

# **20-Bit Audio DAC**

# **AD1862**

#### **FEATURES**

**120 dB Signal-to-Noise Ratio 102 dB D-Range Performance** 6**1 dB Gain Linearity** 6**1 mA Output Current 16-Pin DIP Package 0.0012% THD + N**

#### **APPLICATIONS**

**High Performance Compact Disc Players Digital Audio Amplifiers Synthesizer Keyboards Digital Mixing Consoles High Resolution Signal Processing**

# **PRODUCT DESCRIPTION**

The AD 1862 is a monolithic 20-bit digital audio  $\Delta$ device provides a 20-bit DAC, 20-bit serial-to-parallel input register and voltage reference. T he digital portion of the AD 1862 is fabricated with CM OS logic elements that are provided by Analog Devices' BiMOS II process. The analog portion of the AD 1862 is fabricated with bipolar and MOS devices as well as thin-film resistors.

New design, layout and packaging techniques all combine to produce extremely high performance audio playback. T he design of the AD 1862 incorporates a digital offset circuit which improves low-level distortion performance. Low stress packaging techniques are used to minimize stress-induced parametric shifts. Stress-sensitive circuit elements are located in die areas which are least affected by packaging stress. Laser-trimming of initial linearity error affords extremely low total harmonic distortion. Output glitch is also small, contributing to the overall high level of performance.

The noise performance of the AD1862 is excellent. When used with the recommended two external noise-reduction capacitors, it achieves 120 dB signal-to-noise ratio.

The serial input port consists of the clock, data and latch enable pins. A serial 20-bit, 2s complement data word is clocked into the D AC, M SB first, by the external data clock. A latch-enable signal transfers the input word from the internal serial input

## **FUNCTIONAL BLOCK D IAGRAM**



 $\ell$ egister to the DAC *input register*. The data clock can function at 1/7 MHz, allowing  $16 \times F_S$  operation. The serial input port is compatible with second-generation digital filter chips for  $e$ on sumer audio products such as the NPC  $\beta$ M5813 and SM5818. The ADT862 operates with  $\pm 5 \text{ V}$  to  $\pm 12 \text{ V}$  supplies for the digital power supplies and  $\pm 1/2$  V supplies for the analog supplies. The digital and analog supplies  $cd$  be separated for reduced digital crosstalk. Separate analog and digital  $k$ <sub>ommon</sub> pins are also provided. The AD 1862 typically dissipates less than 300 mW. **OBSOLETE**

> The AD1862 is packaged in a 16-pin plastic DIP. The operating range is guaranteed to be  $-25^{\circ}$ C to  $+70^{\circ}$ C.

#### **P ROD UCT HIGHLIGHTS**

- 1. 120 dB signal-to-noise ratio. (typical)
- 2. 102 dB D -Range performance. (minimum)
- 3.  $\pm$ 1 dB gain linearity @ -90 dB amplitude.
- 4. 20-bit resolution provides 120 dB of dynamic range.
- 5.  $16 \times F_s$  operation.
- 6. 0.0016% THD+N  $@$  0 dB signal amplitude. (typical)
- 7. Space saving 16-pin D IP package.
- 8. ±1 mA output current.

## REV. A

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 $AD1862-SPECIFICATIONS$  (T<sub>A</sub> at +25°C and  $\pm$ 12 V supplies, see Figure 10 for test circuit schematic)

	Min	Typ	Max	Units
<b>RESOLUTION</b>	20			<b>Bits</b>
DIGITAL INPUTS VIH $V_{IL}$ $I_{IH}$ @ $V_{IH}$ = 4.0 V $I_{IL}$ @ $V_{IL} = 0.4 V$ Maximum Clock Input Frequency	2.0 17	4.0 0.4	0.8 1.0 $-10$	V $\mathbf V$ μA μA MHz
<b>ACCURACY</b> Gain Error Midscale Output Error		±2	$\pm 2$ ±5	$\%$ μA
TOTAL HARMONIC DISTORTION + NOISE (EIAJ) <sup>1</sup> $\mathcal{V}\times B$ , 990.5 $\forall$ 4z AD1862N-J AD1862N –20 dB, 990.5 ∏z $ADA$62N$ <sub>N</sub> -J –60 dB, 99¢.5 ∦z / AD 1862 N, N-J $D\$ Range, $\frac{1}{60}$ $\frac{1}{4}$ B $\frac{1}{4}$ A-Weight Filter	102	$-98(0.0012)$ $-94(0.0019)$ $-84(0.0063)$ $-45(0.56)$	$-96(0.0016)$ $-92(0.0025)$ $-80(0.01)$ $-42(0.8)$	$dB(\%)$ $dB(\%)$ $dB(\%)$ $dB(\%)$ dB
SIGNAL-TO NOISE RATIOF: (EIAJ) <sup>I</sup> A-Weight Filter AD1862N AD1862N <b>GAIN LINEARITY</b>	$\overline{13}$ 1 10	119 119		dB dB
$@ -90 dB$ AD1862N-J AD1862N <b>OUTPUT CURRENT</b> Bipolar Range Tolerance Output Impedance $(\pm 30\%)$ Settling Time		$\pm 1$ $\pm 1$ ±1 ±1 2.1 350		dB. m A $\%$ kQ ns
FEEDBACK RESISTOR Value Tolerance		3 ±1	±2	$k\Omega$ $\%$
<b>POWER SUPPLY</b> Voltage $V_L$ and $-V_L$ Voltage $V_S$ and $-V_S$ Current +I, $V_L$ and $V_S$ = 12 V, 17 MHz Clock $-I$ , $-VL$ and $-VS = -12$ V, 17 MHz Clock	4.75 10.8	12.0 12.0 11 13	13.2 13.2 15 16	$\pm V$ $\pm V$ mA mA
POWER DISSIPATION $V_L$ and $V_S = 12$ V, $-V_L$ and $-V_S = -12$ V, 17 MHz Clock		288	372	mW
TEMPERATURE RANGE Specification Operation Storage	$-25$ $-60$	$+25$	$+70$ $+100$	$^{\circ}{\rm C}$ $^{\circ}{\rm C}$ $\rm ^{\circ}C$

**NOTES** 

 $1$ T est M ethod complies with EIAJ Standard CP-307.

 $2T$ he signal-to-noise measurement includes noise contributed by the SE5534A op amp used in the test fixture but does not include the noise contributed by the low pass filter used in the test fixture.

Specifications in **boldface** are tested on all production units at final electrical test.

Specifications subject to change without notice.





Figure 3. Broadband Noise (20 kHz Bandwidth, Midscale)



200

# **ABSOLUTE MAXIMUM RATINGS\***



\*Stresses greater than those listed under "Absolute M aximum Ratings" may cause permanent damage to the device. T his is a stress rating only and functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

# **CAUTION**

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD 1862 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD  $\theta$ rec $\theta$ utions are recommended to avoid performance degradation or loss of functionality.





## **ORDERING GUIDE**



 $*N =$  Plastic DIP.

## **TOTAL HARMONIC D ISTORTION + NOISE**

Total Harmonic Distortion plus Noise  $(THD+N)$  is defined as the ratio of the square root of the sum of the squares of the values of the harmonics and noise to the value of the fundamental input frequency. It is usually expressed in percent  $(\%)$  or decibels (dB).

#### **D - RANGE D ISTORTION**

D-Range Distortion is the ratio of the signal amplitude to the distortion plus noise at –60 dB. In this case, an A-Weight filter is used. T he value specified for D -Range performance is the ratio measured plus 60 dB.

## **SETTLING TIME**

Settling Time is the time required for the output to reach and remain within  $\pm 1/2$  LSB about its final value, measured from the digital input transition. It is a primary measure of dynamic performance and is  $\sqrt{\frac{1}{x}}$  is  $\sqrt{\frac{x^2}{x^2}}$  ressed in nanoseconds (ns).

# **SIGNAL- TO- NOISE RATIO**

The Signal-to-N oise Ratio is defined as the ratio of the amplitude of the output with full-scale present to the amplitude of the output when no signal is present. It is expressed in decibels  $(d\vec{B})$ and measured using an A-Weigh filter

#### **GAIN LINEARITY**

Gain Linearity is a measure of the deviation of the actual output amplitude from the ideal output amplitude. It is determined by measuring the amplitude of the output signal as the amplitude of that output signal is digitally reduced to a low level. A perfect D/A converter exhibits no difference between the ideal and actual amplitudes. Gain linearity is expressed in decibels (dB).

#### **MID SCALE ERROR**

M idscale Error, or bipolar zero error, is the deviation of the actual analog output from the ideal output when the 2s complement input code representing midscale is loaded in the input register. The AD1862 is a current output D/A converter. Therefore, this error is expressed in µA.



AD1862 Block Diagram

## **FUNCTIONAL DESCRIPTION**

The AD1862 is a high performance, monolithic 20-bit audio DAC. Each device includes a voltage reference, a 20-bit DAC,  $2\theta$ -bi $\psi$  input latch and a 20-bit serial-to-parallel input register. A special digital offset circuit, combined with segmentation cir- $\psi$ uit $\psi$ , produces excellent  $\mathcal{I}$ H $\psi$  +N and D-range performance.

Extensive noise/reduction features are utilized to make the noise performance of the  $A$ D 1862 as high as possible. For example, the voltage reference circuit is a low/noike, 9 volt bandgap cell. This cell supplies the reference voltage to the bipolar offset circuit and the DAC. An external noise-reduction capacitor is  $\ell$ onnected to NR1 to form a low-pass filter network. **CONSERVENTION CONSERVER CONSERVER AND**<br>
The digital input fram sitted with a final value, measured from<br>
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Additional noise-reduction techniques are used in the control amplifier of the DAC. By connecting an external noise-reduction capacitor to N R2 output noise contributions from the control portion of the D AC are similarly reduced. T he noise-reduction efforts result in a signal-to-noise ratio of 120 dB.

The design of the AD1862 uses a combination of segmented decoder, R-2R topology and digital offset to produce low distortion at all signal amplitudes. T he digital offset technique shifts the midscale output voltage  $(0 V)$  away from the MSB transition of the device. T herefore, small amplitude signals are not affected by an M SB change. An extra D AC cell is included to avoid clipping the output at full scale.

The DAC supplies  $a \pm 1$  mA output current to an external I-to-V converter. An on-board 3 kΩ feedback resistor is also supplied. Both the output current and feedback resistor are laser-trimmed to  $\pm 2\%$  tolerance, simplifying the selection of external filter and/or deemphasis network components. T he input register and serial-to-parallel converter are fabricated with CM OS logic gates. T hese gates allow the achievement of fast switching speeds and low power consumption. Internal TTLto-CMOS converters are used to insure TTL and 5 V CMOS compatibility.

# **Analog Circuit Considerations**

# **GROUND ING RECOMMEND ATIONS**

The AD1862 has two ground pins, designated analog ground (AGND) and digital ground (DGND). The analog ground pin is the "high-quality" ground reference for the device. T he analog ground pin should be connected to the analog common point in the system. T he reference bypass capacitor, the noninverting terminal of the current-to-voltage conversion op amp, and any output loads should be connected to this point. T he digital ground pin returns ground current from the digital logic portions of the AD 1862 circuitry. T his pin should be connected to the digital common point in the system.

As illustrated in Figure 7, AGND and DGND should be connected together at one point in the system.



Figure 7. Grounding and Bypassing Recommendations

# **POWER SUPPLIES AND DECOUPLING**

The AD 1862 has four power supply input pins.  $\pm V_s$  provide the supply voltages which operate the linear portions of the D AC including the voltage reference and control amplifier. The  $\pm V_s$ supplies are designed to operate with  $\pm 12$  volts.

The  $\pm V_L$  supplies operate the digital portions of the chip including the input shift register, the input latching circuitry and the TTL-to-CMOS level shifters. The  $\pm V_L$  supplies are designed to be operated from  $\pm$ 5 V to  $\pm$ 12 V supplies subject only to the limitation that  $-V_L$  may not be more negative than  $-V_S$ .

D ecoupling capacitors should be used on all power supply input pins. Good engineering practice suggests that these capacitors be placed as close as possible to the package pins and the common points. The logic supplies,  $\pm V_L$ , should be decoupled to DGND and the analog supplies,  $\pm V_s$ , should be decoupled to AGND.

# **EXTERNAL NOISE REDUCTION COMPONENTS**

T wo external capacitors are required to achieve low-noise operation. T heir correct connection is illustrated in Figure 8. Capacitor C1 is connected between the pin labeled NR1 and analog common. C1 forms a low-pass filter element which reduces noise con-

tributed by the voltage reference circuitry. T he proper choice for this capacitor is a tantalum type with value of  $10 \mu$ F or more. This capacitor should be connected to the package pins as closely as possible. T his will minimize the effects of parasitic inductance of the leads and connections circuit connections.



**PIN 1 IS "HIGH QUALITY" RETURN FOR BIAS CAP.**

# Figure 8. Noise Reduction Capacitors

Capacitor  $\sqrt{2}$  is connected between the pin labeled NR2 and the negative analog supply,  $-\nabla_s$ . This capacitor reduces the portion of output noise contributed by the control amplifier circuitry.  $\ell$ 2 should be chosen to be a tantalum sapacitor with a value of about  $1/\mu$ F. Again, the connections between the AD 1862 and  $C2$ should be made as short as possible.

The recommended values for C1 and CL are 10  $\mu$ F and  $+$ respectively. The ratio between  $\mathcal{L}$ 1 and C2/should be approximately 10. Additional noise reduction  $\frac{\hbar}{\hbar}$  be gain $\frac{d}{d}$  by choosing slightly higher values for C1 and C2 such as  $2\not{2} \mu F$  and 2.2 µF. Figure 2 illustrates the noise performance of the AD 1862 with 10  $\mu$ F and 1  $\mu$ F.

# **EXTERNAL AMPLIFIER CONNECTIONS**

The AD1862 is a current-output D/A converter. Therefore, an external amplifier, in combination with the on-board feedback resistor, is required to derive an output voltage. Figure 9 illustrates the proper connections for an external operational amplifier. T he output of the AD 1862 is intended to drive the summing junction of an external current-to-voltage conversion op amp. T herefore, the voltage on the output current pin of the AD 1862 should be approximately the same as that on the AGND pin of the device.

The on-board 3 k $\Omega$  feedback resistor and the  $\pm 1$  mA output current typically have  $\pm 1\%$  tolerance or less. This makes the choice of external components very simple and eliminates additional trimming. For example, if a user wishes to derive an output voltage higher than the  $\pm 3$  V swing offered by the output current and feedback resistor combination, all that is required is to combine a standard value resistor with the feedback resistor to achieve the appropriate output voltage swing. T his technique can be extended to include the choice of elements in the deemphasis network, etc.

# **Testing the AD1862**

### **TOTAL HARMONIC D ISTORTION + NOISE**

The THD figure of an audio DAC represents the amount of undesirable signal produced during reconstruction and playback of an audio waveform. The THD specification, therefore, provides a direct method to classify and choose an audio D AC for a desired level of performance.

By combining noise measurement with the THD measurement, a THD+N specification is realized. This specification indicates all of the undesirable signal produced by the D AC, including harmonic products of the test tone as well as noise.

Analog Devices tests all AD1862s on the basis of  $THD+N$  performance. In this test procedure, a digital data stream representing a 0 dB, –20 dB or –60 dB sine wave is sent to the device under test. The frequency of the waveform is 990.5 Hz. Input data is sent to the AD 1862 at an  $8 \times F_s$  rate (352.8 kHz). The AD 1862 under test produces an output current which is conwerted to an qutput voltage by an external amplifier. Figure 10  $\,$ illustrates the recommended test circuit. Deslitchers and trims are not used/during this test procedure. The automatic test equipment digitizes 4096 samples of the output test waveform,  $\frac{1}{2}$  incorporating  $\beta$ 3 dompleted cycles of the sine wave. FFT is performed on the test data.



Figure 9. External Amplifier Connections

Based upon the harmonics of the fundamental 990.5 Hz test tone, and the noise components in the audio band, the total harmonic distortion + noise of the device is calculated. The AD 1862 is available in two performance grades. T he AD 1862N produces a maximum of  $0.0025\%$  THD+N at 0 dB signal levels. T he higher performance AD 1862N -J produces a maximum of  $0.0016\%$  THD+N at 0 dB signal levels.

#### **SIGNAL- TO- NOISE RATIO**

T he Signal-to-N oise Ratio (SN R) of the AD 1862 is tested in the following manner. The amplitude of a  $0$  dB signal is measured. The *flevice under* test is then set to midscale output voltage  $(0)$ olts). The amplitude of all noise present to 30 kHz is measured. The SNR is the ratio of these two measurements. The  $SNR$  figure for the AD 1862 includes the output hoise contributed by the  $NE$ 55 $\beta$ 4 op amp used in the test fixture but does not include the noise-sontributed by the low-pass filter used in the test fixture. The AD1862N has a minimum SNR of 110  $\rm dB$ . The higher performance AD1862N-J has a minimum SNR of 113 dB The frequency of the waveform is 990.5 Hz. Input in mond clistration + noise of the device is clearlined. The<br>
The AD1862 at an 8 × F<sub>3</sub> rate (352.8 kHz). The AD1862 is available in two performance grades. The AD1862<br>
ADT8



Figure 10. Recommended Test Circuit

## **OP TIONAL TRIM AD JUSTMENT**

The AD 1862 includes an external midscale adjust feature. Should an application require improved distortion performance under small and very small signal amplitudes (–60 dB and lower), an adjustment is possible. T wo resistors and one potentiometer form the adjustment network. Figure 11 illustrates the correct configuration of the external components. Analog Devices recommends that this adjustment be performed with –60 dB signal amplitudes or lower. M inor performance improvement is achieved with larger signal amplitudes such as –20 dB. Almost no improvement is possible when this adjustment is performed with 0 dB signal amplitudes.



Figure 11. External Midscale Adjust



Figure 12a. Input Data

## **TIMING**

Figure 12b illustrates the specific timing requirements that must be met in order for the data transfer to be accomplished successfully. The input pins of the AD  $1862$  are both TTL and 5 V CM OS compatible, independent of the power supplies used in the application. T he input requirements illustrated in Figure

12b are compatible with the data outputs provided by popular digital interpolation filter chips used in digital audio playback systems. The AD1862 input clock will run at 17 MHz allowing data to be transferred at a rate of  $16 \times F_S$ . Of course, it will also function at slower rates such as  $2 \times$ ,  $4 \times$  or  $8 \times F_s$ .



Figure 12b. Timing Requirements

The AD1862 is an extremely high performance DAC designed for high-end consumer and professional digital audio applications. Compact disc players, digital preamplifiers, digital musical instruments and sound processors benefit from the extended dynamic range, low THD+Noise and high signal-to-noise ratio. For the first time, the D/A converter is no longer the basic limitation in the performance of a CD player.

T he performance of professional audio gear, such as mixing consoles, digital tape recorders and multivoice synthesizers can utilize the wide dynamic range and signal-to-noise ratio to achieve greater performance. And, the AD 1862's space saving 16-pin package contributes to compact system design. T his permits a system designer to incorporate more voices in multivoice synthesizers, more tracks in multitrack tape recorders and more channels in multichannel mixing consoles.

Furthermore, high-resolution signal processing and waveform generation applications are equally well served by the AD 1862.

## **HIGH PERFORMANCE CD PLAYER**

Figure 13 illustrates the application of AD 1862s in a high performance CD player. T wo AD 1862s are used, one for the left channel and one for the right channel. T he CXD 11XX chip decodes the digital data coming from the read electronics and sends it to the SM 5813. Input data is sent to each AD 1862 by the SM 5813 digital interpolating filter. T his device operates at 8 times oversampling. T he N E5534 op amps are chosen for current-to-voltage converters due to their low distortion and low noise. T he output filters are 5-pole designs. For the purpose of clarity, all bypass capacitors have been omitted from the schematic.



Figure 13. High Performance 20-Bit  $8 \times$  Oversampling CD Player Application

# **HIGH- RESOLUTION SIGNAL P ROCESSING**

Figure 14 illustrates the AD1862 combined with the DSP56000. In high-resolution applications, the combination of the 24-bit architecture of the D SP56000 and the low noise and high resolution of the AD 1862 can produce a high-resolution, low-noise system.

As shown in Figure 14, the clock signal supplied by the D SP processor must be inverted to be compatible with the input of the AD 1862. T he exact architecture of the output low-pass filter depends on the sample rate of the output data. In general, the higher the oversampling rate, the fewer number of filter poles are required to prevent aliasing.

The 20-bit resolution is particularly suitable for professional audio, mixing or equalization equipment. Its resolution allows 24 dB of equalization to be performed on 16-bit input words without signal truncation. Furthermore, up to sixteen 16-bit input words can be mixed and output directly to the AD 1862. In this case, no loss of signal information would be encountered.



## **OTHER DIGITAL AUDIO COMPONENTS AVAILABLE FROM ANALOG DEVICES**



# **OUTLINE D IMENSIONS**

D imensions shown in inches and (mm).



