

Features and Benefits

- \Box Small size, low cost 16x4 pixels IR array
- \Box Easy to integrate
- \Box Industry standard four lead TO39 package
- \Box Factory calibrated infrared temperature measurement. Calibration parameters stored in EEPROM.
- □ Noise Equivalent Temperature Difference (NETD) 0.20K RMS @4Hz refresh rate
- \Box I²C compatible digital interface
- □ Programmable frame rate 0.5Hz...512Hz
- \Box 2.6V supply voltage
- \Box Current consumption less than 9mA
- \Box Sleep mode consumption less than 7 μ A
- Measurement start trigger for synchronization with external control unit
- 3 FOV 40°x10°, 60°x16° and 120°x25°
- \Box Ta -40°C to 85°C
- To -20°C to 300°C
- \Box Complies with RoHS regulations

Applications Examples

- \Box High precision non-contact temperature measurements;
- \Box Temperature sensing element for residential, commercial and industrial building air conditioning;
- \Box Microwave ovens
- \Box Home appliances with temperature control;
- □ Thermal Comfort sensor in automotive Air Conditioning control system;
- **Q** Passenger classification
- \Box Automotive blind angle detection;
- \Box Industrial temperature control of moving parts;
- \Box Identifying thermal leaks in homes
- \Box Thermal scanners
- \Box Security / safety gates
- □ Intrusion / Movement detection;
- **Presence detection / Person localization**

Ordering Information

Example: MLX90621ESF-BAB-000-TU

Functional diagram General Description

The MLX90621 is a fully calibrated 16x4 pixels IR array in an industry standard 4-lead TO-39 package. It contains 2 chips in one package: the MLX90670 (IR array with signal conditioning electronics) and the 24AA02 (256x8 EEPROM) chip.

The MLX90621 contains 64 IR pixels with dedicated low noise chopper stabilized amplifier and fast ADC integrated. A PTAT (Proportional To Absolute Temperature) sensor is integrated to measure the ambient temperature of the chip. The outputs of both IR and PTAT sensors are stored in internal RAM and are accessible through I^2C .

General Description (continued)

The results of the infrared sensor measurements are stored in RAM:

- 15...18-bit result of IR measurement for each individual sensor (64 words)
- 15…18-bit result of PTAT sensor

Depending on the application, the external microcontroller can read the different RAM data and, based on the calibration data stored in the EEPROM memory, compensate for difference between sensors to build up a thermal image, or calculate the temperature at each spot of the imaged scene.

These constants are accessible by the user microcontroller through the I2C bus and have to be used for external post processing of the thermal data. This post processing includes:

- Ta calculation
- Pixel offset cancelling
- Pixel to pixel sensitivity difference compensation
- Object emissivity compensation
- Object temperature calculation

The result is an image with NETD better than 0.1K RMS at 1Hz refresh rate.

The refresh rate of the array is programmable by means of register settings or directly via I2C command. Changes of the refresh rate have a direct impact on the integration time and noise bandwidth (faster refresh rate means higher noise level). The frame rate is programmable in the range 0.5Hz…512Hz and can be changed to achieve the desired trade-off between speed and accuracy.

The MLX90621 requires a single 2.6V…3.2V although the device is calibrated and performs best at VDD=2.6V.

The MLX90621 is factory calibrated in following temperature ranges:

- -40˚C…85˚C for the ambient temperature sensor
- -50˚C…300˚C for the object temperature.

NOTE: The sensor can detect higher temperatures, but is not calibrated for temperatures above 300°C. See Table 21 for configuration specific properties.

Each pixel of the array measures the average temperature of all objects in its own Field Of View (called nFOV).

It is very important for the application designer to understand that the accuracy of the temperature measurement is very sensitive to the thermal equilibrium isothermal conditions (there are no temperature differences across the sensor package). The accuracy of the thermometer can be influenced by temperature differences in the package induced by causes like (among others): Hot electronics behind the sensor, heaters/coolers behind or beside the sensor or by a hot/cold object very close to the sensor that not only heats the sensing element in the thermometer but also the thermometer package*.*

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2. **Glossary of terms**

Table 1 Glossary of terms

3. **Absolute Maximum ratings**

Table 2 Absolute maximum ratings for MLX90621

Exceeding the absolute maximum ratings may cause permanent damage. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

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4. **Pin definition and description**

Figure 1 Pin description

Table 3 Pin description for MLX90621

5. **Electrical characteristics**

All parameters are valid for $T_A = 25^\circ C$, $V_{DD} = 2.6V$ (unless otherwise specified)

Table 4 Electrical specification parameters of MLX90621

1) The device can be supplied with VDD = 2.6…3.3V but the best performance is achieved at VDD=2.6V. For supply voltages above 2.7V a compensation algorithm should be applied for compensating the temperature readings.

6. **Block diagram**

Figure 2 Block diagram

The device consists of 2 chips packed in single TO-39 package

- IR array and processing electronics
- EEPROM chip

7. **Principle of operation**

The output of all IR sensors and absolute temperature sensors is scanned according to the programmed refresh rate. Using their output data as well as calibration constants written in EEPROM the absolute chip temperature and object temperature, 'seen' by each pixel can be calculated. For this goal several sequential calculations must be done according to the Figure 3 Operation block diagram

Figure 3 Operation block diagram

7.1. Initialization

After the POR is released the external MCU must execute an initialization procedure.

This procedure must start at least 5ms after POR release.

Read the whole EEPROM (see Figure 4). For maximum speed performance MELEXIS recommends that the whole calibration data is stored into the client MCU RAM. However it is possible to read the calibration data from the EEPROM only when needed during calculations. This will result in increased time for temperature calculation i.e. low refresh rate.

Figure 4 Whole EEPROM dump (SA = 0x50, command = 0x00)

- **Store the EEPROM content into customer MCU RAM** This step could be omitted resulting in more data processing time because calibration data needs to be reread for each calculation
- **Write the oscillator trimming value** (extracted from EEPROM content at address 0xF7) into the corresponding register (0x93).

Figure 5 Write oscillator trimming (SA = 0x60, command = 0x04)

Example: If the value that has to be uploaded is 0x0052 the following sequence must be sent:

- 1. Start condition (Falling edge of SDA while SCL is high)
- 2. Slave address (SA=0x60) plus write bit = $0xC0$
- 3. Command = $0x04$
- 4. LSByte check = LSByte $-$ 0xAA = 0x52 $-$ 0xAA = 0xA8
- 5. LSbyte = 0x52
- 6. MSByte check = MSByte $-$ 0xAA = 0x00 $-$ 0xAA = 0x56
- 7. MSbyte = 0x00
- 8. Stop condition (Rising edge of SDA while SCL is high)
- **Write device configuration value**. In EEPROM addresses (0xF5 and 0xF6) MELEXIS provides a typical value of the configuration register (0x463E). So it is up to the user to copy that value or hardcode a new value to be loaded into the configuration register. If the EEPROM value is to be used the 16 bits are combined as follows:

For example: if EEPROM 0xF5 = 0x3E and 0xF6 = 0x46, the Configuration register value is:

$Configuration Register value = \{0xF6: 0xF5\}$

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NOTE: The user must ensure that the bit 10 (POR or Brown-out flag) in Configuration register is set to "1" by the MD. Furthermore, this bit must be checked regularly and if it is cleared it indicates that the device has been reset and the initialisation procedure must be redone.

Example: If the value that has to be uploaded is 0x463E the following sequence must be sent:

- 1. Start condition (Falling edge of SDA while SCL is high)
- 2. Slave address (SA=0x60) plus write bit = $0xC0$
- 3. Command = $0x03$
- 4. LSByte check = LSByte $0x55 = 0x3E 0x55 = 0xE9$
- 5. LSbyte = 0x3E
- 6. MSByte check = MSByte $-$ 0x55 = 0x46 $-$ 0x55 = 0xF1
- 7. MSbyte = $0x46$
- 8. Stop condition (Rising edge of SDA while SCL is high)

The default configuration is:

- IR and Ta refresh rate = 1Hz;
- Normal mode (no sleep);
- $-I^2C$ FM+ mode enabled (maximum bit transfer up to 1000 Kbit/s);
- ADC low reference enabled;

7.1.1. Reading configuration

7.1.1.1 Reading configuration register (EEPROM data)

Start address = 0x92, Address step = 0x00, Number of reads = 0x01)

7.1.1.2 Reading oscillator trimming register (EEPROM data)

Figure 8 Reading configuration register (SA = 0x60, command = 0x02,

Start address = 0x93, Address step = 0x00, Number of reads = 0x01)

7.2. Read measurement data (RAM data)

7.2.1. PTAT data read

Absolute ambient temperature data of the device itself (package temperature) can be read by using following command:

$\emph{PTATdata} = \emph{\{PTATdata}_{MSByte}: PTATdata}_{LSByte}\}$

7.2.2. IR data read

There are four options available for reading IR data: (See section 8.2.1 for an overview of the RAM addresses).

- **Whole frame read** (MELEXIS recommends the whole frame read for maximum refresh rate)

- **Single line read**

Slave address Command Command Address step Number of reads Slave address Start address s_{D4} 1 01 0 0 0 0A 0 0 0 0 0 1 0 AS 0 A 0 0 0 0 1 0 00 A A W 0 0 0 1 0 0 0 0 A S 1 1 0 0 0 0 0 R A 11111111 SCL IR pixel(line, 0) LSByte IR pixel(line, 0) MSByte IR pixel(line, 1) LSByte IR pixel(line, 1) MSByte IR pixel(line, 15) LSByte IR pixel(line, 15) MSByte A AP //A A AP A A A $A A A A A$ *Figure 12 Single line (SA = 0x60, command = 0x02, Start address = 0x00…0x03 (step 0x01), Address step = 0x04, Number of reads = 0x10) measurement result read* - **Single pixel read** Slave address **Command** Command **Address** step Number of reads Slave address Start address IR pixel data IR pixel data LSByte MSByte SDA 1 01 0 0 0 0A 0 0 0 0 0 1 0 AS 0 A A P 0 0 0 0 0 0 00 A A 0 0 0 0 0 0 10 S 1 01 0 0 0 R A0 W A sci *Figure 13 Single pixel (SA = 0x60, command = 0x02, Start address = 0x00…0x3F, Address step = 0x00, Number of reads = 0x01) measurement result read* - **Compensation pixel read**

Address step = 0x00, Number of reads = 0x01) measurement result read

The 16bit data for each pixel is:

 $IRdata(i,j) = \{IRdata(i,j)_{MSByte} : IRdata(i,j)_{LSByte}\}$

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7.3. Calculation

7.3.1. Calculation of absolute chip temperature Ta (sensor temperature)

The output signal of the IR sensors is relative to the cold junction temperature. That is why we need to know the temperature of the die in order to be able to calculate the object temperature 'seen' by each pixel.

The Ta can be calculated using the formula:

$$
T_a = \frac{-K_{T1} + \sqrt{K_{T1}^2 - 4K_{T2}[V_{TH}(25) - PTAT_data]}}{2K_{T2}} + 25, [^{\circ}C]
$$

Constants $V_{TH}(25)$, K_{T1} and K_{T2} are stored in EEPROM at following addresses as two's complement values:

Table 5 EEPROM parameters for Ta calculations

 $V_{TH}(25) = 256 * V_{TH,H} + V_{TH,L}$

$$
If \: V_{TH}(25) > 32767 \rightarrow V_{TH}(25) = \: V_{TH}(25) - 65536
$$

$$
V_{TH}(25) = \frac{V_{TH}(25)}{2^{3-ConfigReg[5:4]}}
$$

$$
K_{T1} = 256 * K_{T1_H} + K_{T1_L}
$$

$$
if\; K_{T1}>32767 \rightarrow K_{T1}=K_{T1}-65536
$$

$$
K_{T1} = \frac{K_{T1}}{2^{EERPOM 0xD2[7:4]} \times 2^{3-ConfigReg[5:4]}}
$$

$$
K_{T2} = 256 * K_{T2,H} + K_{T2,L}
$$

if $K_{T2} > 32767 \rightarrow K_{T2} = K_{T2} - 65536$
 K_{T2}

$$
K_{T2} = \frac{K_{T2}}{2^{EERPOM 0xD2[3:0]+10} * 2^{3-ConfigReg[5:4]}}
$$

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7.3.2. Example for Ta calculations

Let's assume that the values in EEPROM are as follows (Derived using maximum resolution – ConfigRegister[5:4] = $11b$):

Table 6 EXAMPLE for Ta calibration values

Let's assume that the maximum resolution is set in the configuration register:

ConfigRegister[5:4] = 11b

 $V_{TH}(25) = 256 * V_{TH,H} + V_{TH,L} = 256 * 100 + 32 = 25632$

Sign check: 25632 \lt 32768 \rightarrow $V_{TH}(25) = 25632$

$$
V_{TH}(25) = \frac{V_{TH}(25)}{2^{3-ConfigReg[5:4]}} = \frac{25632}{2^{3-3}} = 25632
$$

 $K_{T1} = 256 * K_{T1_H} + K_{T1_L} = 256 * 85 + 137 = 21897$

Sign check: 21897 $<$ 32768 \rightarrow $K_{T1} = 21897$

$$
K_{T1} = \frac{K_{T1}}{2^{EERPOM 0xD2[7:4]} \times 2^{3-ConfigReg[5:4]}} = \frac{21897}{2^8 \times 2^{3-3}} = 85.53515625
$$

 $K_{T2} = 256 * K_{T2_H} + K_{T2_L} = 256 * 94 + 126 = 24190$

Sign check: 24190 $<$ 32768 $\rightarrow K_{T2} = 24190$

 $K_{T2} = \frac{K_{T2}}{2^{EERPOM \space 0 \times D2[3:0]+10}}$ $\frac{K_{T2}}{2^{EERPOM~0xD2[3:0]+10}*2^{3-}ConfigReg[5:4]} = \frac{24190}{2^{11+10}*2^{3-}}$ $\frac{21150}{2^{11+10}*2^{3-3}} = 0.01153469085$

Let's assume that the input data is:

$$
PTAT_data = \textbf{0x67DE} = \textbf{26590 dec}
$$

Thus the ambient temperature is:

 $T_a = \frac{-K_{T1} + \sqrt{K_{T1}^2 - 4K_{T2}[V_{TH}(25) - PTAT_data]}}{2K_{T2}}$ $\frac{2K_{T2}}{2K_{T2}}$ + 25

 $T_a = \frac{-85.53515625 + \sqrt{7316.26295471 - 4*0.01153469085* [25632 - 26590]}}{0.0230693817}$ $\frac{R_{34}}{1 - 4*0.01133469063* [23632 - 26390]} + 25$

 $T_a = \frac{-85.53515625 + \sqrt{7316.26295471 - 0.0461387634*(-958)}}{0.0230693817}$ $\frac{6.26293471 - 0.0461387634*(-936)}{0.0230693817} + 25$

$$
T_a = \frac{-85.53515625 + \sqrt{7360.46389005}}{0.0230693817} + 25 \approx \frac{-85.53515625 + 85.7931459386}{0.0230693817} + 25 \approx 11.1832077 + 25
$$

 $T_a \approx 36.18 \text{ °C}$

The calculated values for the different resolution settings are given in the table below:

Table 7 Calculated values at different resolution settings

7.3.3. Calculation of To

Following formula is used to calculate the temperature seen by specific pixel in the matrix:

$$
T_{O(i,j)} = \sqrt[4]{\frac{V_{IR(i,j)}_{COMPENSATED}}{\alpha_{comp(i,j)}*(1-K_{S4}*273.15) + S_{X(i,j)}} + T_{a_{K}4} - 273.15, [° C]}
$$

Where:

 $V_{IR(i,j)CDCPENSATED}$ is the parasitic free IR compensated signal as calculated in 7.3.3.1

 $\alpha_{comp(i,j)}$ is the compensated sensitivity coefficient for each pixel

 K_{S4} is the compensation factor for the sensitivity – for BAB and BAD, $K_{S4} = 0$, resulting in a simplified formula

 $T_{a_{K^4}} = (T_a + 273.15)^4$ where T_a is the ambient temperature calculated in 7.3.2

 $S_{x(i,j)} = K_{s4} * \sqrt[4]{\alpha_{comp(i,j)}^3 * V_{IR(i,j)_{COMPENSATED}} + \alpha_{comp(i,j)}^4 * T_{a_{K}^4}}$

7.3.3.1 Calculating V_{IR(I,i)} COMPENSATED

1. Offset compensation

$$
V_{IR(i,j)_{OffsetCompensated}} = V_{IR(i,j)} - \left(A_{i(i,j)} + B_{i(i,j)} \times (T_a - T_{a0})\right)
$$

Where:

 $V_{IR(i, j)}$ is an individual pixel IR_data readout (RAM read) $A_{i\left(i,j\right) }$ is an individual pixel offset restored from the EEPROM using the following formula:

$$
A_{i(i,j)} = \frac{A_{common} + \Delta A_{i(i,j)} * 2^{\Delta A_{i}} scale}{2^{3 - ConfigReg[s:4]}}
$$

 A_{common} is the minimum offset value stored in the EEPROM at addresses 0xD0 and 0xD1 as 2's complement value

 ΔA_i is the difference between the individual offset and the minimum value. It is stored in the EEPROM as unsigned values.

 $\Delta A_{i_{scale}}$ is the scaling coefficient for the ΔA_i values and is stored in the EEPROM at address 0xD9[7:4] as an unsigned value

 $B_{\widetilde {l}(i,j)}$ is an individual pixel offset slope coefficient

$$
B_{i(i,j)} = \frac{B_{i(i,j)_{EEPROM}}}{2^{B_{i_{scale} \times 2^{3}-ConfigReg[5:4]}}}
$$

 $B_{i(i,j)_{EEPROM}}$ is the value stored in EEPROM as two's complements

 $B_{i_{scale}}$ is a scaling coefficient for the slopes of IR pixels offset and is stored in the EEPROM at address 0xD9[3:0] as an unsigned value T_a is the ambient temperature calculated in 7.3.2 $T_{a0} = 25$ °C is a constant

NOTE: This applies to the compensation pixel as well (A_{CP} and B_{CP} while $B_{i_{scale}}$ is the same) with the only difference being that A_{CP} is stored in the EEPROM at addresses 0xD3 and 0xD4 as an unsigned value but not calculated

2. Thermal Gradient Compensation (TGC)

 $V_{IR(i,j)_{TGC}{}_{compensated}} = V_{IR(i,j)_0}$ f fsetCompensated $- TGC*V_{IRcp}{}_{Offset}$ Compensated

Where:

 V_{IRcp} _{OffsetCompensated} is the offset compensated IR signal of the thermal gradient compensation

pixel

$$
TGC = \frac{TGC_{EEPROM}}{32}
$$

 TGC_{EEPROM} is a coefficient stored at EEPROM address 0xD8 as a two's complement value

3. Emissivity compensation

$$
V_{IR(i,j)_{COMPENSATED}} = \frac{V_{IR(i,j)_{TGCG}mpensated}}{\varepsilon}
$$

Where:

 ϵ is the emissivity coefficient. The scaled value is stored into EEPROM as unsigned value

$$
\varepsilon = \frac{256 * \varepsilon_H + \varepsilon_L}{32768}
$$

7.3.3.2 Calculating $\alpha_{comp(i,j)}$

$$
\alpha_{comp(i,j)} = (1 + KsTa * (T_a - T_{a0})) * (\alpha_{(i,j)} - TGC * \alpha_{CP})
$$

Where:

 T_a is the ambient temperature calculated in 7.3.2

 T_{a0} is a constant = 25°C

 $KsTa$ is Ta dependence of $\alpha_{comp(i,j)}$ stored in EEPRPOM at addresses 0xE6 and 0xE7 as two's complement value and the scale coefficient is fixed to be 20.

$$
KsTa = \frac{256 * KsTa_H + KsTa_L}{2^{20}}
$$

$$
\alpha_{(i,j)} = \frac{\frac{256 * \alpha_{0H} + \alpha_{0L}}{2} + \frac{\Delta\alpha_{(i,j)}}{2}}{\frac{2}{2} - \frac{\Delta\alpha_{scale}}{2} + \frac{\Delta\alpha_{scale}}{2}}{2}} \alpha_{scale}
$$

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 $\alpha_{CP} = \frac{^{256* \alpha_{CP}}_{H} + \alpha_{CP}}{2^{ \alpha_{0}}_{scale \times 2^3 - ConfigRe}}$ $\frac{256 \cdot \alpha_C P_H \cdot \alpha_C P_L}{2^{\alpha_{0}} scale * 2^{3 - ConfigReg[5:4]}}$

 α_{o_H} , α_{o_L} , α_{CP_H} , α_{CP_L} , $\Delta\alpha_{(i,j)}$, $\alpha_{0_{scale}}$ and $\Delta\alpha_{scale}$ are stored in the EEPROM as unsigned values

7.3.3.1 Calculating K_{s4}

 $K_{s4} = \frac{K_{s4} E E}{2(K_{s} scale)}$ $\frac{K_{S4_EE}}{2(K_{S_scale+B})}$, stored in EEPRPOM at addresses 0x9E as two's complement value

All parameters necessary to calculate To are stored into EEPROM at following addresses:

Table 8 EEPROM parameters for To calculations

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7.3.4. Example for To calculations

Let's assume that we have following EEPROM data for pixel i=2, j=8:

Table 9 EXAMPLE for To calibration values

Let's assume that we have the following input data:

 $V_{IR(2,8)} = 0x01B7 = 439$, decimal value

Sign check 439 < 32768 → $V_{IR(2,8)} = 439$ LSB

 $V_{CP} = 0 \times FFDC = 65500$, decimal value (compensation pixel readings)

Sign check $65500 > 32767 \rightarrow V_{CP} = 65500 - 65536 = -36$ LSB

 $T_a \approx 36.18 \text{ °C}$ (as calculated in 7.3.2)

Reference routine for To computation:

$$
T_{O(i,j)} = \sqrt[4]{\frac{V_{IR(i,j)COMPENSATED}}{\alpha_{comp(i,j)}*(1-K_{S4}*273.15)+S_{X}}} + T_{a_{K}4} - 273.15, [°C]
$$

$$
V_{IR(2,8)offsetCompensated} = V_{IR(2,8)} - \left(A_{i(2,8)} + B_{i(2,8)} * (T_a - T_{a0})\right)
$$

 $A_{i(2,8)} = \frac{A_{common} + \Delta A_{i(2,8)} * 2^{\Delta A_{i}} scale}{2^{(3 - ConfigReg[5:4])}}$ $\frac{100n^{12A_1}(2,8)^{2}}{2(3-ConfigReg[5:4])}$

 $A_{common} = 256 * A_{common_{H}} + A_{common_{L}} = 256 * 255 + 138 = 65418$ LSB decimal value

Sign check $65418 > 32767 \rightarrow A_{common} = 65418 - 65536 = -118$ LSB

$$
\Delta A_i = 33 \; \text{LSB}
$$

$$
A_{i(2,8)} = \frac{A_{common} + \Delta A_{i(2,8)} * 2^{\Delta A_{i_{scale}}}}{2^{(3 - ConfigReg[5:4])}} = \frac{-118 + 33 * 2^0}{2^{(3-3)}} = -85 \text{ LSB}
$$

 $B_{i(2,8)} = \frac{B_{i(2,8)}}{e^{-\frac{B_{i(c,8)}}{2}}}$ $2^{B}i_{scale*2}(3-ConfigReg[5:4])$

 $B_{i(2,8)EE} = 188$

Sign check
$$
188 > 127 \rightarrow B_{i(2,8)} = 188 - 256 = -68
$$

$$
B_{i(2,8)} = \frac{B_{i(2,8)}}{2^{B_{i_{scale}} \times 2^{(3-ConfigReg[5:4])}}} = \frac{-68}{2^{7} \times 2^{(3-3)}} = -0.53125
$$

 $V_{IR(2,8)_{offsetCompensated}} = 439 - (-85 - 0.53125 * (36.18 - 25)) \approx 529.939375 \text{ LSB}$

 $A_{CP} = 256 * A_{CP_H} + A_{CP_L} = 65437$, decimal value

Sign check $65437 > 32768 \rightarrow A_{CP} = 65437 - 65536 = -99$ LSB

$$
A_{CP} = \frac{A_{CP}}{2^{(3-ConfigReg[5:4])}} = \frac{-99}{2^{(3-3)}} = -99
$$

 $B_{CP~EE} = 162$

Sign check $162 > 127 \rightarrow B_{CP} = 162 - 256 = -94$

 $B_{CP} = \frac{B_{CP}}{R_{\text{iccal}} \cdot 2^{(3-C_{CP})}}$ $\frac{B_{CP}}{2^{B_{i}} \, \text{scale} \, * 2 \left(3 - \text{ConfigReg} \left[5 : 4 \right] \right)} = \frac{-94}{2^{7} * 2 \left(3 - \frac{1}{2} \right)}$ $\frac{1}{2^{7}*2^{(3-3)}} = -0.734375$

 V_{IRCP} V_{IRCP} σ fsetCompensated $= V_{CP} - (A_{CP} + B_{CP} * (T_a - T_{a0})) = -36 - (-99 - 0.734375 * (36.18 - 25))$

 $V_{IRCP}}$ of fsetCompensated ≈ 71.2103125 LSB

 $TGC_{EEPROM} = 0x18 = 24$, decimal value

Sign check $24 < 128 \rightarrow TGC_EEPROM = 24$

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 $TGC = \frac{TGC_{EEPROM}}{32}$ $\frac{EPROM}{32} = \frac{24}{32}$ $\frac{24}{32} = 0.75$

 $V_{IR(2,8)_{TGCGompensated}} = V_{IR(2,8)_OffsetCompensated} - TGC*V_{IRcp_{OffsetCompensated}}$

 $V_{IR(2,8)T6CConpensated}$ = 529.939375 − 0.75 * 71.2103125 ≈ 475.531640625 LSB

 $\varepsilon = \frac{256 * \varepsilon_H + \varepsilon_L}{32768}$ $\frac{6 * \varepsilon_H + \varepsilon_L}{32768} = \frac{256 * 128 + 0}{32768}$ $\frac{6*128+0}{32768} = \frac{32768}{32768}$ $\frac{32768}{32768} = 1$

 $V_{IR(2,8)_{COMPENSATED}} = \frac{V_{IR(2,8)}_{IGCCcompensated}}{\varepsilon}$ $\frac{Lompensatea}{\varepsilon}$ = 476.531640625 LSB

 $\alpha_{comp(2,8)} = (1 + KsTa * (T_a - T_{a0})) * (\alpha_{(2,8)} - TGC * \alpha_{CP})$

 $KsTa = 256 * KsTa_H + KsTa_L = 256 * 2 + 12 = 524$, decimal value

Sign check $524 > 32768 → A_{CP} = 524$ LSB

 $KsTa = \frac{524}{2^{20}} = 4.9972534.10^{-4}$ decimal value

 $\alpha_{(2,8)} =$ $\frac{256 * a_{0H} + a_{0L}}{}$ $\frac{\alpha_{0H} + \alpha_{0L}}{2\alpha_{scale}} + \frac{\Delta\alpha_{(2,8)}}{2\Delta\alpha_{scal}}$ $a_2^{\Delta\alpha}$ scale $\frac{2}{2}$ scale $\frac{2}{2}$ scale $\frac{2}{2}$ = 256∗78+174 $\frac{18}{2}$ + $\frac{174}{2}$ + $\frac{205}{231}$ 2^{31} $\frac{56}{2^{(3-3)}}$ = 20142 $\frac{0142}{2^{38}} + \frac{205}{2^{31}}$ 2^{31} $\frac{38}{2^{(3-3)}} \approx 1.68736733031.10^{-7}$ $\alpha_{CP} = \frac{^{256* \alpha_{CP_H} + \alpha_{CP_L}}{2^{ \alpha_{0}} 2^{3 - \text{ConfigRe}}}}$ $\frac{^{256*0}C P_H +^{20}C P_L}{2^{20}c \text{ at } \epsilon \cdot 2^{3-\text{ConfigReg[5:4]}}} = \frac{^{256*15+168}}{2^{38}*2^{(3-3)}}$ $\frac{^{256*15+168}}{^{238*2(3-3)}} = \frac{4008}{2^{38}}$ $\frac{1006}{2^{38}} \approx 1.45810190588.10^{-8}$

 $\alpha_{comm(2,8)} = (1 + 4.9972534.10^{-4} * (36.18 - 25)) * (1.68736733031.10^{-7} - 0.75 * 1.45810190588.10^{-8})$

 $\alpha_{comp(2,8)} = 1.58682591595.10^{-7}$

 $K_{s4} = 158$ decimal value

Sign check $158 > 127 \rightarrow K_{s4} = 158 - 256 = -98$

 $K_{s4} = \frac{K_{s4}}{2(K_{s} - sca)}$ $\frac{K_{S4}}{2^{(K_S_scale+8)}} = \frac{-98}{2^{(9+8)}}$ $\frac{-96}{2(9+8)} = -7.476806640625.10^{-4}$ $T_{a_{K}^4} = (T_a + 273.15)^4 = (36.18 + 273.15)^4 = 9155628583$

$$
S_x = K_{S4} * \sqrt[4]{\alpha_{comp(2,8)}^3 * V_{IR(2,8)}^2}
$$

 $S_x = -7.476806640625.10^{-4} * \sqrt[4]{(1.58682591595.10^{-7})^3 * 476.531640625 + (1.58682591595.10^{-7})^4 * 9155628583}$

$$
S_x = -3.93973510355.10^{-8}
$$

$$
T_{O(2,8)} = \sqrt[4]{\frac{V_{IR(2,8)}_{COMPENSATED}}{\alpha_{comp(2,8)}*(1-K_{S4}*273.15)+S_{\chi}}} + T_{a_{K}4} - 273.15 \text{ °C}
$$

$$
T_{O(2,8)} = \sqrt[4]{\frac{476.531640625}{1.58682591595.10^{-7}*(1-(-7.476806640625.10^{-4})*273.15)+(-3.93973510355.10^{-8})}} + 9155628583 - 273.15 \text{ °C}
$$

$$
T_{O(2,8)} = 59.8546263694257 \approx 59.85 \text{ °C}
$$

The calculated values for the different resolution settings are given in the table below:

Table 10 Calculated values at different resolution settings

8. **Detailed description, Block description**

8.1. Pixel position

The array consists of 64 IR sensors (also called pixels). Each pixel is identified with its row and column position as Pix(*i*,*j*) where *i* is its row number (from 0 to 3) and *j* is its column number (from 0 to 15)

8.2. MLX90621 address map

The MLX90621 address map is shown below:

0x00	RAM					
0x41						
0x42						
	Not used					
0x91						
0x92	Configuration registers					
0x93						
0x93						
	Not used					
0xFF						

Figure 16 Address map

8.2.1. RAM

The on chip 146x16 RAM is accessible for reading via I^2 C. The RAM is used for storing the results of measurements of pixels and Ta sensor and is distributes as follows:

- 64 words for IR sensors. The data is in 2's complement format (see 7.2.2)
- 1 word for measurement result of PTAT sensor. The data is 16 bit without sign. (see 7.2.1)

The memory map of the RAM is shown below:

Table 11: Result address map

For IR sensors results, the addressing can be summarized: IR(x,y) is on address:

$$
IR(x, y)
$$
address = $x + 4.y$

Datasheet

8.2.2. Internal registers

8.2.2.1 Configuration register (0x92)

The configuration register defines the chip operating modes. It can be read and written by the I^2C MD.

Table 12: Configuration register bit meaning

*1 – does not impacting the calibration of the device (may be changed and the calibration remain valid)

*2 – does impact the calibration of the device (if changed the calibration is no longer valid)

8.2.2.2 Trimming register (0x93)

It can be read and written by the I^2C MD.

Table 13 Oscillator trim bit meaning

8.2.3. EEPROM

A 2kbit, organized as 256x8 EEPROM is built in the MIx90621. The EEPROM has a separate I²C address SA=0x50 and is used to store the calibration constants and the configuration of the device.

Table 14: EEPROM map

MLX90621

Detailed descriptions of some of the EEPROM addresses are described here after:

Table 15: C0…C7 EEPROM cell meaning

DF	DE	DD	DC	DB	DA	D ₉	D ₈	EEPROM cell meaning	
							TGC	- Thermal Gradien Coefficient	
						Offset scale	$[7:4]$ - Aiscale		
							$[3:0]$ - Biscale		
				V_{th} H	V_{th} L	- Vth0 of absolute temperatire sensor			
		K_{T1} H	K_{T1} L	$-K_{T1}$ of absolute temperature sensor					
K_{T2} H	K_{T2} L	- Kt2 of absolute temperatire sensor							

Table 17: DF…D8 EEPROM cell meaning

Table 18: E7…E0 EEPROM cell meaning

Table 19: F7…F0 EEPROM cell meaning

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8.3. POR

The Power On Reset (POR) is connected to the Vdd supply. The on-chip POR circuit provides an active level of the POR signal when the Vdd voltage rises above approximately 0.5V and holds the entire Mlx90621 in reset until the Vdd is higher than 2.4V. The device will start approximately 5ms after the POR release.

8.4. ESD

ESD, 4KV Human Body Model (please check with electrical specification)

9. **Communication protocol**

The device supports Fast Mode Plus I²C FM+ (IR array only up to 1MHz while the EEPROM can handle only up to 400 kHz) and will work in slave mode only.

The master device must provide the clock signal (SCL) for the communication. The data line SDA is bidirectional and is driven by the master or the slave depending on the command. The selection of the SDA occupant is done according to the I^2C specification. As the SDA is an open-drain IO, '0' is transmitted by forcing the line 'LOW' and a '1' just by releasing it. During data transfer, the data line could be changed only while SCL is low. Otherwise, it would be interpreted as a start/stop condition

9.1. Communication pins

There are two communication pins SCL and SDA. SCL is an input only for the MLX90621 while the SDA pin is a bidirectional one. The SDA line should be wired in an open-drain configuration.

Figure 17 Communication pin diagram

9.2. Low level communication protocol

9.2.1. Start / Stop condition

Each communication session is initiated by a START condition and ends with a STOP condition. A START condition is initiated by a HIGH to LOW transition of the SDA while a STOP is generated by a LOW to HIGH transition. Both changes must be done while the SCL is HIGH (see the figure)

Figure 18: Start / Stop conditions of I² C

9.2.2. Device addressing

The master is addressing the slave device by sending a 7-bit slave address after the START condition. The first seven bits are dedicated for the address and the 8^{th} is Read/Write (R/W) bit. This bit indicates the direction of the transfer:

- Read (HIGH) means that the master will read the data from the slave
- Write (LOW) means that the master will send data to the slave

Mlx90621 is responding to 2 different slave addresses:

Figure 19: I² C addresses

9.2.3. Acknowledge

During the 9th clock following every byte transfer the transmitter releases the SDA line. The receiver acknowledges (ACK) receiving the byte by pulling SDA line to low or does not acknowledge (NoACK) by letting the SDA 'HIGH'.

9.2.4. Low level communication operation

The low level operation communication is based on 8bits (1byte) transmissions. This includes start/stop event, acknowledgement and errors detection.

Figure 20: I² C communication

9.3. Device modes

The device can operate in following modes:

- Normal mode
- Step mode
- Power saving mode

9.3.1. Normal mode

In this mode the measurements are constantly running. Depending on the selected frame rate Fps in the configuration register, the data for IR pixels and Ta will be updated in the RAM each 1/Fps seconds. In this mode the external microcontroller has full access to the internal registers and memories of the device (both for 90670 and the EEPROM chip).

9.3.2. Step mode

This mode is foreseen for single measurements triggered by an external device (microcontroller). Entering this mode is possible by writing the appropriate code in the configuration register. A measurement is triggered by sending the command StartMeas (see 9.4.1). On detecting the command, the Mlx90621 will start the measurements immediately after the I^2C session is finished (STOP condition detected).

The measurement time is $\frac{1}{F_{ps}}$

While the Step mode measurement is ongoing all 'start new measurement in step mode' commands will be acknowledged but not executed. All other valid commands are executed accordingly.

A flag bit in Configuration register (bit 0x09) is dedicated in order to be able to check whenever the measurement is done.

Figure 21 Write configuration register (SA = 0x60, command LSByte = 0x01 command MSByte = 0x08)

9.3.3. Power saving mode

In this mode the device will be completely shut down and the current consumption will be minimized to less than 6µA. Entering this mode is initiated by writing '1' in the configuration register bit 7. Upon receiving it the device will shut down all electronics, including the internal oscillator. The chip will monitor the I^2C line. Each START condition will wake up the oscillator and the chip will receive and evaluate the slave address. If the address is 0x60 (address programmed in Mlx90621) the device will evaluate the whole command and will execute it. If not, the oscillator will be switched off again.

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16x4 IR array Datasheet

9.4. Communication to IR array

9.4.1. Start measurement command

Opcode – 0x01 (LSByte), 0x08 (MSByte).

This command is used to start measurement cycle in step mode.

Figure 22: Start measurement command structure

9.4.2. Read command

Opcode – 0x02.

The read command is used to read measurement, configuration and other data from the chip to the external master. The read command has the following parameters:

- Start address 8bits. Address in the chip address space (0 to 255). It is the address of the first word read.
- Address step 8bits. On every read word the next address is formed by adding the address step to the current address.
- Number of reads 8bits. Number of the words to be read.

Different combinations are possible in order to read all, one line, one column, one exact pixel of the IR or Ta sensors. They are summarized in the table below:

Table 20 RAM readout options

Figure 23: RAM readout command structure

9.4.3. Write configuration register command

Opcode – 0x03.

This command is used to set the configuration register (16bits) value – all configuration settings. Each data byte is transmitted in two stages:

- First stage \rightarrow Data byte 0x55
- Second stage \rightarrow Data byte

This way of transmitting the data is done in order to have a simple error check. The chip adds 0x55 to the first byte and compares the result with the second one. If both match the configuration register is updated.

Figure 24: Configuration register update command structure

9.4.4. Write trimming command

Opcode – 0x04.

This command is used to set the oscillator trimming oscillator trimming value.

This command is used to set the oscillator trimming register (16bits) value.

- Each data byte is transmitted in two stages:
	- First stage \rightarrow Data byte 0xAA
	- Second stage \rightarrow Data byte

This way of transmitting the data is done in order to have a simple error check. The chip adds 0xAA to the first byte and compares the result with the second one. If both match the oscillator trimming register is updated.

Figure 25*: Oscillator trimming register update command structure*

9.5. Communication to EEPROM

See datasheet of 24AA02. This can be found at https://www.melexis.com/en/product/mlx90621/far-infrared-sensor-array-high-speed-low-noise

10. **Performance Graphs**

10.1. Temperature accuracy of the MLX90621

All accuracy specifications apply under settled isothermal conditions only.

Furthermore, the accuracy is only valid if the object fills the FOV of the sensor completely.

Figure 26: Absolute temperature accuracy for the central four pixels

All accuracy specifications apply under settled isothermal conditions only.

NOTE:

- 1) The accuracy is specified for the four central pixels. The accuracy of the rest of the pixels is according to the uniformity statement
- 2) As a result of long term (years) drift there can be an additional measurement deviation of $\pm 3^{\circ}$ C for object temperatures around room temperature.

10.2. Noise performance and resolution

There are two bits in the configuration register that allow changing the resolution of the MLX90621 measurements. Increasing the resolution decreases the quantization noise and improves the overall noise performance. Measurement conditions for the noise are: To=Ta=25°C

NOTE: It is normal that the noise will decrease for high temperature and increase for lower temperatures

Figure 27: Central pixels noise

Figure 28: Corner pixels noise

The higher resolution limits the maximum object temperature range of the MLX90621.

Table 21 Maximum object temperature at different resolution settings

NOTE: If object temperature exceeds the maximum object temperature specified for the corresponding resolution, the MLX90621 may return invalid data due to measurements overflow.

10.3. Field Of View (FOV)

Figure 29: Field Of View measurement

The specified FOV is calculated for the wider direction, in this case for the 16 pixels. Angular alignment must be 5% of specified FOV and will be valid for both directions. For example for the 60° FOV in the wider direction will come with 16° in the shorter direction.

11. **Applications Information**

11.1. Use of the MLX90621 thermometer in I^2C configuration

Figure 30: MLX90621 I² C connection

As the MLX90621xxx is fully I^2C compatible it allows to have a system in which the MCU may be supplied with VDD=2.5…5V while the sensor it's self is supplied from separate supply VDD1=2.6V (or even left with no supply i.e. VDD=0V), **with the I² C connection running at supply voltage of the MCU.**

12. **Application Comments**

Significant **contamination** at the optical input side (sensor filter) might cause unknown additional filtering/distortion of the optical signal and therefore result in unspecified errors.

IR sensors are inherently susceptible to errors caused by **thermal gradients**. There are physical reasons for these phenomena and, in spite of the careful design of the MLX90621xxx, it is recommended not to subject the MLX90621 to heat transfer and especially transient conditions.

The MLX90621 is designed and calibrated to operate as a non-contact thermometer in **settled conditions**. Using the thermometer in a very different way will result in unknown results.

Capacitive loading on an I²C can degrade the communication. Some improvement is possible with use of current sources compared to resistors in pull-up circuitry. Further improvement is possible with specialized commercially available bus accelerators. With the MLX90621 additional improvement is possible by increasing the pull-up current (decreasing the pull-up resistor values). Input levels for I^2C compatible mode have higher overall tolerance than the I^2C specification, but the output low level is rather low even with the high-power I^2C specification for pull-up currents. Another option might be to go for a slower communication (clock speed), as the MLX90621 implements Schmidt triggers on its inputs in I²C compatible mode and is therefore not really sensitive to rise time of the bus (it is more likely the rise time to be an issue than the fall time, as far as the I^2C systems are open drain with pull-up).

Power dissipation within the package may affect performance in two ways: by heating the "ambient" sensitive element significantly beyond the actual ambient temperature, as well as by causing gradients over the package that will inherently cause thermal gradient over the cap

Power supply decoupling capacitor is needed as with most integrated circuits. MLX90621 is a mixed-signal device with sensors, small signal analog part, digital part and I/O circuitry. In order to keep the noise low power supply switching noise needs to be decoupled. High noise from external circuitry can also affect noise performance of the device. In many applications a 100nF SMD ceramic capacitor close to the Vdd and Vss pins would be a good choice. It should be noted that not only the trace to the Vdd pin needs to be short, but also the one to the Vss pin. Using MLX90621 with short pins improves the effect of the power supply decoupling.

Check www.melexis.com for most recent application notes about MLX90621.

13. **Standard information regarding manufacturability of Melexis products with different soldering processes**

Our products are classified and qualified regarding soldering technology, solderability and moisture sensitivity level according to following test methods:

Wave Soldering THD's (Through Hole Devices)

• EIA/JEDEC JESD22-B106 and EN60749-15 Resistance to soldering temperature for through-hole mounted devices

Iron Soldering THD's (Through Hole Devices)

• EN60749-15 Resistance to soldering temperature for through-hole mounted devices

Solderability THD's (Through Hole Devices)

• EIA/JEDEC JESD22-B102 and EN60749-21 Solderability

For all soldering technologies deviating from above mentioned standard conditions (regarding peak temperature, temperature gradient, temperature profile etc) additional classification and qualification tests have to be agreed upon with Melexis.

Melexis is contributing to global environmental conservation by promoting **lead free** solutions. For more information on qualifications of **RoHS** compliant products (RoHS = European directive on the Restriction Of the use of certain Hazardous Substances) please visit the quality page on our website: http://www.melexis.com/quality.aspx

The MLX90621 is RoHS compliant

14. **ESD Precautions**

Electronic semiconductor products are sensitive to Electro Static Discharge (ESD). Always observe Electro Static Discharge control procedures whenever handling semiconductor products.

15. **FAQ**

When I measure aluminum and plastic parts settled at the same conditions I get significant errors on aluminum. Why?

Different materials have different **emissivity**. A typical value for aluminum (roughly polished) is 0.18 and for plastics values of 0.84…0.95 are typical. IR thermometers use the radiation flux between the sensitive element in the sensor and the object of interest, given by the equation

$$
q = \varepsilon_1 * \alpha_1 * T_1^4 * \sigma * A_1 * F_{a-b} - \varepsilon_2 * T_2^4 * \sigma * A_2
$$

Where:

 ε_1 and ε_2 are the emissivity of the two objects

 α_1 is the absorptivity of the sensor (in this case),

 σ is the the Stefan-Boltzmann constant,

 A_1 and A_2 are the surface areas involved in the radiation heat transfer,

 F_{A-R} is the shape factor,

 T_1 and T_2 are known temperature of the sensor die (measured with specially integrated and calibrated element) and the object temperature that we need.

Note that the temperatures are all in Kelvin, heat exchange knows only physics.

When a body with low emissivity (such as aluminum) is involved in this heat transfer, the portion of the radiation incident to the sensor element that really comes from the object of interest decreases – and the reflected environmental IR emissions take place. (This is all for bodies with zero transparency in the IR band.) The IR thermometer is calibrated to stay within specified accuracy – but it has no way to separate the incoming IR radiation into real object and reflected environmental part. Therefore, measuring objects with low emissivity is a very sophisticated issue and infra-red measurements of such materials are a specialized field.

What can be done to solve that problem? Look at paintings – for example, oil paints are likely to have emissivity of 0.85…0.95 – but keep in mind that the stability of the paint emissivity has inevitable impact on measurements. It is also a good point to keep in mind that not everything that looks black is "black" also for IR. For example, even heavily oxidized aluminum has still emissivity as low as 0.30.

How high is enough? Not an easy question – but, in all cases the closer you need to get to the real object temperature the higher the needed emissivity will be, of course.

With the real life emissivity values the environmental IR comes into play via the reflectivity of the object (the sum of Emissivity, Reflectivity and Absorptivity gives 1.00 for any material). The larger the difference between environmental and object temperature is at given reflectivity (*with an opaque for IR material reflectivity equals 1.00 minus emissivity*) the bigger errors it produces.

After I put the MLX90621 in the dashboard I start getting errors larger than specified in spite that the module was working properly before that. Why?

Any object present in the FOV of the module provides IR signal. It is actually possible to introduce error in the measurements if the module is attached to the dashboard with an opening that enters the FOV. In that case portion of the dashboard opening will introduce IR signal in conjunction with constraining the effective FOV and thus compromising specified accuracy. Relevant opening that takes in account the FOV is a must for accurate

measurements. Note that the basic FOV specification takes 50% of IR signal as threshold (in order to define the area, where the measurements are relevant), while the entire FOV at lower level is capable of introducing lateral IR signal under many conditions.

When a hot (cold) air stream hits my MLX90621 some error adds to the measured temperature I read. What is it?

IR sensors are inherently sensitive to difference in temperatures between the sensitive element and everything incident to that element. As a matter of fact, this element is not the sensor package, but the sensor die inside. Therefore, a thermal gradient over the sensor package will inevitably result in additional IR flux between the sensor package and the sensor die. This is real optical signal that cannot be segregated from the target IR signal and will add errors to the measured temperature.

Thermal gradients with impact of that kind are likely to appear during transient conditions. The sensor used is developed with care about sensitivity to this kind of lateral phenomena, but their nature demands some care when choosing place to use the MLX90621 in order to make them negligible.

I measure human body temperature and I often get measurements that significantly differ from the +37°C I expect.

IR measurements are true surface temperature measurements. In many applications this means that the actual temperature measured by an IR thermometer will be temperature of the clothing and not the skin temperature. Emissivity (explained first in this section) is another issue with clothes that has to be considered.

There is also the simple chance that the measured temperature is adequate – for example, in a cold winter human hand can appear at temperatures not too close to the well-known +37°C.

16. **Mechanical specification**

16.1. Package outline

The height of the can depends on the selected FOV of the array

Figure 31 Overview of the different device FOV options

Figure 32 Mechanical drawing of Wide (120x25) FOV device (MLX90621BAA)

Figure 33 Mechanical drawing of Wide (60x16) FOV device (MLX90621BAB)

Figure 34 Mechanical drawing of Medium (40x10) FOV device (MLX90621BAD)

16.2. Part marking

The MLX90621 is laser marked with 10 symbols. The first is a 1, the next 3 letters indicate the version (BAA, BAB or BAD) and the remaining 7 indicate the lot number.

17. **References**

[1] 1^2 C-bus specification and user manual Rev. 03 – 19 June 2007

http://www.nxp.com/documents/user_manual/UM10204.pdf

18. **Disclaimer**

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Europe, Africa, Asia: America: Phone: +32 1367 0495 Phone: +1 248 306 5400 E-mail: sales_europe@melexis.com E-mail: sales_usa@melexis.com

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