

FEATURES

256-Position Replaces 1, 2, or 4 Potentiometers 1 k Ω , 10 k Ω , 50 k Ω , 100 k Ω **Power Shutdown–Less than 5 µA 3-Wire SPI-Compatible Serial Data Input 10 MHz Update Data Loading Rate 2.7 V to 5.5 V Single-Supply Operation Midscale Preset**

APPLICATIONS

Mechanical Potentiometer Replacement Programmable Filters, Delays, Time Constants Volume Control, Panning Line Impedance Matching Power Supply Adjustment

1-/2-/4-Channel Digital Potentiometers

AD8400/AD8402/AD8403

FUNCTIONAL BLOCK DIAGRAM

GENERAL DESCRIPTION

The AD8400/AD8402/AD8403 provide a single, dual or quad channel, 256 position digitally controlled variable resistor (VR) device. These devices perform the same electronic adjustment function as a potentiometer or variable resistor. The AD8400 contains a single variable resistor in the compact SO-8 package. The AD8402 contains two independent variable resistors in space-saving SO-14 surfacemount packages. The AD8403 contains four independent variable resistors in 24-lead PDIP, SOIC, and TSSOP packages. Each part contains a fixed resistor with a wiper contact that taps the fixed resistor value at a point determined by a digital code loaded into the controlling serial input register. The resistance between the wiper and either endpoint of the fixed resistor varies linearly with respect to the digital code transferred into the VR latch. Each variable resistor offers a completely programmable value of resistance, between the A terminal and the wiper or the B terminal and the wiper. The fixed A to B terminal resistance of 1 kΩ, 10 kΩ, 50 kΩ, or 100 kΩ has a $\pm 1\%$ channel-to-channel matching tolerance with a nominal temperature coefficient of 500 ppm/°C. A unique switching circuit minimizes the high glitch inherent in traditional switched resistor designs avoiding any make-before-break or break-before-make operation.

Each VR has its own VR latch that holds its programmed resistance value. These VR latches are updated from an SPI compatible serialto-parallel shift register that is loaded from a standard 3-wire serial-input digital interface. Ten data bits make up the data word clocked into the serial input register. The data word is decoded where the first two bits determine the address of the VR latch to be loaded, the last eight bits are data. A serial data output pin at the opposite end of the serial register allows simple daisy-chaining in multiple VR applications without additional external decoding logic.

The reset $(\overline{\text{RS}})$ pin forces the wiper to the midscale position by loading 80_H into the VR latch. The $\overline{\text{SHDN}}$ pin forces the resistor

REV. C

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to an end-to-end open circuit condition on the A terminal and shorts the wiper to the B terminal, achieving a microwatt power shutdown state. When $\overline{\text{SHDN}}$ is returned to logic high, the previous latch settings put the wiper in the same resistance setting prior to shutdown. The digital interface is still active in shutdown so that code changes can be made that will produce new wiper positions when the device is taken out of shutdown.

The AD8400 is available in both the SO-8 surface-mount and the 8-lead plastic DIP package.

The AD8402 is available in both surface mount (SO-14) and 14-lead plastic DIP packages, while the AD8403 is available in a narrow body 24-lead plastic DIP and a 24-lead surface-mount package. The AD8402/AD8403 are also offered in the 1.1 mm thin TSSOP-14/TSSOP-24 packages for PCMCIA applications. All parts are guaranteed to operate over the extended industrial temperature range of -40° C to $+125^{\circ}$ C.

Figure 1. RWA and RWB vs. Code

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$\bf{AD8400/AD8402/AD8403—SPECIFICATIONS (V_{DD} = 3 V ± 10% or 5 V ± 10%, V_A = V_{DD}, V_B = 0 V, 0)}$ **–40C** ≤ **T^A** ≤ **+125C unless otherwise noted.)**

ELECTRICAL CHARACTERISTICS-10 kΩ VERSION

NOTES

¹Typicals represent average readings at 25 $\rm{^{\circ}C}$ and V_{DD} = 5 V.

²Resistor position nonlinearity error R-INL is the deviation from an ideal value measured between the maximum resistance and the minimum resistance wiper ¹positions. R-DNL measures the relative step change from ideal between successive tap positions. Parts are guaranteed monotonic. See TPC 29 test circuit. I_W = 50 μA for V_{DD} = 3 V and I_W = 400 μA for V_{DD} = 5 V for the 10 kΩ versions.

 ${}^{3}V_{AB}$ = V_{DD} , Wiper (V_W) = No Connect.

⁴INL and DNL are measured at V_W with the RDAC configured as a potentiometer divider similar to a voltage output D/A converter. V_A = V_{DD} and V_B = 0 V. ¹DNL Specification limits of ±1 LSB maximum are Guaranteed Monotonic operating conditions. See TPC 28 test circuit.

 5 Resistor terminals A, B, W have no limitations on polarity with respect to each other.

⁶Guaranteed by design and not subject to production test. Resistor-terminal capacitance tests are measured with 2.5 V bias on the measured terminal. The remaining resistor terminals are left open circuit.

 17 Measured at the Ax terminals. All Ax terminals are open circuited in shutdown mode.

⁸Worst-case supply current consumed when input logic level at 2.4 V, standard characteristic of CMOS logic. See TPC 20 for a plot of I_{DD} versus logic voltage. ${}^{9}P_{\rm DISS}$ is calculated from (I_{DD} × V_{DD}). CMOS logic level inputs result in minimum power dissipation.

¹⁰All Dynamic Characteristics use $V_{DD} = 5$ V.

¹¹Measured at a V_W pin where an adjacent V_W pin is making a full-scale voltage change.

$\textbf{SPECIFICATIONS}$ (V_{DD} = 3 V \pm 10% or 5 V \pm 10%, V_A = V_{DD}, V_B = 0 V, -40°C \leq T_A \leq +125°C unless otherwise noted.) **ELECTRICAL CHARACTERISTICS-50 k** Ω **and 100 k** Ω **VERSIONS**

NOTES

¹Typicals represent average readings at 25°C and $V_{DD} = 5 V$.

²Resistor position nonlinearity error R-INL is the deviation from an ideal value measured between the maximum resistance and the minimum resistance wiper ¹positions. R-DNL measures the relative step change from ideal between successive tap positions. Parts are guaranteed monotonic. See TPC 29 test circuit. I_W = V_{DD}/R for V_{DD} = 3 V or 5 V for the 50 kΩ and 100 kΩ versions.

 ${}^{3}V_{AB} = V_{DD}$, Wiper $(V_{W}) = N_0$ Connect.

⁴INL and DNL are measured at V_W with the RDAC configured as a potentiometer divider similar to a voltage output D/A converter. V_A = V_{DD} and V_B = 0 V. ¹DNL Specification limits of ±1 LSB maximum are Guaranteed Monotonic operating conditions. See TPC 28 test circuit.

 5 Resistor terminals A, B, W have no limitations on polarity with respect to each other.

⁶Guaranteed by design and not subject to production test. Resistor-terminal capacitance tests are measured with 2.5 V bias on the measured terminal. The remaining resistor terminals are left open circuit.

 7 Measured at the Ax terminals. All Ax terminals are open circuited in shutdown mode.

 $8W$ orst-case supply current consumed when input logic level at 2.4 V, standard characteristic of CMOS logic. See TPC 20 for a plot of I_{DD} versus logic voltage. ${}^{9}P_{\text{DISS}}$ is calculated from $(I_{\text{DD}} \times V_{\text{DD}})$. CMOS logic level inputs result in minimum power dissipation.

 10 All Dynamic Characteristics use $V_{\text{DD}} = 5$ V.

¹¹Measured at a V_W pin where an adjacent V_W pin is making a full-scale voltage change.

ELECTRICAL CHARACTERISTICS-1 K Ω **VERSION**

NOTES

¹Typicals represent average readings at 25 °C and $V_{DD} = 5 V$.

²Resistor position nonlinearity error R-INL is the deviation from an ideal value measured between the maximum resistance and the minimum resistance wiper ¹positions. R-DNL measures the relative step change from ideal between successive tap positions. See TPC 29 test circuit.

I_W = 500 μA for V_{DD} = 3 V and I_W = 2.5 mA for V_{DD} = 5 V for 1 kΩ version.

 ${}^{3}V_{AB} = V_{DD}$, Wiper (V_W) = No Connect.

⁴INL and DNL are measured at V_W with the RDAC configured as a potentiometer divider similar to a voltage output D/A converter. V_A = V_{DD} and V_B = 0 V. DNL Specification limits of ±1 LSB maximum are Guaranteed Monotonic operating conditions. See TPC 28 test circuit.

⁵Resistor terminals A, B, W have no limitations on polarity with respect to each other.

⁶Guaranteed by design and not subject to production test. Resistor-terminal capacitance tests are measured with 2.5 V bias on the measured terminal. The remaining resistor terminals are left open circuit.

 17 Measured at the Ax terminals. All Ax terminals are open circuited in shutdown mode.

⁸Worst-case supply current consumed when input logic level at 2.4 V, standard characteristic of CMOS logic. See TPC 20 for a plot of I_{DD} versus logic voltage. ⁹P_{DISS} is calculated from (I_{DD} \times V_{DD}). CMOS logic level inputs result in minimum power dissipation.

¹⁰All Dynamic Characteristics use $V_{DD} = 5$ V.

¹¹Measured at a V_W pin where an adjacent V_W pin is making a full-scale voltage change.

$\textbf{SPECIFICATIONS}$ (V_{DD} = 3 V \pm 10% or 5 V \pm 10%, V_A = V_{DD}, V_B = 0 V, -40°C \leq T_A \leq +125°C unless otherwise noted.)

ELECTRICAL CHARACTERISTICS–ALL VERSIONS

NOTES

¹Typicals represent average readings at 25 $^{\circ}$ C and V_{DD} = 5 V.

²Guaranteed by design and not subject to production test. Resistor-terminal capacitance tests are measured with 2.5 V bias on the measured terminal. The remaining resistor terminals are left open circuit.

³See timing diagram for location of measured values. All input control voltages are specified with $t_R = t_F = 1$ ns (10% to 90% of V_{DD}) and timed from a voltage level of 1.6 V. Switching characteristics are measured using V_{DD} = 3 V or 5 V. To avoid false clocking, a minimum input logic slew rate of 1 V/µs should be maintained. ⁴Propagation Delay depends on value of V_{DD} , R_L , and C_L —see Applications section.

Figure 2b. Detail Timing Diagram

Figure 2c. Reset Timing Diagram

ABSOLUTE MAXIMUM RATINGS*

*Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those listed in the operational sections of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD8400/AD8402/AD8403 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high-energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

Table I. Serial Data Word Format

ADDR		DATA							
B 9	B8			B7 B6 B5 B4 B3 B2 B1 B0					
A1 MSB 2^9	2^8	A0 D7 D6 D5 D4 D3 D2 D1 D0 LSB MSB 2^7							LSB 2 ⁰

ORDERING GUIDE

NOTES

*N = Plastic DIP; SO = Small Outline; RU = Thin Shrink SO

The AD8400, AD8402, and AD8403 contain 720 transistors.

PIN CONFIGURATIONS

AD8402 PIN FUNCTION DESCRIPTIONS

AD8400 PIN FUNCTION DESCRIPTIONS

AD8403 PIN FUNCTION DESCRIPTIONS

*All AGNDs must be connected to DGND.

*All AGNDs must be connected to DGND.

Typical Performance Characteristics–AD8400/AD8402/AD8403

TPC 1. Wiper to End Terminal Resistance vs. Code

TPC 2. Resistance Linearity vs. Conduction Current

TPC 3. Resistance Step Position Nonlinearity Error vs. Code

TPC 4. 10 kΩ Wiper-Contact-Resistance Histogram

Resistance Histogram

TPC 5. Potentiometer Divider Nonlinearity Error vs. Code

TPC 8. Nominal Resistance vs. **Temperature**

TPC 6. 50 k Ω Wiper-Contact-Resistance Histogram

TPC 9. DV_{WB}/DT Potentiometer Mode Tempco

TPC 7. 100 kΩ Wiper-Contact-

 20_W **R^W (20mV/DIV) CS (5V/DIV)** 500_n **TIME 500ns/DIV**

TPC 10. ∆R_{WB} /∆T Rheostat Mode Tempco

TPC 13. Long-Term Drift Accelerated by Burn-In

TPC 16. Total Harmonic Distortion Plus Noise vs. Frequency

TPC 11. One Position Step Change at Half-Scale (Code 7 F_H to 80 $_H$)

TPC 12. 10 kΩ Gain vs. Frequency

TPC 14. Large Signal Settling Time

TPC 15. 50 kΩ Gain vs. Frequency vs. Code

TPC 17. Digital Feedthrough vs. Time

–10–

TPC 18. 100 kΩ Gain vs. Frequency vs. Code

TPC 19. Normalized Gain Flatness vs. Frequency

TPC 20. Supply Current vs. Digital Input Voltage

TPC 22. –3 dB Bandwidths

TPC 25. 1 kΩ Gain and Phase vs. Frequency

TPC 23. Supply Current vs. Clock Frequency

TPC 26. Shutdown Current vs. **Temperature**

TPC 21. Power Supply Rejection vs. Frequency

TPC 24. AD8403 Incremental Wiper ON Resistance vs. V_{DD}

TPC 27. Supply Current vs. **Temperature**

TEST CIRCUITS

Test Circuit 1. Potentiometer Divider Nonlinearity Error (INL, DNL)

Test Circuit 2. Resistor Position Nonlinearity Error (Rheostat Operation; R-INL, R-DNL)

Test Circuit 3. Wiper Resistance

Test Circuit 4. Power Supply Sensitivity (PSS, PSRR)

Test Circuit 5. Inverting Programmable Gain

Test Circuit 6. Noninverting Programmable Gain

Test Circuit 7. Gain vs. Frequency

Test Circuit 8. Incremental ON Resistance

OPERATION

The AD8400/AD8402/AD8403 provide a single, dual, and quad channel, 256-position digitally controlled variable resistor (VR) device. Changing the programmed VR settings is accomplished by clocking in a 10-bit serial data word into the SDI (Serial Data Input) pin. The format of this data word is two address bits, MSB first, followed by eight data bits, MSB first. Table I provides the serial register data word format. The AD8400/AD8402/AD8403 has the following address assignments for the ADDR decode, which determines the location of VR latch receiving the serial register data in Bits B7 through B0:

$$
VR\# = A1 \times 2 + A0 + 1\tag{1}
$$

The single-channel AD8400 requires $AI = AO = 0$. The dualchannel AD8402 requires $A1 = 0$. VR settings can be changed one at a time in random sequence. The serial clock running at 10 MHz makes it possible to load all four VRs in under 4 µs $(10 \times 4 \times 100 \text{ ns})$ for the AD8403. The exact timing requirements are shown in Figures 2a, 2b, and 2c.

The AD8402/AD8403 resets to midscale by asserting the $\overline{\text{RS}}$ pin, simplifying initial conditions at power up. Both parts have a power shutdown SHDN pin that places the VR in a zero power consumption state where terminals Ax are open circuited and the wiper Wx is connected to Bx resulting in only leakage currents being consumed in the VR structure. In shutdown mode the VR latch settings are maintained so that returning to operational mode from power shutdown, the VR settings return to their previous resistance values. The digital interface is still active in shutdown, except that SDO is deactivated. Code changes in the registers can be made that will produce new wiper positions when the device is taken out of shutdown.

Figure 3. AD8402/AD8403 Equivalent VR (RDAC) Circuit

PROGRAMMING THE VARIABLE RESISTOR Rheostat Operation

The nominal resistance of the VR (RDAC) between terminals A and B is available with values of 1 kΩ, 10 kΩ, 50 kΩ, and 100 kΩ. The final digits of the part number determine the nominal resistance value, e.g., 10 k Ω = 10; 100 k Ω = 100. The nominal resistance (R_{AB}) of the VR has 256 contact points accessed by the wiper terminal, plus the B terminal contact. The 8-bit data word in the RDAC latch is decoded to select one of the 256 possible settings. The wiper's first connection starts at the B terminal for data 00_H . This B terminal connection has a wiper contact resistance of 50 Ω . The second connection (10 k Ω part) is the first tap point located at 89 Ω [= R_{AB} (nominal resistance)/256 + R_W = 39 Ω + 50 Ω] for data 01_H . The third connection is the next tap point representing $78 + 50 = 128 \Omega$ for data 02_H . Each LSB data value increase moves the wiper up the resistor ladder until the last tap point is reached at 10,011 $Ω$. The wiper does not directly connect to the B terminal. See Figure 3 for a simplified diagram of the equivalent RDAC circuit.

The AD8400 contains one RDAC, the AD8402 contains two independent RDACs, and the AD8403 contains four independent RDACs. The general transfer equation that determines the digitally programmed output resistance between Wx and Bx is:

$$
R_{WB}\left(Dx\right) = \left(Dx\right) / 256 \times R_{AB} + R_W \tag{2}
$$

where *Dx* is the data contained in the 8-bit RDAC# latch, and R_{AB} is the nominal end-to-end resistance.

For example, when $V_B = 0$ V and when the A terminal is open circuit, the following output resistance values will be set for the following RDAC latch codes (applies to $10 \text{ k}\Omega$ potentiometers):

Note in the zero-scale condition a finite wiper resistance of 50 Ω is present. Care should be taken to limit the current flow between W and B in this state to a maximum value of 5 mA to avoid degradation or possible destruction of the internal switch contact.

Like the mechanical potentiometer the RDAC replaces, it is totally symmetrical. The resistance between the wiper W and terminal A also produces a digitally controlled complementary resistance R_{WA} . When these terminals are used, the B terminal can be tied to the wiper or left floating. Setting the resistance value for R_{WA} starts at a maximum value of resistance and decreases as the data loaded in the RDAC latch is increased in value. The general transfer equation for this operation is:

$$
R_{WA}(Dx) = (256 - Dx)/256 \times R_{AB} + R_W
$$
\n(3)

where *Dx* is the data contained in the 8-bit RDAC# latch, and *RAB* is the nominal end-to-end resistance. For example, when V_A = 0 V and B terminal is open circuit, the following output resistance values will be set for the following RDAC latch codes (applies to 10 k Ω potentiometers):

The typical distribution of RAB from channel to channel matches within ± 1 %. However, device-to-device matching is process lotdependent, having a $\pm 20\%$ variation. The change in R_{AB} with temperature has a positive 500 ppm/°C temperature coefficient.

The wiper-to-end-terminal resistance temperature coefficient has the best performance over the 10% to 100% of adjustment range where the internal wiper contact switches do not contribute any significant temperature related errors. The graph in TPC 10 shows the performance of R_{WB} tempco versus code. Using the trimmer with codes below 32 results in the larger temperature coefficients plotted.

PROGRAMMING THE POTENTIOMETER DIVIDER Voltage Output Operation

The digital potentiometer easily generates an output voltage proportional to the input voltage applied to a given terminal. For example, connecting A terminal to 5 V and B terminal to ground produces an output voltage at the wiper starting at zero volts up to 1 LSB less than 5 V. Each LSB of voltage is equal to the voltage applied across terminal AB divided by the 256 position resolution of the potentiometer divider. The general equation defining the output voltage with respect to ground for any given input voltage applied to terminals AB is:

$$
V_W(Dx) = Dx/256 \times V_{AB} + V_B \tag{4}
$$

Operation of the digital potentiometer in the divider mode results in more accurate operation over temperature. Here the output voltage is dependent on the ratio of the internal resistors, not the absolute value; therefore, the temperature drift improves to 15 ppm/ C .

At the lower wiper position settings, the potentiometer divider temperature coefficient increases due to the contributions of the CMOS switch wiper resistance becoming an appreciable portion of the total resistance from Terminal B to the wiper. See TPC 9 for a plot of potentiometer tempco performance versus code setting.

DIGITAL INTERFACING

The AD8400/AD8402/AD8403 contain a standard SPI compatible three-wire serial input control interface. The three inputs are clock (CLK), $\overline{\text{CS}}$ and serial data input (SDI). The positiveedge sensitive CLK input requires clean transitions to avoid clocking incorrect data into the serial input register. For best results use logic transitions faster than 1 V/µs. Standard logic families work well. If mechanical switches are used for product evaluation, they should be debounced by a flip-flop or other suitable means. The Figure 4 block diagrams show more detail of the internal digital circuitry. When \overline{CS} is taken active low, the clock loads data into the 10-bit serial register on each positive clock edge (see Table II).

Figure 4. Block Diagrams

Table II. Input Logic Control Truth Table

CLK	$\overline{\text{CS}}$	$\overline{\text{RS}}$	SHDN	Register Activity
L	L	H	H	No SR effect, enables SDO pin.
P	Ī.	H	н	Shift one bit in from the SDI pin. The tenth previously entered bit is shifted out of the SDO pin.
\mathbf{x}	P	H	н	Load SR data into RDAC latch based on A1, A0 decode (Table III).
X	H	H	H	No Operation
\mathbf{x}	\mathbf{X}	L	H	Sets all RDAC latches to midscale, wiper centered, and SDO latch cleared.
X	н	P	H	Latches all RDAC latches to 80_H .
\mathbf{x}	H	н	L	Open circuits all resistor A-terminals, connects W to B, turns off SDO output transistor.

NOTE

 $P =$ positive edge, $X =$ don't care, $SR =$ shift register.

The serial data-output (SDO) pin contains an open drain n-channel FET. This output requires a pull-up resistor in order to transfer data to the next package's SDI pin. The pull-up resistor termination voltage may be larger than the V_{DD} supply (but less than max V_{DD} of 8 V) of the AD8403 SDO output device, e.g., the AD8403 could operate at $V_{DD} = 3.3$ V and the pull-up for interface to the next device could be set at 5 V. This allows for daisy-chaining several RDACs from a single processor serial data line. The clock period needs to be increased when using a pull-up resistor to the SDI pin of the following device in the series. Capacitive loading at the daisy-chain node SDO–SDI between devices must be accounted for to successfully transfer data. When daisy chaining is used, the \overline{CS} should be kept low until all the bits of every package are clocked into their respective serial registers ensuring that the address bits and data bits are in the proper decoding location. This would require 20 bits of address and data complying to the word format provided in Table I if two AD8403 four-channel RDACs are daisy-chained. Note, only the AD8403 has a SDO pin. During shutdown SHDN the SDO output pin is forced to the off (logic high) state to disable power dissipation in the pull-up resistor. See Figure 6 for equivalent SDO output circuit schematic.

The data setup and data hold times in the specification table determine the data valid time requirements. The last 10 bits of the data word entered into the serial register are held when $\overline{\text{CS}}$ returns high. At the same time \overline{CS} goes high it gates the address decoder, which enables one of the two (AD8402) or four (AD8403) positive edge triggered RDAC latches. See Figure 5 detail and Table III Address Decode Table.

Table III. Address Decode Table

Figure 5. Equivalent Input Control Logic

The target RDAC latch is loaded with the last eight bits of the serial data word completing one DAC update. In the case of the AD8403 four separate 10-bit data words must be clocked in to change all four VR settings.

Figure 6. Detail SDO Output Schematic of the AD8403

All digital pins are protected with a series input resistor and parallel Zener ESD structure shown in Figure 7a. This structure applies to digital pins \overline{CS} , SDI, SDO, \overline{RS} , \overline{SHDN} , CLK. The digital input ESD protection allows for mixed power supply applications where 5 V CMOS logic can be used to drive an AD8400, AD8402, or AD8403 operating from a 3 V power supply. The analog pins A, B, and W are protected with a 20 Ω series resistor and parallel Zener (see Figure 7b).

$$
\underbrace{\text{DiffAL}\over\text{PINS}}\underbrace{\text{1k}\Omega}_{\text{PINS}}\underbrace{\text{LOGIC}}_{\text{L}}\\
$$

Figure 7b. Equivalent ESD Protection Circuit (Analog Pins)

CA = 90.4pF (DW / 256) + 30pF

 $C_B = 90.4pF \times [1 - (DW / 256)] + 30pF$

Figure 8. RDAC Circuit Simulation Model for $RDAC = 10 k\Omega$

The ac characteristics of the RDACs are dominated by the internal parasitic capacitances and the external capacitive loads. The –3 dB bandwidth of the AD8403AN10 (10 kΩ resistor) measures 600 kHz at half scale as a potentiometer divider. TPC 22 provides the large signal BODE plot characteristics of the three available resistor versions 10 kΩ, 50 kΩ, and 100 kΩ. The gain flatness versus frequency graph, TPC 25, predicts filter applications performance. A parasitic simulation model has been developed, and is shown in Figure 8. Listing I provides a macro model net list for the 10 kΩ RDAC:

Listing I. Macro Model Net List for RDAC

```
.PARAM DW=255, RDAC=10E3
*
.SUBCKT DPOT (A,W,)
*
CA A 0 {DW/256*90.4E-12+30E-12}
RAW A W {(1-DW/256)*RDAC+50}
CW W 0 120E-12
RBW W B {DW/256*RDAC+50}
CB B 0 {(1-DW/256)*90.4E-12+30E-12}
*
```
.ENDS DPOT

The total harmonic distortion plus noise (THD+N) is measured at 0.003% in an inverting op amp circuit using an offset ground and a rail-to-rail OP279 amplifier, Test Circuit 5. Thermal noise is primarily Johnson noise, typically 9 nV/ \sqrt{Hz} for the 10 kΩ version at f = 1 kHz. For the 100 k Ω device, thermal noise becomes 29 nV/ \sqrt{Hz} . Channel-to-channel crosstalk measures less than -65 dB at $f = 100$ kHz. To achieve this isolation, the extra ground pins provided on the package to segregate the individual RDACs must be connected to circuit ground. AGND and DGND pins should be at the same voltage potential. Any unused potentiometers in a package should be connected to ground. Power supply rejection is typically –35 dB at 10 kHz. Care is needed to minimize power supply ripple in high accuracy applications.

APPLICATIONS

The digital potentiometer (RDAC) allows many of the applications of trimming potentiometers to be replaced by a solid-state solution offering compact size and freedom from vibration, shock and open contact problems encountered in hostile environments. A major advantage of the digital potentiometer is its programmability. Any settings can be saved for later recall in system memory.

The two major configurations of the RDAC include the potentiometer divider (basic 3-terminal application) and the rheostat (2-terminal configuration) connections shown in Test Circuits 1 and 2 (see page 11).

Certain boundary conditions must be satisfied for proper AD8400/ AD8402/AD8403 operation. First, all analog signals must remain within the 0 to V_{DD} range used to operate the single-supply AD8400/AD8402/AD8403 products. For standard potentiometer divider applications, the wiper output can be used directly. For low resistance loads, buffer the wiper with a suitable rail-to-rail op amp such as the OP291 or the OP279. Second, for ac signals and bipolar dc adjustment applications, a virtual ground will generally be needed. Whatever method is used to create the virtual ground, the result must provide the necessary sink and source current for all connected loads, including adequate bypass capacitance. Test Circuit 5 (see page 11) shows one channel of the AD8402 connected in an inverting programmable gain amplifier circuit. The virtual ground is set at 2.5 V, which allows the circuit output to span $a \pm 2.5$ volt range with respect to virtual ground. The rail-to-rail amplifier capability is necessary for the widest output swing. As the wiper is adjusted from its midscale reset position (80_H) toward the A terminal (code FF_H), the voltage gain of the circuit is increased in successfully larger increments. Alternatively, as the wiper is adjusted toward the B terminal (code 00_H), the signal becomes attenuated. The plot in Figure 9 shows the wiper settings for a 100:1 range of voltage gain (V/V). Note the ± 10 dB of pseudo-logarithmic gain around 0 dB (1 V/V). This circuit is mainly useful for gain adjustments in the range of 0.14 V/V to 4 V/V; beyond this range the step sizes become very large and the resistance of the driving circuit can become a significant term in the gain equation.

Figure 9. Inverting Programmable Gain Plot

ACTIVE FILTER

One of the standard circuits used to generate a low-pass, highpass, or band-pass filter is the state variable active filter. The digital potentiometer allows full programmability of the frequency, gain and Q of the filter outputs. Figure 10 shows the filter circuit using a 2.5 V virtual ground, which allows a \pm 2.5 V_P input and output swing. RDAC2 and 3 set the LP, HP, and BP cutoff and center frequencies, respectively. These variable resistors should be programmed with the same data (as with ganged potentiometers) to maintain the best circuit Q. Figure 11 shows the measured filter response at the band-pass output as a function of the RDAC2 and RDAC3 settings which produce a range of center frequencies from 2 kHz to 20 kHz. The filter gain response at the band-pass output is shown in Figure 12. At a center frequency of 2 kHz, the gain is adjusted over a -20 dB to $+20$ dB range determined by RDAC1. Circuit Q is adjusted by RDAC4. For more detailed reading on the state variable active filter, see Analog Devices' application note, AN-318.

Figure 10. Programmable State Variable Active Filter

 Figure 11. Programmed Center Frequency Band-Pass Response

Figure 12. Programmed Amplitude Band-Pass Response

OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

8-Lead SOIC (R-8)

REV. C

OUTLINE DIMENSIONS (continued)

Dimensions shown in inches and (mm).

Revision History

