# **Not Recommended for New Designs**

The MAX495 was manufactured for Maxim by an outside wafer foundry using a process that is no longer available. It is not recommended for new designs. A Maxim replacement or an industry second-source may be available. The data sheet remains available for existing users. **The other parts on the following data sheet are not affected.**

For further information, please see the QuickView data sheet for this part or contact [technical support](http://www.maxim-ic.com/support/request/new.mvp) for assistance.

# **MAXM**

# Single/Dual/Quad, Micropow er, Single-Supply Rail-to-Rail Op Amps

### General Description

The dual MAX492, quad MAX494, and single MAX495 operational amplifiers combine excellent DC accuracy with rail-to-rail operation at the input and output. Since the common-mode voltage extends from VCC to VEE, the devices can operate from either a single supply  $(+2.7V$  to  $+6V$ ) or split supplies  $(\pm 1.35V$  to  $\pm 3V)$ . Each op amp requires less than 150µA supply current. Even with this low current, the op amps are capable of driving a 1kΩ load, and the input referred voltage noise is only 25nV/√Hz. In addition, these op amps can drive loads in excess of 1nF.

The precision performance of the MAX492/MAX494/ MAX495, combined with their wide input and output dynamic range, low-voltage single-supply operation, and very low supply current, makes them an ideal choice for battery-operated equipment and other low-voltage applications. The MAX492/MAX494/MAX495 are available in DIP and SO packages in the industry-standard op-amp pin configurations. The MAX495 is also available in the smallest 8-pin SO: the  $\mu$ MAX package.

### \_Applications

Portable Equipment Battery-Powered Instruments Data Acquisition Signal Conditioning Low-Voltage Applications



# \_\_\_\_\_\_\_\_\_\_Typical Operating Circuit

\_Features

- ♦ **Low-Voltage Single-Supply Operation (+2.7V to +6V)**
- ♦ **Rail-to-Rail Input Common-Mode Voltage Range**
- ♦ **Rail-to-Rail Output Swing**
- ♦ **500kHz Gain-Bandwidth Product**
- ♦ **Unity-Gain Stable**
- ♦ **150µA Max Quiescent Current per Op Amp**
- ♦ **No Phase Reversal for Overdriven Inputs**
- ♦ **200µV Offset Voltage**
- ♦ **High Voltage Gain (108dB)**
- ♦ **High CMRR (90dB) and PSRR (110dB)**
- ♦ **Drives 1k**Ω **Load**
- ♦ **Drives Large Capacitive Loads**
- ♦ **MAX495 Available in µMAX Package—8-Pin SO**

### \_\_\_\_\_\_\_\_\_\_\_\_\_\_Ordering Information



**Ordering Information continued at end of data sheet.** \*Dice are specified at TA =  $+25^{\circ}$ C, DC parameters only.

# **Pin Configurations**



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### **ABSOLUTE MAXIMUM RATINGS**



Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### **DC ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = +25°C, unless otherwise noted.)



### **AC ELECTRICAL CHARACTERISTICS**

( $V_{CC}$  = 2.7V to 6V,  $V_{EE}$  = GND,  $T_A$  = +25°C, unless otherwise noted.)



### **DC ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = 0°C to +70°C, unless otherwise noted.)



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# **DC ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted.)



## **DC ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = -55°C to +125°C, unless otherwise noted.)



Note 1: RL to V<sub>EE</sub> for sourcing and V<sub>OH</sub> tests; RL to V<sub>CC</sub> for sinking and V<sub>OL</sub> tests.

MAX492/MAX494/MAX495 MAX492/MAX494/MAX495



# \_Typical Operating Characteristics

MAX492-02

1000

-180 -120

-<br>COLORAL<br>PHASE (DEG)

PHASE (DEG)

60 120 180

POWER-SUPPLY REJECTION RATIO vs. FREQUENCY 140 MAX492-03 120 120<br>100<br>80<br>60<br>40<br>20<br>0  $\top$ 100  $V_C$ 80 PSRR (dB) 60 IN 40  $V_{\text{IN}} = 2.5V$ 20  $\mathbf 0$  $-20$  <br>0.01 0.1 1 10 100 0.01 10 1000 FREQUENCY (kHz)





COMMON-MODE REJECTION RATIO



SUPPLY CURRENT PER AMPLIFIER vs. TEMPERATURE



INPUT BIAS CURRENT vs. COMMON-MODE VOLTAGE MAX492-07 (nA) INPUT BIAS CURRENT (nA) **BIAS CURRENT** 



 $V_{CM}$  (V)







20

15

10

0

 $\overline{5}$ 

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### Typical Operating Characteristics (continued)

LARGE-SIGNAL GAIN (dB)

ARGE-SIGNAL

 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V,$  unless otherwise noted.)





LARGE-SIGNAL GAIN vs. OUTPUT VOLTAGE



LARGE-SIGNAL GAIN vs. OUTPUT VOLTAGE



MINIMUM OUTPUT VOLTAGE

120  $\begin{array}{r} 110 \\ 100 \\ \hline 60 \\ 90 \\ \hline 60 \\ \hline 7 \\ 90 \\ \hline 0 \end{array}$ MAX492-14 60 100 80  $V<sub>OUT</sub>$  (mV) 500 vs. OUTPUT VOLTAGE 100 90 70 50  $R_L = 100k\Omega$ <br>  $R_L = 10k\Omega$ <br>  $R_L = 10k\Omega$ <br>  $V_{CC} = +2.7V$ <br>  $R_L$  TO V<sub>CC</sub><br>
0 100 200 300 400 500 600<br>
0 100 200 300 400 500 600

LARGE-SIGNAL GAIN







*IVI A* XI*IV*I









# S6tXVM/t6tXVM/Z6tXVM MAX492/MAX494/MAX495

### \_Typical Operating Characteristics (continued)

 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V,$  unless otherwise noted.)







SMALL-SIGNAL TRANSIENT RESPONSE





TOTAL HARMONIC DISTORTION + NOISE vs. PEAK-TO-PEAK SIGNAL AMPLITUDE



SMALL-SIGNAL TRANSIENT RESPONSE



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# \_Typical Operating Characteristics (continued)

 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V,$  unless otherwise noted.)



 $V_{\text{CC}}$  = +5V,  $A_V$  = +1,  $R_L$  = 10k $\Omega$ 

### LARGE-SIGNAL TRANSIENT RESPONSE



 $V_{CC}$  = +5V, A<sub>V</sub> = -1, R<sub>L</sub> = 10kΩ

# \_Pin Description



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### \_\_\_\_\_\_\_\_\_\_Applications Information

The dual MAX492, quad MAX494, and single MAX495 op amps combine excellent DC accuracy with rail-torail operation at both input and output. With their precision performance, wide dynamic range at low supply voltages, and very low supply current, these op amps are ideal for battery-operated equipment and other lowvoltage applications.

### Rail-to-Rail Inputs and Outputs

The MAX492/MAX494/MAX495's input common-mode range extends 0.25V **beyond** the positive and negative supply rails, with excellent common-mode rejection. Beyond the specified common-mode range, the outputs are guaranteed not to undergo phase reversal or latchup. Therefore, the MAX492/MAX494/MAX495 can be used in applications with common-mode signals at or even beyond the supplies, without the problems associated with typical op amps.

The MAX492/MAX494/MAX495's output voltage swings to within 50mV of the supplies with a 100k Ω load. This rail-to-rail swing at the input and output substantially increases the dynamic range, especially in low supplyvoltage applications. Figure 1 shows the input and output waveforms for the MAX492, configured as a unity-gain noninverting buffer operating from a single  $+3V$  supply. The input signal is  $3.0V_{p-p}$ , 1kHz sinusoid centered at +1.5V. The output amplitude is approximately  $2.95V_{p-p}$ .

### Input Offset Voltage

Rail-to-rail common-mode swing at the input is obtained by two complementary input stages in parallel, whic h feed a folded cascaded stage. The PNP stage is active for input voltages close to the negative rail, and the NPN stage is active for input voltages close to the positive rail.

The offsets of the two pairs are trimmed; however, there is some small residual mismatch between them. This mismatch results in a two-level input offset characteristic, with a transition region between the levels occurring at a common-mode voltage of approximately 1.3V. Unlike other rail-to-rail op amps, the transition region has been widened to approximately 600mV in order to minimize the slight degradation in CMRR caused by this mismatch.

To adjust the MAX495's input offset voltage (500µV max at +25°C), connect a 10k Ω trim potentiometer between the two NULL pins (pins 1 and 5), with the wiper connected to VEE (pin 4) (Figure 2). The trim range of this circuit is ±6mV. External offset adjustment is not available for the dual MAX492 or quad MAX494.

The input bias currents of the MAX492/MAX494/MAX495 are typically less than 50nA. The bias current flows into the device when the NPN input stage is active, and it flows out when the PNP input stage is active. To reduce the offset error caused by input bias current flowing through external source resistances, match the effective resistance seen at each input. Connect resistor R3 between the noninverting input and ground when using



Figure 1. Rail-to-Rail Input and Output (Voltage Follower Circuit,  $VCC = +3V$ ,  $VEE = 0V$ 



Figure 2. Offset Null Circuit

the op amp in an inverting configuration (Figure 3a); connect resistor R3 between the noninverting input and the input signal when using the op amp in a noninverting configuration (Figure 3b). Select R3 to equal the parallel combination of R1 and R2. High source resistances will degrade noise performance, due to the thermal noise of the resistor and the input current noise (which is multiplied by the source resistance).

### Input Stage Protection Circuitry

The MAX492/MAX494/MAX495 include internal protection circuitry that prevents damage to the precision input stage from large differential input voltages. This protection circuitry consists of back-to-back diode s between IN+ and IN- with two 1.7k $\Omega$  resistors in series



Figure 3a. Reducing Offset Error Due to Bias Current: Inverting Configuration



Figure 3b. Reducing Offset Error Due to Bias Current: Noninverting Configuration

*IVI A* XI*IV*I

(Figure 4). The diodes limit the differential voltage applied to the amplifiers' internal circuitry to no more than V F, where V F is the diodes' forward-voltage drop (about 0.7V at  $+25^{\circ}$ C).

Input bias current for the ICs  $(\pm 25nA \text{ typical})$  is specified for the small differential input voltages. For large differential input voltages (exceeding V F), this protection circuitry increases the input current at IN+ and IN-:

 $Input Current = \frac{(V_{IN} - V_{IN} -) - V_{F}}{2 \times 1.7 k\Omega}$ 

For comparator applications requiring large differential voltages (greater than V F), you can limit the input current that flows through the diodes with external resistors



Figure 4. Input Stage Protection Circuitry



Figure 5. Capacitive-Load Stable Region Sourcing Current

in series with IN-, IN+, or both. Series resistors are not recommended for amplifier applications, as they may increase input offsets and decrease amplifier bandwidth.

### Output Loading and Stability

Even with their low quiescent current of less than 150µA per op amp, the MAX492/MAX494/MAX495 are well suited for driving loads up to 1k Ω while maintaining DC accuracy. Stability while driving heavy capacitive loads is another key advantage over comparable CMOS railto-rail op amps.



Figure 6. MAX492 Voltage Follower with 1000pF Load ( $R_L = \infty$ )



Figure 7a. MAX492 Voltage Follower with 500pF Load—  $R_L = 5k\Omega$ 

In op amp circuits, driving large capacitive loads increases the likelihood of oscillation. This is especially true for circuits with high loop gains, such as a unitygain voltage follower. The output impedance and a capacitive load form an RC network that adds a pole to the loop response and induces phase lag. If the pol e frequency is low enough—as when driving a large capacitive load—the circuit phase margin is degraded, leading to either an under-damped pulse response or oscillation.



Figure 7b. MAX492 Voltage Follower with 500pF Load—  $R_l = 20k\Omega$ 



Figure 7c. MAX492 Voltage Follower with 500pF Load—  $R_L = \infty$ 

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The MAX492/MAX494/MAX495 can drive capacitive loads in excess of 1000pF under certain conditions (Figure 5). When driving capacitive loads, the greatest potential for instability occurs when the op amp is sourcing approximately 100µA. Even in this case, stability is maintained with up to 400pF of output capacitance. If the output sources either more or less current, stability is increased. These devices perform well with a 1000pF pure capacitive load (Figure 6). Figure 7 shows the performance with a 500pF load in parallel with various load resistors.



Figure 8. Capacitive-Load Driving Circuit



Figure 9a. Driving a 10,000pF Capacitive Load

To increase stability while driving large capacitive loads, connect a pull-up resistor at the output to decrease the current that the amplifier must source. If the amplifier is made to sink current rather than source, stability is further increased.

Frequency stability can be improved by adding an output isolation resistor (RS) to the voltage-follower circuit (Figure 8). This resistor improves the phase margin of the circuit by isolating the load capacitor from the op amp's output. Figure 9a shows the MAX492 driving 10,000pF (RL  $\geq$  100kΩ), while Figure 9b adds a 47Ω isolation resistor.



Figure 9b. Driving a 10,000pF Capacitive Load with a 47Ω Isolation Resistor



Figure 10. Power-Up Test Configuration





Figure 11a. Power-Up Settling Time (V<sub>CC</sub> = +3V) Figure 11b. Power-Up Settling Time (V<sub>CC</sub> = +5V)

Because the MAX492/MAX494/MAX495 have excellent stability, no isolation resistor is required, except in the most demanding applications. This is beneficial because an isolation resistor would degrade the low frequency performance of the circuit.

### Pow er-Up Settling Time

The MAX492/MAX494/MAX495 have a typical supply current of 150µA per op amp. Although supply current is already low, it is sometimes desirable to reduce it further by powering down the op amp and associated ICs for periods of time. For example, when using a MAX494 t o buffer the inputs to a multi-channel analog-to-digital converter (ADC), much of the circuitry could be powered down between data samples to increase battery life. If samples are taken infrequently, the op amps, along with the ADC, may be powered down most of the time.

When power is reapplied to the MAX492/MAX494/ MAX495, it takes some time for the voltages on the supply pin and the output pin of the op amp to settle. Supply settling time depends on the supply voltage, the value of the bypass capacitor, the output impedance of the incoming supply, and any lead resistance or inductance between components. Op amp settling time depends primarily on the output voltage and is slew-rate limited. With the noninverting input to a voltage follower held at mid-supply (Figure 10), when the supply steps from  $0V$  to  $V_{CC}$ , the output settles in approximately  $4\mu s$ for  $V_{CC} = +3V$  (Figure 11a) or 10us for  $V_{CC} = +5V$ (Figure 11b). **14 \_** VCC



### Pow er Supplies and Layout

The MAX492/MAX494/MAX495 operate from a single 2.7V to 6V power supply, or from dual supplies of ±1.35V to ±3V. For single-supply operation, bypass the power supply with a 1µF capacitor in parallel with a 0.1µF ceramic capacitor. If operating from dual sup plies, bypass each supply to ground.

Good layout improves performance by decreasing the amount of stray capacitance at the op amp's inputs and output. To decrease stray capacitance, minimize bot h trace lengths and resistor leads and place external components close to the op amp's pins.

### Rail-to-Rail Buffers

The Typical Operating Circuit shows a MAX495 gain-oftwo buffer driving the analog input to a MAX187 12-bit ADC. Both devices run from a single 5V supply, and the converter's internal reference is 4.096V. The MAX495's typical input offset voltage is 200µV. This results in an error at the ADC input of 400µV, or less than half of one least significant bit (LSB). Without offset trimming, the op amp contributes negligible error to the conversion result.



# \_Ordering Information (continued)

\* Dice are specified at  $T_A = +25\degree C$ , DC parameters only.

### Pin Configurations (continued)



# \_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Chip Topographies



**MAX495**



TRANSISTOR COUNT: 134 (single MAX495) 268 (dual MAX492) 536 (quad MAX494) SUBSTRATE CONNECTED TO VEE



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