxiliary winding of the **[PFC](#page-57-0)** choke inductor. It is used for detecting the valleys of the quasi-resonant oscillation to turn on the **[PFC](#page-57-0)** MOSFET based on the desired valley computed by the multimode **PFC** control. The diode D<sub>1</sub> allows positive voltage at the CSPFC pin as the valley detection is implemented by the internal hysteretic comparator with a positive reference of nominal THR<sub>HYS</sub> for falling edges. The CSPFC pin senses the drain source current of the switching MOSFET. The CS voltage is measured after a programmable blanking time after turn-on of the switch. An appropriate current sensing resistor  $R_{CS,PFC}$  is selected on the basis of the maximum current flowing in the switching MOSFET and the dynamic voltage range of the input pin CSPFC.



**Figure 4 Shared CS/ZCD Schematic**

# **3.1.2 Quasi-resonant Mode**

The quasi-resonant mode maintains a high efficiency level.

For **[PFC](#page-57-0)** operating in **[QRM1](#page-57-0)**, the main switch is turned on with a constant on-time for a line and load condition, while the off-time/demagnetization time varies within an **[Alternating Current \(AC\)](#page-55-0)** half-cycle depending on the instantaneously rectified <mark>[AC](#page-55-0)</mark> input voltage V<sub>g</sub>. Subsequently, the switching frequency varies within each <mark>AC</mark> halfcycle with the lowest switching frequency at the peak of the **[AC](#page-55-0)** input voltage and the highest switching frequency near the zero crossings of the input voltage. A new switching cycle starts immediately when the first QR valley is reached.



### <span id="page-9-0"></span>**Functional Description**

**[QRM1](#page-57-0)** is ideal for full-load operation, where the on-time is large. However, the on-time reduces at light loads, resulting in very high switching frequencies, particularly near the zero crossings of the input voltage. The high switching frequency will increase switching losses, resulting in poor efficiency at light loads. The **[PFC](#page-57-0)** multimode control can lower the switching frequency by selecting further valleys to achieve QRM2 up to  $N_{\text{vallev,max,PFC}}$  operation. The switching frequency is limited within a defined range and the efficiency at light loads improves.



#### **Figure 5 PFC QRM2 Waveforms**

The equations for the quasi-resonant operation are shown below, where  $t_w$  is an additional delay in each switching cycle when selecting subsequent valleys after the first QR valley and n is the valley number in *[QRMn](#page-57-0)*.

 $i_{L,pk}$  =  $V_g \cdot t_{on}$ L  $t_{disch}$  =  $i_{L,pk} \cdot L$  $V_{bus} - V_g$  $t_{1stV}$  =  $t_{disch}$  +  $t_{osc}$ /2  $t_w = t_{osc} \cdot (n-1)$  $t_{sw} = t_{on} + t_{1stV} + t_w$  $t_{off} = t_{1stV} + t_w$ 

**Equation 1**

# **3.1.3 Bus Voltage Sensing**

The bus voltage is measured at the VS pin.

The VS pin implements **[PFC](#page-57-0)** bus voltage sensing for bus voltage regulation. The bus voltage is scaled down using a simple resistor divider. A capacitor could in certain cases be added at the pin to ground to filter highfrequency switching noise. The bus voltage sensing is a low leakage input and no additional measures are needed to reduce the current consumption.



### <span id="page-10-0"></span>**Functional Description**



**Figure 6 Bus Voltage Sensing Schematic**

The **[Analog-to-Digital Converter \(ADC\)](#page-55-0)** input at the VS pin utilizes two voltage ranges. The wider voltage range from 0 to V<sub>REF</sub> results in lower resolution. The narrower voltage range from 5/6 V<sub>REF</sub> to 7/6 V<sub>REF</sub> gives better voltage resolution. Steady state operation therefore normally takes place in the high-resolution range and soft start operation in the low-resolution range.



**Figure 7 Sensing Ranges**

# **3.1.4 Input Voltage Sensing**

The input voltage is sensed using the HV pin.

The input voltage is used for protection, to generate **[AC](#page-55-0)** zero-crossing signals and to detect the AC/DC source.



#### <span id="page-11-0"></span>**Functional Description**



**Figure 8 Input Voltage Sensing Schematic**

The R<sub>HV</sub> probing resistor is usually split into two, or three or more resistors for safety purposes. In fact in case of a resistor being shorted by damage, the high resistive path is maintained by the other resistors avoiding fire, shock to the user and further damage to the application.

A RC filter structure making use of the split resistors filters the unwanted noise for the high voltage input voltage measurement. The filtering effect is kept high due to the usage of the high impedance split resistors and the addition of small capacitance high voltage capacitors.

# **3.1.5 Control Scheme**

The **[PFC](#page-57-0)** bus voltage controller embeds a PIT1 controller that calculates a control output representing load and line conditions from the bus voltage error signal.

The bus voltage controller implements regulation during both soft start and steady states.

# **3.1.5.1 Startup**

At system startup, the **[PFC](#page-57-0)** initiates a soft start to minimize the switching stress for the power MOSFET, diode and inductor.

The soft start is executed when the bus voltage is higher than the V<sub>bus,start,PFC</sub> threshold. This is the brown-in condition. The soft start is aborted if the input under- or overvoltage protection fire. During soft start, the **[PFC](#page-57-0)** stays in **[QRM1](#page-57-0)** operation. Once the V<sub>bus,stdy,entr,UV</sub> threshold is reached, the steady state **[PFC](#page-57-0)** operation starts.



#### <span id="page-12-0"></span>**Functional Description**



**Figure 9** V<sub>bus</sub> Soft Start and Regulation

# **3.1.6 Multimode Control Scheme**

The multimode control scheme provides a **[PFC](#page-57-0)** option to dynamically change the operating point by switching between the MOSFET V<sub>ds</sub> voltage valleys while following a frequency law and applying **[THD](#page-57-0)** optimization.

The multimode controller uses two different modes of operation:

- **[QRM1](#page-57-0)**: This operation maximizes the efficiency by switching on the 1st valley of the **[PFC](#page-57-0)** ZCD signal. This ensures zero current switching with a minimum of switching losses.
- **[QRMn](#page-57-0)**: The controller will extend to the next switching valley after the 1st valley to control the bus voltage following a frequency law.

The multimode optimization consists of the following:

- Frequency law
- THD optimization

# **3.1.6.1 Frequency Law**

The output of the **[PFC](#page-57-0)** PIT1 bus voltage controller gives the desired on-time, which is constant within each **[AC](#page-55-0)** half cycle. A <mark>[PFC](#page-57-0)</mark> is used to emulate a resistive load r<sub>e</sub> to the <mark>[AC](#page-55-0)</mark> input such that i<sub>ac</sub> follows v<sub>ac</sub> in both wave shape and phase. The output of the **[PFC](#page-57-0)** bus voltage controller t<sub>on,des,PFC</sub> is inversely proportional to the emulated resistive load r<sub>e</sub> such that a smaller r<sub>e</sub> or a higher I<sub>ac,rms</sub> will give a larger t<sub>on,des,PFC</sub>. Thus, t<sub>on,des,PFC</sub> is different for the same load at different line voltages and is proportional to the RMS input current  $I_{\text{ac,rms}}$ .

The rule for selecting **[QRMn](#page-57-0)** is based on the frequency law. A maximum switching frequency f<sub>swmax</sub> and a minimum switching frequency f<sub>swmin</sub> are defined for the complete t<sub>on,des,PFC</sub>/I<sub>ac,rms</sub> range. The frequency law ensures that the switching frequency is within the desired frequency range. The frequency law is depicted in the figure below.



### <span id="page-13-0"></span>**Functional Description**



#### **Figure 10 PFC Frequency Law**

As long as the **[PFC](#page-57-0)** controller operating mode fulfills the frequency law, the operating mode does not change. The QR-valley is increased when the highest frequency limit is reached. The QR-valley is decremented when the lowest frequency limit is reached.

To ensure good ZCD detection before the ZCD signal becomes too small in amplitude, only the first up to Nvalley,max,PFC valleys operations are supported.

# **3.1.6.2 THD Optimization**

**[THD](#page-57-0)** optimization reduces the **[THD](#page-57-0)** in the case of light loads and in the case of high **[AC](#page-55-0)** input voltages.

The selection of higher valleys helps to reduce the switching frequency but it also distorts the input current waveform with constant on-time control and thus affects the **[PFC](#page-57-0) [THD](#page-57-0)** performance. The multimode **PFC** control also consists of a **[THD](#page-57-0)** optimization algorithm that optimizes the applied on-time in order to ensure good input current shaping and improved **[PFC](#page-57-0) [THD](#page-57-0)** performance.

# **3.1.7 Peak Current Limitation**

The peak current through the switching MOSFET is read via the **[PFC](#page-57-0)** shunt resistor R<sub>CS</sub> <sub>PFC</sub> to limit the maximum current through the MOSFET, the choke, and freewheeling diode so as to avoid potential hard failure or lifetime stress.

The OCP causes the current to be limited to cases in which an overcurrent condition occurs. **[Overcurrent](#page-56-0) [Protection Level 1 \(OCP1\)](#page-56-0)** is implemented by hardware. If the voltage V<sub>CS,PFC</sub> across the shunt resistor exceeds the overcurrent threshold V<sub>CS,OCP1, PFC</sub> for longer than the blanking time t<sub>blank,OCP1,PFC</sub>, the MOSFET is turned off. The MOSFET is turned on when ZCD occurs or the PFC maximum period time-out signal triggers the start of the next switching cycle. **[Overcurrent Protection Level 2 \(OCP2\)](#page-57-0)** is a second-level overcurrent protection implemented by hardware. The **[OCP2](#page-57-0)** overcurrent threshold is fixed. The **OCP2** blanking time is t<sub>blank,OCP2,PFC.</sub>

# **3.1.8 Bus Undervoltage Protection**

Undervoltage detection of the bus voltage  $V_{bus}$  is provided by measurement using the VS pin.

The bus voltage is compared to a configurable undervoltage protection threshold V<sub>bus,UV</sub>. If the threshold is exceeded for longer than the blanking time  $t_{\text{blankYbus,UV}}$ , the protection will be triggered.



# <span id="page-14-0"></span>**3.1.9 Bus Overvoltage Protection**

Overvoltage detection of the bus voltage  $V_{\text{bus}}$  is provided by the measurement using the VS pin.

The bus voltage is compared to a configurable overvoltage protection threshold V<sub>bus, OVP1</sub> in *[Firmware \(FW\)](#page-56-0)*. If a threshold is exceeded for longer than the blanking time  $t_{blank,Vbus,OVP1}$ , the gate driver stops. The gate driver operation is resumed when  $V_{bus}$  falls below  $V_{bus, stdv, entr, OV}$ .

V<sub>bus, OVP2</sub> is implemented in **[Hardware \(HW\)](#page-56-0)** and it is fixed at a voltage which is represented as 2.8 V at the bus voltage sensing pin (VS). The HW permits a blanking time  $t_{\text{blank.Vbus.OVP2}}$  to be programmed.



**Figure 11 Vbus protections**

# **3.1.10 Input Undervoltage Protection**

Undervoltage detection of the input voltage  $V_{in}$  is provided by measurement using the HV pin.

Values of V<sub>in,rms</sub> are compared to a configurable input undervoltage protection threshold V<sub>in,UV</sub>. If the threshold is exceeded for longer than the blanking time  $t_{blank}$  Vin, UV, the protection will be triggered. XDPL8220 features a configurable startup threshold  $V_{in, start,min}$  to create hysteresis for flicker-free operation before the second stage starts switching. After startup checks when t<sub>rms,reset,PFC</sub> expires, the comparison is restored to the threshold value V<sub>in,UV</sub>.

# **3.1.11 Input Overvoltage Protection**

Overvoltage detection of the input voltage  $V_{in}$  is provided by measurement using the HV pin.

Values of V<sub>in,rms</sub> are compared to a configurable input overvoltage protection threshold V<sub>in,OV</sub>. If the threshold is exceeded for longer than the blanking time  $t_{\text{blank,Vin.OV}}$ , the protection will be triggered. XDPL8220 features a configurable startup threshold  $V_{in,start,max}$  to create hysteresis for flicker-free operation before the second stage starts switching. After startup checks when t<sub>rms, reset, PFC</sub> expires, the comparison is restored to the threshold value V<sub>in.OV</sub>.

Note: In the csv file the input OVP shall be disabled by default.



### <span id="page-15-0"></span>**Functional Description**



**Figure 12 Vin protections**

# **3.1.12 Other PFC Protections**

#### **CS Resistor Short Protection**

The input circuit breaker (fuse) shall be chosen appropriately in order to protect in case of current-sense resistor short.

#### **CS Resistor Open Protection**

The external circuitry for shared CS/ZCD pulls the CSPFC pin high in case of CS resistor missing so that the OCP2 protection is triggered.

#### **CSPFC Pin Short to GND Protection**

In case of CSPFC pin short to ground the lack of quasi-resonant oscillations shall trigger the CCM Protection.

#### **CCM Protection**

Continuous conduction mode (CCM) operation may occur during **[PFC](#page-57-0)** startup for a limited time. It is considered as a failure in the system only if CCM operation of the **[PFC](#page-57-0)** converter is observed over a longer period of time. The **[PFC](#page-57-0)** converter may run into CCM operation for a longer period due to a shorted bypass diode, a heavy load step that is out of specification or very low input voltage outside the normal operating range.

When CCM occurs, the magnetizing current in the **[PFC](#page-57-0)** choke does not have the chance to decay to zero before the MOSFET turns on. No quasi-resonant oscillation will be seen at the ZCD signal before the maximum switching period time-out is reached that turns the MOSFET on. This turn-on event without ZCD oscillation is monitored to protect the **[PFC](#page-57-0)** converter from continuous CCM operation. The CCM protection is implemented by firmware.

If any quasi-resonant oscillation is seen at the ZCD signal for longer than the blanking time t<sub>blank,CCM,PFC</sub>, the protection is triggered.

#### **Soft Start Failure**

The soft start may take a long time, potentially never reaching steady state operation due to heavy loads or very low input voltages. If t<sub>start,PFC</sub> reaches t<sub>start,max,PFC</sub> before the soft start has ended, the protection is triggered.



# <span id="page-16-0"></span>**3.2 Flyback Controller Features**

The **[FB](#page-56-0)** stage provides primary side control that avoids secondary side control feedback loop circuitry usually needed in isolated power converters. This approach supports a low part count to reduce costs.

The **[FB](#page-56-0)** stage features multi-mode operation and it selects the best mode of operation based on operating conditions.

# **3.2.1 Primary Side Regulation**

The **[FB](#page-56-0)** in XDPL8220 provides primary side control of output current and output voltage. No external feedback components are necessary for the current control as the primary side regulation control loop is fully integrated.

**[Figure 13](#page-17-0)** shows typical current and voltage waveforms of the **[FB](#page-56-0)** application operating in **[QRM1](#page-57-0)**.

In **[DCM](#page-56-0)**, the next switching cycle will not start at the first valley of  $V_{AUV}$ , but is instead delayed. As a consequence, the switching losses in **[DCM](#page-56-0)** will be higher.

The primary peak current  $I_{p,pk}$ , the period of conduction of the output diode  $t_{\text{demag}}$  and the switching period  $t<sub>swFB</sub>$  are used to calculate the average output current.

The voltage signal  $V_{AUX}$  of the auxiliary winding of the transformer contains information on the reflected output voltage  $V_{\text{out}}$ . The reflected output voltage is measured at the ZCD pin using a resistor divider.



### <span id="page-17-0"></span>**Functional Description**



**Figure 13 Typical Waveforms of a Flyback Converter**

# **3.2.1.1 Primary Side Current Sensing**

The primary side peak current  $I_{p,pk}$  is controlled by the control loop using the  $V_{CS,OCP1}$  level at the CSFB pin. This control scheme ensures suppression of any variation in the bus voltage.

Several delays exist from the time at which the **[OCP1](#page-56-0)** level V<sub>CS,OCP1</sub> is exceeded at the CSFB pin until the gate switches off and the transformer current finally reaches its peak value. For a higher accuracy, the primary peak current V<sub>CS,SH</sub> is sampled a fixed time before turn-off of the gate. The primary side peak current is used to calculate the secondary side current and for protection. The propagation delay compensation parameter t<sub>PDC</sub> allows optimization of the accuracy of the primary side peak current:

 $I_{p, \text{pk}} =$  $V_{\text{CS, SH}}$  $\frac{V_{\text{CS, SH}}}{R_{\text{CS, FB}}} \cdot \frac{t_{\text{on, FB}} + t_{\text{PDC}}}{t_{\text{on, FB}} - t_{\text{CSFB, opt}}}$  $t_{\sf on, FB}$   $^ t_{\sf CSFB, offset}$ 

#### **Equation 2**



<span id="page-18-0"></span>Note: If an RC low pass filter is added in front of the CSFB pin, the related low pass filter delay has to be included in  $t_{PDC}$ .



**Figure 14 Propagation Delay Compensation for accurate Primary Peak Current Calculation**

# **3.2.1.2 Primary Side Output Voltage Sensing**

The output voltage is determined by measuring the reflected output voltage on the auxiliary winding. A resistor divider adapts the voltage to the operating range of the ZCD pin.

The output voltage is measured at the ZCD pin using the voltage  $V_{ZCD,SH}$  at the end of the demagnetization time at the time t<sub>zCD,sample</sub>. The voltage measured at the ZCD pin, the dimensioning of the resistor dividers  $R_{ZCD,FB,1}$ and  $R_{\sf ZCD,FB,2}$  , transformer turns  $N_s$  and  $N_a$  as well as an offset  $V_{\sf out,offset}$  (caused by the secondary diode, for example) are used to calculate the output voltage  $V_{\text{out}}$  as follows:

$$
V_{\text{out}} = V_{\text{ZCD, SH}} \frac{R_{\text{ZCD, FB,1}} + R_{\text{ZCD, FB,2}}}{R_{\text{ZCD, FB,2}}} \frac{N_s}{N_a} + V_{\text{out, offset}}
$$

#### **Equation 3**

Vout is used for **[Primary Side Regulated \(PSR\)](#page-57-0)** control loops in **[CV](#page-55-0)** and **[LP](#page-56-0)** modes as well as for output over- and undervoltage protections.



**Figure 15 Primary Side Output Voltage Sensing using ZCD S&H**

Note: Any relation between VCC and ZCD in self-supplied applications can be decoupled – e.g. by adding a linear regulator for VCC.



<span id="page-19-0"></span>**Attention**: **Please note that the time (tdemag) has to be longer than 2.0 μs to ensure that the reflected output voltage can be sensed correctly at the ZCD pin.**

# **3.2.1.3 Flyback Bus Voltage Sensing**

The **[FB](#page-56-0)** can sense the bus voltage using the reflection of bus voltage on the auxiliary winding while the gate is turned on. A resistor divider adapts the negative voltage to the operating range of the ZCD pin. This second measurement path is required to protect against component failures in the VS measurement path (open loop protection for the **[PFC](#page-57-0)** stage).

The reflected bus voltage appears as a negative voltage at  $V_{AUX}$ . This negative voltage is internally clamped at the ZCD pin to the negative voltage V<sub>INPCLN</sub>. The internal clamping current I<sub>ZCD</sub> is measured at the end of the ontime at the time  $t_{CS,sample}$ . The measured clamping current of the ZCD pin, the dimensioning of the resistor dividers R<sub>ZCD,FB,1</sub> and R<sub>ZCD,FB,2</sub> as well as the number of transformer turns N<sub>a</sub> and N<sub>p</sub> are used to calculate the bus voltage  $V_{\text{bus,FB}}$  as follows:

$$
V_{\text{bus, FB}} = \left( \left| I_{\text{ZCD}} + \frac{V_{\text{INPCLN}}}{R_{\text{ZCD, FB, 2}}} \right| R_{\text{ZCD, FB, 1}} + V_{\text{INPCLN}} \right) \frac{N_p}{N_a}
$$

#### **Equation 4**

 $V_{\text{bus,FB}}$  is used for plausibility checks with the voltage  $V_{\text{bus}}$  as measured using the VS pin.



**Figure 16 Voltage Sensing using ZCD Clamp Current**

# **3.2.1.4 Output Current Calculation**

The output current is calculated based on the primary side peak current and the timing of the switching cycle.

The output current  $I_{out}$  is calculated using the duration of conduction of the output diode  $t_{demag}$ , the switching period  ${\sf t}_{\sf sw,FB}$  as well as the number of transformer turns  ${\sf N_p,N_s}$  and the transformer coupling  ${\sf K}_{\sf coupling}.$  The following equation is valid both in **[QRM1](#page-57-0)** and **[DCM](#page-56-0)**:

$$
I_{\text{out}} = \frac{1}{2} I_{p, \text{pk}} \cdot \frac{N_p}{N_s} \cdot K_{\text{coupling}} \cdot \frac{t_{\text{demag}}}{t_{\text{sw, FB}}}
$$

#### **Equation 5**

The coupling of the transformer can be approximated using the transformer primary inductance  $L<sub>p</sub>$  and the transformer primary leakage inductance  $L_{p,lk}$  as follows:

$$
K_{\text{coupling}} \approx \frac{L_p}{L_p + L_{p, \text{lk}}}
$$

#### **Equation 6**

The calculated current I<sub>out</sub> is used for the control loop in the modes **[CC](#page-55-0)** and **[LP](#page-56-0)**. The calculated current is also used for output overcurrent protection.



# <span id="page-20-0"></span>**3.2.1.5 Output Control Scheme**

The XDPL8220 includes three different control schemes for a **[CC](#page-55-0), [CV](#page-55-0)** or [LP](#page-56-0) output.

Different use cases require the controller to operate according to different operation schemes:

- In the case of typical LED strings, the forward voltage of the LED string determines the output voltage of the driver. XDPL8220 operates in [CC](#page-55-0) and drives a constant output current I<sub>out.full</sub> to the load. The forward voltage of the connected LED string has to be below a configurable maximum value  $V_{\text{out set}}$ .
- In the case of LED loads including a power stage (e.g. Infineon BCR linear regulators or Infineon DC/DC buck ILD2111), XDPL8220 operates in [CV](#page-55-0), ensuring a constant voltage V<sub>out,set</sub> to the load. The total output current drawn by the load has to be below a configurable maximum value  $I_{\text{out-full}}$ .
- In the case of a high output current setpoint  $I_{\text{out,full}}$  and an overly long LED string which exceeds the configurable power limit P<sub>out,set</sub>, XDPL8220 operates in [LP](#page-56-0) to ensure that the power limit of the driver is not exceeded. The controller reduces the output current automatically, ensuring light output without any interruption even for overly long LED strings. The forward voltage of the connected LED string has to be below a configurable maximum value  $V_{\text{out sept}}$ .

For every update of the control loop, the control scheme is selected on the basis of the current operation conditions (output voltage V<sub>out</sub> and output current  $I_{out}$ ) and their distance to the three limiting setpoints  $(V_{\text{out,set}}, P_{\text{out,set}})$  and  $I_{\text{out,full}}$ :

- For [CC](#page-55-0) schemes, the internal reference current I<sub>out,full</sub> is weighted according to thermal management and a dimming curve to yield I<sub>out,set</sub>. The calculated output current I<sub>out</sub> is compared with the weighted reference current  $I_{out.set}$  to generate an error signal for the output current.
- For [CV](#page-55-0) schemes, the sensed output voltage V<sub>out</sub> at the ZCD pin is compared to a reference voltage V<sub>out,set</sub> to generate an error signal for the output voltage.
- For [LP](#page-56-0) schemes, the output current is limited to a maximum of  $I_{out.set} = P_{out.set} / V_{out}$ .

Out of these three schemes, for each step the most critical error is selected (see **Figure 17** ):

- **1.** If any setpoint is exceeded, the largest error for power decrease is selected to bring the controller back to the desired operating point as quickly as possible.
- **2.** If the current operating conditions are below all three setpoints, the smallest error for power increase is selected to avoid overshooting any setpoint.

The selected error signal is fed into a compensator to control the gate driver switching parameters (i.e. duty cycle and frequency) for the power MOSFET of the **[FB](#page-56-0)**.



**Figure 17 Control Scheme for CC/CV/LP Modes (Non-Dimmed)**

In dimming cases, the output current setpoint  $I_{out.set}$  is located between  $I_{out,min}$  and  $I_{out,full}$  and varies according to the sensed **[PWM](#page-57-0)** duty cycle D<sub>DIM</sub>. Dimming can be visualized by moving the vertical line for the output current setpoint in **Figure 18** from right to left.



#### <span id="page-21-0"></span>**Functional Description**

Note: An operation in limited power mode can cause dimmer dead-travel until the controller enters constant current mode.



**Figure 18 Control Scheme for CC/CV/LP Modes (including Dimming)**

One or more of the output control schemes can be deactivated by configuration of the setpoints. Some examples are given below:

- The [LP](#page-56-0) scheme is not active for P<sub>out,set</sub> > V<sub>out,set</sub> \* I<sub>out,full</sub>. For such a configuration, the controller will only select between a **[CC](#page-55-0)** and **[CV](#page-55-0)** scheme.
- The [CV](#page-55-0) scheme is not active for  $V_{\text{out.set}} = V_{\text{out.OV}}$  as the output overvoltage protection will be triggered.
- The **[CC](#page-55-0)** scheme is not active for  $I_{\text{out,full}} = I_{\text{out,OC}}$  as the output overcurrent protection will be triggered.

# **3.2.1.6 Multimode Scheme**

The control loop of XDPL8220 uses two different switching modes. **[QRM1](#page-57-0)** is optimized for high efficiency at high loads while **[DCM](#page-56-0)** is used in light load conditions.



**Figure 19 Flyback Multimode Operation Scheme**

- **[QRM1](#page-57-0)**: This mode maximizes the efficiency by switching on the 1st valley of the V<sub>AUX</sub> signal. This ensures zero current switching with a minimum of switching losses. The power is controlled by regulating the primary peak current using  $V_{CS,OCP1}$ .
- **[DCM](#page-56-0):** This mode is used if V<sub>CS,OCP1</sub> has reached its minimum value V<sub>CS,min,FB</sub>. To allow lower output power, the controller extends the switching period later than the 1st valley .



#### <span id="page-22-0"></span>**Functional Description**

The minimum power is limited by the transformer primary inductance  $L_p$ , maximum switching period  $t_{sw,max,FB}$  and minimum primary peak current  $I_{p,pk,min}$ :

$$
P_{\min} = \frac{1}{2} \cdot L_p \cdot I_{p, \text{pk, min}}^2 \cdot \frac{1}{t_{\text{sw, max, FB}}}
$$

#### **Equation 7**

The minimum primary peak current  $I_{p,pk,min}$  is restricted by:

$$
I_{p, \, \text{pk, min}} = t_{\text{demag, min}} \cdot \frac{N_p}{N_s} \cdot \frac{V_{\text{out, OV}}}{L_p}
$$

#### **Equation 8**

Note: If the load drops below the minimum load of  $P_{\text{min}}$ , the output voltage will rise up to the output overvoltage threshold  $V_{\text{out,OV}}$  and trigger the protection. An auto-restart can be used to keep the output voltage close to  $V_{\text{out,OV}}$  until the load increases again.

# **3.2.2 Flyback Startup**

After startup, the [FB](#page-56-0) of the XDPL8220 initiates a soft start to minimize the switching stress for the power MOSFET and secondary diode.

The cycle-by-cycle current limit is increased in steps of  $V_{CS,step}$  with a configurable duration  $t_{softstart}$  for each step. After the final V<sub>CS,OCP1,start</sub> limit level has been reached, the output will be charged until the minimum output voltage V<sub>out,start</sub>, which ensures self-supply has been reached. At this condition, **[Continuous Conduction](#page-55-0) [Mode \(CCM\)](#page-55-0)** protection as well as output undervoltage protection are activated and the control loop takes over. The starting point for the control loop is to operate in DCM at lowest switching frequency and shortest on-time. These switching parameters avoid any overshoot of output current for short LED string in dimmed conditions.



**Figure 20 Flyback Startup Sequence**



# <span id="page-23-0"></span>**3.2.3 Protection Features**

Protections ensure the operation of the controller under restricted conditions. Protections are triggered if fault conditions are present longer than the blanking times configured for each protection**3)**. The controller will react to a triggered protection as configured.

#### Attention: The controller may continue operation after exceeding protection thresholds because of **blanking times. All protection thresholds have to be set with respect to tolerances, blanking times and worst case transients.**



**Figure 21 Blanking Times cause Excess of Threshold**

# **3.2.3.1 Primary Overcurrent Protection**

The primary side overcurrent protection implemented in hardware covers fault conditions like a short in the transformer primary winding or an open CS pin.

The primary side current is compared to a configurable overcurrent protection threshold  $V_{CS,OCP2}$ . If the threshold is exceeded for longer than the blanking time  $t_{OCP2,FB}$ , the protection will be triggered.

# **3.2.3.2 Output Undervoltage Protection**

In the case of a short in the output, the output voltage may drop to a very low level. Detection of undervoltage in the output voltage  $V_{out}$  is enabled by measurement of the reflected voltage at the ZCD pin.

During operation, the output voltage is compared to a configurable undervoltage protection threshold V<sub>out,UV</sub>. If the threshold is exceeded for longer than the blanking time  $t_{\text{blank,out,UV}}$ , the protection will be triggered. This protection threshold  $V_{\text{out.UV}}$  is disabled during startup.

During startup, the protection operates differently: In case the [FB](#page-56-0) cannot charge the output voltage to V<sub>out,start</sub> during a timeout of t<sub>start,max,[FB](#page-56-0)</sub>, the protection will be triggered. This timeout starts when the FB is started.

Note: The startup threshold V<sub>out, start</sub> has to be configured over and above the undervoltage threshold V<sub>out,UV</sub> to allow undershoots at startup which may occur, especially for resistive loads.

# **3.2.3.3 Output Overvoltage Protection**

In case of a open output, the output voltage may rise to a high level. Overvoltage detection of the output voltage  $V_{\text{out}}$  is provided by measurement at the ZCD pin.

The output voltage is compared to a configurable overvoltage protection threshold  $V_{out,OV}$ . If the threshold is exceeded for longer than the blanking time  $t_{\text{blank.out.OV}}$ , the protection will be triggered.

<sup>&</sup>lt;sup>3</sup> except VCC undervoltage protection



<span id="page-24-0"></span>Note: The blanking time t<sub>blank,Vout,OV</sub> should be set to the minimum value to minimize overshoots of the output voltage above the protection threshold.

# **3.2.3.4 Output Overcurrent Protection**

Overcurrent detection in the output current I<sub>out</sub> is provided on the basis of the calculated output current.

The calculated output current is compared to a configurable overcurrent protection threshold  $I_{out,OC}$ . If the threshold is exceeded for longer than the blanking time  $t_{\text{blank.out.OC}}$ , the protection will be triggered.

# **3.2.3.5 Output Overpower Protection**

Overpower detection in the output power P<sub>out</sub> is provided on the basis of the calculated output power.

The calculated output power is compared to a configurable overpower protection threshold  $P_{out,OP}$ . If the threshold is exceeded for longer than the blanking time  $t_{\text{blank.out.OP}}$ , the protection will be triggered.

# **3.2.3.6 Other Flyback Protections**

XDPL8220 includes additional protections to ensure the integrity and correct flow of the firmware.

- A hardware weak pull-up protects against an open CSFB pin.
- A firmware watchdog protects against the CSFB pin becoming shorted to GND.
- A firmware state monitor supervises correct operation of the flyback in **[QRM1](#page-57-0)** or **[DCM](#page-56-0)**. A protection is triggered if the flyback enters **[CCM](#page-55-0)**.
- A firmware check ensures that the **[PFC](#page-57-0)** has already boosted the bus voltage sufficiently before the [FB](#page-56-0) starts.
- A firmware plausibility check ensures that the bus voltage measurement using the VS pin is correct.

Note: This protection is usually triggered if the output is open or the output load drops below the minimum load P<sub>min</sub>.



# <span id="page-25-0"></span>**3.3 General Controller Features**

XDPL8220 provides general features for firmware task scheduling, VCC control and temperature control which are independent of the target application.

# **3.3.1 External Temperature Sensing**

The external temperature is measured by measuring the voltage of an **[NTC](#page-56-0)** with respect to the internal V<sub>RFF</sub> voltage.



#### **Figure 22 External Temperature Sensing using NTC**

The controller calculates the resistance of the NTC based on the measured voltage  $V_{Temp}$ , the internal reference voltage  $V_{RFF}$  and the internal pull-up resistance  $R_{PU}$ :

$$
R_{\text{NTC}} = \frac{v_{\text{Temp}} \cdot R_{\text{PU}}}{v_{\text{REF}} - v_{\text{Temp}}}
$$

#### **Equation 9**

# **3.3.2 Adaptive Temperature Protection**

XDPL8220 offers adaptive temperature protection using internal and/or external temperature sensors. This feature reduces the output current according to temperature to protect the load and driver against overtemperature.

Whenever the temperature  $T_{hot}$  is exceeded, the current is gradually reduced from the maximum current  $I_{out.set}$ , as shown in **Figure 23** . If the temperature drops below T<sub>hot</sub>, the output current is increased again. This allows the controller to ensure operation at or below a temperature of  $T_{hot}$ .

If a reduction down to a minimum current  $I_{out,red}$  is not able to compensate for any continued increase in temperature, XDPL8220 will eventually trigger overtemperature protection if  $T_{critical}$  is exceeded. If the controller is configured to react with auto-restart to the overtemperature protection, it will only restart after the temperature dropped below  $T_{hot}$ .



**Figure 23 Adaptive Temperature Protection**



<span id="page-26-0"></span>Note: Please note that the internal temperature sensor can only protect external components which have sufficient thermal coupling to XDPL8220. The external temperature sensor can be used to protect the temperature of external components (e.g. power MOSFETs or linear regulators).

# **3.3.3 PWM Dimming Interface**

The duty cycle sensed at the PWM pin is used to determine the output current level. The XDPL8220 can be configured to use either a linear or a quadratic dimming curve. Either normal or inverted dimming curves can be selected.

**Figure 24** shows the relationship of the **[PWM](#page-57-0)** duty cycle to the output current target value. Configurable levels  $D_{\text{DIM,min}}$  and  $D_{\text{DIM,max}}$  ensure that the minimum current  $I_{\text{out,min}}$  and maximum current  $I_{\text{out,set}}$  can always be achieved, thereby making the application robust against component tolerances.

An optional hysteresis can be enabled for the sensing of the PWM signal. This hysteresis can suppress jitter in the PWM signal. Any change of the PWM duty cycle within the hysteresis will not affect the output current.



**Figure 24 Selectable Dimming Curves**

Using the optional Dim-to-Off feature, the light output can be stopped without removal of input voltage. In Dimto-Off, the controller will enter auto-restart operation to minimize power consumption. The auto-restart recharges the output voltage to a minimum output voltage of V<sub>out,start</sub> to measure the PWM duty cycle. With this feature, the output voltage can be maintained in a specific range by configuration of the startup voltage  $V_{\text{out.start}}$ and auto-restart time t<sub>AR</sub>, and by dimensioning of an active or passive output bleeder. If V<sub>out, start</sub> is configured to be low enough below the minimum forward voltage of the **[LED](#page-56-0)** string, the **[LED](#page-56-0)**s will show no light in this state.

Note: Either an active or passive output bleeder is required to allow the controller to maintain the output voltage if the Dim-to-Off feature is enabled.



### <span id="page-27-0"></span>**Functional Description**

Dim-to-Off is entered if the **[PWM](#page-57-0)** duty cycle exceeds the configurable threshold D<sub>DIM, off</sub> (see purple line in *[Figure](#page-26-0)* 24). As soon as the duty cycle exceeds D<sub>DIM,on</sub>, the controller will start to continuously regulate output voltage or output current again.

# **3.3.4 Protection Features**

Protections ensure the operation of the controller under restricted conditions. Protections are triggered if fault conditions are present longer than the blanking times configured for each protection**4)**. The controller will react to a triggered protection as configured.

#### Attention: The controller may continue operation after exceeding protection thresholds because of **blanking times. All protection thresholds have to be set with respect to tolerances, blanking times and worst case transients.**



**Figure 25 Blanking Times cause Excess of Threshold**

# **3.3.4.1 Overtemperature Protection**

Overtemperature protection initiates a shutdown once the critical temperature level  $T_{critical}$  is exceeded.

**Figure 26** shows the temperature hysteresis formed by the critical temperature T<sub>critical</sub> and maximum turn-on threshold  $T_{hot}$  if auto-restart is enabled for temperature protection.

If latch mode is selected instead, the IC will turn off and only restart after recycling of input power with a temperature below  $T_{critical}$ .





<sup>4</sup> except VCC undervoltage protection



# <span id="page-28-0"></span>**3.3.4.2 VCC Undervoltage Protection**

A **[Undervoltage Lockout \(UVLO\)](#page-58-0)** is implemented in hardware. It ensures defined enabling and disabling of the **[Integrated Circuit \(IC\)](#page-56-0)** operation depending on the supply voltage V<sub>VCC</sub> at the VCC pin in accordance with defined thresholds.

The **[UVLO](#page-58-0)** contains a hysteresis with the voltage thresholds V<sub>VCC.on</sub> for enabling the [IC](#page-56-0) and V<sub>VCC.off</sub> for disabling the IC. Once the mains input voltage is applied, current flows through an external resistor into the HV pin via the integrated depletion cell and diode to the VCC pin. The **[IC](#page-56-0)** is enabled once V<sub>VCC</sub> exceeds the threshold V<sub>VCC on</sub> and enters normal operation if no fault condition is detected. In this phase,  $V_{VCC}$  will drop until either external supply or the self-supply via the auxiliary winding takes over the supply at the VCC pin.

In the case of output short or strong capacitive loading, the auxiliary winding cannot provide power to  $V_{VCC}$ . A timeout of  $t_{start,max}$  is available to respond to this failure condition.

- Note: The self-supply via the auxiliary winding must be in place before the output short timeout occurs or before V<sub>VCC</sub> falls below the V<sub>VCC off</sub> threshold. Otherwise, the system will perform a fast restart.
- Note: It is possible to supply VCC externally from an auxiliary power supply. In this case, the VCC also needs initially to ramp to  $V_{\text{VCC,on}}$  to enable the IC.

# **3.3.4.3 VCC Overvoltage Protection**

Overvoltage protection ensures that the voltage at the VCC pin is not exceeded.

The VCC voltage is compared to a configurable overvoltage protection threshold  $V_{VCC,OV}$ . If the threshold is exceeded for longer than the blanking time  $t_{\text{blank}VCC,OV}$ , the protection will be triggered.

Note: The reaction to this protection is fixed to stop mode to ensure a discharge of VCC.

# **3.3.4.4 Other General Controller Protections**

XDPL8220 includes several protections to ensure the integrity and correct flow of the firmware.

- A hardware watchdog checks correct execution of firmware. A protection is triggered in the event that the firmware does not service the watchdog within a defined period.
- A hardware **[Random Access Memory \(RAM\)](#page-57-0)** parity check triggers a protection if a bit in the memory changes unintentionally.
- A hardware clock check watchdog checks that no clock oscillator is failing.
- A firmware **[Cyclic Redundancy Check \(CRC\)](#page-55-0)** at each startup verifies the integrity of firmware code and its parameters.
- A firmware task execution watchdog triggers a protection if the firmware tasks are not executed as expected.

# **3.3.5 Protection Reactions**

The reaction to each protection can be separately selected. Available reactions may include auto restart, fast auto restart, latch or stop mode.

**[Figure 27](#page-29-0)** depicts the timing of an auto-restart reaction:

- **1.** If a protection threshold is exceeded for longer than the related blanking time  $t_{\text{blank}}$ , the protection is triggered.
- $\boldsymbol{2.}$  Within a maximum t $_1$  = 4 \* 32 µs, the gate driver of the power stage related to the protection is disabled.
- **3.** Within a maximum  $t_2$  = 4  $^{\star}$  32  $\mu$ s, the gate drivers of other stages are disabled.
- **4.** The reaction depends on the configuration of the protection:
	- In case of latch mode, the application will enter latch mode at this time. No further steps are done, the reaction ends here.



#### <span id="page-29-0"></span>**Functional Description**

- In case of stop mode, the application will stop and enter UART parametrization mode which allows to read out the error code. No further steps are done, the reaction ends here.
- In case of a (fast) auto-restart reaction, the controller will enter a power saving mode for the auto-restart time  $t_{AR}$  or  $t_{AR,fast}$  respectively.
- **5.** The auto restart may include a new VCC charging cycle. The time  $\mathsf{t}_3$  typically depends on the input voltage.
- **6.** The first power stage will enable its gate driver according to its startup sequence (soft start) again.
- **7.** The second power stage will enable its gate driver according to its startup sequence (soft start) again. The startup of a subsequent power stage may be delayed by a time  $\mathsf{t}_4$  depending on any startup condition for the subsequent stage.



**Figure 27 Protection Reaction for auto-restart**

# **3.3.5.1 Auto restart**

When auto restart mode is activated, XDPL8220 stops switching at the GD pins. After a configurable auto restart time  $t_{AP}$ , XDPL8220 initiates a new startup with soft start.

During the time in which the gate is not switching, the internal HV startup cell is automatically enabled and disabled to keep the VCC voltage between the V<sub>UVLO</sub> and V<sub>OVLO</sub> thresholds for the supply of XDPL8220.

# **3.3.5.2 Fast Auto Restart**

When fast auto restart mode is activated, XDPL8220 stops switching at the GD pins. After a configurable fast auto restart time  $t_{AR,fast}$ , XDPL8220 initiates a new startup with soft start.

During the time in which the gate is not switching, the internal HV startup cell is automatically enabled and disabled to keep the VCC voltage between the V<sub>UVLO</sub> and V<sub>OVLO</sub> thresholds for the supply of XDPL8220.



# <span id="page-30-0"></span>**3.3.5.3 Latch Mode**

When latch mode is activated, XDPL8220 stops switching at the GD pins. The device stays in this state until input voltage is completely removed and the VCC voltage drops below the V<sub>UVLO</sub> threshold. Only then can XDPL8220 be restarted by applying input voltage.

To maintain this state, the internal HV startup cell is automatically enabled and disabled to keep the VCC voltage between the V<sub>UVLO</sub> and V<sub>OVLO</sub> thresholds for the supply of XDPL8220. The current consumption is reduced to a minimum.

# **3.3.5.4 Stop Mode**

When stop mode is activated, XDPL8220 stops switching at the GD pins. XDPL8220 enters **[UART](#page-58-0)** communication mode to allow debugging of the system state.

Note: The VCC for XDPL8220 needs to be supplied by an external source. Without an external supply, VCC will drain to  $V_{UVLO}$  and XDPL8220 performs a restart.



### <span id="page-31-0"></span>**Design Support**

# **4 Design Support**

XDPL8220 is a configurable digital platform product. It can be configured to meet a wide range of application requirements.

# **4.1 Design Procedure**

Infineon provides support of the design procedure for lighting applications using Infineon's digital platform **[IC](#page-56-0)**s.

A lighting application is designed in a few simple steps using Infineon's digital platform **[IC](#page-56-0)**s as follows:

- **1.** The Infineon XDPL8220 reference board and the XDPL8220 Reference Board Test Report demonstrate the features and performance of the XDPL8220 in a typical application.
- **2.** Parameters of the XDPL8220 reference board can easily be fitted to any application's requirements. The isolated .dp Interface Gen2 is connected to XDPL8220 via **[Universal Serial Bus \(USB\)](#page-58-0)**. The **[GUI](#page-56-0)** tool .dp Vision is included with the *.dp Interface Gen2*. .dp Vision allows interactive changing of parameters. The usage of .dp Vision is explained in the .dp Vision User Manual.
- **3.** To further adapt the XDPL8220 to application requirements, customers can design their own specific boards. The steps used to design a board are explained in the XDPL8220 Design Guide. .dp Vision can be used together with the .dp Interface Gen2 to connect to customer-specific designs based on XDPL8220. This setup can be used for rapid prototyping. The tooling allows fine-tuning of parameters and development of multiple parameter sets – e.g. to reuse the same for different product variants of an application.
- **4.** For mass production, the XDPL8220 Programming Manual documents the necessary interfacing and procedures to integrate the parameter configuration of XDPL8220 into the production line. **Figure 28** shows two options to easily apply the configuration of the **[IC](#page-56-0)** during production tests:
	- One option is to use the isolated .dp Interface Gen2, which can be accessed with **[USB](#page-58-0)** commands.
	- Another option is to directly use the **[UART](#page-58-0)** interface of the XDPL8220. The correct VCC voltage and **[UART](#page-58-0)** communication have to be controlled by the production process in this case.



#### **Figure 28 Setup for Parametrization using .dp Interface Gen2 for Interactive Development (top) and Production (middle and bottom)**

# **4.2 List of Configurable Parameters**

This list provides information about configurable parameters, including their permitted range and granularity. Typical example values are also provided.







# **Design Support**

### **Table 2 Parameters for Hardware Configuration (continued)**



#### **Table 3 Parameters for PFC Protections**

<b>Symbol</b>	<b>Description</b>	<b>Example</b>	<b>Minimum</b> Value	<b>Maximum</b> Value	Granularity
t <sub>blank</sub> , V <sub>bus</sub> , OVP 2	Blanking time for bus overvoltage threshold, level 2	200 ns	0 <sub>s</sub>	640 ns	$1/f_{mclk}$
t <sub>blank</sub> , V <sub>bus</sub> , OVP	Blanking time for bus overvoltage threshold, level 1	400 us	0 <sub>s</sub>	1 <sub>ms</sub>	$t_{slot}$
$V_{bus, OVP1}$	Bus overvoltage threshold, level 1	490V	V <sub>bus,stdy,entr,</sub> <b>OV</b>	600 V <sup>3</sup>	1/16V
t <sub>blank</sub> , V <sub>bus</sub> , UV	Blanking time for bus undervoltage threshold	500 us	0 <sub>S</sub>	1 <sub>ms</sub>	$t_{slot}$
$V_{bus,UV}$	Bus undervoltage threshold	300 V	V <sub>bus, start, PFC</sub>	V <sub>bus,stdy,entr,U</sub> V	1/16V
t <sub>start, max, PFC</sub>	Maximum <b>PFC</b> soft start time to settle the bus voltage at startup	$200 \text{ ms}$	0 <sub>s</sub>	500 ms	$t_{slot}$
t <sub>blank</sub> , Vin, OV	Blanking time for input overvoltage threshold	$100 \text{ ms}$	0 <sub>s</sub>	200 ms	$t_{slot}$
t <sub>blank</sub> , Vin, UV	Blanking time for input undervoltage threshold	100 ms	0 <sub>s</sub>	200 ms	$t_{slot}$

<sup>&</sup>lt;sup>1</sup> Limited by VCC -  $0.5$  V

 $2$  Limited by VCC - 0.5 V

 $3$  Limited by the voltage rating of the bus capacitors



# **Design Support**

### **Table 3 Parameters for PFC Protections (continued)**



### **Table 4 Parameters for Flyback Protections**





# **Design Support**

### **Table 4 Parameters for Flyback Protections (continued)**



#### **Table 5 Parameters for General Protections**





# **Design Support**

# **Table 5 Parameters for General Protections (continued)**



#### **Table 6 Parameters for Adaptive Temperature Protection**



#### **Table 7 Parameters for Startup and Shutdown**



#### **Table 8 Parameters for PFC Control Loop**





# **Design Support**

### **Table 8 Parameters for PFC Control Loop (continued)**



#### **Table 9 Parameters for Flyback Control Loop**

Symbol	<b>Description</b>	<b>Example</b>	<b>Minimum</b> Value	<b>Maximum</b> <b>Value</b>	Granularity
$b_{0,DCM}$	$b_0$ gain of control loop in <b>DCM</b>	5353/ $f_{mclk}/256$	0	8192/ $f_{mclk}/256$	$1/f_{\text{mclk}}/256$
$b_{1,DCM}$	$b_1$ gain of control loop in <b>DCM</b>	$-53/$ $f_{mclk}/256$	$-8192/$ $f_{mclk}/256$	$\mathbf{0}$	$1/f_{\text{mclk}}/256$
$b_{0,QRM1}$	$b_0$ gain of control loop in <b>QRM1</b>	6060 / 65536 v	0V	16384/ 65536V	1/65536V
$b_{1,QRM1}$	$b_1$ gain of control loop in <b>QRM1</b>	$-60/65536$ V	$-16384/$ 65536V	0 <sub>V</sub>	1/65536V
K <sub>P,CV</sub>	Proportional gain for CV mode	1.9	$\Omega$	16	0.125
$K_{D,CV}$	Derivative gain for CV mode		28	128	0.125
$P_{\text{out},\text{set}}$	Output power limit	100W	0	150W	0.5W
l <sub>out,full</sub>	Non-dimmed output current	2.0A	$I_{\text{out,min}}$	3A	0.5 <sub>mA</sub>
$V_{\text{out},\underline{\text{set}}}$	Output voltage setpoint	48 V	$V_{\text{out,UV}}$	$V_{\text{out,OV}}$	0.125V
$t_{on,max,FB}$	Maximum on-time limit	15 <sub>us</sub>	$V_{CS,max,FB}/$ $R_{CS,FB}^{\prime} \times L_p /$ V <sub>bus, UV</sub> <sup>4)</sup>	25 <sub>us</sub>	$1/f_{mclk}$
$t_{\text{sw,max,FB}}$	Maximum switching period	$1/20$ kHz	$t_{\text{sw,min,FB}}$	$1/16$ kHz	$1/f_{mclk}$
$t_{\text{sw,min},\text{FB}}$	Minimum switching period	$1/150$ kHz	$1/150$ kHz	$t_{\text{sw,max,FB}}$	$1/f_{mclk}$
$V_{CS,max,FB}$	Maximum peak current voltage	1.09 V	$V_{CS,min,FB}$	92% * 1.214 ۷	$0.125$ mV

<sup>4</sup> Maximum on-time occurs if maximum power is transferred at minimum bus voltage.



# **Design Support**

#### **Table 9 Parameters for Flyback Control Loop (continued)**



### **Table 10 Parameters for Dimming**



#### **Table 11 Parameters for Fine Tuning**

Symbol	<b>Description</b>	<b>Example</b>	<b>Minimum</b> Value	<b>Maximum</b> Value	Granularity
K <sub>coupling</sub>	<b>FB</b> transformer coupling coefficient	0.98	0.5	2	0.001
$t_{LEB,FB}$	<b>FB</b> Current sense leading edge blanking	200 ns	$1/f_{mclk}$	600 ns	$1/f_{mclk}$
$t_{OCP2,FB}$	<b>FB</b> OCP2 blanking time	250 ns	$1/f_{mclk}$	63 / $f_{mclk}$	$1/f_{mclk}$
$t_{PDC}$	<b>FB</b> Propagation delay compensation	500 ns	$t_{OCP1,FB}$	2 <sub>us</sub>	$1/f_{mclk}$
$t_{OCP1,FB}$	FB OCP1 spike suppression filter	$100$ ns	$50$ ns	500 ns	$1/f_{mclk}$
t <sub>CSFB, offset</sub>	<b>FB</b> sampling offset	200 ns	$50$ ns	500 ns	$1/f_{mclk}$
$t_{sw,hysteresis}$	FB switching period hysteresis for QRM/DCM mode changes	600 ns	$20$ ns	$1000$ ns	$1/f_{mclk}$
$t_{rsup,FB}$	<b>FB</b> ZCD ringing suppression	1.2 <sub>us</sub>	$1/f_{mclk}$	2 <sub>us</sub>	$1/f_{mclk}$
$t_{\mathsf{ZCD},\mathsf{PD},\mathsf{FB}}$	<b>FB</b> Delay of zero-crossing signal	200 ns	0 <sub>s</sub>	1 <sub>us</sub>	$1/f_{mclk}$
t <sub>ZCD,PD,RE,FB</sub>	<b>FB</b> Rising edge delay of zero-crossing signal	450 ns	0 <sub>s</sub>	1 <sub>us</sub>	$1/f_{mclk}$
$t_{\text{gate,}on}$	<b>FB</b> Turn-on delay of MOSFET	$100$ ns	0 <sub>s</sub>	1 <sub>us</sub>	$1/f_{mclk}$
t <sub>LEB,PFC</sub>	<b>PFC</b> On-time leading edge blanking	200 ns	$1/f_{mclk}$	600 ns	$1/f_{mclk}$

<sup>&</sup>lt;sup>5</sup> The minimum peak current must ensure that  $t_{\text{demag,min,FB}}$  is maintained.



# <span id="page-38-0"></span>**Design Support**

#### **Table 11 Parameters for Fine Tuning (continued)**



# **4.3 List of Fixed Parameters**

This list shows the fixed parameters and their associated values – i.e. parameters whose values cannot be changed.

#### **Table 12 List of Fixed Parameters**





<span id="page-39-0"></span>**Electrical Characteristics and Parameters**

# **5 Electrical Characteristics and Parameters**

All signals are measured with respect to the ground pin, GND. The voltage levels are valid provided other ratings are not violated.

# **5.1 Package Characteristics**

#### **Table 13 Package Characteristics**



# **5.2 Absolute Maximum Ratings**

#### **Attention**: **Stresses above the values listed above may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may ƛ" 1 device reliability. Maximum ratings are absolute ratings; exceeding only one of these values may cause irreversible damage to the integrated circuit. These values are not tested during production test.**

#### **Table 14 Absolute Maximum Ratings**



<sup>1</sup> According to JESD22-A111 Rev A.

<sup>&</sup>lt;sup>2</sup> Latch-up capability according to JEDEC JESD78D,  $T_A = 85^{\circ}$ C.

<sup>3</sup> ESD-HBM according to ANSI/ESDA/JEDEC JS-001-2012.

<sup>4</sup> ESD-CDM according to JESD22-C101F.



### <span id="page-40-0"></span>**Electrical Characteristics and Parameters**

#### **Table 14 Absolute Maximum Ratings (continued)**



# **5.3 Operating Conditions**

The recommended operating conditions are shown for which the DC Electrical Characteristics are valid.

#### **Table 15 Operating Range**





<span id="page-41-0"></span>**Electrical Characteristics and Parameters**

# **5.4 DC Electrical Characteristics**

The electrical characteristics provide the spread of values applicable within the specified supply voltage and junction temperature range, T $_{\textrm{\scriptsize{J}}}$  from -40 °C to +125 °C.

Devices are tested in protection at  $T_A = 25$  °C. Values have been verified either with simulation models or by device characterization up to 125 °C.

Typical values represent the median values related to  $T_A = 25$  °C. All voltages refer to GND, and the assumed supply voltage is  $V_{VCC}$  = 18 V if not otherwise specified.

Note: Not all values given in the tables are tested during production testing. Values not tested are explicitly marked.

#### **Attention**: **The Vcc pin voltage must be higher than 3.4V before the voltage of any other pins (except GND and HV pins) exceeds 1.2V.**



#### **Table 16 Power Supply Characteristics**

<sup>&</sup>lt;sup>5</sup> Tested at  $V_{VCC}$  = 5.5 V



### **Electrical Characteristics and Parameters**



#### **Table 16 Power Supply Characteristics (continued)**

 $\overline{6}$  Theoretical minimum value, real minimum value is related to V<sub>UVOFF</sub> threshold.

<sup>7</sup> Operational values.

<sup>8</sup> Note that the system is turned off if  $V_{VCC} < V_{UFOFF}$ .



# **Electrical Characteristics and Parameters**

#### **Table 17 Electrical Characteristics of the GDFB Pin**



 $9$  referred to GDx\_CFG.CUR = 16



# **Electrical Characteristics and Parameters**

#### **Table 18 Electrical Characteristics of the CSFB Pin**





### **Electrical Characteristics and Parameters**

### **Table 18 Electrical Characteristics of the CSFB Pin (continued)**



### **Table 19 Electrical Characteristics of the ZCD Pin**





# **Electrical Characteristics and Parameters**

#### **Table 19 Electrical Characteristics of the ZCD Pin (continued)**



<sup>&</sup>lt;sup>10</sup> Limits the minimum gate driver  $T_{on}$  time.



# **Electrical Characteristics and Parameters**





#### **Table 20 Electrical Characteristics of the VS Pin**





# **Electrical Characteristics and Parameters**

#### **Table 21 Electrical Characteristics of the HV Pin**



#### **Table 22 Electrical Characteristics of the PWM Pin**





### **Electrical Characteristics and Parameters**

# **Table 22 Electrical Characteristics of the PWM Pin (continued)**



#### **Table 23 Electrical Characteristics of the TEMP Pin**



#### **Table 24 Electrical Characteristics of the CSPFC Pin**





# **Electrical Characteristics and Parameters**

### **Table 24 Electrical Characteristics of the CSPFC Pin (continued)**





# **Electrical Characteristics and Parameters**

#### **Table 25 Electrical Characteristics of the UART Pin**



### **Table 26 Electrical Characteristics of the GDPFC Pin**





### **Electrical Characteristics and Parameters**



#### **Table 26 Electrical Characteristics of the GDPFC Pin (continued)**

#### **Table 27 Electrical Characteristics of the A/D Converter**



<sup>&</sup>lt;sup>11</sup> referred to GDx\_CFG.CUR =  $16$ 

<sup>&</sup>lt;sup>12</sup> ADC capability measured via channel MFIO without errors due to switching of neighbouring pins, e.g. gate drivers, measured with STC = 5. MFIO buffer non-linearity masked out by taking ADC output values  $\geq$  30 only.



### **Electrical Characteristics and Parameters**

# **Table 28 Electrical Characteristics of the Reference Voltage**



#### **Table 29 Electrical Characteristics of the OTP Programming**



#### **Table 30 Electrical Characteristics of the Clock Oscillators**



### **Table 31 Electrical Characteristics of the Temperature Sensor**





### <span id="page-54-0"></span>**Package Dimensions**

# **6 Package Dimensions**

The package dimensions of PG-DSO-16 are provided.



#### **Figure 29 Package Dimensions for PG-DSO-16**

Note: Dimensions in mm.

Note: You can find all of our packages, packing types and other package information on our Infineon Internet page "Products": http://www.infineon.com/products.



### <span id="page-55-0"></span>**References**

# **7 References**

- **1.** Infineon Technologies AG: XDPL8220 Reference Board Test Report
- **2.** Infineon Technologies AG: .dp Interface Gen2: Can be ordered at **[http://ehitex.com/programmer/486/.dp](http://ehitex.com/programmer/486/.dp-interface-board-gen2)[interface-board-gen2](http://ehitex.com/programmer/486/.dp-interface-board-gen2)**
- **3.** Infineon Technologies AG: .dp Vision User Manual
- **4.** Infineon Technologies AG: .dp Interface Gen2 User Manual
- **5.** Infineon Technologies AG: XDPL8220 Design Guide
- **6.** Infineon Technologies AG: XDPL8220 Programming Manual

# **Abbreviations**

#### **AC**

Alternating Current (AC)

An Alternating Current is a form of power supply in which the flow of electric charge periodically reverses direction.

#### **ADC**

#### Analog-to-Digital Converter (ADC)

An analog-to-digital converter is a device that converts a continuous physical quantity (usually voltage) to a digital number that represents the quantity's amplitude.

#### **BOM**

Bill of Materials (BOM)

A bill of materials is a list of the raw materials, sub-assemblies, intermediate assemblies, sub-components, parts and the quantities of each needed to manufacture an end product.

### **CC**

#### Constant Current (CC)

Constant Current is a mode of a power supply in which the output current is kept constant regardless of the load.

#### **CCM**

#### Continuous Conduction Mode (CCM)

Continuous Conduction Mode is an operational mode of a switching power supply in which the current is continuously flowing and does not return to zero.

#### **CRC**

### Cyclic Redundancy Check (CRC)

A cyclic redundancy check is an error-detecting code commonly used to detect accidental changes to raw data.

#### **CV**

#### Constant Voltage (CV)

Constant Voltage is a mode of a power supply in which the output voltage is kept constant regardless of the load.

#### **DAC**

#### Digital-to-Analog Converter (DAC)

A digital-to-analog converter is a device that converts digital data into an analog signal (typically voltage).

#### **DC**

#### Direct Current (DC)

A Direct Current is a form of power supply in which the flow of electric charge is only into one direction.



### <span id="page-56-0"></span>**Abbreviations**

### **DCM**

### Discontinuous Conduction Mode (DCM)

Discontinuous Conduction Mode is an operational mode of a switching power supply in which the current starts and returns to zero.

### **ECG**

### Electronic Control Gear (ECG)

An electronic control gear is a power supply which provides one or more light module(s) with the appropriate voltage or current.

### **FB**

### Flyback (FB)

A flyback converter is a power converter with the inductor split to form a transformer, so that the voltage ratios are multiplied with an additional advantage of galvanic isolation between the input and any outputs.

#### **FW**

Firmware (FW)

A proprietary software exploiting a set of functions.

### **GUI**

### Graphic User Interface (GUI)

A graphical user interface is a type of interface that allows users to interact with electronic devices through graphical icons and visual indicators.

### **HW**

#### Hardware (HW)

The collection of physical elements that comprise a computer system.

### **IC**

### Integrated Circuit (IC)

A miniaturized electronic circuit that has been manufactured in the surface of a thin substrate of semiconductor material. An IC may also be referred to as micro-circuit, microchip, silicon chip, or chip.

# **IIR**

### Infinite Impulse Response (IIR)

Infinite impulse response is a property applying to many linear time-invariant systems. Common examples of linear time-invariant systems are most electronic and digital filters. Systems with this property have an impulse response which does not become exactly zero past a certain point, but continues indefinitely.

### **LED**

# Light Emitting Diode (LED)

A light-emitting diode is a two-lead semiconductor light source which emits light when activated.

# **LP**

### Limited Power (LP)

Limited Power is a mode of a power supply in which the output power is limited regardless of the load.

### **NTC**

Negative Temperature Coefficient Thermistor (NTC)

A negative temperature coefficient thermistor is a type of resistor whose resistance declines over temperature.

### **OCP1**

### Overcurrent Protection Level 1 (OCP1)

The Overcurrent Protection Level 1 is limiting the current in a switched-mode power supply to limit the power delivered to the output of the power supply.



### <span id="page-57-0"></span>**Abbreviations**

### **OCP2**

Overcurrent Protection Level 2 (OCP2)

The Overcurrent Protection Level 2 is protecting the current in a switched-mode power supply from exceeding a maximum threshold.

### **OTP**

### One Time Programmable Memory (OTP)

A One-Time Programmable memory is a form of memory to which data can be written once. After writing, the data is stored permanently and cannot be further changed.

### **PF**

### Power Factor (PF)

Power factor is the ratio between the real power and the apparent power.

### **PFC**

### Power Factor Correction (PFC)

Power factor correction increases the power factor of an AC power circuit closer to 1 which corresponds to minimizing the reactive power of the power circuit.

#### **PSR**

### Primary Side Regulated (PSR)

A Primary Side Regulated power supply is controlling its operation based on a property sensed on primary side of an isolated power supply.

#### **PWM**

#### Pulse Width Modulation (PWM)

Pulse-width modulation is a technique to encode an analog value into the duty cycle of a pulsing signal with arbitrary amplitude.

#### **QRM**

#### Quasi-Resonant Mode (QRM)

Quasi-Resonant Mode is an operating mode of a switched-mode power supply which maximizes efficiency. This is achieved by only switching at preferred times when switching losses are low.

### **QRM1**

### Quasi-Resonant Mode, switching in valley 1 (QRM1)

Quasi-Resonant Mode is an operating mode of a switched-mode power supply which maximizes efficiency. This is achieved by switching at the occurrence of the first valley of a signal which corresponds to a time when switching losses are low.

#### **QRMn**

### Quasi-Resonant Mode, switching in valley n (QRMn)

Quasi-Resonant Mode is an operating mode of a switched-mode power supply which maximizes efficiency. This is achieved by switching at the occurence of an nth valley of a signal which corresponds to a time when switching losses are low.

#### **RAM**

#### Random Access Memory (RAM)

Random-access memory is a form of computer data storage which allows data items to be read and written regardless of the order in which data items are accessed.

#### **THD**

#### Total Harmonic Distortion (THD)

The total harmonic distortion of a signal is a measurement of the harmonic distortion present and is defined as the ratio of the sum of the powers of all harmonic components to the power of the fundamental frequency.



#### <span id="page-58-0"></span>**Revision History**

#### **UART**

Universal Asynchronous Receiver Transmitter (UART)

A universal asynchronous receiver transmitter is used for serial communications over a peripheral device serial port by translating data between parallel and serial forms.

#### **USB**

Universal Serial Bus (USB)

Universal Serial Bus is an industry standard that defines cables, connectors and communications protocols used in a bus for connection, communication, and power supply between computers and electronic devices.

#### **UVLO**

Undervoltage Lockout (UVLO)

The Undervoltage-Lockout is an electronic circuit used to turn off the power of an electronic device in the event of the voltage dropping below the operational value.

# **Revision History**

Major changes since previous revision



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**Edition 2016-11-4 Published by Infineon Technologies AG 81726 Munich, Germany**

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