

The Future of Analog IC Technology

## DESCRIPTION

The MP2171 is a monolithic, step-down, switchmode converter with integrated, internal, power MOSFETs. The MP2171 can achieve up to 1A of continuous output current from a 2.5V to 5.5V input voltage with excellent load and line regulation. The output voltage can be regulated as low as 0.6V.

Constant-on-time (COT) control provides fast transient response and eases loop stabilization. Full protection features include cycle-by-cycle current limiting and thermal shutdown.

The MP2171 is ideal for a wide range of applications, including automotive infotainment, clusters, telematics, and portable instruments.

The MP2171 requires only a minimal number of readily available, standard, external components and is available in a small TSOT23-8 package.

# *MP2171* 5.5V, 1A, 2.6MHz, Synchronous, Step Down Converter

## **FEATURES**

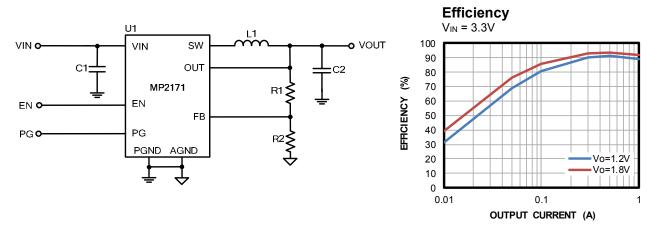
- Wide 2.5V to 5.5V Operating Input Range
- Output Voltage as Low as 0.6V
- 100% Duty Cycle in Dropout
- Up to 1A Output Current
- 90m $\Omega$  and 50m $\Omega$  Internal Power MOSFET Switches
- Default 2.6MHz Switching Frequency with 3.3V Input and 1.8V Output
- EN and Power Good for Power Sequencing
- Cycle-by-Cycle Over-Current Protection
   (OCP)
- Auto-Discharge at Power-Off
- Short-Circuit Protection (SCP) with Hiccup Mode
- Stable with Low ESR Output Ceramic Capacitors
- Available in a TSOT23-8 Package

## **APPLICATIONS**

- Automotive Infotainment
- Automotive Clusters
- Automotive Telematics
- Low-Voltage I/O System Power
- Handheld/Battery-Powered Systems

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## **TYPICAL APPLICATION**



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## ORDERING INFORMATION

Part Number *	Package	Top Marking		
MP2171GJ	TSOT23-8	See Below		

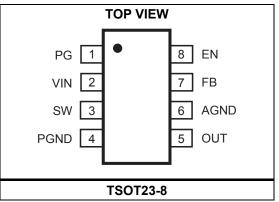
\* For Tape & Reel, add suffix –Z (e.g.: MP2171GJ–Z).

## **TOP MARKING**

### BAZY

BAZ: Product code of MP2171GJ Y: Year code

## PACKAGE REFERENCE



## ABSOLUTE MAXIMUM RATINGS (1)

Supply voltage (V <sub>IN</sub> )6V	
V <sub>SW</sub> 0.3V (-5V for <10ns)	
to V <sub>IN</sub> + 0.3V (8V for <10ns)	
All other pins0.3V to +6V	
Junction temperature 150°C	
Lead temperature	
Continuous power dissipation $(T_A = 25^{\circ}C)$ <sup>(2)</sup>	
Storage temperature65°C to +150°C	
$\mathbf{P}_{\mathbf{r}} = \mathbf{P}_{\mathbf{r}} = $	

#### **Recommended Operating Conditions** <sup>(3)</sup>

# Thermal Resistance <sup>(4)</sup> $\theta_{JA}$ $\theta_{JC}$

TSOT23-8 ..... °C/W

#### NOTES:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature T<sub>J</sub> (MAX), the junction-to-ambient thermal resistance θ<sub>JA</sub>, and the ambient temperature T<sub>A</sub>. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P<sub>D</sub> (MAX) = (T<sub>J</sub> (MAX)-T<sub>A</sub>)/θ<sub>JA</sub>. Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the device to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.



## **ELECTRICAL CHARACTERISTICS**

 $V_{IN}$  = 5V,  $T_J$  = -40°C to +125°C <sup>(6)</sup>, unless otherwise noted, typical values are at  $T_J$  = +25°C.

Parameter	Symbol	Condition	Min	Тур	Max	Units	
Quiescent current	IQ	$V_{IN} = 5V, V_{EN} = 2V,$ $V_{FB} = 0.63V,$ no switching		520	720	μA	
Supply current (shutdown)	launu	V <sub>EN</sub> = 0V, T <sub>J</sub> = +25°C		0.1	2	μA	
Supply current (Shutdown)	ISHDN	$V_{EN}$ = 0V, $T_{J}$ = -40°C to +125°C		0.1	35		
Feedback voltage	V <sub>FB</sub>	T <sub>J</sub> = +25°C	591	600	609	mV	
T EEUDACK VOILAGE	v ⊢B	$T_{J} = -40^{\circ}C$ to $+125^{\circ}C$	588	600	612		
Feedback current	I <sub>FB</sub>	V <sub>FB</sub> = 0.63V		10	100	nA	
P-FET switch on resistance	Rdson_p			90	135	mΩ	
N-FET switch on resistance	Rdson_n			50	83	mΩ	
Switch leakage		$V_{\text{EN}}$ = 0V, $V_{\text{IN}}$ = 5V, $V_{\text{SW}}$ = 0V and 5V, $T_{\text{J}}$ = +25°C		0.1	2		
Switch leakage		$V_{\text{EN}}$ = 0V, $V_{\text{IN}}$ = 5V, $V_{\text{SW}}$ = 0V and 5V, $T_J$ = -40°C to +125°C		0.1	35	μA	
P-FET current limit		T <sub>J</sub> = +25°C	3	4	6	А	
		V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.2V	135	150	180		
On time	tou	V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.8V	190	210	270	ns	
On time	ton	V <sub>IN</sub> = 5V, V <sub>OUT</sub> = 1.2V	95	110	130		
		V <sub>IN</sub> = 5V, V <sub>OUT</sub> = 1.8V	130	150	190		
	fs	V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.2V	1850	2400	2700	kHz	
Switching frequency		V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.8V	2000	2600	2800		
		V <sub>IN</sub> = 5V, V <sub>OUT</sub> = 1.2V	1850	2200	2500		
		V <sub>IN</sub> = 5V, V <sub>OUT</sub> = 1.8V	1850	2380	2700		
		V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.2V					
	t <sub>MIN-OFF</sub>	V <sub>IN</sub> = 3.3V, V <sub>OUT</sub> = 1.8V		60	90	ns	
Minimum off time		V <sub>IN</sub> = 5V, V <sub>OUT</sub> = 1.2V			50	ns	
		$V_{IN} = 5V, V_{OUT} = 1.8V$		30			
Soft-start time (5)	tss-on	V <sub>IN</sub> = 3.6V, V <sub>OUT</sub> = 1.5V, 10% to 90%	0.6	1.3	2.2	ms	
Soft-stop time (5)	tss-off	V <sub>IN</sub> = 3.6V, V <sub>OUT</sub> = 1.5V, 90% to 10%	0.4	0.9	1.6	ms	
Power good upper trip threshold rising	PG <sub>H-R</sub>	FB rising when PG turns to high voltage	110	115	120	%	
Power good upper trip threshold falling	PG <sub>H-F</sub>	FB falling when PG turns to high voltage	105	110	115	%	
Power good upper trip hysteresis	PG <sub>H-Hys</sub>			5		%	
Power good lower trip threshold rising		FB rising when PG turns to high voltage	85	90	95	%	
Power good lower trip Threshold falling	PG <sub>L-F</sub>	FB falling when PG turns to high voltage	80	85	90	%	
Power good lower trip hysteresis	PG <sub>L-Hys</sub>			5		%	



**ELECTRICAL CHARACTERISTICS** *(continued)*  $V_{IN} = 5V$ ,  $T_J = -40^{\circ}C$  to  $+125^{\circ}C$ <sup>(6)</sup>, unless otherwise noted, typical values are at  $T_J = +25^{\circ}C$ .

Parameter	Symbol	Condition	Min	Тур	Мах	Units
Power good delay	PGD		30	110	200	μs
Power good sink current capability	V <sub>PG-L</sub>	Sink 1mA		250	400	mV
Power good logic high voltage	V <sub>PG-H</sub>	V <sub>IN</sub> = 5V, V <sub>FB</sub> = 0.6V	4.85			V
Power good internal pull-up resistor	R <sub>PG</sub>		200	500	800	kΩ
Under-voltage lockout threshold rising			2.0	2.2	2.4	V
Under-voltage lockout threshold hysteresis				150		mV
EN input logic low voltage					0.4	V
EN input logic high voltage			1.2			V
		V <sub>EN</sub> = 0V		0.1	0.2	μA
EN input current		V <sub>EN</sub> = 2V		2	4	μA
Thermal shutdown (5)				170		°C
Thermal hysteresis (5)				30		°C

NOTE:

5) Not tested in production and guaranteed by design and characterization.

6) Not tested in production and guaranteed by over-temperature correction.



#### Efficiency Efficiency $V_{IN} = 3.3V$ $V_{IN} = 5V$ 100 100 90 90 80 80 %) 70 70 %) **EFFICIENCY** 60 60 EFFICIENCY 50 50 40 40 30 30 20 20 Vo=1.8V Vo=1.2V 10 Vo=1.2V 10 Vo=1.8V 0 0 0.1 0.01 1 0.01 0.1 1 **OUTPUT CURRENT (A)** OUTPUT CURRENT (A) Line Regulation Load Regulation 0.4 0.4 0.3 0.3 LOAD REGULATION (%) (%) 0.2 0.2 LINE REGULATION 0.1 0.1 0 0 -0.1 -0.1 -0.2 -0.2 Vo=1.2V lo=1A -0.3 -0.3 Vo=1.8V lo=0A -0.4 -0.4 0 0.2 0.4 0.6 8.0 1 3 4 5 2 6 OUTPUT CURRENT (A) INPUT VOLTAGE (V) **Case Temperature Rise** Shutdown Current vs. Input Voltage V<sub>IN</sub> = 3.3V 10 0.5 CASE TEMPRETURE RISE (°C) 8 0.4 CURRENT (µA) 0.3 6 0.2 4 2 0.1 Vo=1.2V Vo=1.8V 0 0 5 6 0.2 0.4 0.8 2.5 3 3.5 4 4.5 5.5 0 0.6 1 2 OUTPUT CURRENT (A) INPUT VOLTAGE (V)

## **TYPICAL PERFORMANCE CHARACTERISTICS**

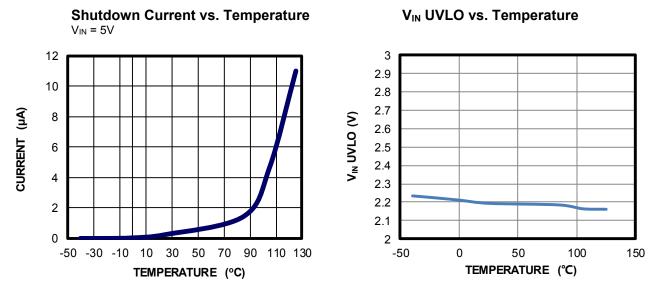
 $V_{IN}$  = 3.3V,  $V_{OUT}$  = 1.2V, L = 1µH,  $C_{OUT}$  = 22µF,  $T_A$  = +25°C, unless otherwise noted.

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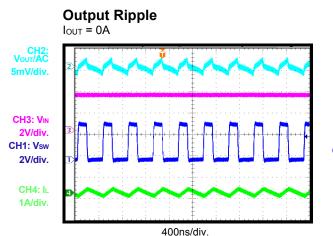


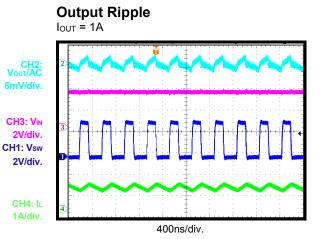
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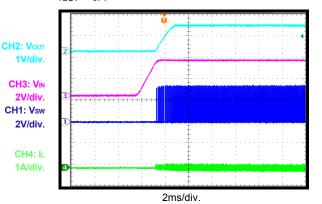


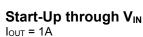
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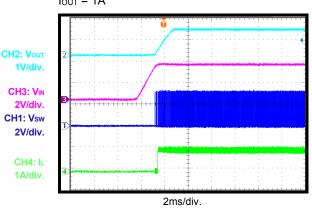


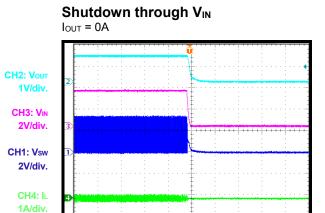


Start-Up through V<sub>IN</sub> Iout = 0A



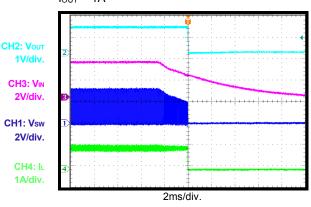






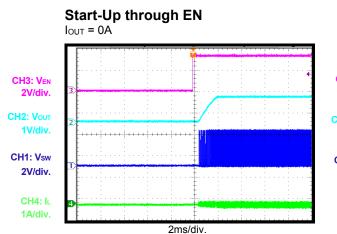
100ms/div.

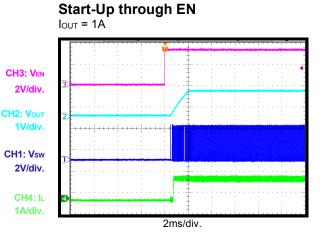
#### Shutdown through V<sub>IN</sub> Iout = 1A



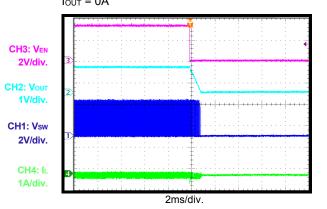


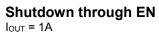
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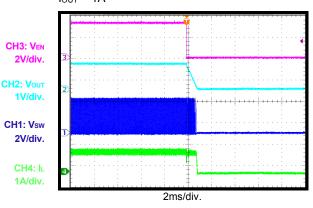


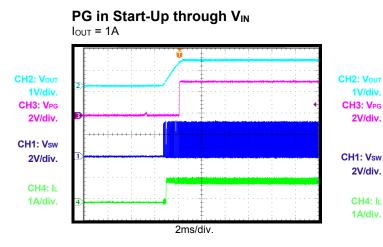


Shutdown through EN Iout = 0A

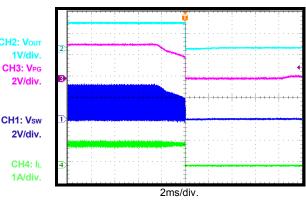










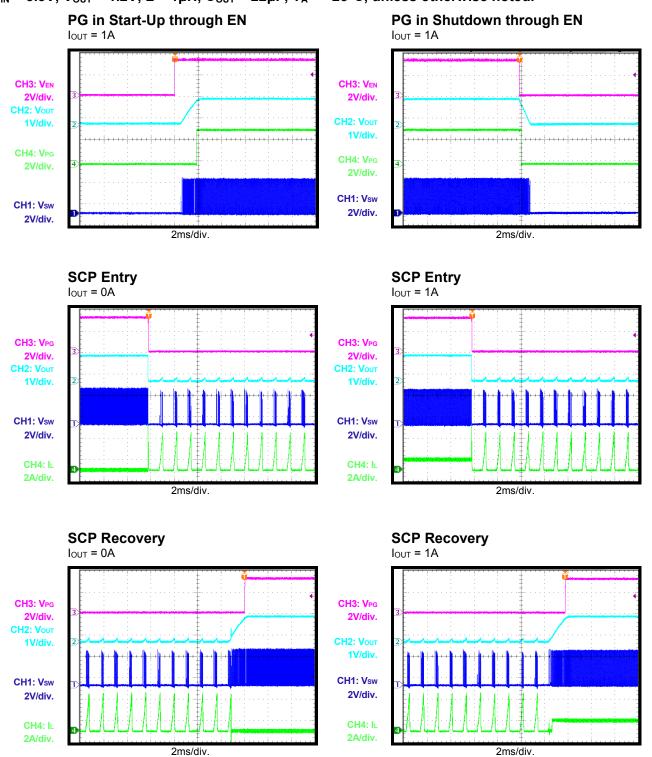


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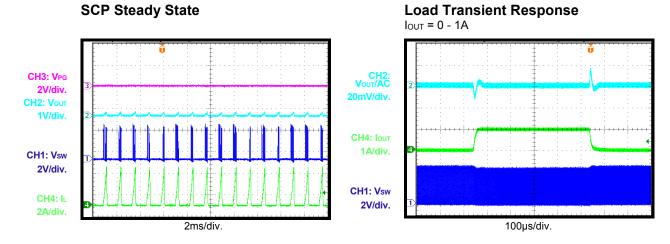


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## **PIN FUNCTIONS**

Package Pin #	Name	Description
1	PG	<b>Power good indicator.</b> The output of PG is an open drain that connects to VIN via an internal pull-up resistor. PG goes high if the output voltage is within $\pm 10\%$ of the nominal voltage.
2	VIN	<b>Input supply.</b> The MP2171 operates from a 2.5V to 5.5V input rail. A capacitor (C1) prevents large voltage spikes from appearing at the input.
3	SW	Switch output. SW is the output of the internal power switch.
4	PGND	<b>Power ground.</b> PGND is the reference ground of the power device and requires careful consideration during PCB layout. For best results, connect PGND with copper pours and vias.
5	OUT	Input sense. OUT is for the output voltage feedback.
6	AGND	Analog ground. AGND is the reference ground of the internal control circuit.
7	FB	<b>Feedback.</b> Connect FB to the tap of an external resistor divider from the output to AGND to set the output voltage.
8	EN	<b>Enable.</b> Pull EN high to enable the MP2171. Float EN or connect EN to ground to disable the MP2171.



## **BLOCK DIAGRAM**

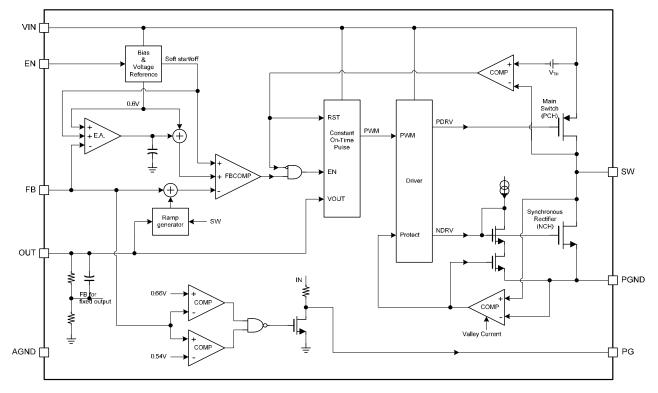


Figure 1: Functional Block Diagram



## **OPERATION**

The MP2171 uses constant-on-time (COT) control with input voltage feed-forward to stabilize the switching frequency over its entire input range. The MP2171 achieves up to 1A of continuous output current from a 2.5V to 5.5V input voltage with excellent load and line regulation. The output voltage can be regulated as low as 0.6V.

### Constant-On-Time (COT) Control

Compared to fixed-frequency pulse-width modulation (PWM) control, constant-on-time (COT) control offers a simpler control loop and faster transient response. By using input voltage feed-forward, the MP2171 maintains a nearly constant switching frequency across the entire input and output voltage range. The switching pulse on time can be estimated with Equation (1):

$$T_{on}(\mu s) = V_{OUT}/V_{IN} \times 0.33 + 0.03 \mu s$$
 (1)

Where 0.03µs is the loop delay.

For the specific value of the on time, refer to the EC table on page 3.

To prevent inductor current runaway during the load transient, the MP2171 implements a minimum off time in each cycle. This minimum off time limit does not affect the operation of the MP2171 in steady state in any way.

#### Enable (EN)

When the input voltage exceeds the undervoltage lockout (UVLO) threshold (typically 2.2V) the MP2171 is enabled by pulling the enable pin (EN) above 1.2V. Float EN or connect EN to ground to disable the MP2171. There is an internal  $1M\Omega$  resistor from EN to ground.

#### Soft-Start/Soft-Stop

The MP2171 has a built-in soft start that ramps up the output voltage at a constant slew rate to avoid overshooting during start-up. The softstart time is about 1.3ms, typically. When disabled, the MP2171 ramps down the internal reference voltage to allow the load to discharge the output linearly.

#### Power Good (PG) Indicator

The MP2171 has an open drain with a  $500k\Omega$  pull-up resistor pin for power good indication (PG). When FB is within ±10% of the regulation voltage (0.6V), PG is pulled up to VIN by the internal resistor. If the FB voltage is outside the ±10% window, PG is pulled to ground by an internal MOSFET.

#### **Current Limit**

The MP2171 has a 4A current limit for the highside switch (HS-FET). When the HS-FET reaches its current limit, the MP2171 enters hiccup mode until the current drops to prevent the inductor current from building and damaging the components.

#### Short Circuit and Recovery

The MP2171 enters short-circuit protection (SCP) mode when it reaches the current limit and attempts to recover from the short circuit with hiccup mode. In SCP, the MP2171 disables the output power stage, discharges a soft-start capacitor, and then enacts a soft-start procedure. If the short-circuit condition still remains after the soft-start ends, the MP2171 repeats this operation until the short circuit is removed and the output rises back to the regulation level.



## **APPLICATION INFORMATION**

#### Setting the Output Voltage

The external resistor divider sets the output voltage. The feedback resistor (R1) must account for both stability and dynamic response and therefore cannot be too large or too small. Choose R1 to be around  $41.2k\Omega$ . R2 can then be calculated with Equation (2):

$$R2 = \frac{R1}{\frac{V_{out}}{0.6} - 1}$$
 (2)

The feedback circuit is shown in Figure 2.

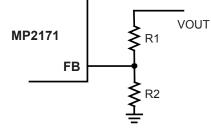


Figure 2: Feedback Network

Table 1 lists the recommended resistor values for common output voltages.

 Table 1: Resistor Values for Common Output

 Voltages

Vout (V)	R1 (kΩ)	R2 (kΩ)
1.0	41.2 (1%)	60.4 (1%)
1.2	41.2 (1%)	41.2 (1%)
1.8	41.2 (1%)	20.5 (1%)
3.3	41.2 (1%)	9.09 (1%)

#### Selecting the Inductor

A 0.47 - 1.5 $\mu$ H inductor is recommended for most applications. For the highest efficiency, chose an inductor with a DC resistance less than 15m $\Omega$ . For most designs, the inductance value can be derived from Equation (3):

$$L_{1} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_{L} \times f_{OSC}}$$
(3)

Where  $\Delta I_L$  is the inductor ripple current.

Choose the inductor current to be approximately 30% of the maximum load current. The maximum inductor peak current can be calculated with Equation (4):

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_{L}}{2}$$
(4)

#### Selecting the Input Capacitor

The input current to the step-down converter is discontinuous therefore and requires а capacitor to supply AC current to the step-down converter while maintaining the DC input voltage. Use low ESR capacitors for the best performance. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR values and small temperature coefficients. For most applications, a 10µF capacitor is sufficient. For higher output voltages, use a 47µF capacitor to improve system stability.

Since the input capacitor absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated with Equation (5):

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$
(5)

The worst-case condition occurs at  $V_{IN} = 2V_{OUT}$ , shown in Equation (6):

$$I_{C1} = \frac{I_{LOAD}}{2}$$
(6)

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, place a small, high-quality, ceramic capacitor ( $0.1\mu$ F) as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to prevent excessive voltage ripple at the input. The input voltage ripple caused by the capacitance can be estimated with Equation (7):

$$\Delta V_{\rm IN} = \frac{I_{\rm LOAD}}{f_{\rm S} \times C1} \times \frac{V_{\rm OUT}}{V_{\rm IN}} \times \left(1 - \frac{V_{\rm OUT}}{V_{\rm IN}}\right)$$
(7)



#### Selecting the Output Capacitor

The output capacitor (C2) maintains the output DC voltage. Use low ESR, ceramic capacitors to keep the output voltage ripple low. The output voltage ripple can be estimated with Equation (8):

$$\Delta V_{\text{out}} = \frac{V_{\text{out}}}{f_{\text{S}} \times L_{1}} \times \left(1 - \frac{V_{\text{out}}}{V_{\text{IN}}}\right) \times \left(R_{\text{ESR}} + \frac{1}{8 \times f_{\text{S}} \times C2}\right)$$
(8)

Where  $L_1$  is the inductor value, and  $R_{\text{ESR}}$  is the equivalent series resistance of the output capacitor.

For ceramic capacitors, the impedance at the switching frequency is dominated by the capacitance. The output voltage ripple is caused mainly by the capacitance. For simplification, the output voltage ripple can be estimated with Equation (9):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{8 \times f_{\text{s}}^{2} \times L_{1} \times C2} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \quad (9)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be approximated with Equation (10):

$$\Delta V_{\text{out}} = \frac{V_{\text{out}}}{f_{s} \times L_{1}} \times \left(1 - \frac{V_{\text{out}}}{V_{\text{IN}}}\right) \times R_{\text{ESR}}$$
(10)

The characteristics of the output capacitor also affect the stability of the regulation system.

#### PCB Layout Guidelines

Proper layout of the switching power supplies is critical for stable operation. For high-frequency switching converters, a poor layout can lead to poor line or load regulation and stability issues. For best results, refer to Figure 3 and follow the guidelines below.

- Place high current paths (GND, VIN, and SW) very close to the device using short, direct, and wide traces.
- 2. Place the input capacitor as close to VIN and GND as possible.
- 3. Place the external feedback resistors next to FB.
- 4. Keep the switching node SW short and away from the feedback network.

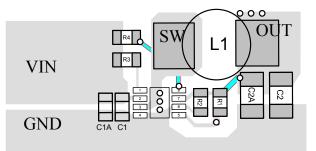


Figure 3: Layout Recommendation



# **TYPICAL APPLICATION CIRCUITS**

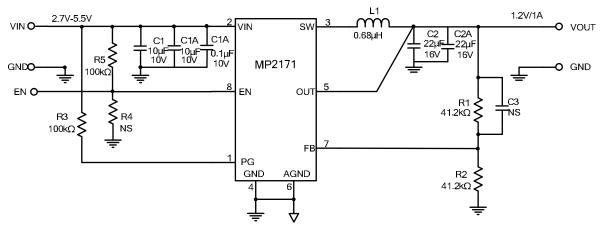


Figure 4: V<sub>OUT</sub> = 1.2V Typical Application Circuit

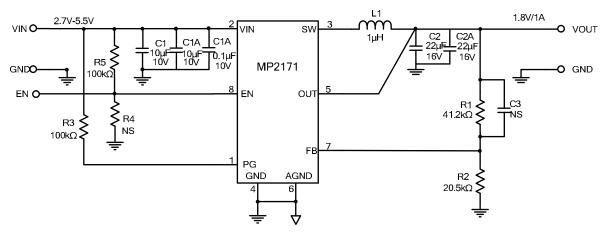
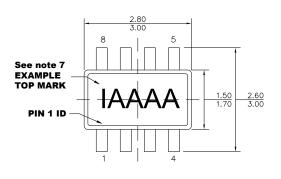


Figure 5: Vout = 1.8V Typical Application Circuit

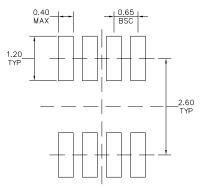


## PACKAGE INFORMATION

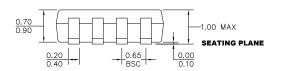




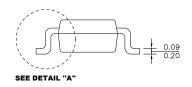
**TOP VIEW** 



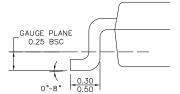
#### **RECOMMENDED LAND PATTERN**



FRONT VIEW



SIDE VIEW



DETAIL "A"

## NOTE:

 ALL DIMENSIONS ARE IN MILLIMETERS.
 PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSION OR GATE BURR.
 PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
 LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
 JEDEC REFERENCE IS MO-193, VARIATION BA.
 DRAWING IS NOT TO SCALE.
 PIN 1 IS LOWER LEFT PIN WHEN READING TOP MARK FROM LEFT TO RIGHT, (SEE EXAMPLE TOP MARK)

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