## **Data Sheet, Version 1.1, 2007-02-26**

# TDA5252 G2 ASK/FSK-915MHz Wireless Transceiver

seem and seemed

# Wireless Control Components

A Road



N e v e r s t o p t h i n k i n g .

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# TDA5252 G2 ASK/FSK 915MHz Wireless Transceiver

# Wireless Control Components



Never stop thinking.

#### **Data Sheet**



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## **ASK/FSK 915MHz Wireless Transceiver TDA5252 G2**

## **Product Info**

#### **General Description**

The IC is a low power consumption single chip FSK/ASK Transceiver for half duplex low datarate communication in the 915MHz band. The IC offers a very high level of integration and needs only a few external components. It contains a highly efficient power amplifier, a low noise amplifier (LNA) with AGC, a double balanced mixer, a complex direct conversion stage, I/ Q limiters with RSSI generation, an FSK demodulator, a fully integrated VCO and PLL synthesizer, a tuneable crystal oscillator, an onboard data filter, a data comparator (slicer), positive and negative peak detectors, a data rate detection circuit and a 2/3-wire bus interface. Additionally there is a power down feature to save battery power.



## **Features**

- Low supply current (I<sub>s</sub> = 9mA typ. receive, I<sub>s</sub> = 13mA typ. transmit mode)
- $-$  Supply voltage range 2.1 5.5V
- Power down mode with very low supply current consumption
- $-$  FSK and ASK modulation and demodulation capability
- Fully integrated VCO and PLL synthesizer and loop filter on-chip with on chip crystal oscillator tuning

## **Application**

- Low Bitrate Communication **Systems**
- Keyless Entry Systems
- Remote Control Systems
- Alarm Systems
- Telemetry Systems
- $-$  I<sup>2</sup>C/3-wire µController Interface
- On-chip low pass channel select filter and data filter with tuneable bandwidth
- $-$  Data slicer with self-adjusting threshold and 2 peak detectors
- FSK sensitivity < -109dBm, ASK sensitivity < -109dBm
- $-$  Transmit power up to  $+13$ dBm
- $-$  Self-polling logic with ultra fast data rate detection
- Electronic Metering
- Home Automation Systems





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## <span id="page-7-1"></span>**1.1 Overview**

The IC is a low power consumption single chip FSK/ASK Transceiver for the ISM frequency band 915MHz. The IC combines a very high level of integration and minimum external part count. The device contains a low noise amplifier (LNA), a double balanced mixer, a fully integrated VCO, a PLL synthesizer, a crystal oscillator with FSK modulator, a limiter with RSSI generator, an FSK demodulator, a data filter, a data comparator (slicer), a positive and a negative data peak detector, a highly efficient power amplifier and a complex digital timing and control unit with  $I<sup>2</sup>C/3$ -wire microcontroller interface. Additionally there is a power down feature to save battery power.

The transmit section uses direct ASK modulation by switching the power amplifier, and crystal oscillator detuning for FSK modulation. The necessary detuning load capacitors are external. The capacitors for fine tuning are integrated. The receive section is using a novel single-conversion/ direct-conversion scheme that is combining the advantages of both receive topologies. The IF is contained on the chip, no RF channel filters are necessary as the channel filter is also on the chip.

The self-polling logic can be used to let the device operate autonomously as a master for a decoding microcontroller.

## <span id="page-7-2"></span>**1.2 Features**

- Low supply current (I<sub>s</sub> = 9 mA typ. receive, I<sub>s</sub> = 13mA typ. transmit mode, both at 3 V supply voltage, 25°C)
- $-$  Supply voltage range 2.1 V to 5.5 V
- $-$  Operating temperature range -40°C to +85°C
- Power down mode with very low supply current consumption
- $-$  FSK and ASK modulation and demodulation capability without external circuitry changes, FM demodulation capability
- Fully integrated VCO and PLL synthesizer and loop filter on-chip with on-chip crystal oscillator tuning, therefore no additional external components necessary
- $-$  Differential receive signal path completely on-chip, therefore no external filters are necessary
- On-chip low pass channel select and data filter with tuneable bandwith
- Data slicer with self-adjusting threshold and 2 peak detectors
- $-$  Self-polling logic with adjustable duty cycle and ultrafast data rate detection and timer mode providing periodical interrupt
- FSK and ASK sensitivity < -109 dBm
- Adjustable LNA gain
- Digital RSSI and Battery Voltage Readout
- Provides Clock Out Pin for external microcontroller
- $-$  Transmit power up to +13 dBm in 50 $\Omega$  load at 5V supply voltage
- $-$  1<sup>2</sup>C/3-wire microcontroller interface, working at max. 400kbit/s



## **Product Description**

## <span id="page-8-0"></span>**1.3 Application**

- Low Bitrate Communication Systems
- Keyless Entry Systems
- Remote Control Systems
- Alarm Systems
- Telemetry Systems
- Electronic Metering
- Home Automation Systems

## <span id="page-8-1"></span>**1.4 Package Outlines**



#### **Figure 1-1 PG-TSSOP-38 package outlines**



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## <span id="page-16-0"></span>**2.3 Functional Block Diagram**





## <span id="page-17-0"></span>**2.4 Functional Block Description**

## <span id="page-17-1"></span>**2.4.1 Power Amplifier (PA)**

The power amplifier is operating in C-mode. It can be used in either high or low power mode. In high-power mode the transmit power is approximately +13dBm into 50 Ohm at 5V and +6dBm at 2.1V supply voltage. In low power mode the transmit power is approximately -3dBm at 5V and -30dBm at 2.1V supply voltage using the same matching network. The transmit power is controlled by the **D0**-bit of the **CONFIG** register (subaddress 00H) as shown in the following **Table 2-2**. The default output power mode is high power mode.



In case of ASK modulation the power amplifier is turned fully on and off by the transmit baseband data, i.e. 100% On-Off-Keying.

## <span id="page-17-2"></span>**2.4.2 Low Noise Amplifier (LNA)**

The LNA is an on-chip cascode amplifier with a voltage gain of 15 to 20dB and symmetrical inputs. It is possible to reduce the gain to 0 dB via logic.



## <span id="page-17-3"></span>**2.4.3 Downconverter 1st Mixer**

The Double Balanced 1<sup>st</sup> Mixer converts the input frequency (RF) in the range of 915MHz down to the intermediate frequency (IF) at approximately 305MHz. The local oscillator frequency is generated by the PLL synthesizer that is fully implemented on-chip as described in **Section 2.4.5**. This local oscillator operates at approximately 1220MHz in receive mode providing the above mentioned IF frequency of 305MHz. The mixer is followed by a low pass filter with a corner frequency of approximately 350MHz in order to prevent RF and LO signals from appearing in the 305MHz IF signal.

## <span id="page-17-4"></span>**2.4.4 Downconverter 2nd I/Q Mixers**

The Low pass filter is followed by 2 mixers (inphase I and quadrature Q) that convert the 305MHz IF signal down to zero-IF. These two mixers are driven by a signal that is generated by dividing the local oscillator signal by 4, thus equalling the IF frequency.



## <span id="page-18-0"></span>**2.4.5 PLL Synthesizer**

The Phase Locked Loop synthesizer consists of two VCOs (i.e. transmit and receive VCO), a divider by 4, an asynchronous divider chain with selectable overall division ratio, a phase detector with charge pump and a loop filter and is fully implemented on-chip. The VCOs are including spiral inductors and varactor diodes. The center frequency of the transmit VCO is 915MHz, the center frequency of the receive VCO is 1220MHz.

Generally in receive mode the relationship between local oscillator frequency  $f_{\rm{osc}}$ , the receive RF frequency f<sub>RF</sub> and the IF frequency f<sub>IF</sub> and thus the frequency that is applied to the I/Q Mixers is given in the following formula:

$$
f_{osc} = 4/3 f_{RF} = 4 f_{IF}
$$
 [2 - 1]

The VCO signal is applied to a divider by 4 which is producing approximately 305MHz signals in quadrature. The overall division ratio of the divider chain following the divider by 4 is 12 in transmit mode and 16 in receive mode as the nominal crystal oscillator frequency is 19.0625MHz. The division ratio is controlled by the **RxTx** pin (pin 5) and the **D10** bit in the **CONFIG** register.

## <span id="page-18-1"></span>**2.4.6 I/Q Filters**

The I/Q IF to zero-IF mixers are followed by baseband  $6<sup>th</sup>$  order low pass filters that are used for RF-channel filtering.



iq\_filter.wmf

## **Figure 2-3 One I/Q Filter stage**

The bandwidth of the filters is controlled by the values set in the filter-register. It can be adjusted between 50 and 350kHz in 50kHz steps via the bits D1 to D3 of the **LPF** register (subaddress 03H).

## <span id="page-18-2"></span>**2.4.7 I/Q Limiters**

The I/Q Limiters are DC coupled multistage amplifiers with offset-compensating feedback circuit and an overall gain of approximately 80dB each in the frequency range of 100Hz up to 350kHz.



Receive Signal Strength Indicator (RSSI) generators are included in both limiters which produce DC voltages that are directly proportional to the input signal level in the respective channels. The resulting I- and Q-channel RSSI-signals are summed to the nominal RSSI signal.

## <span id="page-19-0"></span>**2.4.8 FSK Demodulator**

The output differential signals of the I/Q limiters are fed to a quadrature correlator circuit that is used to demodulate frequency shift keyed (FSK) signals. The demodulator gain is 2.4mV/kHz, the maximum frequency deviation is ±300kHz as shown in **Figure 2-4** below.

The demodulated signal is applied to the ASK/FSK mode switch which is connected to the input of the data filter. The switch can be controlled by the **ASKFSK** pin (pin 4) and via the D11 bit in the CONFIG register.

The modulation index *m* must be significantly larger than 2 and the deviation at least larger than 25kHz for correct demodulation of the signal.



Qaudricorrelator.wmf

#### **Figure 2-4 Typical Quadricorrelator Demodulation Characteristic**

## <span id="page-19-1"></span>**2.4.9 Data Filter**

The 2-pole data filter has a Sallen-Key architecture and is implemented fully on-chip. The bandwidth can be adjusted between approximately 5kHz and 102kHz via the bits **D4** to **D7** of the **LPF** register (see also Table 2-18).





data\_filter.wmf

## **Figure 2-5 Data Filter architecture**

## <span id="page-20-0"></span>**2.4.10 Data Slicer**

The data slicer is a fast comparator with a bandwidth of 100kHz. The self-adjusting threshold is generated by a RC-network (LPF) or by use of one or both peak detectors depending on the baseband coding scheme. This can be controlled by the **D15** bit of the **CONFIG** register as shown in the following table.



## <span id="page-20-1"></span>**2.4.11 Peak Detectors**

Two separate Peak Detectors are available. They are generating DC voltages in a fast-attack and slow-release manner that are proportional to the positive and negative peak voltages appearing in the data signal. These voltages may be used to generate a threshold voltage for non-Manchester encoded signals, for example. The time-constant of the fast-attack/slow-release action is determined by the RC network with external capacitor.

## <span id="page-20-2"></span>**2.4.12 Crystal Oscillator**

The reference oscillator is an NIC oscillator type (Negative Impedance Converter) with a crystal operating in serial resonance. The nominal operating frequency of 19.0625MHz and the frequencies for FSK modulation can be adjusted via 3 external capacitors. Via microcontroller and bus interface the chip-internal capacitors can be used for finetuning of the nominal and the FSK modulation frequencies. This finetuning of the crystal oscillator allows to eliminate frequency errors due to crystal or component tolerances.

## <span id="page-20-3"></span>**2.4.13 Bandgap Reference Circuitry and Powerdown**

A Bandgap Reference Circuit provides a temperature stable 1.2V reference voltage for the device. A power down mode is available to switch off all subcircuits that are controlled by the bidirectional Powerdown&DataDetect **PwdDD** pin (pin 27) as shown in the following table. Power down mode can either be activated by pin 27 or bit D14 in Register 00h. In power down mode also pin 28 (DATA) is affected (see **Section 2.4.17**).





## <span id="page-21-0"></span>**2.4.14 Timing and Data Control Unit**

The timing and data control unit contains a wake-up logic unit, an  $I^2C/3$ -wire microcontroller interface, a "data valid" detection unit and a set of configuration registers as shown in the subsequent figure.



logic.wmf

#### **Figure 2-6 Timing and Data Control Unit**

The  $I^2C$  / 3-wire Bus Interface gives an external microcontroller full control over important system parameters at any time.

It is possible to set the device in three different modes: Slave Mode, Self Polling Mode and Timer Mode. This is done by a state machine which is implemented in the WAKEUP LOGIC unit. A detailed description is given in **Section 2.4.16**.



The DATA VALID DETECTOR contains a frequency window counter and an RSSI threshold comparator. The window counter uses the incoming data signal from the data slicer as the gating signal and the crystal oscillator frequency as the timebase to determine the actual datarate. The result is compared with the expected datarate.

The threshold comparator compares the actual RSSI level with the expected RSSI level.

If both conditions are true the **PwdDD** pin is set to LOW in self polling mode as you can see in **Section 2.4.16**. This signal can be used as an interrupt for an external µP. Because the **PwdDD** pin is bidirectional and open drain driven by an internal pull-up resistor it is possible to apply an external LOW thus enabling the device.

## <span id="page-22-0"></span>**2.4.15 Bus Interface and Register Definition**

The TDA5252 supports the  $1^2C$  bus protocol (2 wire) and a 3-wire bus protocol. Operation is selectable by the **BusMode** pin (pin 2) as shown in the following table. All bus pins (BusData, BusCLK, **EN**, BusMode) have a Schmitt-triggered input stage. The BusData pin is bidirectional where the output is open drain driven by an internal 15k $\Omega$  pull up resistor.





i2c\_3w\_bus.wmf

#### **Figure 2-7 Bus Interface**

**Note:** The Interface is able to access the internal registers at any time, even in POWER DOWN mode. There is no internal clock necessary for Interface operation.



## **I <sup>2</sup>C Bus Mode**

In this mode the **BusMode** pin (pin 2) = LOW and the **EN** pin (pin 24) = LOW.

#### Data Transition:

Data transition on the pin BusData can only occur when BusCLK is LOW. BusData transitions while BusCLK is HIGH will be interpreted as start or stop condition.

#### Start Condition (STA):

A start condition is defined by a HIGH to LOW transition of the BusData line while BusCLK is HIGH. This start condition must precede any command and initiate a data transfer onto the bus.

#### Stop Condition (STO):

A stop condition is defined by a LOW to HIGH transition of the BusData line while BusCLK is HIGH. This condition terminates the communication between the devices and forces the bus interface into the initial state.

#### Acknowledge (ACK):

Indicates a successful data transfer. The transmitter will release the bus after sending 8 bit of data. During the 9th clock cycle the receiver will set the SDA line to LOW level to indicate it has received the 8 bits of data correctly.

#### Data Transfer Write Mode:

To start the communication, the bus master must initiate a start condition (STA), followed by the 8bit chip address. The chip address for the TDA5252 is fixed as "1110000" (MSB at first). The last bit (LSB=A0) of the chip address byte defines the type of operation to be performed:

A0=0, a write operation is selected and A0=1 a read operation is selected.

After this comparison the TDA5252 will generate an ACK and awaits the desired sub address byte (00H...0FH) and data bytes. At the end of the data transition the master has to generate the stop condition (STO).

#### Data Transfer Read Mode:

To start the communication in the read mode, the bus master must initiate a start condition (STA), followed by the 8 bit chip address (write: A0=0), followed by the sub address to read (80H, 81H), followed by the chip address (read: A0=1). After that procedure the data of the selected register (80H, 81H) is read out. During this time the data line has to be kept in HIGH state and the chip sends out the data. At the end of data transition the master has to generate the stop condition (STO).



## **Bus Data Format in I2C Mode**









\* mandatory HIGH

#### **3-wire Bus Mode**

In this mode pin 2 (BusMode)= HIGH and Pin 16 (BusData) is in the data input/output pin. Pin 24  $(\overline{EN})$  is used to activate the bus interface to allow the transfer of data to / from the device. When pin 24 ( $\overline{\text{EN}}$ ) is inactive (HIGH), data transfer is inhibited.

Data Transition:

Data transition on pin 16 (BusData) can only occur if the clock BusCLK is LOW. To perform a data transfer the interface has to be enabled. This is done by setting the EN line to LOW. A serial transfer is done via BusData, BusCLK and  $\overline{\text{EN}}$ . The bit stream needs no chip address.

Data Transfer Write Mode:

To start the communication the EN line has to be set to LOW. The desired sub address byte and data bytes have to follow. The subaddress (00H...0FH) determines which of the data bytes are transmitted. At the end of data transition the EN must be HIGH.

Data transfer Read Mode:

To start the communication in the read mode, the EN line has to be set to LOW followed by the sub address to read (80H, 81H). Afterwards the device is ready to read out data. At the end of data transition EN must be HIGH.



## **Bus Data Format 3-wire Bus Mode**





## **Register Definition**

#### **Sub Addresses Overview**



register\_overview.wmf

#### **Figure 2-8 Sub Addresses Overview**



## **Subaddress Organization**





## **Data Byte Specification**



**Note D3:** Function is only active in selfpolling and timer mode. When D3 is set to LOW the RX path is not enabled if PwdDD pin is set to LOW. A delayed setting of D3 results in a delayed power ON of the RX building blocks.



























## <span id="page-29-0"></span>**2.4.16 Wakeup Logic**



#### **Figure 2-9 Wakeup Logic States**



**SLAVE MODE:** The receive and transmit operation is fully controlled by an external control device via the respective **RxTx**, **AskFsk**, **PwdDD**, and **Data** pins. The wakeup logic is inactive in this case.

After RESET or 1<sup>st</sup> Power-up the chip is in SLAVE MODE. By setting MODE\_1 and MODE\_2 in the CONFIG register the mode may be changed.

**SELF POLLING MODE:** The chip turns itself on periodically to receive using a built-in 32kHz RC oscillator. The timing of this is determined by the **ON\_TIME** and **OFF\_TIME** registers, the duty cycle can be set between 0 and 100% in 31.25µs increments. The data detect logic is enabled and a 15µs LOW impulse is provided at **PwdDD** pin (Pin 27), if the received data is valid.



timing\_selfpllmode.wmf

#### **Figure 2-10 Timing for Self Polling Mode (ADC & Data Detect in one shot mode)**



**Note:** The time delay between start of ON time and the 15µs LOW impulse is 2.6ms + 3 period of data rate.

If ADC & Data Detect Logic are in continuous mode the 15µs LOW impulse is applied at **PwdDD** after each data valid decision.

In self polling mode if D9=0 (Register 00h) and when **PwdDD** pin level is HIGH the CLK output is on during ON time and off during OFF time. If D9=1, the CLK output is always on.

**TIMER MODE:** Only the internal Timer (determined by the **ON\_TIME** and **OFF\_TIME** registers) is active to support an external logic with periodical Interrupts. After ON\_TIME + OFF\_TIME a 15µs LOW impulse is applied at the **PwdDD** pin (Pin 27).



timing\_timermode.wmf

## **Figure 2-11 Timing for Timer Mode**

## <span id="page-30-0"></span>**2.4.17 Data Valid Detection, Data Pin**

Data signals generate a typical spectrum and this can be used to determine if valid data is on air.



data\_rate\_detect.wmf

#### **Figure 2-12 Frequency and RSSI Window**

The "data valid" criterion is generated from the result of RSSI-TH3 comparison and t<sub>GATE</sub> between TH1 and TH2 result as shown below. In case of Manchester coding the 0,5\*TH1 and 0,5\*TH2 gives improved performance.

The use of permanent data valid recognition makes it absolutely necessary to set the RSSI-ADC and the Window counter into continuous mode (Register 00H, Bit  $D5 = D6 = 1$ ).





data\_valid.wmf

## **Figure 2-13 Data Valid Circuit**

D\_OUT and RX\_DATA\_INV from the CONFIG register determine the output of data at Pin 28. **RxTxint** and TX ON are internally generated signals.

In RX and power down mode Data pin (Pin 28) is tied to GND.



data\_switch.wmf

#### **Figure 2-14 Data Input/Output Circuit**

## <span id="page-31-0"></span>**2.4.18 Sequence Timer**

The sequence timer has to control all the enable signals of the analog components inside the chip. The time base is the 32 kHz RC oscillator.

After the first POWER ON or RESET a 1.06MHz clock is available at the clock output pin. This clock output can be used by an external  $\mu$ P to set the system into the desired state and outputs valid data after 500 µs (see **Figure 2-15** and **Figure 2-16**,  $t_{\text{CI KSI}}$ )

There are two possibilities to start the device after a reset or first power on:

- PWDDD pin is LOW: Normal operation timing is performed after t<sub>SYSSU</sub> (see Figure 2-15).
- − PWDDD pin is HIGH (device in power down mode): A clock is offered at the clock output pin until the device is activated (PWDDD pin is pulled to LOW). After the first activation the time t<sub>SYSSU</sub> is required until normal operation timing is performed (see Figure 2-16). This could be used to extend the clock generation without device programming or activation.

**Note:** It is **required** to activate the device for the duration of  $\frac{1}{2}$  after first power on or a reset. Only if this is done the normal operation timing is performed.



With default settings the clock generating units are disabled during PD, therefore no clock is available at the clock output pin. It is possible to offer a clock signal at the clock output pin every time (also during PD) if the CLK\_EN Bit in the CONFIG register is set to HIGH.



Sequenzer\_Timing\_pupstart.wmf

### **Figure 2-15 1st start or reset in active mode**

**Note:** The time values are typical values



Sequenzer\_Timing\_pdstart.wmf

#### **Figure 2-16 1st start or reset in PD mode**

\* State is either "I" or "O" depending on time of setting into powerdown.

**Note:** The time values are typical values



This means that the device needs  $t_{\text{DDSU}}$  setup time to start the data detection after RX is activated. When activating TX it requires  $t_{TXSU}$  setup time to enable the power amplifier. For timing information refer to **Table 4-3**.

For test purposes a TESTMODE is provided by the Sequencer as well. In this mode the BLOCK\_PD register be set to various values. This will override the Sequencer timing. Depending on the settings in Config Register 00H the corresponding building blocks are enabled, as shown in the subsequent figure.



#### **Figure 2-17 Sequencerës capability**

## <span id="page-33-0"></span>**2.4.19 Clock Divider**

It supports an external logic with a programmable Clock at **pin 26 (CLKDIV)**.



clk\_div.wmf

#### **Figure 2-18 Clock Divider**

The Output Selection and Divider Ratio can be set in the CLK\_DIV register.





**Note:** Data are valid 500 µs after the crystal oscillator is enabled (see **Figure 2-15** and **Figure 2- 16**, t<sub>CLKSU</sub>).



**Note:** As long as default settings are used, there is no clock available at the clock output during Power Down. It is possible to enable the clock during Power Down by setting CLK\_EN (Bit D9) in the Config Register (00H) to HIGH.

## <span id="page-34-0"></span>**2.4.20 RSSI and Supply Voltage Measurement**

The input of the 6Bit-ADC can be switched between two different sources: the RSSI voltage (default setting) or a resistor network dividing the Vcc voltage by 5.





To prevent wrong interpretation of the ADC information (read from Register 81H: ADC) you can use the ADC- Power Down feedback Bit (D7) and the SELECT feedback Bit (D6) which correspond to the actual measurement.

**Note:** As shown in **Section 2.4.18** there is a setup time of 2.6ms after RX activating. Thus the measurement of RSSI voltage does only make sense after this setup time.


# **3 Application**

## **3.1 LNA and PA Matching**

## **3.1.1 RX/TX Switch**



RX/TX\_Switch.wmf

### **Figure 3-1 RX/TX Switch**

The RX/TX-switch combines the PA-output and the LNA-input into a single 50 Ohm SMAconnector. Two pin-diodes are used as switching elements. If no current flows through a pin diode, it works as a high impedance for RF with very low capacitance. If the pin-diode is forward biased, it provides a low impedance path for RF. (some Ω)

### **3.1.2 Switch in RX-Mode**

The RX/TX-switch is set to the receive mode by either applying a high level or an open to the RX/ TX-jumper on the evalboard or by leaving it open. Then both pin-diodes are not biased and therefore have a high impedance.





### **Figure 3-2 RX-Mode**

The RF-signal is able to run from the RF-input-SMA-connector to the LNA-input-pin LNI via C1, C2, C7, L3 and C9. R1 does not affect the matching circuit due to its high resistance. The other input of the differential LNA LNIX can always be AC-grounded using a large capacitor without any loss of performance. In this case the differential LNA can be used as a single ended LNA, which is easier to match. The S11 of the LNA at pin LNI on the evalboard is 0.931 / -44° (equals a resistor of 1.2kOhm in parallel to a capacitor of 1.4pF) for both high and low-gain-mode of the LNA. (pin LNIX AC-grounded) This impedance has to be matched to 50 Ohm with the parts C9, L3, C7 and C2. C1 is a DC-decoupling-capacitor. On the evalboard the most important matching components are (shunt) L3 and (series)C7, C2. The capacitors is mainly a DC-decoupling-capacitor and may be used for some fine tuning of the matching circuit. A good CAE tool (featuring smith-chart) may be used for the calculation of the values of the components. However, the final values of the matching components always have to be found on the board because of the parasitics of the board, which highly influence the matching circuit at RF.



#### Measured Magnitude of S11 of evalboard:



S11\_measured\_915.pcx.

#### **Figure 3-3 S11 measured**

Above you can see the measured S11 of the evalboard. The -3dB-points are at 851MHz and 989MHz. So the 3dB-bandwidth is:

$$
B = f_U - f_L = 989MHz - 851MHz = 138MHz
$$
\n
$$
Q_L = \frac{f_{center}}{B} = \frac{915MHz}{138MHz} = 6.63
$$
\n[3 - 2]

The unloaded Q of the resonant circuit is equal to the Q of the inductor due to its losses.

$$
Q_U = Q_{INDUCTOR} \approx 36@915MHz
$$
 [3-3]

An approximation of the losses of the input matching network can be made with the formula:

$$
Loss = -20 * log\left[1 - \frac{Q_L}{Q_U}\right] = -20 * log\left[1 - \frac{6.63}{36}\right] = 1,8dB
$$
\n[3 - 4]



The noise figure of the LNA-input-matching network is equal to its losses. The input matching network is always a compromise of sensitivity and selectivity. The loaded Q should not get too high because of 2 reasons:

more losses in the matching network and hence less sensitivity

tolerances of components affect matching too much. This will cause problems in a tuning-free mass production of the application. A good CAE-tool will help to see the effects of component tolerances on the input matching more accurate by tweaking each value.

A very high selectivity can be reached by using SAW-filters at the expense of higher cost and lower sensitivity which will be reduced by the losses of the SAW-Filter of approx. 4dB.

#### *Image-suppression:*

Due to the quite high 1<sup>st</sup>-IF of the frontend, the image frequency is quite far away. The image frequency of the receiver is at:

$$
f_{\text{IMAGE}} = f_{\text{SIGNAL}} + 2 \cdot f_{\text{IF}} = 915 \, \text{MHz} + 2 \cdot 305 = 1525 \, \text{MHz}
$$
\n
$$
[3 - 5]
$$

The image suppression on the evalboard is about 17dB.

#### LO-leakage:

The LO of the  $1<sup>st</sup>$  Mixer is at:

$$
f_{LO} = f_{RECEIVE} * \frac{4}{3} = 915 MHz * \frac{4}{3} = 1220 MHz
$$
 [3 - 6]

The LO-leakage of the evalboard on the RF-input is about -90dBm.

### **3.1.3 Switch in TX-Mode**

The evalboard can be set into the TX-Mode by grounding the RX/TX-jumper on the evalboard or programming the TDA5255 to operate in the TX-Mode. If the IC is programmed to operate in the TX-Mode, the RX/TX-pin will act as an open drain output at a logical LOW. Then a DC-current can flow from VCC to GND via L1, L2, D1, R1 and D2.

$$
I_{\text{PIN-DIODE}} = \frac{Vcc - 2*V_{\text{FORWARDPIN-DIODE}}}{R_1}
$$

Now both pin-diodes are biased with a current of approx. 0.3mA@3V and have a very low impedance for RF.





TX\_Mode.wmf

### **Figure 3-4 TX\_Mode**

R1 does not influence the matching because of its very high resistance. Due to the large capacitance of C1, C6 and C5 the circuit can be further simplified for RF:



#### **Figure 3-5 TX\_Mode\_simplified**

The LNA-matching is RF-grounded now, so no power is lost in the LNA-input. The PA-matching consists of C2, C3 L2, C4 and L1.

When designing the matching of the PA, C2 must not be changed anymore because its value is already fixed by the LNA-input-matching.



## **3.1.4 Power-Amplifier**

The power amplifier operates in a high efficient class C mode. This mode is characterized by a pulsed operation of the power amplifier transistor at a current flow angle of  $\theta \lt \lt \pi$ . A frequency selective network at the amplifier output passes the fundamental frequency component of the pulse spectrum of the collector current to the load. The load and its resonance transformation to the collector of the power amplifier can be generalized by the equivalent circuit of **Figure 3-6**. The tank circuit L//C//RL in parallel to the output impedance of the transistor should be in resonance at the operating frequency of the transmitter.



Equivalent\_power\_wmf.

#### **Figure 3-6 Equivalent power amplifier tank circuit**

The optimum load at the collector of the power amplifier for "critical" operation under idealized conditions at resonance is:

$$
R_{LC} = \frac{V_s^2}{2P_o} \tag{3-8}
$$

A typical value of  $\mathsf{R}_{\mathsf{LC}}$  for an RF output power of  $\mathsf{P}_{\mathsf{O}}$ = 13mW is:

 $=350\Omega$ ∗  $=\frac{3}{2 \cdot 2 \cdot 3} = 350$  $2 * 0.013$  $3<sup>2</sup>$  $R_{LC} = \frac{3}{2 \times 0.012} = 350 \Omega$  [3 - 9]

Criticalî operation is characterized by the RF peak voltage swing at the collector of the PA transistor to just reach the supply voltage  $V_S$ . The high efficiency under "critical" operating conditions can be explained by the low power loss at the transistor.

During the conducting phase of the transistor there is no or only a very small collector voltage present, thus minimizing the power loss of the transistor ( $i<sub>C</sub>$ \*u<sub>CE</sub>). This is particularly true for low current flow angles of  $\theta \leq \pi$ . In practice the RF-saturation voltage of the PA transistor and other parasitics will reduce the "critical"  $R_{LC}$ .

The output power P<sub>O</sub> will be reduced when operating in an "overcritical" mode at a R<sub>L</sub> > R<sub>LC</sub>. As shown in Figure 3-7, however, power efficiency E (and bandwidth) will increase by some degree when operating at higher  $\mathsf{R}_\mathsf{L}.$  The collector efficiency E is defined as



$$
E = \frac{P_o}{V_s I_c} \tag{3-10}
$$

The diagram of Figure 3-7 has been measured directly at the PA-output at  $V_S$ =3V. A power loss in the matching circuit of about 3dB will decrease the output power. As shown in the diagram, 250 Ohm is the optimum impedance for operation at 3V. For an approximation of  $R_{\text{OPT}}$  and  $P_{\text{OUT}}$  at other supply voltages those 2 formulas can be used:

$$
R_{OPT} \sim V_s \tag{3-11}
$$

and

$$
P_{OUT} \sim R_{OPT} \tag{3-12}
$$

The behaviour of the power amplifier over the impedance and frequency is in principle the same as of the TDA5250, but of course strongly depends on the matching network. (see also specification of TDA5250)



Power\_E\_vs\_RL.wmf

## **Figure 3-7 Output power P**o **(mW) and collector efficiency E vs. load resistor R**L **.**

The DC collector current I<sub>C</sub> of the power amplifier and the RF output power P<sub>O</sub> vary with the load resistor R<sub>L</sub>. This is typical for overcritical operation of class C amplifiers. The collector current will show a characteristic dip at the resonance frequency for this type of "overcritical" operation. The depth of this dip will increase with higher values of  $\mathsf{R}_\mathsf{L}.$ 



As **Figure 3-8** shows, detuning beyond the bandwidth of the matching circuit results in a significant increase of collector current of the power amplifier and in some loss of power. This diagram shows the data of the circuit of the test board around the center frequency of 915MHz.



PA-out\_&\_I-collector\_vs\_frequency.wmf

#### **Figure 3-8 PA-out & I-collector vs. frequency**

C4, L2 and C3||C2 are the main matching components which are used to transform the 50 Ohm load at the SMA-RF-connector to a higher impedance at the PA-output (250Ohm@3V). L1 can be used for finetuning of the resonance frequency but should not be too low in order to keep its loss low.

The transformed impedance of 250Ohm+j0 at the PA-output-pin can be verified with a network analyzer using this measurement procedure:

- 1. Calibrate your network analyzer.
- 2. Connect a short, low-loss 50 Ohm cable to your network analyzer with an open end on one side. Semirigid cable works best.
- 3. Use the "Port Extension" feature of your network analyzer to shift the reference plane of your network analyzer to the open end of the cable.
- 4. Connect the center-conductor of the cable to the solder pad of the pin "PA" of the IC. The shield has to be grounded. Very short connections must be used. Do not remove the IC or any part of the matching-components!
- 5. Screw a 50Ohm-dummy-load on the RF-I/O-SMA-connector
- 6. The TDA5255 has to be in ASK-TX-Mode, Data-Input=LOW.
- 7. Be sure that your network analyzer is AC-coupled and turn on the power supply of the IC.
- 8. Measure the S-parameter



The evalboard has been optimized for 3V. The load is about 250+j0 at 915MHz.

A tuning-free realization requires a careful design of the components within the matching network. A simple linear CAE-tool will help to see the influence of tolerances of matching components.

Suppression of spurious harmonics may require some additional filtering within the antenna matching circuit. Both can be seen in **Figure 3-9** and **Figure 3-10** The total spectrum of the evalboard can be summarized as:

- Carrier fc +9dBm
- fc-18.1MHz -69dBm
- fc+18.1MHz -72dBm
- 2<sup>nd</sup> harmonic -45dBm
- 3<sup>rd</sup> harmonic -49dBm



spectrum\_13.2GHz.bmp







spektrum\_300MHz.bmp

#### **Figure 3-10 Transmit Spectrum 300MHz**

## **3.2 Crystal Oscillator**

The equivalent schematic of the crystal with its parameters specified by the crystal manufacturer can be taken from the subsequent figure.

Here also the load capacitance of the crystal  $C_\mathsf{L}$ , which the crystal wants to see in order to oscillate at the desired frequency, can be seen.



#### **Figure 3-11 Crystal**

- $L_1$ : : motional inductance of the crystal
- $C_1$ : : motional capacitance of the crystal
- $C_0$ : : shunt capacitance of the crystal

 $[3 - 14]$ 



## Therefore the **Resonant Frequency f<sub>S</sub> of the crystal is defined as:**

$$
f_S = \frac{1}{2\pi\sqrt{L_1 * C_1}}\tag{3-13}
$$

The **Series Load Resonant Frequency f**S<sup>t</sup> of the crystal is defined as:

$$
f_s = \frac{1}{2\pi\sqrt{L_1 * C_1}} * \sqrt{1 + \frac{C_1}{C_0 + C_L}}
$$

regarding **Figure 3-11**

f<sub>s</sub>' is the nominal frequency of the crystal with a specified load when tested by the crystal manufacturer.

**Pulling Sensitivity** of the crystal is defined as the magnitude of the relative change in frequency relating to the variation of the load capacitor.

$$
\frac{\delta D}{\delta C_L} = \frac{\delta f'_s}{\delta C_L} = \frac{-C_1}{2(C_0 + C_L)^2}
$$
 [3 - 15]

Choosing C<sub>L</sub> as large as possible results in a small pulling sensitivity. On the other hand a small C<sub>L</sub> keeps the influence of the serial inductance and the tolerances associated to it small (see **formula [3-17]**).

#### **Start-up Time**

where: -R: is the negative impedance of the oscillator see **Figure 3-11**  $R_{\mathsf{ext}}$ : is the sum of all external resistances (e.g.  $R_1$  or any other resistance that may be present in the circuit, see **Figure 3-10** *start*  $\left| -R \right| - R_{ext}$  $t_{Start} \sim \frac{L}{1 - L}$ −−  $\sim \frac{L_1}{|S_1 - S_2|}$  [3 – 16]

The proportionality of L<sub>1</sub> and C<sub>1</sub> of the crystal is defined by **formula [3-13]**. For a crystal with a small  $C_1$  the start -up time will also be slower. Typically the lower the value of the crystal frequency, the lower the  $\textsf{C}_1.$ 

A short **conclusion** regarding crystal and crystal oscillator dependencies is shown in the following table:





The crystal oscillator in the TDA5252 is a NIC (negative impedance converter) oscillator type. The input impedance of this oscillator is a negative impedance in series to an inductance. Therefore the load capacitance of the crystal  $C_{L}$  (specified by the crystal supplier) is transformed to the capacitance C<sub>v</sub> as shown in **formula [3-17].** 



QOSZ\_NIC.wmf

### **Figure 3-12 Crystal Oscillator**

$$
C_L = \frac{1}{\frac{1}{C_V} - \omega^2 L_{\text{osc}}} \leftrightarrow C_V = \frac{1}{\frac{1}{C_L} + \omega^2 L_{\text{osc}}}
$$
 [3 - 17]



With the aid of this formula it becomes obvious that the higher the serial capacitance  $C_V$  is, the higher is the influence of  $L<sub>OSC</sub>$ .

The tolerance of the internal oscillator inductivity is much higher, so the inductivity is the dominating value for the tolerance.

FSK modulation and tuning are achieved by a variation of  $C_{v}$ .



In case of small frequency deviations (up to +/- 1000 ppm), the desired load capacitances for FSK modulation are frequency depending and can be calculated with the formula below.

$$
C_{L \pm} = \frac{C_{L} \mp C_{0} \cdot \frac{\Delta f}{N \cdot f} \cdot \left(1 + \frac{2 \cdot (C_{0} + C_{L})}{C_{1}}\right)}{1 \pm \frac{\Delta f}{N \cdot f} \cdot \left(1 + \frac{2 \cdot (C_{0} + C_{L})}{C_{1}}\right)}
$$
 [3 - 18]  
C<sub>L</sub>: crystal load capacitance for nominal frequency

 $C_0$ : : shunt capacitance of the crystal

 $C_1$ : : motional capacitance of the crystal

- f: crystal oscillator frequency
- N: division ratio of the PLL
- ∆f: peak frequency deviation

With  $C_{L+}$  and  $C_{L-}$  the necessary  $C_{v+}$  for FSK HIGH and  $C_{v-}$  for FSK LOW can be calculated.

Alternatively, an external AC coupled (10nF in series to 1kΩ) signal can be applied at **pin 19 (Xout)**. The drive level should be approximately 100mVpp.

### **3.2.1 Synthesizer Frequency setting**

Generating ASK and FSK modulation 3 setable frequencies are necessary.

## **3.2.1.1 Possible crystal oscillator frequencies**

The resulting possible crystal oscillator frequencies are shown in the following **Figure 3-13**



free\_reg.wmf

#### **Figure 3-13 possible crystal oscillator frequencies**

In ASK receive mode the crystal oscillator is set to frequency  $\mathsf{f}_2$  to realize the necessary frequency offset to receive the ASK signal at  $f_0^{\star}N$  (N: division ratio of the PLL).



To set the 3 different frequencies 3 different  $C_{\rm v}$  are necessary. Via internal switches 3 external capacitors can be combined to generate the necessary  $C_{\rm v}$  in case of ASK- or FSK-modulation. Internal banks of switchable capacitors allow the finetuning of these frequencies.

## **3.2.2 Transmit/Receive ASK/FSK Frequency Assignment**

Depending on whether the device operates in transmit or receive mode or whether it operates in ASK or FSK the following cases can be distinguished:

## **3.2.2.1 FSK-mode**

In **transmit** mode the two frequencies representing logical HIGH and LOW data states have to be adjusted depending on the intended frequency deviation and separately according to the following formulas:

 $f_{\text{COSC HI}} = (f_{\text{RF}} + f_{\text{DEV}})/48$   $f_{\text{COSC LOW}} = (f_{\text{RF}} - f_{\text{DEV}})/48$ e.g.  $f_{\text{COSC HI}} = (915E6 + 50E3) / 48 = 19,0635167 \text{MHz}$  $f_{\text{COSC}\,\text{LOW}}$  = (915E6 - 50E3) / 48 = 19,0614583MHz  $[3 - 19]$ 

with a frequency deviation of 50kHz.

**Figure 3-14** shows the configuration of the switches and the capacitors to achieve the 2 desired frequencies. Gray parts of the schematics indicate inactive parts. For FSK modulation the ASKswitch is always open.

For FSK LOW the FSK-switch is closed and  $C_{v2}$  and  $C_{tune2}$  are bypassed. The effective  $C_{v-}$  is given by:

 $C_{V^-} = C_{v1} + C_{ture1}$  $[3 - 20]$ 

For finetuning C<sub>tune1</sub> can be varied over a range of 8 pF in steps of 125fF. The switches of this Cbank are controlled by the bits **D0** to **D5** in the **FSK** register (subaddress 01H, see **Table 3-6**).

For **FSK HIGH** the FSK-switch is open. So the effective  $C_{v+}$  is given by:

$$
C_{V^+} = \frac{(C_{V1} + C_{tune1}) \cdot (C_{V2} + C_{tune2})}{C_{V1} + C_{tune1} + C_{V2} + C_{tune2}}
$$
 [3 - 21]

The C-bank C $_{\text{tune2}}$  can be varied over a range of 16 pF in steps of 250fF for finetuning of the FSK HIGH frequency. The switches of this C-bank are controlled by the bits **D8** to **D13** in the **FSK** register (subaddress 01H, **see Table 3-6**).





QOSC\_FSK.wmf

 $[3 - 22]$ 

#### **Figure 3-14 FSK modulation**

In **receive** mode the crystal oscillator frequency is set to yield a direct-to-zero conversion of the receive data. Thus the frequency may be calculated as

 $f<sub>COSC</sub> = f<sub>RF</sub> / 48$ ,

e.g.

 $f_{\text{COSC}}$  = 915E6 / 48 = 19.0625MHz

which is identical to the ASK transmit case.



QOSC\_ASK.wmf

#### **Figure 3-15 FSK receive**

In this case the ASK-switch is closed. The necessary  $C_{vm}$  is given by:



$$
C_{vm} = \frac{(C_{v1} + C_{tune1}) \cdot (C_{v2} + C_{v3} + C_{tune2})}{C_{v1} + C_{tune1} + C_{v2} + C_{v3} + C_{tune2}}
$$
 [3 - 23]

The C-bank C<sub>tune2</sub> can be varied over a range of 16 pF in steps of 250fF for finetuning of the FSK receive frequency. In this case the switches of the C-bank are controlled by the bits **D0** to **D5** of the **XTAL\_TUNING** register (subaddress 02H, **see Table 3-5**).

## **3.2.2.2 ASK-mode:**

In **transmit** mode the crystal oscillator frequency is the same as in the FSK receive case, **see Figure 3-15**.

In **receive** mode a receive frequency offset is necessary as the limiters feedback is AC-coupled. This offset is achieved by setting the oscillator frequency to the FSK HIGH transmit frequency, **see Figure 3-14**.

### **3.2.3 Parasitics**

For the correct calculation of the external capacitors the parasitic capacitances of the pins and the switches  $(C_{20}, C_{21}, C_{22})$  have to be taken into account.



QOSC\_parasitics.wmf







With the given parasitics the actual  $\mathsf{C}_\mathsf{v}$  can be calculated:

$$
C_{V} = C_{V1} + C_{tune1} + C_{21}
$$
 [3 – 24]

$$
C_{v+} = \frac{(C_{v1} + C_{tune1}) \cdot (C_{v2} + C_{20} + C_{tune2})}{C_{v1} + C_{tune1} + C_{v2} + C_{20} + C_{tune2}} + C_{21}
$$
 [3 - 25]

$$
C_{vm} = \frac{(C_{v1} + C_{tune1}) \cdot (C_{v2} + C_{20} + C_{v3} + C_{22} + C_{tune2})}{C_{v1} + C_{tune1} + C_{v2} + C_{20} + C_{v3} + C_{22} + C_{tune2}} + C_{21}
$$
 [3 - 26]

**Note**: Please keep in mind also to include the Pad parasitics of the circuit board.

### **3.2.4 Calculation of the external capacitors**

1. Determination of necessary crystal frequency using **formula [3-19].**

e.g.  $f_{FSK}$  =  $f_{COSC \,LOW}$ 

2. Determine corresponding C<sub>Load</sub> applying **formula [3-18]**.

e.g. CL FSK- = CL ±

3. Necessary  $C_V$  using **formula [3-17]**.

e.g.

$$
C_{V-} = \frac{1}{\frac{1}{C_{L,FSK-}} + (2\pi f_{FSK-})^2 * L_{OSC}}
$$

1. When the necessary  $C_{\rm v}$  for the 3 frequencies ( $C_{\rm v}$  for FSK LOW,  $C_{\rm v+}$  for FSK HIGH and  $C_{\rm v<sub>m</sub>}$  for FSK-receive) are known the external capacitors and the internal tuning caps can be calculated using the following formulas:



-FSK: 
$$
C_{v1}
$$

$$
C_{v1} + C_{tune1} = C_{v} - C_{21}
$$
 [3-27]

$$
+ FSK:
$$

$$
C_{v2} + C_{tune2} = \frac{(C_{v1} + C_{tune1}) \cdot (C_{v+} - C_{21})}{(C_{v1} + C_{tune1}) - (C_{v+} - C_{21})} - C_{20}
$$
 [3-28]

 $C_{\text{v3}} + C_{\text{tune2}}$  $(C_{\text{v1}} + C_{\text{tune1}}) \cdot (C_{\text{vm}} - C_{21})$  $= \frac{C_{v1} + C_{tunel}}{(C_{v1} + C_{tunel}) - (C_{vm} - C_{21})} - C_{20} - C_{v2} - C_{22}$ FSK\_RX:

To compensate frequency errors due to crystal and component tolerance  $C_{v1}$ ,  $C_{v2}$  and  $C_{v3}$  have to be varied. To enable this correction, half of the necessary capacitance variation has to be realized with the internal C-banks.

If no finetuning is intended it is recommended to leave XIN (Pin 21) open. So the parasitic capacitance of Pin 21 has no effect.

**Note**: Please keep in mind also to include the Pad parasitics of the circuit board.

In the suitable range for the serial capacitor, either capacitors with a tolerance of 0.1pF or 1% are available.

A spreadsheet, which can be used to predict the total frequency error by simply entering the crystal specification, may be obtained from Infineon.

## **3.2.5 FSK-switch modes**

The FSK-switch can be used either in a bipolar or in a FET mode. The mode of this switch is controlled by bit **D0** of the **XTAL\_CONFIG** register (subaddress 0EH).

In the bipolar mode the FSK-switch can be controlled by a ramp function. This ramp function is set by the bits D1 and D2 of the XTAL\_CONFIG register (subadress 0EH). With these modes of the FSK-switch the bandwidth of the FSK spectrum can be influenced.

When working in the FET mode the power consumption can be reduced by about 200 µA.

The default mode is bipolar switch with no ramp function ( $D0 = 1$ ,  $D1 = D2 = 0$ ), which is suitable for all bitrates.





## **3.2.6 Finetuning and FSK modulation relevant registers**

**Case FSK-RX or ASK-TX (C**tune2**)**:



# **Case FSK-TX or ASK-RX (C**tune1 **and C**tune2**):**



#### **Default values**

In case of using the evaluation board, the crystal with its typical parameters (fp=19,0625MHz, C<sub>1</sub>=8fF, C<sub>0</sub>=2,1pF, C<sub>L</sub>=20pF) and external capacitors with Cv1=8.2pF, Cv2=6.8pF, Cv3=22pF each are used the following default states are set in the device.





## **3.2.7 Chip and System Tolerances**

Quartz: fp=19.0625MHz; C1=8fF; C0=2.1pF; CL=20pF (typical values) Cv1=8.2pF, Cv2=6.8pF, Cv3=22pF





Tolerance values in **Table 3-8** are valid, if pin 21 is not connected. Establishing the connection to pin 21 the tolerances increase.

Concerning the frequency tolerances of the whole system also crystal tolerances (tuning tolerances, temperature stability, tolerance of  $\mathtt{C}_\mathsf{L}$ ) have to be considered.

In addition to the chip tolerances also the crystal and external component tolerances have to be considered in the tuning and non-tuning case.

In case of internal tuning: The crystal on the evaluation board has a temperature stability of +/- 20ppm (or +/- 18kHz of the RF), which must be added to the total tolerances.

In case of default setup (without internal tuning and without usage of pin 21) the temperature stability and tuning tolerance of the crystal as well as the tolerance of the external capacitors (+/- 0.1pF) have to be added. The crystal on the evaluation board has a temperature stability of +/- 20ppm (means +/- 18kHz of the RF) and a tuning tolerance of +/- 10ppm (means +/- 9kHz of the RF). The external capacitors add a tolerance of +/- 3.5ppm (or +/- 3.2kHz regarding to the RF).

The frequency stabilities of both the receiver and the transmitter and the modulation bandwidth set the limit for the bandwidth of the IQ filter. To achieve a high receiver sensitivity and efficient



suppression of adjacent interference signals, the narrowest possible IQ bandwidth should be realized (**see Section 3.3**).

### **3.3 IQ-Filter**

The IQ-Filter should be set to values corresponding to the RF-bandwidth of the received RF signal via the **D1** to **D3** bits of the **LPF** register (subaddress 03H).





**Figure 3-17 I/Q Filter Characteristics**





**Figure 3-18 IQ Filter and frequency characteristics of the receive system**

## **3.4 Data Filter**

The Data-Filter should be set to values corresponding to the bandwidth of the transmitted Data signal via the D4 to D7 bits of the LPF register (subaddress 03H).





## **3.5 Limiter and RSSI**

The I/Q Limiters are DC coupled multistage amplifiers with offset-compensating feedback circuit and an overall gain of approximately 80dB each in the frequency range of 100Hz up to 350kHz. Receive Signal Strength Indicator (RSSI) generators are included in both limiters which produce DC voltages that are directly proportional to the input signal level in the respective channels. The resulting I- and Q-channel RSSI-signals are summed to the nominal RSSI signal.



limiter input.wmf

#### **Figure 3-19 Limiter and Pinning**

The DC offset compensation needs 2.2ms after Power On or Tx/Rx switch. This time is hard wired and independent from external capacitors  $C_{\text{C}}$  on pins 31 to 38. The maximum value for this capacitors is 47nF.

#### **RSSI accuracy settling time** = 2.2ms + 5\*RC=2.2ms+5\*37k\*2.2nF=2.6ms

R - internal resistor; C - external capacitor at Pin 29







**Figure 3-20 Limiter frequency characteristics**



**Figure 3-21 Typ. RSSI Level (Eval Board) @3V**



## **3.6 Data Slicer - Slicing Level**

The data slicer is an analog-to-digital converter. It is necessary to generate a threshold value for the negative comparator input (data slicer). The TDA5255 offers an RC integrator and a peak detector which can be selected via logic. Independent of the choice, the peak detector outputs are always active.

### **3.6.1 RC Integrator**



Necessary external component (Pin14): C<sub>SLC</sub>

This integrator generates the mean value of the data filter output. For a stable threshold value, the cut-off frequency has to be lower than the lowest signal frequency. The cutoff frequency results from the internal resistance R=100k $\Omega$  and the external capacitor C<sub>SLC</sub> on **Pin14**.

Cut-off frequency:

$$
f_{\text{cut-off}} = \frac{1}{2\pi \cdot 100 \, k\Omega \cdot C_{\text{SLC}}} < \text{Min} \left\{ f_{\text{Signal}} \right\} \tag{3-30}
$$

Component calculation: (rule of thumb)

 ${\sf T}_{\sf L}$  – longest period of no signal change

$$
C_{\text{SLC}} \ge \frac{3 \cdot T_L}{100 \cdot k\Omega} \tag{3-31}
$$



**Figure 3-22 Slicer Level using RC Integrator**



### **3.6.2 Peak Detectors**



The TDA5252 has two peak detectors built in, one for positive peaks in the data stream and the other for the negative ones.

Necessary external components: **- Pin12:**  $C_N$ 

**- Pin13: Cp** 



SLC\_PkD.wmf

#### **Figure 3-23 Slicer Level using Peak Detector**

For applications requiring fast attack and slow release from the threshold value it is reasonable to use the peak detectors. The threshold value is generated by an internal voltage divider. The release time is defined by the internal resistance values and the external capacitors.

$$
\tau_{posPkD} = 100 \ k \ \Omega \cdot C_p \tag{3-32}
$$

$$
\tau_{negPkD} = 100 k \Omega \cdot C_n \tag{3-33}
$$





PkD\_timing.wmf

### **Figure 3-24 Peak Detector timing**

Component calculation: (rule of thumb)

$$
C_p \ge \frac{2 \cdot T_{L1}}{100k\Omega} \tag{3-34}
$$

 $T_{11}$  – longest period of no signal change (LOW signal)

$$
C_n \geq \frac{2 \cdot T_{L2}}{100k\Omega}
$$

 $T_{12}$  – longest period of no signal change (HIGH signal)  $[3 - 35]$ 

# **3.6.3 Peak Detector - Analog output signal**

The TDA5255 data output can be digital (pin 28) or in analog form by using the peak detector output and changing some settings.

To get an analog data output the slicer must be set to **lowpass mode (Reg. 0, D15 = LP = 0)** and the peak detector capacitor at pin 12 or 13 has to be changed to a resistor of about 47kOhm.





PkD\_analog.wmf

#### **Figure 3-25 Peak Detector as analog Buffer (v=1)**

### **3.6.4** Peak Detector – Power Down Mode

For a safe and fast threshold value generation the peak detector is turned on by the sequencer circuit (see **Section 2.4.18**) only after the entire receiving path is active.

In the off state the output of the positive peak detector is tied down to GND and the output of the negative peak detector is pulled up to VCC.



### **Figure 3-26 Peak detector - power down mode**





PkD\_PWDN3.wmf

#### **Figure 3-27 Power down mode**

## **3.7 Data Valid Detection**

In order to detect valid data two criteria must be fulfilled.

One criteria is the data rate, which can be set in register 06h and 07h. The other one is the received RF power level, which can be set in register 08h in form of the RSSI threshold voltage. Thus for using the data valid detection FSK modulation is recommended.

Timing for data detection looks like the following. Two settings are possible: "Continuous" and "Single Shot", which can be set by D5 and D6 in register 00H.



### **Figure 3-28 Frequency Detection timing in continuous mode**



Note 1: Chip internal signal "Sequencer enables data detection" has a LOW to HIGH transition about 2.6ms after RX is activated (see **Figure 2-15**).

Note 2: The positive edge of the "Window Count Complete" signal latches the result of comparison of the analog to digital converted RSSI voltage with TH3 (register 08H). A logic combination of this output and the result of the comparison with single/double TH<sub>x</sub> defines the internal signal "data valid".

**Figure 3-27** shows that the logic is ready for the next conversion after 3 periods of the data signal.



Timing in Single Shot mode can be seen in the subsequent figure:

Frequ\_Detect\_Timing\_singleShot\_wmf

#### **Figure 3-29 Frequency Detection timing in Single Shot mode**

## **3.7.1 Frequency Window for Data Rate Detection**

The high time of data is used to measure the frequency of the data signal. For Manchester coding either the data frequency or half of the data frequency have to be detected corresponding to one high time or twice the high time of data signal.

A time period of 3\*2\*T is necessary to decide about valid or invalid data.





window\_count\_timing.wmf

#### **Figure 3-30 Window Counter timing**

Example to calculate the thresholds for a given data rate:

- Data signal manchester coded
- Data Rate: 2kbit//s
- $f_{\text{clk}} = 19.0625 \text{ MHz}$
- Then the period equals to

0,5ms 2kbit/s  $2 \cdot T = \frac{1}{6! \cdot 1 \cdot 1!} = 0,5 \text{ms}$  [3 – 36]

respectively the high time is 0,25ms.

We set the thresholds to  $+10\%$  and get: T1= 0,225ms and T2= 0,275ms

The thresholds TH1 and TH2 are calculated with following formulas

$$
TH1 = T1 \cdot \frac{f_{clk}}{4}
$$
 [3 - 37]

$$
TH2 = T2 \cdot \frac{f_{clk}}{4} \qquad [3-38]
$$

This yields the following results:

TH1~ 1072 = 010000110000<sub>b</sub> TH2~ 1310 = 010100011110<sub>b</sub>

which have to be programmed into the **D0** to **D11** bits of the **COUNT\_TH1** and **COUNT\_TH2** registers (subaddresses 06H and 07H), respectively.

Default values (window counter inactive):

 $TH1 = 000000000000<sub>b</sub>$ 

TH2=  $000000000001<sub>b</sub>$ 

**Note:** The timing window of  $+10\%$  of a given high time T in general does not correspond to a frequency window +-10% of the calculated data frequency.

## **3.7.2 RSSI threshold voltage - RF input power**

The RF input power level is corresponding to a certain RSSI voltage, which can be seen in Section 3.5. The threshold TH3 of this RSSI voltage can be calculated with the following formula:



 $TH3 = \frac{desired \quad RSSI \quad threshold \quad voltage}{1.04 \quad voltage} \cdot (2^6 - 1)$  [3 – 39]  $1.2V$ 

As an example a desired RSSI threshold voltage of 500mV results in TH3~26=011010<sub>b</sub>, which has to be written into D0 to D5 of the RSSI\_TH3 register (sub address 08H). Default value (RSSI detection inactive):

 $TH3=111111<sub>b</sub>$ 

## **3.8 Calculation of ON\_TIME and OFF\_TIME**



**Example:**  $t_{ON}$ = 0,005s,  $t_{OFF}$ = 0,055s,  $f_{RC}$ = 32300Hz ON= 65535-(32300\*0,005) ~ 65373= 1111111101011101<sub>b</sub> OFF= 65535-(32300\*0,055) ~ 63758= 1111100100001110<sub>b</sub>

The values have to be written into the **D0** to **D15** bits of the **ON\_TIME** and **OFF\_TIME** registers (subaddresses 04H and 05H).

Default values: ON=  $65215 = 1111111011000000<sub>b</sub>$ OFF=  $62335 = 1111001110000000<sub>b</sub>$  $t_{ON}$  ~10ms @  $f_{RC}$ = 32kHz  $t_{\text{OFF}}$  ~100ms @  $t_{\text{RC}}$ = 32kHz

## **3.9 Example for Self Polling Mode**

The settings for Self Polling Mode depend very much on the timing of the transmitted Signal. To create an example we consider following data structure transmitted in FSK.





data\_timing011.wmf

#### **Figure 3-31 Example for transmitted Data-structure**

According to existing synchronization techniques there are some synchronization bursts in front of the data added (code violation!). A minimum of 4 Frames is transmitted. Data are preferably Manchester encoded to get fastest respond out of the Data Rate Detection.

#### Target Application:

- received Signal has code violation as described before
- total mean current consumption below 1mA
- data reception within max. 400ms after first transmitted frame

#### One possible Solution:

 $t_{ON}$  = 15ms,  $t_{OFF}$ = 135ms

This gives 15ms ON time of a total period of 150ms which results in max. 0.9mA mean current consumption in Self Polling Mode. The resulting worst case timing is shown in the following figure:





### **Figure 3-32 3 possible timings**

Description:

Assumption: the ON time comes right after the first frame (Case A). If OFF time is 135ms the receiver turns on during Sync-pulses and the PwdDD- pulse wakes up the µP.

If the ON time is in the center of the 50ms gap of transmission (Case B), the Data Detect Logic will wake up the µP 135ms later.

If ON time is over just before Sync-pulses (Case C), next ON time is during Data transmission and Data Detect Logic will trigger a PwdDD- pulse to wake up the  $\mu$ P.

**Note:** In this example it is recommended to use the Peak Detector for slicer threshold generation, because of its fast attack and slow release characteristic. To overcome the data zero gap of 50ms larger external capacitors than noted in **Section 4.4** at pin12 and 13 are recommended. Further information on calculating these components can be taken from **Section 3.6.2**.



# **3.10 Default Setup**

Default setup is hard wired on chip and effective after a reset or return of power supply.





### **Reference**

# **4 Reference**

**4.1 Electrical Data**

## **4.1.1 Absolute Maximum Ratings**



## **WARNING**

The maximum ratings may not be exceeded under any circumstances, not even momentarily and individually, as permanent damage to the IC may result. The AC/DC characteristic limits are not guaranteed.



## **4.1.2 Operating Range**

Within the operational range the IC operates as explained in the circuit description.




# **4.1.3 AC/DC Characteristics**

AC/DC characteristics involve the spread of values guaranteed within the specified voltage and ambient temperature range. Typical characteristics are the median of the production. The device performance paramter marked with x are not part of the production test, but were either verified by design or measured in an Infineon Evalboard as described in Section 4-2.

<span id="page-72-0"></span>

#### **RECEIVER Characteristics**







1: without pin diode current (RX/TX-switch) 130uA@2.1V; 310uA@3V; 720uA@5V



<span id="page-74-0"></span>

"X" Not part of the production test - either verified by design or measured in an Infineon Evalboard as described in Section 4-2.



# **4.1.4 Digital Characteristics**

## <sup>2</sup>C Bus Timing



<span id="page-75-0"></span>

#### 3-wire Bus Timing



<span id="page-75-1"></span>**Figure 4-2 3-wire Bus Timing**



<span id="page-76-0"></span>

#### **Bus Interface Characteristics**







X: Not part of the production test - either verified by design or measured in an Infineon Evalboard as described in Section 4-2.

1: limited by transmission channel bandwidth and depending on transmit power level; ETSI regulation EN 300 220 fullfilled.

2:  $C_b$ = capacitance of one bus line



## **4.2 Test Circuit**

The device performance parameters marked with X in **Section 4.1.3** were either verified by design or measured on an Infineon evaluation board (IFX board).



## <span id="page-78-0"></span>**Figure 4-3 Schematic of the Evaluation Board**



# **4.3 Test Board Layout**

Gerberfiles for this Testboard are available on request.



TDA5250\_v42\_layout.pdf

#### <span id="page-79-0"></span>**Figure 4-4 Layout of the Evaluation Board**

**Note 1:** The LNA and PA matching network was designed for minimum required space and maximum performance and thus via holes were deliberately placed into solder pads.

In case of reproduction please bear in mind that this may not be suitable for all automatic soldering processes.

**Note 2:** Please keep in mind not to layout the CLKDIV line directly in the neighborhood of the crystal and the associated components.

**Note 3:** The opto part (X4) should be supplied by connecting to X3.



## **4.4 Bill of Materials**

<span id="page-80-0"></span>







# **List of Tables**





# **List of Tables**





# **List of Figures**





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