# **RICHTEK**

## **2.4A, 36V, 100kHz Asynchronous Step-Down Converter with Load Line Compensation**

## **General Description**

The RT6266 is a high-efficiency, monolithic asynchronous step-down DC/DC converter that can deliver up to 2.4A output current from a 7.5V to 36V input supply. The RT6266's current mode architecture with internal compensation is optimized for 5V car charger application over a wide range of loads and output capacitors. Cycle-by-cycle current limit provides protection against shorted outputs and soft-start eliminates input current surge during start-up. The RT6266 also provides output over voltage protection output under voltage protection and thermal shutdown protection. The low current  $( $3\mu$ A)$  shutdown mode provides output disconnect, enabling easy power management in battery-powered systems. The RT6266 is available in a SOP-8 (Exposed Pad) package.

## **Ordering Information**

### RT6266□□

Lead Plating System G : Green (Halogen Free and Pb Free) Package Type SP: SOP-8(Exposed Pad-Option 2)

Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes.

### **Features**

- **2% High Accuracy Feedback Voltage**
- **7.5V to 36V Input Voltage Range**
- **2.4A Continuous Output Current (2.7A Peak)**
- **CC/CV Mode Control**
- **Adjustable Load Line Compensation**
- **Short Circuit Protection**
- **Integrated N-MOSFET Switches**
- **Current Mode Control**
- **Fixed Frequency Operation : 100kHz**
- **Programmable Output Current Limit**
- **110m Internal Power MOSFET Switch**
- **Lowe EMI signature**
- **Up to 95% Efficiency**
- **Cycle-by-Cycle Over Current Protection**
- **Input Under Voltage Lockout**
- **Output Under Voltage Protection**
- **Thermal Shutdown Protection**

### **Applications**

- USB Power Supplies
- Automotive Cigarette Lighter Adapters
- Power Supply for Linear Chargers
- DC/DC Converters with Current Limited

### **Marking Information**

RT6266GSP : Product Number YMDNN : Date Code

## **Simplified Application Circuit**



RT6266 GSPYMDNN

## **Pin Configurations**

(TOP VIEW)



SOP-8 (Exposed Pad)

## **Functional Pin Description**



## **RICHTEK** RT6266

## **Function Block Diagram**



## **Operation**

The RT6266 is a constant frequency, current mode asynchronous step-down converter with CC and CV control. In normal operation, the high side N-MOSFET is turned on when the S-R latch is set by the oscillator and is turned off when the current comparator resets the S-R latch. While the N-MOSFET is turned off, the inductor current conducts through the external diode.

### **Error Amplifier**

The error amplifier adjusts its output voltage by comparing the feedback signal (VFB) with the internal 0.8V reference. When the load current increases, it causes a drop in the feedback voltage relative to the reference, the error amplifier's output voltage then rises to allow higher inductor current to match the load current.

### **Oscillator**

The internal oscillator runs at fixed frequency 100kHz. In short circuit condition, the frequency is reduced to 20kHz for low power consumption.

#### **Internal Regulator**

The regulator provides low voltage power to supply the internal control circuits and the bootstrap power for high side gate driver.

#### **Enable**

The converter is turned on when the EN pin is higher than 1.4V and turned off when the EN pin is lower than 0.4V. Attach this pin to VIN with a 100k $\Omega$  pull up resistor for automatic startup.

### **Soft-Start (SS)**

An internal current source charges an internal capacitor to build a soft-start ramp voltage. The FB voltage will track the internal ramp voltage during soft-start interval. The typical soft-start time is 3.5ms.

### **Output Line Drop Compensation**

If the trace from RT6266 output terminator to the load is too long, there will be a voltage drop on the long trace which is variable with load current. RT6266 is capable of compensating the output voltage drop to keep a constant voltage at load, whatever the load current is. The output voltage is compensated by feeding a current to the top feedback resistance R1. The load line compensation gain can be programmed according to RSENSE and Rtrace values.





### **Output Over Voltage Protection (OVP)**

The V<sub>OUT</sub> Over Voltage is sensed by CSN pin. When  $CSN > 5.8V$ , the high side switch will be turned off immediately. When CSN < 5.5V, the driver will recovers to normal state automatically.

### **External Current Limit Protection**

The external current limit is set by outside resistance (RSENSE). The average current is limited according to the following equation :

SENSE Average Current\_Limit (A) =  $\frac{100 \text{mV}}{R_{\text{SENSE}}}$  $=$ 

### **Internal Current Limit Protection**

When the external R<sub>SENSE</sub> is too small and the external peak current is higher than 4.4A, the high-side switch will turn off immediately and then turn at the next clock cycle. The inductor's peak current will be limited at 4.4A by internal current limit.

### **Output Short-Circuit Protection**

When  $V_{\text{OUT}}$  is short (V<sub>FB</sub> < 0.3V), the short-circuit protection function can be started that restart the regulator cycle by cycle. The cycle time is set by the driver internally. The internal current limit time is t1 and the regulator off time is t2. The typically  $t1 = 5$ ms,  $t2 =$ 200ms.



### **Under Voltage Lockout (UVLO)**

To avoid mis-operation at low input voltage, when input voltage falls below 6.2V, and under voltage lockout is induced and the device is disabled.

### **Thermal Shutdown**

The over temperature protection function will shut down the switching operation when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately  $30^{\circ}$ C, the converter will automatically resume switching.

## **RICHTEK** RT6266

## **Absolute Maximum Ratings** (Note 1)



### **Recommended Operating Conditions** (Note 4)



## **Electrical Characteristics**

 $(V_{\text{IN}} = 12V, V_{\text{OUT}} = 5V, T_A = 25^{\circ}C,$  Load Current = 0A, unless otherwise specified)







**Note 1.** Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

**Note 2.**  $\theta_{JA}$  is measured at  $T_A = 25^\circ$ C on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package.

**Note 3.** Devices are ESD sensitive. Handling precaution recommended.

**Note 4.** The device is not guaranteed to function outside its operating conditions.

## **Typical Application Circuit**



## **Typical Operating Characteristics**









**Output Current vs. Temperature**





**RICHTEK** 











## **RICHTEK** RT6266

## **Application Information**

### **Output Voltage Setting**

The resistive divider allows the FB pin to sense the output voltage as shown in Figure 1.



Figure 1. Output Voltage Setting

The output voltage is set by an external resistive voltage divider according to the following equation :

 $V_{\text{OUT}} = V_{\text{REF}} \left( 1 + \frac{R1}{R2} \right)$ 

Where  $V_{\text{RFF}}$  is the reference voltage (0.8V typ.).

### **External Bootstrap Diode**

Connect a  $0.1\mu$ F low ESR ceramic capacitor between the BOOT pin and SW pin. This capacitor provides the gate driver voltage for the high side MOSFET.

### **Inductor Selection**

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current  $\Delta I_L$  increases with higher V<sub>IN</sub> and decreases with higher inductance.

$$
\Delta I_L = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]
$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. High frequency with small ripple current can achieve the highest efficiency operation. However, it requires a large inductor to achieve this goal.

For the ripple current selection, the value of  $\Delta I_L =$  $0.24$ ( $MAX$ ) will be a reasonable starting point. The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation :

$$
L=\!\!\left[\frac{V_{OUT}}{f\times\Delta I_{L(MAX)}}\right]\!\!\times\!\!\left[1\!-\!\frac{V_{OUT}}{V_{IN(MAX)}}\right]
$$

The inductor's current rating (caused a  $40^{\circ}$ C temperature rising from  $25^{\circ}$ C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit. Please see Table 2 for the inductor selection reference.

### **Table 2. Suggested Inductors for Typical Application Circuit**



### **C**IN **and C**OUT **Selection**

The input capacitance, C<sub>IN</sub>, is needed to filter the trapezoidal current at the source of the high side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The approximate RMS current is given :

$$
I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}
$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I$ <sub>RMS</sub> =  $I_{OUT}/2$ . This simple worst case condition is commonly used for design because even significant deviations do not offer much relief. Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design. For the input capacitor, two  $10\mu$ F low ESR ceramic capacitors are Suggested. For the Suggested capacitor, please refer to Table 3 for more details. The selection of  $C<sub>OUT</sub>$  is determined by the required ESR to minimize voltage ripple. Moreover, the amount of bulk capacitance is also a key for  $C<sub>O</sub>$ <sub>UT</sub> selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section.

The output ripple,  $\Delta V_{\text{OUT}}$  , is determined by :

 $\Delta V_{\text{OUT}} \leq \Delta I_L \left[ ESR + \frac{1}{8fC_{\text{OUT}}} \right]$ 

Copyright © 2015 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation.

The output ripple will be the highest at the maximum input voltage since  $\Delta I_L$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input, V<sub>IN</sub>. At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at V<sub>IN</sub> large enough to damage the part.

### **Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

 $P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$ 

where T<sub>J(MAX)</sub> is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is  $125^{\circ}$ C. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For SOP-8 (Exposed Pad) package, the thermal resistance,  $\theta$ JA, is 49°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A = 25^{\circ}$ C can be calculated by the following formula :

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (49^{\circ}C/W) = 2.041W$  for SOP-8 (Exposed Pad) package

The maximum power dissipation depends on the operating ambient temperature for fixed TJ(MAX) and thermal resistance,  $\theta$ JA. The derating curve in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.



**RICHTEK** 



### **Layout Consideration**

Follow the PCB layout guidelines for optimal performance of the RT6266.

- $\triangleright$  Keep the traces of the main current paths as short and wide as possible.
- $\triangleright$  Put the input capacitor as close as possible to the device pins (VIN and GND).
- ► SW node is with high frequency voltage swing and should be kept at small area. Keep analog components away from the SW node to prevent stray capacitive noise pick-up.
- Connect feedback network behind the output capacitors. Keep the loop area small. Place the feedback components near the RT6266.
- ▶ An example of PCB layout quide is shown in Figure 3 for reference.



#### Figure 3. PCB Layout Guide



### **Outline Dimension**





### **8-Lead SOP (Exposed Pad) Plastic Package**

### **Richtek Technology Corporation**

14F, No. 8, Tai Yuen 1<sup>st</sup> Street, Chupei City Hsinchu, Taiwan, R.O.C. Tel: (8863)5526789

Richtek products are sold by description only. Richtek reserves the right to change the circuitry and/or specifications without notice at any time. Customers should obtain the latest relevant information and data sheets before placing orders and should verify that such information is current and complete. Richtek cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Richtek product. Information furnished by Richtek is believed to be accurate and<br>reliable. However, no responsibility is assumed by Richte result from its use. No license is granted by implication or otherwise under any patent or patent rights of Richtek or its subsidiaries.