



## ULTRALOW-NOISE, HIGH-PSRR, FAST, RF, 250-mA LOW-DROPOUT LINEAR REGULATORS

Check for Samples: TPS794xx-Q1

#### **FEATURES**

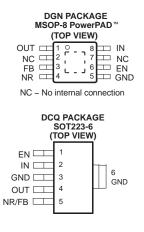
- Qualified for Automotive Applications
- AEC-Q100 Qualified with the Following Results:
  - Device Temperature Grade 1: –40°C to 125°C Ambient Operating Temperature Range
  - Device HBM ESD Classification Level H2
  - Device CDM ESD Classification Level C2
- 250-mA Low-Dropout Regulator With Enable
- Available in Fixed and Adjustable (1.2 V to 5.5 V) Versions
- High PSRR (60 dB at 10 kHz)
- Ultralow Noise (32 μVrms, TPS79428-Q1)
- Fast Start-Up Time (50 μs)
- Stable With a 2.2-μF Ceramic Capacitor
- Excellent Load/Line Transient Response
- Very Low Dropout Voltage (155 mV at Full Load)
- Available in MSOP-8 and SOT-223-6 Packages

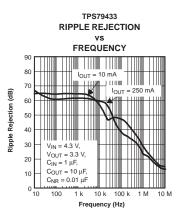
#### **APPLICATIONS**

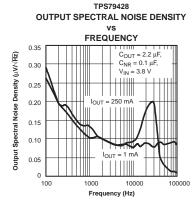
- RF: VCOs, Receivers, ADCs
- Audio
- Bluetooth<sup>®</sup>, Wireless LAN
- Cellular and Cordless Telephones
- · Handheld Organizers, PDAs

#### **DESCRIPTION**

The TPS794xx-Q1 family of low-dropout (LDO) linear voltage regulators features high power-supply rejection ratio (PSRR), ultralow-noise, fast start-up, and excellent line and load transient responses in small outline, MSOP-8 PowerPAD™ and SOT-223-6 packages. Each device in the family is stable with a small 2.2-µF ceramic capacitor on the output. The family uses an advanced, proprietary BiCMOS fabrication process to yield extremely low dropout voltages (for example, 155 mV at 250 mA). Each device achieves fast start-up times (approximately 50 μs with a 0.001-μF bypass capacitor) while consuming low quiescent current (170 µA typical). Moreover, when the device is placed in standby mode, the supply current is reduced to less than 1 μA. The TPS79428-Q1 exhibits approximately 32 μV<sub>RMS</sub> of output voltage noise at 2.8 V output with a 0.1-µF bypass capacitor. Applications with analog components that are noise-sensitive, such as portable RF electronics, benefit from the high PSRR and low noise features as well as the fast response time.







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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### **ABSOLUTE MAXIMUM RATINGS**

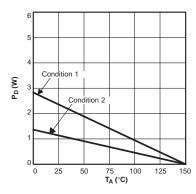
over operating temperature range unless otherwise noted(1)

	VALUE
V <sub>IN</sub> range	-0.3 V to 6 V
V <sub>EN</sub> range	-0.3 V to V <sub>IN</sub> + 0.3 V
V <sub>OUT</sub> range	-0.3 V to 6 V
Peak output current	Internally limited
ESD rating, HBM	2 kV
ESD rating, CDM <sup>(2)</sup>	250 V
Continuous total power dissipation	See Dissipation Ratings Table
Junction temperature range, T <sub>J</sub>	-40°C to 150°C
Storage temperature range, T <sub>stg</sub>	-65°C to 150°C

- (1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) ESD CDM rating is 500 V for all pins except for pin 1.

#### PACKAGE DISSIPATION RATINGS

PACKAGE	AIR FLOW (CFM)	R <sub>θJC</sub> (°C/W)	R <sub>θJA</sub> (°C/W)	T <sub>A</sub> ≤ 25°C POWER RATING	T <sub>A</sub> = 70°C POWER RATING	T <sub>A</sub> = 85°C POWER RATING
	0	8.47	55.09	2.27 W	1.45 W	1.18 W
DGN	150	8.21	49.97	2.50 W	1.60 W	1.30 W
	250	8.20	48.10	2.60 W	1.66 W	1.35 W



CONDITIONS	PACKAGE	PCB AREA	θЈА
1	SOT223	4in <sup>2</sup> Top Side Only	53°C/W
2	SOT223	0.5in <sup>2</sup> Top Side Only	110°C/W

Figure 1. SOT-223 Power Dissipation

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#### **ELECTRICAL CHARACTERISTICS**

Over recommended operating temperature range ( $T_A = -40^{\circ}C$  to 125°C),  $V_{EN} = V_{IN}$ ,  $V_{IN} = V_{OUT(nom)} + 1$   $V^{(1)}$ ,  $I_{OUT} = 1$  mA,  $C_{OUT} = 10$   $\mu$ F,  $C_{NR} = 0.01$   $\mu$ F, unless otherwise noted. Typical values are at 25°C.

	PARAMETER		TEST CO	NDITIONS	MIN	TYP	MAX	UNIT	
Input voltage, V <sub>IN</sub> <sup>(1)</sup>				2.7		5.5	V		
Continuous output current, I <sub>OUT</sub>					0		250	mA	
	Output voltage range	TPS79401-Q1	1-Q1		1.225		5.5 – V <sub>DO</sub>	V	
Output voltage		TPS79401-Q1 <sup>(2)</sup>	$0 \mu A \le I_{OUT} \le 250 \text{ mA}, V$	0.97(V <sub>OUT</sub> )	V <sub>OUT</sub>	1.03(V <sub>OUT</sub> )	V		
voltage	Accuracy	Fixed V <sub>OUT</sub>	$0 \mu A \le I_{OUT} \le 250 \text{ mA, V}$	$V_{OUT} + 1 \text{ V} \le V_{IN} \le 5.5$	-3		3	%	
Output volta	ge line regulation (ΔV <sub>OUT</sub>	%/ΔV <sub>IN</sub> ) <sup>(1)</sup>	V <sub>OUT</sub> + 1 V ≤ V <sub>IN</sub> ≤ 5.5 V	,		0.05	0.12	%/V	
Load regulat	ion (ΔV <sub>OUT</sub> %/ΔI <sub>OUT</sub> )		0 μA ≤ I <sub>OUT</sub> ≤ 250 mA			10		mV	
	(0)	TPS79428-Q1	I <sub>OUT</sub> = 250 mA			155	210		
Dropout volta		TPS79430-Q1	I <sub>OUT</sub> = 250 mA			155	210	mV	
$V_{IN} = V_{OUT(nom)} - 0.1 \text{ V}$		TPS79433-Q1	I <sub>OUT</sub> = 250 mA		145	200			
Output curre	nt limit		V <sub>OUT</sub> = 0 V			925		mA	
Ground pin o	current		0 μA ≤ I <sub>OUT</sub> ≤ 250 mA		170	220	μA		
Shutdown current <sup>(4)</sup>			V <sub>EN</sub> = 0 V, 2.7 V ≤ V <sub>IN</sub> ≤		0.07	1	μA		
FB pin current			V <sub>FB</sub> = 1.225 V			1	μA		
			f = 100 Hz, I <sub>OUT</sub> = 250 m	nA		65			
Power-suppl	y ripple rejection	TPS79428-Q1	f = 10 kHz, I <sub>OUT</sub> = 250 mA			60		dB	
			f = 100 kHz, I <sub>OUT</sub> = 250	f = 100 kHz, I <sub>OUT</sub> = 250 mA			40		
				C <sub>NR</sub> = 0.001 μF	55				
Output palage	voltage	TD070400 04	BW = 100 Hz to 100	C <sub>NR</sub> = 0.0047 µF		36		/	
Output noise	voltage	TPS79428-Q1	kHz, I <sub>OUT</sub> = 250 mA	C <sub>NR</sub> = 0.01 µF		33		$\mu V_{RMS}$	
				C <sub>NR</sub> = 0.1 μF	32			1	
				C <sub>NR</sub> = 0.001 µF		50			
Time, start-u	р	TPS79428-Q1	$R_L = 14 \Omega$ , $C_{OUT} = 1 \mu F$	$C_{NR} = 0.0047 \ \mu F$		70		μs	
				C <sub>NR</sub> = 0.01 µF		100			
High-level enable input voltage			2.7 V ≤ V <sub>IN</sub> ≤ 5.5 V	1.7		$V_{IN}$	V		
Low-level enable input voltage			2.7 V ≤ V <sub>IN</sub> ≤ 5.5 V	0		0.7	V		
EN pin current			V <sub>EN</sub> = 0	-1		1	μA		
UVLO threshold			V <sub>CC</sub> rising	2.25		2.65	V		
UVLO hysteresis						100		mV	

- Minimum  $V_{\text{IN}}$  is 2.7 V or  $V_{\text{OUT}} + V_{\text{DO}}$ , whichever is greater. Tolerance of external resistors not included in this specification.

- Dropout is not measured for the TPS79418-Q1 and TPS79425-Q1 because minimum  $V_{\text{IN}} = 2.7 \text{ V}$ . For adjustable versions, this applies only after  $V_{\text{IN}}$  is applied; then  $V_{\text{EN}}$  transitions high to low.

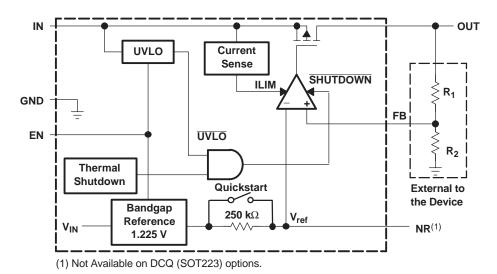


Figure 2. FUNCTIONAL BLOCK DIAGRAM—ADJUSTABLE VERSION

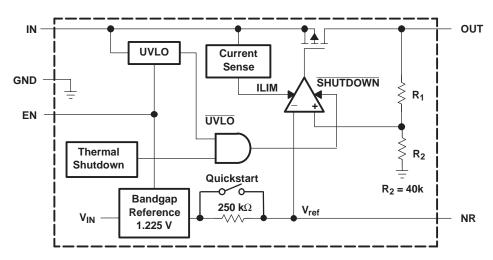


Figure 3. FUNCTIONAL BLOCK DIAGRAM—FIXED VERSION

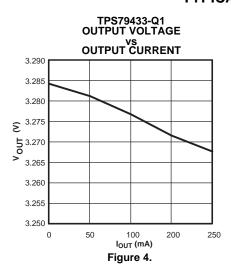
#### **Pin Functions**

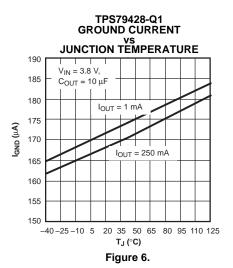
	PIN								
NAME	DGN (MSOP)	DCQ (SOT-223)	DESCRIPTION						
NR	4	5	Connecting an external capacitor to this pin bypasses noise generated by the internal bandgap, which improves power-supply rejection and reduces output noise.						
EN	6	1	The EN terminal is an input that enables or shuts down the device. When EN is a logic high, the device is enabled. When the device is a logic low, the device is in shutdown mode.						
FB	3	5	Feedback input voltage for the adjustable device.						
GND	5, PAD	3, 6	Regulator ground						
IN	8	2	Unregulated input to the device.						
NC	2, 7		No internal connection.						
OUT	1	4	Regulator output						

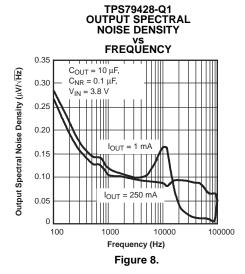
PRODUCT PREVIEW

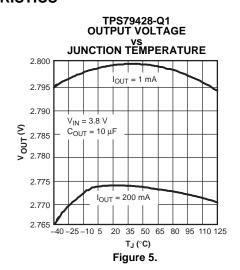


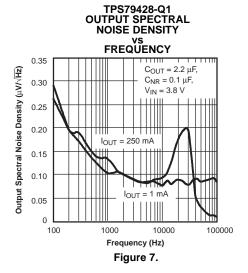
#### TYPICAL CHARACTERISTICS

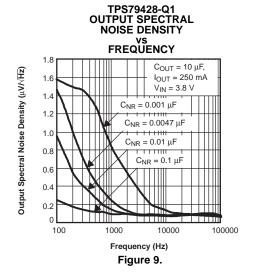




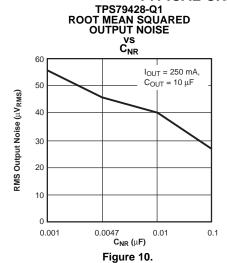


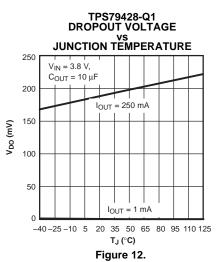


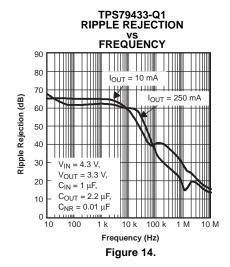


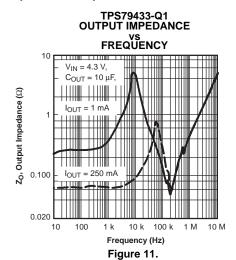


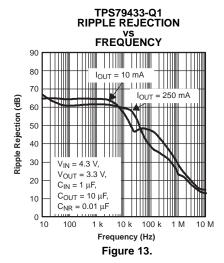
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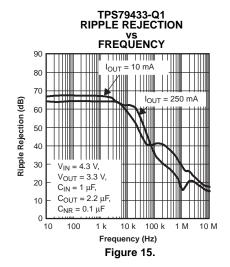














#### TYPICAL CHARACTERISTICS (continued)

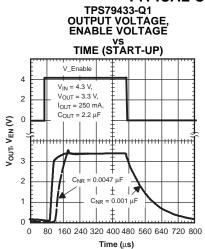


Figure 16.

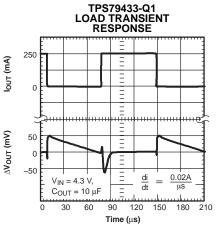
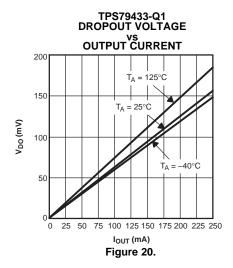


Figure 18.



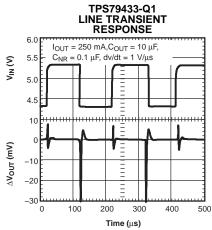
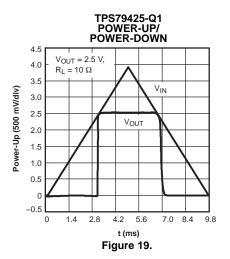


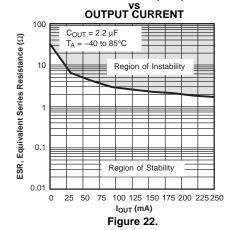
Figure 17.



TPS79401-Q1 DROPOUT VOLTAGE INPUT VOLTAGE 250 T<sub>A</sub> = 25°C 200 150 V<sub>DO</sub> (mV) 100  $T_A = -40^{\circ}C$ 50  $C_{OUT} = 10 \mu F$  $C_{NR} = 0.01 \mu F$  $I_{OUT} = 250 \text{ mA}$ 3.0 4.5 4.0 5.0 V<sub>IN</sub> (V) Figure 21.

## TYPICAL CHARACTERISTICS (continued)

## TPS79428-Q1 TYPICAL REGIONS OF STABILITY EQUIVALENT SERIES RESISTANCE (ESR)



# TPS79428-Q1 TYPICAL REGIONS OF STABILITY EQUIVALENT SERIES RESISTANCE (ESR)

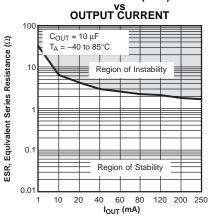


Figure 23.



#### **APPLICATION INFORMATION**

The TPS794xx-Q1 family of low-dropout (LDO) regulators is optimized for use in noise-sensitive equipment. The device features extremely low dropout voltages, high PSRR, ultralow output noise, low quiescent current (265 μA typically), and an enable input to reduce supply currents to less than 1 μA when the regulator is turned off.

A typical application circuit is shown in Figure 24.

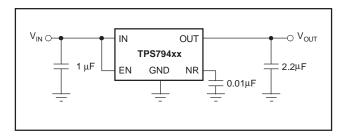


Figure 24. Typical Application Circuit

#### **EXTERNAL CAPACITOR REQUIREMENTS**

A 1-µF or larger ceramic input bypass capacitor, connected between IN and GND and located close to the TPS794xx-Q1, is required for stability and improves transient response, noise rejection, and ripple rejection. A higher-value input capacitor may be necessary if large, fast-rise-time load transients are anticipated and the device is located several inches from the power source.

Like most low-dropout regulators, the TPS794xx-Q1 requires an output capacitor connected between OUT and GND to stabilize the internal control loop. The minimum recommended capacitance is 1  $\mu$ F. Any 1  $\mu$ F or larger ceramic capacitor is suitable.

The internal voltage reference is a key source of noise in an LDO regulator. The TPS794xx-Q1 has an NR pin which is connected to the voltage reference through a 250-k $\Omega$  internal resistor. The 250-k $\Omega$  internal resistor, in conjunction with an external bypass capacitor connected to the NR pin, creates a low-pass filter to reduce the voltage reference noise and, therefore, the noise at the regulator output. In order for the regulator to operate properly, the current flow out of the NR pin must be at a minimum, because any leakage current creates an IR drop across the internal resistor, thus creating an output error. Therefore, the bypass capacitor must have minimal leakage current. The bypass capacitor should be no more than 0.1- $\mu$ F in order to ensure that it is fully charged during the quickstart time provided by the internal switch shown in the Functional Block Diagram.

For example, the TPS79430-Q1 exhibits only 33  $\mu V_{RMS}$  of output voltage noise using a 0.1- $\mu F$  ceramic bypass capacitor and a 10- $\mu F$  ceramic output capacitor. Note that the output starts up slower as the bypass capacitance increases because of the RC time constant at the bypass pin that is created by the internal 250- $k\Omega$  resistor and external capacitor.

#### BOARD LAYOUT RECOMMENDATION TO IMPROVE PSRR AND NOISE PERFORMANCE

To improve ac measurements such as PSRR, output noise, and transient response, it is recommended that the board be designed with separate ground planes for  $V_{IN}$  and  $V_{OUT}$ , with each ground plane connected only at the ground pin of the device. In addition, the ground connection for the bypass capacitor should connect directly to the ground pin of the device.

#### **REGULATOR MOUNTING**

The tab of the SOT-223-6 package is electrically connected to ground. For best thermal performance, the tab of the surface-mount version should be soldered directly to a circuit-board copper area. Increasing the copper area improves heat dissipation.

Solder pad footprint recommendations for the devices are presented in Application Report SBFA015, Solder Pad Recommendations for Surface-Mount Devices, available from the TI website (www.ti.com).

#### PROGRAMMING THE TPS79401-Q1 ADJUSTABLE LDO REGULATOR

The output voltage of the TPS79401-Q1 adjustable regulator is programmed using an external resistor divider as shown in Figure 25. The output voltage is calculated using Equation 1:

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R_1}{R_2}\right) \tag{1}$$

where:

V<sub>REF</sub> = 1.2246 V typ (the internal reference voltage)

Resistors  $R_1$  and  $R_2$  should be chosen for approximately 40- $\mu$ A divider current. Lower value resistors can be used for improved noise performance, but the device wastes more power. Higher values should be avoided, as leakage current at FB increases the output voltage error.

The recommended design procedure is to choose  $R_2 = 30.1 \text{ k}\Omega$  to set the divider current at 40  $\mu$ A,  $C_1 = 15 \text{ pF}$  for stability, and then calculate  $R_1$  using Equation 2:

$$R_1 = \left(\frac{V_{\text{OUT}}}{V_{\text{REF}}} - 1\right) \times R_2 \tag{2}$$

In order to improve the stability of the adjustable version, it is suggested that a small compensation capacitor be placed between OUT and FB.

The approximate value of this capacitor can be calculated as Equation 3:

$$C_1 = \frac{(3 \times 10^{-7}) \times (R_1 + R_2)}{(R_1 \times R_2)}$$
(3)

The suggested value of this capacitor for several resistor ratios is shown in the table within Figure 25. If this capacitor is not used (such as in a unity-gain configuration), then the minimum recommended output capacitor is  $2.2 \, \mu F$  instead of  $1 \, \mu F$ .

#### REGULATOR PROTECTION

The TPS794xx-Q1 PMOS-pass transistor has a built-in back diode that conducts reverse current when the input voltage drops below the output voltage (for example, during power down). Current is conducted from the output to the input and is not internally limited. If extended reverse voltage operation is anticipated, external limiting might be appropriate.

The TPS794xx-Q1 features internal current limiting and thermal protection. During normal operation, the TPS794xx-Q1 limits output current to approximately 2.8 A. When current limiting engages, the output voltage scales back linearly until the overcurrent condition ends. While current limiting is designed to prevent gross device failure, care should be taken not to exceed the power dissipation ratings of the package. If the temperature of the device exceeds approximately 165°C, thermal-protection circuitry shuts it down. Once the device cools down to below approximately 140°C, regulator operation resumes.

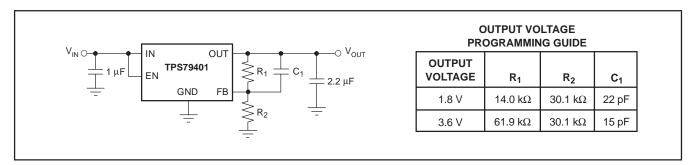


Figure 25. TPS79401-Q1 Adjustable LDO Regulator Programming

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#### THERMAL INFORMATION

The amount of heat that an LDO linear regulator generates is directly proportional to the amount of power it dissipates during operation. All integrated circuits have a maximum allowable junction temperature ( $T_J$ max) above which normal operation is not assured. A system designer must design the operating environment so that the operating junction temperature ( $T_J$ ) does not exceed the maximum junction temperature ( $T_J$ max). The two main environmental variables that a designer can use to improve thermal performance are air flow and external heatsinks. The purpose of this information is to aid the designer in determining the proper operating environment for a linear regulator that is operating at a specific power level.

In general, the maximum expected power (P<sub>D</sub>max) consumed by a linear regulator is computed as shown in Equation 4:

$$P_{D} \max = (V_{IN(avg)} - V_{OUT(avg)}) \times I_{OUT(avg)} + V_{I(avg)} \times I_{Q}$$
(4)

#### where:

- V<sub>IN(avg)</sub> is the average input voltage
- V<sub>OUT(avq)</sub> is the average output voltage
- I<sub>OUT(avg)</sub> is the average output current
- I<sub>O</sub> is the quiescent current

For most TI LDO regulators, the quiescent current is insignificant compared to the average output current; therefore, the term  $V_{IN(avg)}$  x  $I_Q$  can be neglected. The operating junction temperature is computed by adding the ambient temperature ( $T_A$ ) and the increase in temperature due to the regulator's power dissipation. The temperature rise is computed by multiplying the maximum expected power dissipation by the sum of the thermal resistances between the junction and the case ( $R_{\Theta JC}$ ), the case to heatsink ( $R_{\Theta CS}$ ), and the heatsink to ambient ( $R_{\Theta SA}$ ). Thermal resistances are measures of how effectively an object dissipates heat. Typically, the larger the device, the more surface area available for power dissipation and the lower the object's thermal resistance.

Figure 26 illustrates these thermal resistances for a SOT-223 package mounted in a JEDEC low-K board.

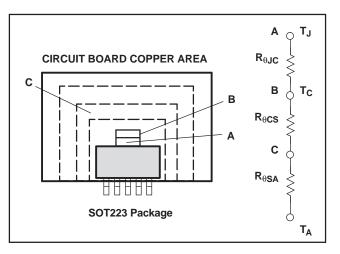


Figure 26. Thermal Resistances

Equation 5 summarizes the computation:

$$T_{J} = T_{A} + P_{D} \max \times (R_{\theta JC} + R_{\theta CS} + R_{\theta SA})$$
 (5)

The  $R_{\Theta JC}$  is specific to each regulator as determined by its package, lead frame, and die size provided in the regulator's data sheet. The  $R_{\Theta SA}$  is a function of the type and size of heatsink. For example, *black body radiator* type heatsinks can have  $R_{\Theta CS}$  values ranging from 5°C/W for very large heatsinks to 50°C/W for very small heatsinks. The  $R_{\Theta CS}$  is a function of how the package is attached to the heatsink. For example, if a thermal compound is used to attach a heatsink to a SOT-223 package,  $R_{\Theta CS}$  of 1°C/W is reasonable.

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Product Folder Links: *TPS794xx-Q1* 

Even if no external black body radiator type heatsink is attached to the package, the board on which the regulator is mounted provides some heatsinking through the pin solder connections. Some packages, like the DDPAK and SOT-223 packages, use a copper plane underneath the package or the circuit board ground plane for additional heatsinking to improve their thermal performance. Computer-aided thermal modeling can be used to compute very accurate approximations of an integrated circuit's thermal performance in different operating environments (for example, different types of circuit boards, different types and sizes of heatsinks, different air flows, and so forth). Using these models, the three thermal resistances can be combined into one thermal resistance between junction and ambient ( $R_{\Theta JA}$ ). This  $R_{\Theta JA}$  is valid only for the specific operating environment used in the computer model.

Equation 5 simplifies into Equation 6:

$$T_{J} = T_{A} + P_{D} \max \times R_{\theta J A}$$
 (6)

Rearranging Equation 6 gives Equation 7:

$$R_{\theta JA} = \frac{T_J - T_A}{P_D \max} \tag{7}$$

Using Equation 6 and the computer model generated curves shown in Figure 27, a designer can guickly compute the required heatsink thermal resistance/board area for a given ambient temperature, power dissipation, and operating environment.

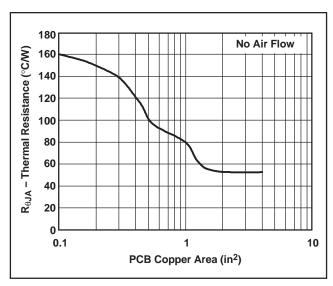


Figure 27. SOT-223 Thermal Resistance vs PCB Copper Area

#### **SOT-223 POWER DISSIPATION**

The SOT-223 package provides an effective means of managing power dissipation in surface-mount applications. The SOT-223 package dimensions are provided in the Mechanical Data section at the end of the data sheet. The addition of a copper plane directly underneath the SOT-223 package enhances the thermal performance of the package.

To illustrate, the TPS79425-Q1 in a SOT-223 package was chosen. For this example, the average input voltage is 3.3 V, the output voltage is 2.5 V, the average output current is 1 A, the ambient temperature 55°C, no air flow is present, and the operating environment is the same as documented below. Neglecting the guiescent current, the maximum average power is Equation 8:

$$P_D \max = (3.3 - 2.5)V \times 1A = 800 \text{mW}$$
 (8)

Substituting T<sub>J</sub>max for T<sub>J</sub> into Equation 4 gives Equation 9:

$$R_{\theta JA} \max = (125 - 55)^{\circ} C/800 \text{ mW} = 87.5^{\circ} C/W$$
 (9)



From Figure 27,  $R_{\theta JA}$  vs PCB Copper Area, the ground plane needs to be 0.55 in<sup>2</sup> for the part to dissipate 800 mW. The operating environment used to construct Figure 27 consisted of a board with 1 oz. copper planes. The package is soldered to a 1 oz. copper pad on the top of the board. The pad is tied through thermal vias to the 1 oz. ground plane.

From the data in Figure 27 and rearranging Equation 6, the maximum power dissipation for a different ground plane area and a specific ambient temperature can be computed, as shown in Figure 28.

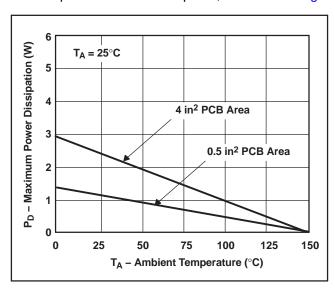


Figure 28. SOT-223 Maximum Power Dissipation vs Ambient Temperature



#### PACKAGE OPTION ADDENDUM

30-Apr-2013

#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	_	Pins	Package	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Top-Side Markings		Samples
	(1)		Drawing		Qty	(2)		(3)			(4)	
TPS79433QDCQRQ1	PREVIEW	SOT-223	DCQ	6	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR	-40 to 125	79433Q		

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

**Pb-Free** (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free** (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

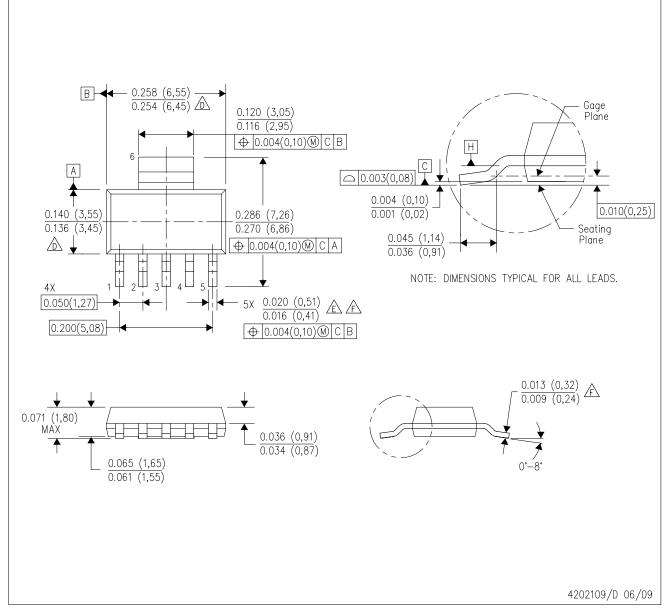
(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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### DCQ (R-PDSO-G6)

#### PLASTIC SMALL-OUTLINE



NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. Controlling dimension in inches.

Body length and width dimensions are determined at the outermost extremes of the plastic body exclusive of mold flash, tie bar burrs, gate burrs, and interlead flash, but including any mismatch between the top and the bottom of the plastic body.

Lead width dimension does not include dambar protrusion.

- Lead width and thickness dimensions apply to solder plated leads.
  - G. Interlead flash allow 0.008 inch max.
  - H. Gate burr/protrusion max. 0.006 inch.
  - I. Datums A and B are to be determined at Datum H.



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