# | ANALOG<br>| DEVICES

# 16-Bit, 2.5 MHz/5 MHz/10 MHz, 30 MSPS to 160 MSPS Dual Continuous Time Sigma-Delta ADC

# AD9262

#### <span id="page-0-0"></span>**FEATURES**

**SNR: 83 dB (85 dBFS) to 10 MHz input SFDR: −87 dBc to 10 MHz input Noise figure: 15 dB Input impedance: 1 kΩ Power: 600 mW 1.8 V analog supply operation 1.8 V to 3.3 V output supply Selectable bandwidth 2.5 MHz/5 MHz/10 MHz real 5 MHz/10 MHz/20 MHz complex Output data rate: 30 MSPS to 160 MSPS Integrated dc and quadrature correction Integrated decimation filters Integrated sample rate converter On-chip PLL clock multiplier On-chip voltage reference Offset binary, Gray code, or twos complement data format Serial control interface (SPI)** 

#### <span id="page-0-1"></span>**APPLICATIONS**

**Baseband quadrature receivers: CDMA2000, W-CDMA, multicarrier GSM/EDGE, 802.16x, and LTE Quadrature sampling instrumentation Medical equipment Radio detection and ranging (RADAR)** 

#### <span id="page-0-2"></span>**GENERAL DESCRIPTION**

The AD9262 is a dual channel, 16-bit analog-to-digital converter (ADC) based on a continuous time (CT) sigma-delta ( $\Sigma$ - $\Delta$ ) architecture that achieves −87 dBc of dynamic range over a 10 MHz input bandwidth. The integrated features and characteristics unique to the continuous time  $\Sigma$ - $\Delta$  architecture significantly simplify its use and minimize the need for external components.

The AD9262 has a resistive input impedance that relaxes the requirements of the driver amplifier. In addition, a 32× oversampled fifth-order continuous time loop filter significantly attenuates out-of-band signals and aliases, reducing the need for external filters at the input.

An external clock input or the integrated integer-N PLL provides the 640 MHz internal clock needed for the oversampled continuous time Σ-Δ modulator. On-chip decimation filters and sample rate converters reduce the modulator data rate from 640 MSPS to a user-defined output data rate between 30 MSPS and 160 MSPS, enabling a more efficient and direct interface.

#### **Rev. A**

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#### **FUNCTIONAL BLOCK DIAGRAM**

<span id="page-0-3"></span>

The AD9262 incorporates an integrated dc correction and quadrature estimation block that corrects for gain and phase mismatch between the two channels. This functional block proves invaluable in complex signal processing applications such as direct conversion receivers.

The digital output data is presented in offset binary, Gray code, or twos complement format. A data clock output (DCO) is provided to ensure proper timing with the receiving logic. The AD9262 has the added feature of interleaving Channel A and Channel B data onto one 16-bit bus, simplifying on-board routing.

The ADC is available in three different bandwidth options of 2.5 MHz, 5 MHz, and 10 MHz, and operates on a 1.8 V analog supply and a 1.8 V to 3.3 V digital supply, consuming 600 mW. The AD9262 is available in a 64-lead LFCSP and is specified over the industrial temperature range (−40°C to +85°C).

#### <span id="page-0-4"></span>**PRODUCT HIGHLIGHTS**

- 1. Continuous time Σ-Δ architecture efficiently achieves high dynamic range and wide bandwidth.
- 2. Passive input structure reduces or eliminates the requirements for a driver amplifier.
- 3. An oversampling ratio of 32× and high order loop filter provide excellent alias rejection reducing or eliminating the need for antialiasing filters.
- 4. An integrated decimation filter, sample rate converter, PLL clock multiplier, and voltage reference provide ease of use.
- 5. Integrated dc correction and quadrature error correction.
- 6. Operates from a single 1.8 V analog power supply and 1.8 V to 3.3 V output supply.

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#### <span id="page-1-0"></span>**REVISION HISTORY**



1/10-Revision 0: Initial Version



### <span id="page-2-0"></span>**SPECIFICATIONS**

#### <span id="page-2-1"></span>**DC SPECIFICATIONS**

All power supplies set to 1.8 V, 640 MHz sample rate, 0.5 V internal reference, PLL disabled, 40 MSPS output data rate,  $AIN<sup>1</sup> = -2.0$  $AIN<sup>1</sup> = -2.0$  $AIN<sup>1</sup> = -2.0$  dBFS, unless otherwise noted.

#### **Table 1.**



<span id="page-2-3"></span><span id="page-2-2"></span>1 Input power is referenced to full scale. Therefore, all measurements were taken with a 2 dB signal below full scale, unless otherwise noted. 2 Measured with a low input frequency, full-scale sine wave.

#### <span id="page-3-0"></span>**AC SPECIFICATIONS**

All power supplies set to 1.8 V, 640 MHz sample rate, 0.5 V internal reference, PLL disabled, 40 MSPS output data rate, AIN = −2.0 dBFS, unless otherwise noted.

#### <span id="page-3-7"></span>**Table 2.**



<span id="page-3-2"></span><span id="page-3-1"></span><sup>1</sup> See the AN-835 Application Note, *Understanding High Speed ADC Testing and Evaluation,* for a complete set of definitions.<br><sup>2</sup> Data guaranteed over the full temperature range for the AD9262BCPZ only.

<span id="page-3-3"></span><sup>3</sup> Data guaranteed over the full temperature range for the AD9262BCPZ-5 only.

<span id="page-3-5"></span><span id="page-3-4"></span>4 Data guaranteed over the full temperature range for the AD9262BCPZ-10 only. 5 Noise figure with respect to 50 Ω. AD9262 internal impedance is 1000 Ω differential. See the AN-835 Application Note for a definition.

<span id="page-3-6"></span>6 Crosstalk measured with an input signal on both channels at different frequencies and the leakage of one on to the other.

#### <span id="page-4-0"></span>**DIGITAL DECIMATION FILTERING CHARACTERISTICS**

All power supplies set to 1.8 V, 640 MHz sample rate, 0.5 V internal reference, PLL disabled, 40 MSPS output data rate, AIN = −2.0 dBFS, unless otherwise noted.

#### **Table 3.**



<span id="page-4-1"></span><sup>1</sup> See the AN-835 Application Note, Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions.

#### <span id="page-5-0"></span>**DIGITAL SPECIFICATIONS**

All power supplies set to 1.8 V, 640 MHz sample rate, 0.5 V internal reference, PLL disabled, 40 MSPS output data rate, AIN = −2.0 dBFS, unless otherwise noted.



<span id="page-5-1"></span><sup>1</sup> See the AN-835 Application Note, Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions.

#### <span id="page-6-0"></span>**SWITCHING SPECIFICATIONS**

All power supplies set to 1.8 V, 640 MHz sample rate, 0.5 V internal reference, PLL disabled, 40 MSPS output data rate, AIN = −2.0 dBFS unless otherwise noted.



<span id="page-6-1"></span><sup>1</sup> See the AN-83 5 Application Note, Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions.

2 Data skew is measured from DCO 50% transition to data (D0x to D15x) 50% transition, with 5 pF load.

<span id="page-6-4"></span><span id="page-6-3"></span><span id="page-6-2"></span>3 Typical measured value for the AD9262BCPZ-10. For the AD9262BCPZ-5 and the AD9262BCPZ, typical values double and quadruple the number of cycles, respectively. 4 Cycles refers to modulator clock cycles.

<span id="page-6-5"></span> $^5$  Wake-up time is dependent on the value of the decoupling capacitor, value shown with 10uF capacitor on VREF and CFILT.

<span id="page-6-6"></span>6 Se[e Figure 60 a](#page-25-2)nd th[e Serial Port Interface \(SPI\) s](#page-25-0)ection.

#### <span id="page-6-7"></span>**Timing Diagram**



### <span id="page-7-0"></span>ABSOLUTE MAXIMUM RATINGS

**Table 6.** 



Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### <span id="page-7-1"></span>**THERMAL RESISTANCE**

The exposed paddle must be soldered to the ground plane for the LFCSP package. Soldering the exposed paddle to the PCB increases the reliability of the solder joints, maximizing the thermal capability of the package.

#### **Table 7. Thermal Resistance**



Typical  $\theta_{JA}$  and  $\theta_{JC}$  are specified for a 4-layer board in still air. Airflow increases heat dissipation, effectively reducing  $\theta_{JA}$ . In addition, metal in direct contact with the package leads from metal traces, through holes, ground, and power planes reduces the  $\theta_{JA}$ .

#### <span id="page-7-2"></span>**ESD CAUTION**



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

### <span id="page-8-0"></span>PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



**NOTES 1. THE EXPOSED PAD MUST BE SOLDERED TO THE GROUND PLANE FOR THE LFCSP PACKAGE. SOLDERING THE EXPOSED PADDLE TO THE PCB INCREASES THE RELIABILITY OF THE SOLDER JOINTS, MAXIMIZING THE THERMAL CAPACITY OF THE PACKAGE.** 07772-003

Figure 3. Pin Configuration





### <span id="page-9-0"></span>TYPICAL PERFORMANCE CHARACTERISTICS

All power supplies set to 1.8 V, 640 MHz sample rate, 2 V p-p differential input, 0.5 V internal reference, PLL disabled, AIN = −2.0 dBFS,  $T_A = 25$ °C, output data rate 40 MSPS, unless otherwise noted.

#### <span id="page-9-1"></span>**AD9262BCPZ**





Figure 5. AD9262BCPZ Single-Tone FFT with  $f_{IN} = 1.2$  MHz





Figure 7. AD9262BCPZ Single-Tone SNR and SFDR vs. Input Amplitude with  $f_{IN} = 600$  kHz



Figure 8. AD9262BCPZ Two-Tone FFT with  $f_{IN1} = 1.8$  MHz,  $f_{IN2} = 2.1$  MHz



Figure 9. AD9262BCPZ Two-Tone SFDR/IMD3 vs. Input Amplitude with  $f_{IN1} = 1.8$  MHz,  $f_{IN2} = 2.1$  MHz

#### <span id="page-10-0"></span>**AD9262BCPZ-5**



Figure 10. AD9262BCPZ-5 Single-Tone FFT with  $f_{IN} = 1.2$  MHz



Figure 11. AD9262BCPZ-5 Single-Tone FFT with  $f_{IN} = 2.4$  MHz





Figure 13. AD9262BCPZ-5 Single-Tone SNR and SFDR vs. Input Amplitude with  $f_{IN}$  = 1.2 MHz



Figure 14. AD9262BCPZ-5 Two-Tone FFT with  $f_{IN1} = 1.8$  MHz,  $f_{IN2} = 2.1$  MHz



Figure 15. AD9262BCPZ-5 Two-Tone SFDR/IMD3 vs. Input Amplitude with  $f_{IN1} = 2.1$  MHz,  $f_{IN2} = 2.4$  MHz

#### <span id="page-11-0"></span>**AD9262BCPZ-10**



Figure 16. AD9262BCPZ-10 Single-Tone FFT with  $f_{IN} = 2.4$  MHz



Figure 17. AD9262BCPZ-10 Single-Tone FFT with  $f_{IN} = 4.2$  MHz



Figure 18. AD9262BCPZ-10 Single-Tone FFT with  $f_{IN} = 8.4$  MHz



Figure 19. AD9262BCPZ-10 Two-Tone FFT with  $f_{INI} = 2.1$  MHz,  $f_{IN2} = 2.4$  MHz



Figure 20. AD9262BCPZ-10 Two-Tone FFT with  $f_{INI} = 3.6$  MHz,  $f_{IN2} = 4.2$  MHz



Figure 21. AD9262BCPZ-10 Two-Tone FFT with  $f_{INI} = 7.2$  MHz,  $f_{IN2} = 8.4$  MHz



Figure 22. AD9262BCPZ-10 Single-Tone SNR/SFDR vs. Input Amplitude with  $f_{IN} = 2.4$  MHz



Figure 23. AD9262BCPZ-10 Two-Tone SFDR/IMD3 vs. Input Amplitude with  $f_{IN1} = 2.1$  MHz,  $f_{IN2} = 2.4$  MHz



Figure 24. AD9262BCPZ-10 SNR/SFDR vs. Output Data Rate with  $f_{IN} = 2.4$  MHz



Figure 25. AD9262BCPZ-10 SNR/SFDR vs. Input Frequency



Figure 26. AD9262BCPZ-10 SFDR/SNR vs. Temperature with  $f_{IN} = 2.4$  MHz





<span id="page-13-0"></span>Figure 28. AD9262BCPZ-10 Single-Tone SNR vs. PLL Divide Ratio



# <span id="page-14-0"></span>EQUIVALENT CIRCUITS



Figure 30. Equivalent Analog Input Circuit



<span id="page-14-1"></span>Figure 31. Equivalent Clock Input Circuit



Figure 32. Equivalent SDIO Input Circuit



Figure 33. Equivalent SCLK Input Circuit



Figure 34. Equivalent CSB Input Circuit



Figure 35. Equivalent Digital Output Circuit



Figure 36. Equivalent VREF Circuit

### <span id="page-15-0"></span>THEORY OF OPERATION

The AD9262 uses a continuous time Σ- $Δ$  modulator to convert the analog input to a digital word. The digital word is processed by the decimation filter and rate-adjusted by the sample rate converter (se[e Figure 37\)](#page-15-2). The modulator consists of a continuous time loop filter preceding a quantizer that samples at  $f_{\text{MOD}} =$ 640 MSPS. This produces an oversampling ratio (OSR) of 32 for a 10 MHz input bandwidth. The output of the quantizer is fed back to a DAC that ideally cancels the input signal. The incomplete input cancellation residue is filtered by the loop filter and is used to form the next quantizer sample.



<span id="page-15-2"></span>The quantizer produces a nine-level digital word. The quantization noise is spread uniformly over the Nyquist band (se[e Figure 38\)](#page-15-3), but the feedback loop causes the quantization noise present in the nine-level output to have a nonuniform spectral shape. This noise-shaping technique (see [Figure 39\)](#page-15-4) pushes the in-band noise out of band; therefore, the amount of quantization noise in the frequency band of interest is minimal.

The digital decimation filter that follows the modulator removes the large out-of-band quantization noise (see [Figure 40\)](#page-15-5), while also reducing the data rate from f<sub>MOD</sub> to f<sub>MOD</sub>/16. If the internal PLL is enabled, the sample rate converter generates samples at the same frequency as the input clock frequency. If the internal PLL is disabled, the sample rate converter can be programmed to give an output frequency that is a divide ratio of the modulator clock. The sample rate converter is designed to attenuate images outside the band of interest (se[e Figure 41\)](#page-15-6).

<span id="page-15-4"></span><span id="page-15-3"></span>

<span id="page-15-5"></span>

#### <span id="page-15-6"></span><span id="page-15-1"></span>**ANALOG INPUT CONSIDERATIONS**

The continuous time modulator removes the need for an antialias filter at the input to the AD9262. A discrete time converter aliases signals around the sample clock frequency and its multiples to the band of interest (se[e Figure 42\)](#page-15-7). Therefore, an external antialias filter is needed to reject these signals.



Figure 42. Discrete Time Converter

<span id="page-15-7"></span>In contrast, the continuous time  $\Sigma$ - $\Delta$  modulator used within the AD9262 has inherent antialiasing. The antialiasing property results from sampling occurring at the output of the loop filter (see [Figure 43\)](#page-15-8), and thus aliasing occurs at the same point in the loop as quantization noise is injected; aliases are shaped by the same mechanism as quantization noise. The quantization noise transfer function, NTF(f), has zeros in the band of interest and in all alias bands because NTF(f) is a discrete time transfer function, whereas the loop filter transfer function, LF(f), is a continuous time transfer function, which introduces poles only in the band of interest. The signal transfer function, being the product of NTF(f) and LF(f), only has zeros in alias bands and therefore suppresses all aliases.



<span id="page-15-8"></span>Figure 43. Continuous Time Converter

#### **Input Common Mode**

The analog inputs of the AD9262 are not internally dc biased. In ac-coupled applications, the user must provide this bias externally. Setting the device such that  $V_{CM} = AVDD$  is recommended for optimum performance. The analog inputs are 500 Ω resistors, and the internal reference loop aims to develop 0.5 V across each input resistor (see [Figure 44\)](#page-16-0). With 0 V differential input, the driver sources 1 mA into each analog input.



#### <span id="page-16-0"></span>**Differential Input Configurations**

The AD9262 can also be configured for differential inputs. The ADA4937-2 differential driver provides excellent performance and a flexible interface to the ADC. The output common-mode voltage of the ADA4937-2 is easily set by connecting AVDD to the  $V_{OCM2}$  pin of the ADA4937-2 (se[e Figure 45\)](#page-16-1). The noise and linearity of the ADA4937-2 need important consideration because the system performance may be limited by the ADA4937-2.



Figure 45. Differential Input Configuration Using the ADA4937-2

<span id="page-16-1"></span>For frequencies offset from dc, where SNR is a key parameter, differential transformer coupling is the recommended input configuration. An example is shown in [Figure 46.](#page-16-2) The center tap of the secondary winding of the transformer is connected to AVDD to bias the analog input.

The signal characteristics must be considered when selecting a transformer. Most RF transformers saturate at frequencies below a couple of megahertz (MHz), and excessive signal power can cause core saturation, which leads to distortion.



#### <span id="page-16-2"></span>**Voltage Reference**

A stable and accurate 0.5 V voltage reference is built into the AD9262. The reference voltage should be decoupled to minimize the noise bandwidth using a  $10 \mu$ F capacitor. The reference is used to generate a bias current into a matched resistor such that, when used to bias the current in the feedback DAC, a voltage of AVDD − 0.5 V is developed at the internal side of the input resistors (se[e Figure 47\)](#page-16-3). The current bias circuit should also be decoupled on the CFILT pin with a 10 μF capacitor. For this reason, the VREF voltage should always be 0.5 V.



#### <span id="page-16-3"></span>**Internal Reference Connection**

To minimize thermal noise, the internal reference on the AD9262 is an unbuffered 0.5 V. It has an internal 10 kΩ series resistor, which, when externally decoupled with a 10 μF capacitor, limits the noise (se[e Figure 48\)](#page-16-4). The unbuffered reference should not be used to drive any external circuitry. The internal reference is used by default and when Serial Register 0x18[6] is reset.



<span id="page-16-4"></span>Figure 48. Internal Reference Configuration

#### **External Reference Operation**

If an external reference is desired, the internal reference can be disabled by setting Serial Register 0x18[6] high. [Figure 49 s](#page-17-1)hows an application using th[e ADR130B a](http://www.analog.com/ADR130)s a stable external reference.



Figure 49. External Reference Configuration

#### <span id="page-17-1"></span><span id="page-17-0"></span>**CLOCK INPUT CONSIDERATIONS**

The AD9262 offers two modes of sourcing the ADC sample clock (CLK+ and CLK−). The first mode uses an on-chip clock multiplier that accepts a reference clock operating at the lower input frequency. The on-chip phase-locked loop (PLL) then multiplies the reference clock to a higher frequency, which is then used to generate all the internal clocks required by the ADC

The clock multiplier provides a high quality clock that meets the performance requirements of most applications. Using the on-chip clock multiplier removes the burden of generating and distributing the high speed clock.

The second mode bypasses the clock multiplier circuitry and allows the clock to be directly sourced. This mode enables the user to source a very high quality clock directly to the  $\Sigma$ - $\Delta$ modulator. Sourcing the ADC clock directly may be necessary in demanding applications that require the lowest possible ADC output noise. Se[e Figure 28,](#page-13-0) which shows the degradation in SNR performance for the various PLL settings.

In either case, when using the on-chip clock multiplier or sourcing the high speed clock directly, it is necessary that the clock source have low jitter to maximize the ADC noise performance. High speed, high resolution ADCs are sensitive to the quality of the clock input. As jitter increases, the SNR performance of the AD9262 degrades from that specified i[n Table 2.](#page-3-7) The jitter inherent in the part due to the PLL root sum squares with any external clock jitter, thereby degrading performance. To prevent jitter from dominating the performance of the AD9262, the input clock source should be no greater than 1 ps rms of jitter.

The CLK± inputs are self-biased to 450 mV (se[e Figure 31\)](#page-14-1); if the inputs are dc-coupled, it is important to maintain the specified 450 mV input common-mode voltage. Each input pin can safely swing from 200 mV p-p to 1 V p-p single-ended about the 450 mV common-mode voltage. The recommended clock inputs are CMOS or LVPECL.

The specified clock rate of the  $\Sigma$ - $\Delta$  modulator, f<sub>MOD</sub>, is 640 MHz. The clock rate possesses a direct relationship to the available input bandwidth of the ADC.

Bandwidth =  $f_{MOD} \div 64$ 

In either case, using the on-chip clock multiplier to generate the Σ-Δ modulator clock rate or directly sourcing the clock, any deviation from 640 MHz results in a change in input bandwidth. The input range of the clock is limited to 640 MHz  $\pm$  5%. In situations where the AD9262 loses its clock and then later regains it, it is important that the sample rate converter be reset and reprogrammed before the desired output data rate is achieved.

#### **Direct Clocking**

The default configuration of the AD9262 is for direct clocking where the PLL is bypassed[. Figure 50](#page-17-2) shows one preferred method for clocking the AD9262. A low jitter clock source is converted from a single-ended signal to a differential signal using an RF transformer. The back-to-back Schottky diodes across the secondary side of the transformer limits clock excursions into the AD9262 to approximately 0.8 V p-p differential. This helps prevent the large voltage swings of the clock from feeding through to other portions of the AD9262 while preserving the fast rise and fall times of the signal, which are critical to achieving low jitter.



Figure 50. Transformer-Coupled Differential Clock

<span id="page-17-2"></span>If a differential clock is not available, the AD9262 can be driven by a single-ended signal into the CLK+ terminal with the CLK− terminal ac-coupled to ground[. Figure 51](#page-17-3) shows the circuit configuration.



Figure 51. Single-Ended Clock

<span id="page-17-3"></span>Another option is to ac couple a differential LVPECL signal to the sample clock input pins, as shown i[n Figure 52.](#page-17-4) Th[e AD951x](http://www.analog.com/en/prod/0%2C2877%2CAD9510%2C00.html)  family of clock drivers is recommended because it offers excellent jitter performance.



<span id="page-17-4"></span>

#### **Internal PLL Clock Distribution**

The alternative clocking option available on the AD9262 is to apply a low frequency reference clock and use the on-chip clock multiplier to generate the high frequency  $f_{\text{MOD}}$  rate. The internal clock architecture is shown i[n Figure 53.](#page-18-0)



Figure 53. Internal Clock Architecture

<span id="page-18-0"></span>The clock multiplication circuit operates such that the VCO outputs a frequency, f<sub>VCO</sub>, equal to the reference clock input multiplied by N.

 $f_{VCO} = (CLK\pm) \times (N)$ 

where N is the PLL multiplication (PLLMULT) factor.

The  $\Sigma$ - $\Delta$  modulator clock frequency, f<sub>MOD</sub>, is equal to

 $f_{MOD} = f_{VCO} \div 2$ 

The reference clock, CLK±, is limited to 30 MHz to 160 MHz when configured to use the on-chip clock multiplier. Given the input range of the reference clock and the available multiplication factors, the f<sub>VCO</sub> is approximately 1280 MHz. This results in the desired f<sub>MOD</sub> rate of 640 MHz with a 50% duty cycle.

Before the PLL enable register bit (PLLENABLE) is set, the PLL multiplication factor should be programmed into Register 0x0A[5:0]. After setting the PLLENABLE bit, the PLL locks and reports a locked state in Register 0x0A[7]. If the PLL multiplication factor is changed, the PLL enable bit should be reset and set again. Some common clock multiplication factors are shown in [Table 11.](#page-19-1) 

The recommended sequence for enabling and programming the on-chip clock multiplier is shown in [Table 9.](#page-18-1)

<span id="page-18-1"></span>**Table 9. Sequence for Enabling and Programming the PLL** 

<b>Step</b>	Procedure
	Apply a reference clock to the $CLK±$ pins.
2	Program the PLL multiplication factor in Register 0x0A[5:0]. See Table 10.
3	Enable the PLL; Register $0x09 = 04$ (decimal).
	Enable PLL autoband select.
5	Initiate an SRC reset; Register $0x101[5:0] = 0$ .
6	Set SRC to desired value via Register 0x101[5:0].

#### **PLL Autoband Select**

The PLL VCO has a wide operating range that is covered by overlapping frequency bands. For any desired VCO output frequency, there are multiple valid PLL band select values. The AD9262 possesses an automatic PLL band select feature on chip that determines the optimal PLL band setting. This feature can be enabled by writing to Register 0x0A[6]and is the recommended configuration with the PLL clocking option. When the device is taken out of sleep or standby mode, Register 0x0A[6] must be toggled to reinitiate the autoband detect. Se[e Table 9 f](#page-18-1)or information about enabling the autoband select along with configuring the PLL.



#### <span id="page-18-2"></span>**Table 10. PLL Multiplication Factors**

CLK <sub>±</sub> (MHz)	0x0A[5:0] (PLLMULT)	f <sub>vco</sub> (MHz)	f <sub>MOD</sub> (MHz)	BW (MHz)
30.72	42	1290.24	645.12	10.08
39.3216	32	1258.29	629.15	9.83
52.00	25	1300.00	650.00	10.16
61.44	21	1290.24	645.12	10.08
76.80	17	1305.60	652.80	10.20
78.00	17	1326.00	663.00	10.36
78.6432	16	1258.29	629.15	9.83
89.60	15	1344.00	672.00	10.50
92.16	14	1290.24	645.12	10.08
122.88	10	1228.80	614.40	9.60
134.40	10	1344.00	672.00	10.50
153.60	8	1228.80	614.40	9.60
157.2864	8	1258.29	629.15	9.83

<span id="page-19-1"></span>**Table 11. Common Modulator Clock Multiplication Factors** 

#### **Jitter Considerations**

The aperture jitter requirements for continuous time  $\Sigma$ - $\Delta$  converters may be more forgiving than Nyquist rate converters. The continuous time Σ-Δ architecture is an oversampled system and to accurately represent the analog input signal to the ADC, a large number of output samples must be averaged together. As a result, the jitter contribution from each sample is root sum squared, resulting in a more subtle impact on noise performance as compared to Nyquist converters where aperture jitter has a direct impact on each sampled output.

In the block diagram of the continuous time  $\Sigma$ - $\Delta$  modulator (see [Figure 37\)](#page-15-2), the two building blocks most susceptible to jitter are the quantizer and the DAC. The error introduced through the sampling process is reduced by the loop gain and shaped in the same way as the quantization noise and, therefore, its effect can be neglected. On the contrary, the jitter error associated with the DAC directly adds to the input signal, thus increasing the in-band noise power and degrading the modulator performance. The SNR degradation due to jitter can be represented by the following equation.

 $SNR = -20 \log (2 \pi f_{analog} t_{iitter\ rms}) dB$ 

where  $f_{analog}$  is the analog input frequency and  $t_{jitter\_rms}$  is the jitter.

The SNR performance of the AD9262 remains constant within the input bandwidth of the converter, from DC to 10 MHz. Therefore, the minimal jitter specification is determined at the highest input frequency. From the calculation, the aperture jitter of the input clock must be no greater than 1 ps to achieve optimal SNR performance.

#### <span id="page-19-0"></span>**POWER DISSIPATION AND STANDBY MODE**

The AD9262 power consumption can be further reduced by configuring the chip in channel power-down, standby, or sleep mode. The low power modes turn off internal blocks of the chip, including the reference. As a result, the wake-up time is dependent on the amount of circuitry that is turned off. Fewer internal circuits that are powered down result in proportionally shorter wake-up time. The low power modes are shown in [Table 12.](#page-19-2)  In the standby mode, all clock related activity and the output channels are disabled. Only the references and CMOS outputs remain powered up to ensure a short recovery and link integrity. During sleep mode, all internal circuits are powered down, putting the device into its lowest power mode, and the CMOS outputs are disabled.

Each ADC channel can be independently powered down or both channels can be set simultaneously by writing to the channel index, Register 0x05[1:0].

<span id="page-19-2"></span>**Table 12. Low Power Modes** 

Mode	0x08[1:0]	<b>Analog Circuitry</b>	Clock	<b>Ref</b>
Normal	0x0	On	On	On
Power-Down	0x1	Off	On	On
Standby	0x2	Off	Off	On
Sleep	0x3	Off	Off	Off

#### <span id="page-20-0"></span>**DIGITAL ENGINE**

#### **Bandwidth Selection**

The digital engine (see [Figure 54\)](#page-20-1) selects the decimation signal bandwidth by cascading third-order sinc (sinc<sup>3</sup>) decimate-by-2 filters. For a 10 MHz signal band, no filters are cascaded; for a 5 MHz signal band, a single filter is used; and for a 2.5 MHz signal band, the 5 MHz filter is cascaded with a second filter. Depending on the signal bandwidth, this drops the data rate into the fixed decimation filter. As a result, lower signal bandwidth options result in lower power. Bandwidth selection is determined by setting Serial Register 0x0F[6:5]. [Table 13 s](#page-20-2)ummarizes the available bandwidth options.

#### <span id="page-20-2"></span>**Table 13. Output Bandwidth Options**



#### **Decimation Filters**

The fixed decimation filters reduce the sample rate from 640 MSPS to 40 MSPS. A fixed frequency low-pass filter is used to define the signal band. This filter incorporates magnitude equalization for the droop of the preceding sinc decimation filters and the sinc filters of the sample rate converter. [Table 14 a](#page-20-3)n[d Table 15](#page-20-4)  detail the coefficients for the DEC4 and LPF/EQZ filters. Sinc filter implementation for all sinc filters is standard.

#### <span id="page-20-3"></span>**Table 14. DEC4 Filter Coefficients**



#### <span id="page-20-4"></span>**Table 15. LPF/EQZ Filter Coefficients**



<span id="page-20-1"></span>

Figure 54. Digital Engine

#### **Sample Rate Converter**

The sample rate converter (SRC) allows the flexibility of a user-defined output sample rate, enabling a more efficient and direct interface to the digital receiver blocks.

The sample rate converter performs an interpolation and resampling procedure to provide an output data rate of 20 MSPS to 168 MSPS. [Table 16 a](#page-21-0)nd [Table 17 d](#page-21-1)etail the coefficients for the INT1 and INT2 filters. The sinc filters are a standard implementation.

The relationship between the output sample rate and the  $\Sigma$ - $\Delta$ modulator clock rate is expressed as follows:

 $f_{OUT} = f_{MOD} \div K_{OUT}$ 

[Table 18 s](#page-21-2)hows the available K<sub>OUT</sub> conversion factors.

<span id="page-21-0"></span>



#### <span id="page-21-1"></span>**Table 17. INT2 Filter Coefficients**



If the main clocking source of the AD9262 is provided by the PLL, it is important, once the PLL has been programmed and locked, to initiate an SRC reset before programming the desired  $K<sub>OUT</sub> factor. This is done by first writing  $0x101[5:0] = 0$  and$ then rewriting to the same register with the appropriate  $K<sub>OUT</sub>$ value. In addition, if the AD9262 loses its clock source and then later regains it, an SRC reset should be initiated.

Table 18. SRC Conversion Factors					
0x101[5:0]	<b>Kout</b>	0x101[5:0]	$K_{\text{OUT}}$	0x101[5:0]	<b>Kout</b>
0	<b>SRC</b> reset	22	11	44	22
1	4	23	11.5	45	22.5
$\overline{2}$	4	24	$12 \overline{ }$	46	23
3	4	25	12.5	47	23.5
4	4	26	13	48	24
5	4	27	13.5	49	24.5
6	4	28	14	50	25
$\overline{7}$	4	29	14.5	51	25.5
8	4	30	15	52	26
9	4.5	31	15.5	53	26.5
10	5	32	16	54	27
11	5.5	33	16.5	55	27.5
12	6	34	17	56	28
13	6.5	35	17.5	57	28.5
14	7	36	18	58	29
15	7.5	37	18.5	59	29.5
16	8	38	19	60	30
17	8.5	39	19.5	61	30.5
18	9	40	20	62	31
19	9.5	41	20.5	63	31.5
20	10	42	21		
21	10.5	43	21.5		

<span id="page-21-2"></span>**Table 18. SRC Conversion Fact** 

#### **Cascaded Filter Responses**

The cascaded filter responses for the three signal bandwidth settings are for a 160 MSPS output data rate, as shown i[n Figure 55,](#page-22-1) [Figure 56,](#page-22-2) an[d Figure 57.](#page-22-3)

<span id="page-22-1"></span>

<span id="page-22-3"></span><span id="page-22-2"></span>Figure 57. 2.5 MHz Signal Bandwidth, 160 MSPS

#### <span id="page-22-0"></span>**DC AND QUADRATURE ERROR CORRECTION (QEC)**

In direct conversion or other quadrature systems, mismatches between the real (I) and imaginary (Q) signal paths cause frequencies in the positive spectrum to image into the negative spectrum and vice versa. From an RF point of view, this is equivalent to information above the LO frequency interfering with information below the LO frequency, and vice versa. These mismatches may occur from gain and/or phase mismatches in the analog quadrature demodulator or in any components in the ADC signal chain itself. In a single-carrier zero-IF system where the carrier has been placed symmetrically around dc, this causes self-distortion of the carrier as the two sidebands fold onto one another and degrade the EVM of the signal.

In a multicarrier communication system, this can be even more problematic because carriers of widely different power levels can interfere with one another. For example, a large carrier centered at +f1 can have an image appear at –f1 that can be larger than the desired carrier at this frequency.

The integrated quadrature error correction (QEC) algorithm of the AD9262 attempts to measure and correct the amplitude and phase imbalances of the I and Q signal paths to achieve higher levels of image suppression than is achievable by analog means alone. These errors can be corrected in an adapted manner where the I and Q gain and quadrature phase mismatches are constantly estimated and corrected. This allows changes in the mismatches due to slow supply and temperature changes to be constantly tracked.

The quadrature errors are corrected in a frequency independent manner on the AD9262; therefore, systems with significant mismatch in the baseband chain may have reduced image suppression. The AD9262 QEC still corrects the systematic imbalances.

The convergence time of the QEC algorithm is dependent on the statistics of the input signal. For large signals and large imbalance errors, this convergence time is typically less than two million samples of the AD9262 output data rate.

#### **LO Leakage (DC) Correction**

In a direct conversion receiver subsystem, LO to RF leakage of the quadrature modulator shows up as dc offsets at baseband. These offsets are added to dc offsets in the baseband signal paths, and both contribute to a carrier at dc. In a zero-IF receiver, this dc energy can cause problems because it appears in band of a desired channel. As part of the AD9262 QEC function, the dc offset is suppressed by applying a low frequency notch filter to form a null around dc. The 3 dB bandwidth of this notch filter vs. the AD9262 output data rates is shown in [Figure 58.](#page-23-1) 



<span id="page-23-1"></span>Figure 58. DC Correction Low Frequency Notch Filter 3 dB Bandwidth vs. Output Data Rate

In applications where constant tracking of the dc offsets and quadrature errors are not needed, the algorithms can be independently frozen to save power. When frozen, the image and LO leakage (dc) correction are still performed, but changes are no longer tracked. Register 0x112[5:3] disables the respective correction when frozen.

The quadrature gain, quadrature phase, and dc correction algorithms can also be disabled independently for system debugging or to save power by setting Register 0x112[2:0].

The default configuration on the AD9262 has the QEC and dc correction blocks disabled, and Register 0x101[6] must be pulled high to enable the correction blocks. After the QEC is enabled and a correction value has been calculated, the value remains active as long as any one of the QEC functions (DC, gain, or phase correction) is used.

#### **QEC and DC Correction Range**

[Table 19 g](#page-23-2)ives the minimum and maximum correction ranges of the algorithms on the AD9262 If the mismatches are greater than these ranges, an imperfect correction results.

<span id="page-23-2"></span>



#### <span id="page-23-0"></span>**DIGITAL OUTPUTS**

#### **Digital Output Format**

The AD9262 offers a variety of digital output formats for ease of system integration. The digital output on each channel consists of 16 data bits and an output clock signal (DCO) for data latching. The data bits can be configured for offset binary, twos complement, or Gray code by writing to Register 0x14[1:0]. In addition, the voltage swing of the digital outputs can be configured to 3.3 V TTL levels or a reduced voltage swing of 1.8 V by accessing Register 0x14[7]. When 3.3 V voltage levels are desirable, the DRVDD power supply must be set to 3.3 V.

#### **Interleaved Outputs**

The AD9262 has the added feature of interleaving Channel A and Channel B data onto one 16-bit bus. This feature is available for integer values of K<sub>OUT</sub> greater than 8 and does not apply to half values of K<sub>OUT</sub>. The interleave function can be accessed by writing to Register 0x14[5]. The data from both Channel A and Channel B are interleaved and presented on the Channel A bus, whereas the Channel B bus is internally grounded. Channel A is sampled on the falling edge of DCO and Channel B on the rising edge. The output of Channel A and Channel B can be interchanged by inverting the DCO clock, Register 0x16[7]. In this case, Channel B is sampled on the falling edge and Channel A on the rising edge.



Figure 59. Interleaved Output Mode

#### <span id="page-23-3"></span>**Overrange (OR) Condition**

The ORA and ORB (ORx) pins serve as indicators for an overrange condition. The ORx pins are triggered by in-band signals that exceed the full-scale range of the ADC. In addition, the AD9262 possesses out-of-band gain above 10 MHz. Therefore, a large out-of-band signal may trip an overrange condition.

The ORx pins are synchronous outputs that are updated at the output data rate. Ideally, ORx should be latched on the falling edge of DCO to ensure proper setup-and-hold time. However, because an overrange condition typically extends well beyond one clock cycle (that is, it does not toggle at the DCO rate) data can usually be successfully detected on the rising edge of DCO or monitored asynchronously.

The AD9262 has two trip points that can trigger an overrange condition: analog and digital. The analog trip point is located in the modulator ,and the second trip point is in the digital engine. In normal operation, it is possible for the analog trip point to toggle the ORx pin for a number of clock cycles as the analog input approaches full scale. Because the ORx pin is a pulse-width modulated (PWM) signal, as the analog input increases in amplitude, the duration of overrange pin toggling increases. Eventually, when the ORx pin is high for an extended period of time, the ADC is overloaded, whereby there is little correspondence between analog input and digital output.

The second trip point is in the digital block. If the input signal is large enough to cause the data bits to clip to its maximum fullscale level, an overrange condition occurs. The overrange trip point can be adjusted by specifying a threshold level.

[Table 20 s](#page-24-1)hows the corresponding threshold level in dBFS vs. register setting. If the input signal crosses this level, the ORx pin is set. In the case where 0x111[5:0] is set to all 0s, the threshold level is set to the maximum code of 32,76710. This feature provides a means of reporting the instantaneous amplitude as it crosses a user-provided threshold. This gives the user a sense of the signal level without needing to perform a full power measurement.

The user has the ability to select how the overrange conditions are reported, and this is controlled through Register 0x111 via AUTORST, OR\_IND, and ORTHRESH (se[e Table 21\)](#page-24-2). By enabling the AUTORST bit, Register 0x111[7], if an overrange occurs, the ADC automatically resets itself. The ORx pins remain high until the automatic reset has completed. If an analog trip

#### <span id="page-24-1"></span>**Table 20. OR Threshold Levels**

occurs, the modulator resets itself after 16 consecutive clock cycles of overrange.

If the AD9262 is used in a system that incorporates automatic gain control (AGC), the ORx signal can be used to indicate that the signal amplitude should be reduced. This may be particularly effective for use in maximizing the signal dynamic range if the signal includes high occurrence components that occasionally exceed full scale by a small amount.

#### <span id="page-24-0"></span>**TIMING**

The AD9262 provides a data clock out (DCO) pin to assist in capturing the data in an external register. The data outputs are valid on the rising edge of DCO, unless changed by setting Serial Register 0x16[7] (see the [Serial Port Interface \(SPI\)](#page-25-0)  section). Se[e Figure 2 f](#page-6-7)or a graphical timing description.



#### <span id="page-24-2"></span>**Table 21. ORx Conditions**



# <span id="page-25-0"></span>SERIAL PORT INTERFACE (SPI)

The AD9262 serial port interface (SPI) allows the user to configure the converter for specific functions or operations through a structured register space provided inside the ADC. This provides the user added flexibility and customization depending on the application. Addresses are accessed via the serial port and can be written to or read from via the port. Memory is organized into bytes that are further divided into fields, as documented in th[e Memory Map s](#page-29-0)ection. For detailed operational information, see the AN-877 Application Note, Interfacing to High Speed ADCs via SPI.

#### <span id="page-25-1"></span>**CONFIGURATION USING THE SPI**

As summarized i[n Table 22,](#page-25-3) three pins define the SPI of this ADC. The SCLK pin synchronizes the read and write data presented to the ADC. The SDIO pin allows data to be sent and read from the internal ADC memory map registers. The CSB pin is an active low control that enables or disables the read and write cycles.

#### <span id="page-25-3"></span>**Table 22. Serial Port Interface Pins**



The falling edge of CSB in conjunction with the rising edge of SCLK determines the start of the framing[. Figure 60 a](#page-25-2)n[d Table 23](#page-25-4)  provide an example of the serial timing and its definitions.

Other modes involving CSB are available. CSB can be held low indefinitely to permanently enable the device (this is called streaming). CSB can stall high between bytes to allow for additional external timing. When CSB is tied high, SPI functions are placed in a high impedance mode.

During an instruction phase, a 16-bit instruction is transmitted. Data follows the instruction phase, and the length is determined by the W0 bit and the W1 bit. All data is composed of 8-bit words. The first bit of each individual byte of serial data indicates whether a read or write command is issued. This allows the serial data input/output (SDIO) pin to change direction from an input to an output.

In addition to word length, the instruction phase determines if the serial frame is a read or write operation, allowing the serial port to be used to both program the chip and to read the contents of the on-chip memory. If the instruction is a readback operation, performing a readback causes the serial data input/output (SDIO) pin to change direction from an input to an output at the appropriate point in the serial frame.

Data can be sent in MSB-first or in LSB-first mode. MSB first is the default setting on power-up and can be changed via the configuration register. For more information, see the AN-877 Application Note, Interfacing to High Speed ADCs via SPI.

#### <span id="page-25-4"></span>**Table 23. SPI Timing Diagram Specifications**



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<span id="page-25-2"></span>

Figure 60. Serial Port Interface Timing Diagram

#### <span id="page-26-0"></span>**HARDWARE INTERFACE**

The pins described in [Table 22 c](#page-25-3)omprise the physical interface between the programming device of the user and the serial port of the AD9262. The SCLK and CSB pins function as inputs when using the SPI interface. The SDIO pin is bidirectional, functioning as an input during write phases and as an output during readback.

The SPI interface is flexible enough to be controlled by either PROM or PIC microcontrollers. This provides the user with the ability to use an alternate method to program the ADC. One such method is described in detail in the AN-812 Application Note, MicroController-Based Serial Port Interface (SPI) Boot Circuit.

# <span id="page-27-0"></span>APPLICATIONS INFORMATION

#### <span id="page-27-1"></span>**FILTERING REQUIREMENT**

The need for antialias protection often requires one or two octaves for a transition band, which reduces the usable bandwidth of a Nyquist converter to between 25% and 50% of the available bandwidth. A CT Σ-Δ converter maximizes the available signal bandwidth by forgoing the need for an anti-aliasing filter because the architecture possesses inherent anti-aliasing. Although a high order, sharp cutoff antialiasing filter may not be necessary because of the unique characteristics of the architecture, a low order filter may still be required to precede the ADC for out-of-band signal handling.

Depending on the application and the system architecture, this low order filter may or may not be necessary. The signal transfer function (STF) of a continuous time feedforward ADC usually contains out-of-band peaks. Because these STF peaks are typically one or two octaves above the pass-band edge, they are not problematic in applications where the bulk of the signal energy is in or near the pass band. However, in applications with large far-out interferers, it is necessary to either add a filter to attenuate these problematic signals or to allocate some of the ADC dynamic range to accommodate them.

[Figure 61 s](#page-27-2)hows the normalized STF of the AD9262 CT Σ-Δ converter. The figure shows out-of-band peaking beyond the band edge of the ADC. Within the 10 MHz band of interest, the STF is maximally flat with less than 0.1 dB of gain. Maximum peaking occurs at 60 MHz with 10 dB of gain. To put this into perspective, for a fixed input power, a 5 MHz in-band signal appears at −5 dBFS, a 25 MHz tone appears at −2 dBFS and 60 MHz tone at +5 dBFS. Because the maximum input to the ADC is −2 dBFS, large out-of-band signals can quickly saturate the system. This implies that, under these conditions, the digital outputs of the ADC no longer accurately represent the input. See the [Overrange \(OR\) Condition s](#page-23-3)ection for details on overrange detection and recovery.

<span id="page-27-2"></span>

[Figure 61 s](#page-27-2)hows the gain profile of the AD9262, and this can be interpreted as the level at which the signal power should be scaled back to prevent an overload condition. This is the ultimate trip point and before this point is reached, the in-band noise (IBN) slowly degrades. As a result, it is recommended that the low-pass filter be designed to match the profile o[f Figure 62,](#page-27-3) which shows the maximum input signal for a 3 dB degradation of in-band noise. The input signal is attenuated to allow only 3 dB of noise degradation over frequency.

The noise performance is normalized to a −2 dBFS in-band signal. The AD9262 STF and NTF are flat within the band of interest and should result in almost no change in input level and IBN. Beyond the bandwidth of the AD9262, out-of-band peaking adds gain to the system, therefore requiring the input power to be scaled back to prevent in-band noise degradation. The input power is scaled back to a point where only 3 dB of noise degradation is allowed, therefore resulting in the response shown in [Figure 62.](#page-27-3) 



Figure 62. Maximum Input Level for 3 dB Noise Degradation

<span id="page-27-3"></span>An example third-order, low-pass Chebyshev II type filter is shown in [Figure 63.](#page-27-4) [Table 24 s](#page-28-0)ummarizes the components and manufacturers used to build the circuit.



<span id="page-27-4"></span>Figure 63. Third-Order, Low-Pass Chebyshev II Filter

Table 27. Chebyshev II Flittle Components			
<b>Parameter</b>	Value	<b>Unit</b>	Manufacturer
$\mathsf{C}1$	18	рF	Murata GRM188 series, 0603
l 1	180	nH	Coil Craft 0603 LS, 2%
C <sub>2</sub>	390	pF	Murata GRM188 series, 0603
	150	pF	Murata GRM188 series, 0603

<span id="page-28-0"></span>**Table 24. Chebyshev II Filter Components** 

In addition to matching the profile o[f Figure 62,](#page-27-3) group delay and channel matching are important filter design criteria. Low tolerance components are highly recommended for improved channel matching, which translates to minimal degradation in image rejection for quadrature systems.

# <span id="page-29-0"></span>MEMORY MAP

#### **Table 25. Memory Map**



#### <span id="page-29-1"></span>**MEMORY MAP DEFINITIONS**

#### **Table 26. Memory Map Definitions**





#### <span id="page-31-0"></span>OUTLINE DIMENSIONS **0.60 MAX 9.00 BSC SQ 0.60 MAX PIN 1 INDICATOR** Ġ. **64 49 1 48 PIN 1 INDICATOR** annanananan **0.50 BSC 6.35 6.20 SQ BSC SQ TOP VIEW 8.75 EXPOSED PAD (BOTTOM VIEW) 6.05 0.50 0.40 33 16** 7 **17 32 0.30 0.25 MIN 7.50 REF 1.00 12° MAX 0.80 MAX 0.65 TYP 0.85 FOR PROPER CONNECTION OF THE EXPOSED PAD, REFER TO THE PIN CONFIGURATION AND FUNCTION DESCRIPTIONS SECTION OF THIS DATA SHEET. 0.05 MAX 0.80** + 1 .................... **0.02 NOM 0.30 SEATING PLANE 0.20 REF 0.23 0.18 091707-C COMPLIANT TO JEDEC STANDARDS MO-220-VMMD-4**

Figure 64. 64-Lead Lead Frame Chip Scale Package [LFCSP\_VQ] 9 mm × 9 mm Body, Very Thin Quad (CP-64-4) Dimensions shown in millimeters

#### <span id="page-31-1"></span>**ORDERING GUIDE**



<span id="page-31-2"></span> $1 Z =$  RoHS Compliant Part.

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