# **SKYWORKS**

## DATA SHEET

## AAT2630: Wireless Data Card PMIC 10-Channel DC-DC Converter

## **Applications**

- Wireless mini, or half-mini PCI express cards
- Express cards
- USB wireless modules
- SDIO modules
- On-board wireless modems

## Features

- $\bullet$  VIN range: 3.0 V to 5.5 V
- Two 1.92 MHz synchronous step-down converters:
	- $-180^\circ$  out-of-phase operation
	- $-$  Buck1: 1.375 V, 500 mA output
	- $-$  Buck2: 2.1 V, 500 mA output
	- $-$  Light load, low noise switching mode
- Eight LDO regulators:
	- Two with 300 mA output: LDO1 for MSME: 1.8 V LDO3 for MSMA: 2.6 V
	- $-$  Three with 150 mA output: LDO2 for MSMP: 2.6 V LDO4 for MMC: 3.0 V LDO8 for RFRX: 2.75 V
	- Three with 50mA output: LDO5 for RUIM: 1.8 V/3.0 V LDO6 for TCXO: 2.85 V LDO7 for USB: 3.1 V
	- $-$  High PSRR (70 dB  $@1$  KHz)
- Over-current and over-temperature protection
- Power-on reset
- Power up with defined sequence
- 1.25 V voltage reference
- 19.2 MHz clock buffer
- 32.7645 kHz frequency output
- WLCSP (49-bump, 3 mm  $\times$  3 mm) package (MSL1, 260 °C per JEDEC J-STD-020)

## **Description**

The AAT2630 contains two fully integrated, step-down converters, eight low-dropout (LDO) regulators, a 1.25 V voltage reference, a 19.2 MHz clock buffer, a 32 kHz frequency output, and three LED drivers in a 3 mm  $\times$  3 mm Wafer Level Chip Scale Package (WLCSP), making it ideal for wireless data cards or modules and on-board modems.

The two step-down converters are synchronous with internal compensation. Switching at 1.92 MHz, they operate 180° out of phase to minimize the number and size of the external components and to provide efficiencies higher than 90%.

The eight LDOs are high PSRR type, requiring only a small output ceramic capacitor for stability.

Power-on reset and automatic power-up sequence, which are common in system architectures involving a processor, are defined for the supplies. The AAT2630 also includes over-current and over-temperature protection.

The AAT2630 is available in a 49-bump, 3 mm  $\times$  3 mm WLCSP package.

A typical application circuit is shown in Figure 1. The pin configurations are shown in Figure 2. Signal pin assignments descriptions are provided in Table 1.



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#### DATA SHEET • AAT2630 WIRELESS DATA CARD PMIC 10-CHANNEL DC-DC CONVERTER



Figure 1. AAT2630 Typical Application Circuit



(Top View)





## Table 1. AAT2630 Signal Descriptions (2 of 2)



## Electrical and Mechanical Specifications

The absolute maximum ratings of the AAT2630 are provided in

Table 2, the thermal information is listed in Table 3, and electrical specifications are provided in Table 4.

## Table 2. AAT2630Absolute Maximum Ratings (Note 1)



Note 1: Exposure to maximum rating conditions for extended periods may reduce device reliability. There is no damage to device with only one parameter set at the limit and all other parameters set at or below their nominal value. Exceeding any of the limits listed may result in permanent damage to the device.

## Table 3. AAT2630 Thermal Information (Note 1)



Note 1: Mounted on an FR4 board.

CAUTION: Although this device is designed to be as robust as possible, electrostatic discharge (ESD) can damage this device. This device must be protected at all times from ESD. Static charges may easily produce potentials of several kilovolts on the human body or equipment, which can discharge without detection. Industry-standard ESD precautions should be used at all times.

## Table 4. AAT2630 Electrical Specifications (1 of 5) (Note 1)

(VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF, COUTB = 10  $\mu$ F, CVREF = 2.2  $\mu$ F, CINL = 4.7  $\mu$ F, COUTL = 2.2  $\mu$ F, CBYP = 0.1  $\mu$ F, CVBUS = 0.47  $\mu$ F, TA = -40 °C to +85 °C, Typical Values are  $TA = 25 °C$ , Unless Otherwise Noted)



#### Table 4. AAT2630 Electrical Specifications (2 of 5) (Note 1)

(VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF, COUTB = 10 µF, CVREF = 2.2 µF, CINL = 4.7 µF, COUTL = 2.2 µF, CBYP = 0.1 µF, CVBUS = 0.47 µF, TA = -40 °C to +85 °C, Typical Values are TA = 25  $\degree$ C, Unless Otherwise Noted)

<b>Parameter</b>	<b>Symbol</b>	<b>Test Condition</b>	Min	<b>Typical</b>	Max	<b>Units</b>
<b>LDO1 (MSME)</b>						
Normal operating input voltage range	<b>VIN MSME</b>			VOUTB2		V
Output voltage	VOUT1	$I$ out $1 = 10$ mA	1.75	1.8	1.85	V
Temperature coefficient	∆V0UT1/°C			±100		ppm/°C
Maximum output current	<b>IOUT1</b>		300	450		mA
Dropout voltage	VLD01_D0	$I$ out $1 = 300$ mA		150	300	mV
Load regulation		$I$ out t = 10 mA to 300 mA		6	50	mV
Line regulation		VIN_MSME = $2.0$ V to 2.2 V, $100T1 = 50$ mA		0.1		$\%N$
	<b>VNOISE</b>	$100T1 = 50$ mA, 10 Hz to 10 kHz		350		<b>µVRMS</b>
		$100T1 = 50$ mA, 10 Hz to 10 kHz, CBYP = 1 $\mu$ F		60		<b>µVRMS</b>
Power supply rejection ratio	PSRROUT1	$f = 1$ kHz, $I$ out $1 = 50$ mA, $V$ in _MSME = 2.1 V		70		dB
		$f = 10$ kHz, $I$ out $1 = 50$ mA, $V$ in _MSME = 2.1 V		50		dB
<b>LDO2 (MSMP)</b>						
Output voltage	VOUT2	$I$ outz = 10 mA	2.52	2.6	2.68	V
Temperature coefficient	∆VOUT2/°C			±100		ppm/°C
Maximum output current	<b>IOUT2</b>		300	500		mA
Dropout voltage	VLD02_D0	$I$ outz = 150 mA		150	300	mV
Load regulation		$100T2 = 10$ mA to 150 mA		5	50	mV
Line regulation		$VDD$ IN4 = 3.0 V to 4.0 V, Iout2 = 50 mA		0.1		$\%N$
	<b>VNOISE</b>	$100T2 = 50$ mA, 10 Hz to 10 kHz		350		<b>µVRMS</b>
		$100T2 = 50$ mA, 10 Hz to 10 kHz, CBYP = 1 $\mu$ F		60		<b>µVRMS</b>
Power supply rejection ratio	PSRROUT2	$f = 1$ kHz, $I$ out $2 = 50$ mA, $V$ $D$ $D$ $N = 2.1$ V		70		dB
		$f = 10$ kHz, $I = 50$ mA, VDD $I = 2.1$ V		50		dB
<b>LDO3 (MSMA)</b>						
Output voltage	VOUT3	$I$ out $3 = 10$ mA	2.52	2.6	2.68	V
Temperature coefficient	∆VOUT3/°C			±100		ppm/°C
Maximum output current	IOUT3		300	550		mA
Dropout voltage	VLD03_D0	$I$ <sub>0</sub> $T$ 3 = 300 mA		200	400	mV
Load regulation		$I$ out $3 = 10$ mA to 300 mA		5	50	mV
Line regulation		$VDD_{IN4} = 3.0 V$ to 4.0 V, louts = 50 mA		0.1		$\% / V$
	<b>VNOISE</b>	$100T3 = 50$ mA, 10 Hz to 10 kHz		350		<b>µVRMS</b>
		$100T3 = 50$ mA, 10 Hz to 10 kHz, CBYP = 1 $\mu$ F		60		<b>µVRMS</b>
Power supply rejection ratio	PSRROUT3	$f = 1$ kHz, $I$ out $3 = 50$ mA, $VDD$ IN3 = $VOUT3 + 1$ V		70		dB
		$f = 10$ kHz, $I$ out $3 = 50$ mA, $VDD$ _IN3 = $V$ OUT3 + 1 V		50		dB

## Table 4. AAT2630 Electrical Specifications (3 of 5) (Note 1)

(VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF,  $\frac{1}{2}$  COUTB = 10  $\mu$ F, CVREF = 2.2  $\mu$ F, Clu $\mu$  = 4.7  $\mu$ F, Coutl = 2.2  $\mu$ F, CBYP = 0.1  $\mu$ F, CvBUS = 0.47  $\mu$ F, TA = –40 °C to +85 °C, Typical Values are TA = 25  $\degree$ C, Unless Otherwise Noted)



## Table 4. AAT2630 Electrical Specifications (4 of 5) (Note 1)

(VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF,  $\frac{1}{2}$  COUTB = 10  $\mu$ F, CVREF = 2.2  $\mu$ F, CINL = 4.7  $\mu$ F, CoUTL = 2.2  $\mu$ F, GBYP = 0.1  $\mu$ F, CVBUS = 0.47  $\mu$ F, TA = –40 °C to +85 °C, Typical Values are TA = 25  $\degree$ C, Unless Otherwise Noted)



## Table 4. AAT2630 Electrical Specifications (5 of 5) (Note 1)

(VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF,  $\frac{1}{2}$  COUTB = 10  $\mu$ F, CVREF = 2.2  $\mu$ F, CML = 4.7  $\mu$ F, Coutl = 2.2  $\mu$ F, CBYP = 0.1  $\mu$ F, CvBUS = 0.47  $\mu$ F, TA = –40 °C to +85 °C, Typical Values are TA =  $25 °C$ , Unless Otherwise Noted)



Note 1: Performance is guaranteed only under the conditions listed in this table.

Note 2: Guaranteed by design.

## TYPICAL PERFORMANCE CHARACTERISTICS

VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF, COUTB = 10 µF, CVREF = 2.2 µF, CINL = 4.7 µF, COUTL = 2.2 µF, CBYP = 0.1 µF, CVBUS = 0.47 µF, TA = -40 °C TO +85 °C, **TYPICAL VALUES ARE TA = 25 °C. UNLESS OTHERWISE NOTED** 

Typical performance characteristics of the AAT2630 are illustrated in Figures 3 through 12.



Figure 3. Standby Current vs Temperature (VIN =  $3.6$  V)



Figure 5. Buck1 Efficiency vs Output Current







Figure 4. LDO Power Supply Rejection Ratio, PSRR (IOUT = 50 mA)



Figure 6. Buck2 Efficiency vs Output Current





## Typical Performance Characteristics

VBUS = VDD\_IN1 = VDD\_IN2 = VDD\_IN3 = VDD\_IN4 = 3.6 V, VPOWER\_ON = 3.6 V, VEN\_TCXO = VEN\_RUIM = 3.6 V, VSEL\_RUIM = 3.6 V, CINB = 10 µF, COUTB = 10 µF, CVREF = 2.2 µF, CINL = 4.7 µF, COUTL = 2.2 µF, CBYP = 0.1 µF, CVBUS = 0.47 µF, TA = -40 °C TO +85 °C, TYPICAL VALUES ARE TA =  $25^{\circ}$ C, UNLESS OTHERWISE NOTED



Figure 9. Power-On Threshold Voltage vs Input Voltage



Figure 11. SEL\_RUIM Threshold Voltage vs Input Voltage



Figure 10. EN\_RUIM Threshold Voltage vs Input Voltage



Figure 12. LED\_EN Threshold Voltage vs Input Voltage



Figure 13. AAT2630 Functional Block Diagram

## Functional Description

The AAT2630 is targeted for data cards, data modules, and onboard circuit blocks for wireless communication function. It is designed for half or mini-half PCI Express cards, Express Card modules, USB dongles and SDIO modules. The AAT2630 is sourced from a 3 V to 5.5 V power supply with supply currents ranging from 500 mA for USB 2.0, up to 2.7 A for half or minihalf PCI express cards. It has two high efficiency step-down converters to reduce power dissipation in space restricted modules. Automatic power-up and shutdown sequence feature is used in card slots without a power switch.

Figure 13 shows the functional block diagram for the AAT2630.

## Enable and Selection Functions

The AAT2630 features five enable/disable functions for the three LEDs, LD05 (REG\_RUIM) and TCXO output that are

controlled by LED\_EN1, LED\_EN2, LED\_EN3, EN\_RUIM and EN TCXO. These signals are active high and are compatible with CMOS logic. The EN pin voltage level must be greater than 1.4 V to turn on the LED. The LED will turn off when the voltage on the EN pin falls below 0.4 V.

The AAT2630 also features a LDO regulator voltage selection function (SEL\_RUIM) for LDO5 (REG\_RUIM). With SEL\_RUIM = 1 (high logic) the LDO5 output (REG\_RUIM) will be set to 3V. When SEL\_RUIM  $= 0$  (low logic), the LDO5 output (REG\_RUIM) is set to 1.8 V.

## Power-on and Shutdown Sequence

The AAT2630 POWER\_ON pin is used for power-on reset.

The AAT2630 starts the power on procedure when the POWER\_ON pin is asserted. Upon POWER\_ON assertion, Buck1 and Buck2 are enabled in sequence. When Buck2 is within 10% of its' final regulation voltage, LDO\_MSME, LDO\_RFRX, LDO\_MSMP, LDO\_MSMA, LDO\_TCXO and VREF are sequenced in cascade fashion – where each regulator is enabled after the previous regulator is within 10% of its final voltage.

After VREF is within 10% of its final voltage and the RESET delay expires, the RESET pin is released (RESET goes high). When RESET is de-asserted (High), LDO\_USB and LDO\_MMC are enabled. Note that once RESET is de-asserted it is latched in the high state, regardless of any of the regulators falling out of regulation, until the power on procedure starts again. The power on and shutdown sequence is shown in Figure 14.

## TCXO Sequence

- 1. Once the AAT2630 LDO2 for MSMP starts to output 2.6 V, the external oscillator (TCXO) starts to generate a 19.2 MHz sine wave input signal. The setup time of the external oscillator is less than 6 ms.
- 2. After the 6 ms set-up time, the TCXO buffer can be enabled.
- 3. The 32.7645 kHz signal is generated from the 19.2 MHz signal in the AAT2630. There is no additional delay from 19.2 MHz input to the 32 kHz output.

The TCXO sequence is shown in Figure 15.







Figure 15. AAT2630 TCXO Timing Sequence

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## Application Information

The AAT2630 contains two buck regulators in close proximity and switching at high frequency. Its pad arrangement is carefully designed for easy placement and layout. Chip inductors should be placed in different directions to reduce the coupling between the regulators.

## **RESET**

RESET is an open-drain output with 100 k $\Omega$  pull up resistor to VREG\_MSMP internally.

## LED Indication

LED1 (LED\_BLUE), LED2 (LED\_RED) and LED3 (LED\_GREEN) are open drain outputs which sink up to 10 mA current. This is a high current level for most LEDs. Optional resistors in series with the LEDs can restrict the current to a preferable level for specific LED selections.

## Step-down Converter

## Input Capacitor

Select a 10  $\mu$ F X7R or X5R ceramic capacitor for the input. To estimate the required input capacitor size, determine the acceptable input ripple voltage level (VPP) and solve for C using the equations shown below. The calculated value varies with input voltage and is a maximum when VIN is double the output voltage.

$$
C_{IN} = \frac{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}{\left(\frac{V_{PP}}{I_{OUT}} - ESR\right) \times f_{SW}}
$$

$$
C_{IN(MIN)} = \frac{1}{4 \times \left(\frac{V_{PP}}{I_{OUT}} - ESR\right) \times f_{SW}}
$$

CIN is the input capacitance, VIN is the input voltage, Vout is the output voltage, fsw is the switching frequency, lour is the output current, and ESR is the equivalent series resistor of the input capacitor.

The maximum input capacitor RMS current is:

$$
I_{RMS} = I_{OUT} \times \sqrt{\frac{V_{OUT}}{V_{IN}}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)
$$

The input capacitor RMS ripple current varies with the input and output voltages and is always less than or equal to half of the total DC load current.

$$
I_{RMS(MAX)} = \frac{I_{OUT}}{2}
$$

The maximum input voltage ripple also appears at 50% duty cycle.

The input capacitor provides a low impedance loop for the edges of pulsed current drawn by the AAT2630. Low ESR/ESL X7R and X5R ceramic capacitors are ideal for this function. To minimize parasitic inductances, the capacitor should be placed as close as possible to the IC. This keeps the high frequency content of the input current localized, minimizing EMI and input voltage ripple.

The proper placement of the input capacitors (C2, C4) is shown in the evaluation board layout in Figure 18.

A laboratory test setup typically consists of two long wires running from the bench power supply to the evaluation board input voltage pins. The inductance of these wires, along with the low-ESR ceramic input capacitor, can create a high Q network that may affect converter performance, in the form of excessive ringing in the output voltage during load transients. Errors can also result in the loop phase and gain measurements. Since the inductance of a short PCB trace feeding the input voltage is significantly lower than the power leads from the bench power supply, most applications do not exhibit this problem.

In applications where the input power source lead inductance cannot be reduced to a level that does not affect the converter performance, place a high ESR tantalum or aluminum electrolytic capacitor in parallel with the low ESR/ESL bypass ceramic capacitor. This dampens the high Q network and stabilizes the system.

## Output Capacitor

The output capacitor limits the output voltage ripple and provides holdup during large load transitions. A 4.7 LF X5R or X7R ceramic capacitor typically provides sufficient bulk capacitance to stabilize the output during large load transitions and has the ESR and ESL characteristics necessary for low output ripple voltage.

The output voltage droop due to a load transient is dominated by the capacitance of the ceramic output capacitor. During a step increase in load current, the ceramic output capacitor alone supplies the load current until the loop responds. Within two or three switching cycles, the loop responds and the inductor current increases to match the load current demand. The relationship of the output voltage droop during the three switching cycles to the output capacitance can be estimated by:

$$
C_{OUT} = \frac{3 \times \Delta I_{LOAD}}{V_{DROOP} \times f_{SW}}
$$

Once the average inductor current increases to the DC load level, the output voltage recovers. The above equation establishes a limit on the minimum value for the output capacitor with respect to load transients.

#### Output Inductor

For most designs, the AAT2630 operates with inductor values of 2.2  $\mu$ H to 4.7  $\mu$ H. Inductors with low inductance values are physically smaller but generate higher inductor current ripple leading to higher output voltage ripple. The inductor value can be derived from the following equation:

$$
L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_{LOAD} \times f_{SW}}
$$

Where  $\Delta$ ILOAD is inductor ripple current. Large value inductors result in lower ripple current and small value inductors result in high ripple current. Choose inductor ripple current approximately 30% of the maximum load current 0.5 A, or

$$
\Delta I_{LOAD} = 150 mA
$$

Manufacturer's specifications list both the inductor DC current rating, which is a thermal limitation, and the peak current rating, which is determined by the saturation characteristics. The inductor should not show any appreciable saturation under normal load conditions. The DC current rating of the inductor should be at least equal to the maximum load current plus half the inductor ripple current to prevent core saturation  $(0.5 A + 150 mA)$ .

Some inductors may meet the peak and average current ratings yet result in excessive losses due to a high DCR.

Always consider the losses associated with the DCR and its effect on the total converter efficiency when selecting an inductor.

Table 5 lists the recommended inductors.

#### Table 5. Recommended Inductors



## Thermal Calculations

There are three types of losses associated with the AAT2630 step-down converters: switching losses (PSW), conduction losses (PCOND), and quiescent current losses (PQC). Conduction losses are associated with the RDS(ON) characteristics whereas switching losses are dominated by the gate charge of the power output switching devices. At full load, with continuous conduction mode (CCM), a simplified form of the losses is given by:

$$
P_{BUCK} = P_{SW} + P_{COND} + P_{QC}
$$

The three components of the total continuos conduction mode are given by:

$$
P_{\scriptscriptstyle SW} = t_{\scriptscriptstyle SW} \times f_{\scriptscriptstyle SW} \times I_{\scriptscriptstyle OUT} \times V_{\scriptscriptstyle IN}
$$

$$
P_{COND} = I_{OUT}^2 \times \left[ R_{DS(ON)P} \times \frac{V_{OUT}}{V_{IN}} + R_{DS(ON)N} \times \left( 1 - \frac{V_{OUT}}{V_{IN}} \right) \right]
$$
  

$$
P_{QC} = I_{OUT} \times V_{IN}
$$

Where IQ is the step-down converter quiescent current, tsw is the switching time, RDS(ON)P and RDS(ON)N are the high side and low side switching MOSFETs' on-resistance. VIN, VOUT and IOUT are the input voltage, the output voltage and the load current.

Since RDS(ON), quiescent current and switching losses vary with input voltage, the total losses should be investigated over the complete input voltage range.

Given the total losses, the maximum junction temperature can be derived from the  $\theta$ JA for the package.

$$
T_{J(MAX)} = P_{TOTAL} \times \theta_{JA} + T_A
$$

## Thermal Shutdown

Thermal overload protection limits the total power dissipation of the AAT2630. When internal thermal sensors detect a die temperature in excess of 140 °C all buck outputs are immediately shut down to allow the IC to cool. When the die temperature has dropped below the 15 °C hysteresis, the buck outputs automatically turn on again in sequence.

#### Low Drop Out Regulator

## Input Capacitor

Typically, a 4.7 μF or larger capacitor is recommended for CIN in most applications. A CIN capacitor is not required for basic LDO regulator operation. However, if the LDO is physically located more than 1 or 2 centimeters from the input power source, a CIN capacitor is needed for stable operation. CIN should be located as close to the device input pin as practically possible. CIN values greater than 4.7  $\mu$ F offer superior input line transient response and assist in maximizing the power supply ripple rejection.

Ceramic, tantalum, or aluminum electrolytic capacitors may be selected for CIN because there is no specific capacitor ESR requirement. For better performance, ceramic capacitors are recommended for CIN due to their inherent capability over tantalum capacitors to withstand input current surges from low impedance sources such as batteries in portable devices.

## Output Capacitor

For proper load voltage regulation and operational stability, a capacitor, COUT, is required between pins VOUT and GND. The COUT capacitor connection to the LDO regulator ground pin should be made as direct as practically possible for maximum device performance. Although the AAT2630 LDOs have been specifically designed to function with very low ESR ceramic

capacitors, the device is stable over a very wide range of capacitor ESR. The AAT2630 also works with some higher ESR tantalum or aluminum electrolytic capacitors. For best performance, ceramic capacitors are recommended.

The value of Cout typically ranges from 1  $\mu$ F to 10  $\mu$ F; however, 2.2  $\mu$ F is sufficient for most operating conditions.

## Short-Circuit and Thermal Protection

The AAT2630 LDOs are protected by both current limit and over-temperature protection circuitry. The internal short-circuit current limit is designed to activate when the output load demand exceeds the maximum rated output. If a short-circuit condition continually draws more than the current limit threshold, the LDO regulator's output voltage drops to a level necessary to supply the current demanded by the load. Under short-circuit or other over-current operating conditions, the output voltage drops, and the AAT2630's die temperature rapidly increases. Once the regulator's power dissipation capacity has been exceeded and the internal die temperature reaches approximately 140 °C, the system thermal protection circuit becomes active. The internal thermal protection circuit actively turns off the LDO regulator output pass device to prevent the possibility of over-temperature damage. The LDO regulator output remains in a shutdown state until the internal die temperature falls back below the 125 °C trip point.

The interaction between short circuit and thermal protection systems allows the LDO regulator to withstand indefinite shortcircuit conditions without sustaining permanent damage.

## No-Load Stability

The AAT2630 LDO is designed to maintain output voltage regulation and stability under operational no-load conditions. This is an important characteristic for applications where the output current may drop to zero. An output capacitor is required for stability under no-load operating conditions. Refer to the Output Capacitor section of this datasheet for recommended typical output capacitor values.

## LDO Minimum Input Voltage

The power supply of the LDO has to be at least the VOUT  $(nominal) + VLDOX$  po to regulate the output voltage. If the power supply is lower than the VOUT (nominal) value, the output voltage will be  $V_{IN} - V_{LDOX}$  po.

For example, if the LDO output is  $3.3V$ , VLDOX,  $Do = 150$  mV, VIN should be larger than  $3.3 + 0.150 = 3.45$  (V). If VIN = 3.2 V, then Vout is  $3.2 - 0.15 = 3.05$  (V).

Figure 16 indicates the typical applications.





## Layout Considerations

The suggested PCB layout for the AAT2630 is shown in Figures 5 to 10. The following guidelines are recommended to ensure a proper layout:

- Keep the power traces (GND, LX, IN) short, direct, and wide to allow large current flow. Place sufficient multiple-layer pads when needed to change the trace layer.
- Connect the output capacitors C3, C5 and inductors L1, L2 as close as possible. Keep the connection of L1, L2 to the LX1, LX2 pins as short as possible and route no signal lines under the inductors.
- Separate OUT pins (B1, G4) from any power trace and connect as close as possible to the load point. Sensing along a highcurrent load trace will degrade DC load regulation.
- Keep the resistance of the trace from the load returns to PGND to a minimum. This will help to minimize any error in DC regulation due to differences in the potential of the internal signal ground and the power ground.
- Connect the ground pin to PGND with a single point to decrease the effect of large power ground noise on the analog ground.

## Evaluation Board Description

The AAT2630 Evaluation Board is used to test the performance of the AAT2630. An Evaluation Board schematic diagram is provided in Figure 17. Layer details for the Evaluation Board are shown in Figure 18. The Evaluation Board has additional components for easy evaluation; the actual bill of materials

required for the system is shown in Table 6. Table 7 explains the terms and acronyms.

## Package Information

Package dimensions for the 49-bump WLCSP package are shown in Figure 19.









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## Table 7. Terms and Acronyms





Figure 18. AAT2630 Evaluation Board Layer Details



Figure 19. AAT2630 49-bump WLCSP Package Dimensions

## Ordering Information



Note 1:  $XY =$  assembly and date code.

Note 2: Sample stock is generally held on part numbers listed in **BOLD**.

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