

## **Fully Integrated PMIC for Safety-Related Systems**

**with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

### **FEATURES AND BENEFITS DESCRIPTION**

- A<sup>2</sup>-SIL™ product—device features for safety-critical systems
- Automotive AEC-Q100 qualified
- Wide input voltage range, 3.8 to 36  $V<sub>IN</sub>$  operating range,  $40 V_{\text{IN}}$  maximum
- 2.2 MHz buck or buck/boost pre-regulator (VREG: 5.35 V)
- Four internal linear regulators with foldback short-circuit protection
	- $\Box$  VUC: selectable output (3.3 V / 5.0 V) regulator for microcontroller
	- □ V5C: 5 V general purpose LDO regulator
	- □ V5P1 and V5P2: two LDO regulators (track VUC voltage) with short-to-battery protection for remote sensors
- Q&A Watchdog and Window Watchdog timer
- Floating gate drivers with charge pump for external isolator NFET control
- Control and diagnostic reporting through a serial peripheral interface (SPI)
- Logic enable input (ENB) for microprocessor control
- Ignition enable input (ENBAT)
- Frequency dithering and controlled slew rate help reduce EMI/EMC
- Undervoltage protection for all output rails
- Thermal shutdown protection
- $-40^{\circ}$ C to 150°C junction temperature range

### **APPLICATIONS**

- Provides system power for (microcontroller/DSP, CAN, sensors, etc.) and high current isolation FET gate driver in automotive control modules, such as:
	- □ Electronic power steering (EPS)
	- □ Advanced braking systems (ABS)
	- $\Box$  Other automotive applications

## **PACKAGE: 38-Pin eTSSOP (suffix LV)**



The ARG82801-1 is a power management IC that integrates a buck or buck/boost pre-regulator, four LDOs, and four floating gate drivers. The pre-regulator uses a buck or buck/boost topology to efficiently convert automotive battery voltages into a tightly regulated intermediate voltage complete with control, diagnostics, and protections.

The output of the pre-regulator supplies a 3.3 V or 5.0 V selectable 350 mA linear regulator, a  $5 \text{ V}/115 \text{ mA}$  linear regulator, and two 120 mA protected linear regulators which track VUC output. Designed to supply power for microprocessors, sensors, and CAN transceivers, the ARG82801-1 is ideal for underhood applications.

The independent floating gate drivers have the capability of controlling N-channel MOSFETs through SPI. These MOSFETs can be configured as phase or battery isolation devices in high current motor applications. An integrated charge pump allows the driver outputs to maintain the power MOSFETs in the on state over the full supply range with high phase-voltage slew rates.

Enable inputs to the ARG82801-1 include a logic level (ENB) and a high voltage (ENBAT). The ARG82801-1 also provides flexibility with disable function of the individual output rails through a serial peripheral interface (SPI).

Diagnostic outputs from the ARG82801-1 include a power-onreset output (NPOR) and a fault flag output (FFn) to alert the microprocessor that a fault has occurred. The microprocessor can read fault status through SPI. Dual bandgaps, one for regulation and one for fault checking, improve safety coverage and fault detection of the ARG82801-1.

The ARG82801-1 contains two types of watchdog functions: Q&A and Window Watchdog timer. The watchdog timer is activated once it receives a valid SPI command from a processor. The watchdog can be put into flash mode or be reset via secure SPI commands.

The ARG82801-1 is supplied in a low-profile (1.2 mm maximum height) 38-lead eTSSOP package (suffix "LV") with exposed power pad.



**ARG82801-1 Simplified Block Diagram** 



#### **SELECTION GUIDE**





[1] Contact Allegro for additional packing options.

#### **ABSOLUTE MAXIMUM RATINGS [2]**



<sup>[2]</sup> Stresses beyond those listed in this table may cause permanent damage to the device. The absolute maximum ratings are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the Electrical Characteristics table is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

[3] The higher ENBAT ratings (-13 V and 40 V) are measured at node "A" in the following circuit configuration:





**THERMAL CHARACTERISTICS:** May require derating at maximum conditions; see application information



[4] Additional thermal information available on the Allegro website.



### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

### **Table of Contents**







### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **FUNCTIONAL BLOCK DIAGRAM**





Allegro MicroSystems 955 Perimeter Road Manchester, NH 03103-3353 U.S.A. www.allegromicro.com

#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **Terminal List Table**



#### **Package LV, 38-Pin eTSSOP Pinout Diagram**





#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **ELECTRICAL CHARACTERISTICS [1]: Valid at 3.8 V [4] ≤ VVIN ≤ 36 V, –40°C ≤ T<sup>J</sup> ≤ 150°C, VENB = High or VENBAT = High,**  unless otherwise specified



[1] For input and output current specifications, negative current is defined as coming out of the node or pin (sourcing), positive current is defined as going into the node or pin (sinking).

<sup>[2]</sup> Ensured by design and characterization, not production tested.

[3] Specifications at 25°C or 85°C are guaranteed by design and characterization, not production tested.

[4] The lowest operating voltage is only valid if the conditions V<sub>VIN</sub> > V<sub>VIN(START)</sub> and V<sub>VCP</sub> – V<sub>VIN</sub> > V<sub>VCP(UV,H)</sub> and V<sub>VREG</sub> in regulating are satisfied before V<sub>VIN</sub> is reduced.



#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **ELECTRICAL CHARACTERISTICS (continued) [1]: Valid at 3.8 V [4] ≤ VVIN ≤ 36 V, –40°C ≤ T<sup>J</sup> ≤ 150°C, VENB = High or**   $V_{ENBAT}$  = High, unless otherwise specified



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#### **ELECTRICAL CHARACTERISTICS (continued) [1]: Valid at 3.8 V [4] ≤ VVIN ≤ 36 V, –40°C ≤ T<sup>J</sup> ≤ 150°C, VENB = High or**   $V_{ENBAT}$  = High, unless otherwise specified



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 $X =$  do not exceed Watchdog Config timeout; Z = high-impedance (tri-state)

![](_page_12_Picture_10.jpeg)

#### **ELECTRICAL CHARACTERISTICS (continued) [1]: Valid at 3.8 V [4] ≤ VVIN ≤ 36 V, –40°C ≤ T<sup>J</sup> ≤ 150°C, VENB = High or**   $V_{ENBAT}$  = High, unless otherwise specified

![](_page_13_Picture_367.jpeg)

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![](_page_13_Picture_8.jpeg)

#### **ELECTRICAL CHARACTERISTICS (continued) [1]: Valid at 3.8 V [4] ≤ VVIN ≤ 36 V, –40°C ≤ T<sup>J</sup> ≤ 150°C, VENB = High or**   $V_{ENBAT}$  = High, unless otherwise specified

![](_page_14_Picture_210.jpeg)

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![](_page_14_Picture_8.jpeg)

![](_page_15_Picture_173.jpeg)

#### **Table 1: Startup and Shutdown Logic (signal names consistent with Block Diagram)**

**X** = DON'T CARE

**EN** = ENBAT + ENB  $MPOR = VCC_UV + VCPX_UV + BG1_UV + BG2_UV + TSD + D1<sub>MISSING</sub> (latched) + I<sub>LIM(LX)</sub> (latched)$ 

![](_page_15_Picture_6.jpeg)

![](_page_16_Figure_2.jpeg)

**Figure 2: Startup Timing Diagram**

![](_page_16_Picture_4.jpeg)

![](_page_17_Figure_2.jpeg)

All outputs start to decay  $t_{d(EN)}$  seconds after ENB and ENBAT are low.

Time for outputs to drop to zero,  $t_{\text{OUT(FALL)}}$ , various for each output and depends on load current and capacitance. NPOR falls when VUC reaches its UV point.

#### **Figure 3: Shutdown Timing Diagram**

![](_page_17_Picture_6.jpeg)

#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

![](_page_18_Figure_2.jpeg)

**TIMING DIAGRAMS (not to scale)** 

\* = internal signal/threshold, + is for "or"

![](_page_18_Figure_5.jpeg)

![](_page_18_Figure_6.jpeg)

**Figure 5: Hiccup Mode Operation with VREG Overloaded (RLOAD ≈ 0.5 Ω)**

![](_page_18_Picture_8.jpeg)

#### **Table 2: Summary of Fault Mode Operation**

![](_page_19_Picture_1021.jpeg)

*Continued on next page...*

![](_page_19_Picture_5.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **Table 2: Summary of Fault Mode Operation (continued)**

![](_page_20_Picture_518.jpeg)

![](_page_20_Picture_4.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

## **FUNCTIONAL DESCRIPTION**

### **Overview**

The ARG82801-1 is a power management IC designed for safetycritical applications. It contains one switching and four linear regulators to create the voltages necessary for typical automotive applications such as electrical power steering.

The ARG82801-1 pre-regulator can be configured as a buck converter or buck boost. Buck boost is suitable for when applications must work with extremely low battery voltages. This pre-regulator generates a fixed 5.35 V to power the internal or external post-regulators. These post-regulators generate the various voltage levels for the end system.

### **Pre-Regulator**

The pre-regulator incorporates an internal high-side buck switch and a boost switch gate driver. An external freewheeling diode and LC filter are required to complete the buck converter. By adding a MOSFET and boost diode, the pre-regulator can now maintain all outputs with input voltages down to 3.8 V.

The pre-regulator provides many protection and diagnostic functions:

- 1. Pulse-by-pulse and hiccup mode current limit
- 2. Undervoltage detection and reporting
- 3. Shorted switch node to ground
- 4. Open freewheeling diode protection
- 5. High voltage rating for load dump

## **Bias Supply**

The bias supply  $(V_{CC})$  is generated by an internal linear regulator. This supply is the first rail to start up. Most of the internal control circuitry is powered by this supply. The bias supply includes some unique features to ensure safe operation of the ARG82801- 1. These features include:

- 1. Input voltage undervoltage lockout
- 2. Output undervoltage detection and reporting
- 3. Overcurrent and short-circuit limit
- 4. Dual input, VIN and VREG, for low battery voltage operation

### **Charge Pump**

Charge pump circuits provide the voltage necessary to drive highside N-channel MOSFETs in the pre-regulator, linear regulators, and floating gate drivers. Four external capacitors are required for charge pump operation. During the first cycle of the charge pump

action, the flying capacitor between pins CP1C1 and CP1C2 is charged either from VIN or VREG, whichever is highest. During the second cycle, the voltage on the flying capacitor charges the VCP1 capacitor and the flying capacitor, between pins CP2C1 and CP2C2. During the next cycle, the voltage on the flying capacitor charges the VCP2 capacitor. The charge pump incorporates some safety features:

- 1. Undervoltage and overvoltage detection and reporting
- 2. Overcurrent safe mode protection

## **Bandgap**

Dual bandgaps are implemented within the ARG82801-1. One bandgap is dedicated to the voltage regulation loops within each of the regulators, VCC, VCPx, VREG, and the four postregulators. The second is dedicated to the monitoring function of all the regulators undervoltage and overvoltage. This improves safety coverage and fault reporting from the ARG82801-1.

Should the regulation bandgap fail, then the outputs will be out of specification and the monitoring bandgap will report the fault.

If the monitoring bandgap fails, the outputs will remain in regulation, but the monitoring circuits will report the outputs as out of specification and trip the fault flag.

The bandgap circuits include two other bandgaps that are used to monitor the undervoltage state of the main bandgaps.

### **Enable**

Two Enable pins are available on the ARG82801-1. A high signal on either of these pins enables the regulated outputs of the ARG82801-1. One Enable (ENB) is logic-level compatible. The second enable (ENBAT), is battery-level rated and can be connected to the ignition switch.

### **Linear Regulators**

The ARG82801-1 has four linear regulators: one 5 V regulator, one 5 V or 3.3 V selectable regulator, and two protected regulators which track VUC (5 V or 3.3 V).

All linear regulators provide the following protection features:

- 1. Current limit with foldback
- 2. Undervoltage and overvoltage detection and reporting

The protected regulators (V5P1 and V5P2) include protection against connection to the battery voltage. This makes these outputs suitable for powering remote sensors or circuitry where short to battery is possible.

![](_page_21_Picture_38.jpeg)

The pre-regulator powers these linear regulators which reduces power dissipation and temperature.

![](_page_22_Picture_378.jpeg)

## **Fault Detection and Reporting**

There is extensive fault detection within the ARG82801-1; most have been discussed previously. There are two fault reporting mechanisms used by the ARG82801-1: one through hardwired pins and the other through a serial communications interface (SPI).

Two hardwired pins on the ARG82801-1 are used for fault reporting. The first pin, NPOR, reports on the status of the VUC output. This signal goes low if this output is out of regulation. The second pin, FFn (active low fault flag), reports on all other faults. FFn goes low if a fault within the ARG82801-1 exists. The FFn pin can be used by the processor as an alert to check the status of the ARG82801-1 via SPI and see where the fault occurred.

## **Startup Self-Test**

The ARG82801-1 includes self-test which is performed during the startup sequence. This self-test verifies the operation of the undervoltage and overvoltage detection circuits for the main outputs.

In the event the self-test fails, the ARG82801-1 will report the failure through SPI.

## **Undervoltage Detect Self-Test**

The undervoltage (UV) detectors are verified during startup of the ARG82801-1. A voltage that is higher than the undervoltage threshold is applied to each UV comparator; this should cause the relative undervoltage fault bit in the diagnostic registers to change state. If the diagnostic UV register bits change state, the corresponding verify register bits will latch high. When the test of all UV detectors is complete, the verify register bits will remain high if the test passed. If any UV bits in the verify registers, after test, are not set high, then the verification has failed. The following UV detectors are tested: VREG, VUC, V5C, V5P1, and V5P2.

### **Overvoltage Detect Self-Test**

The overvoltage (OV) detectors are verified during startup of the ARG82801-1. A voltage is applied to each OV comparator that is higher than the overvoltage threshold; this should cause the relative overvoltage fault bit in the diagnostic registers to change state. If the diagnostic OV register bits change state, the corresponding verify register bits will latch high. When the test of all OV detectors is complete, the verify register bits will remain high if the test passed. If any OV bits in the verify registers after test are not set high, then the verification has failed. The following OV detectors are tested: VREG, VUC, V5C, V5P1, and V5P2.

### **Overtemperature Shutdown Self-Test**

The overtemperature shutdown (TSD) detector is verified on startup of the ARG82801-1. A voltage is applied to the comparator that is lower than the overtemperature threshold and should cause the general fault flag to be active and an overtemperature fault bit, TSD, to be latched in the Verify Result register 0. When the test is complete, the general fault flag will be cleared and the overtemperature fault will remain in the Verify Result register 0 until reset. If the TSD bit is not set, then the verification has failed.

## **Power-On Enable Self-Test**

The ARG82801-1 also incorporates continuous self-testing of the power-on enable (POE) output. It compares the status of the POE pin with the internal demanded status. If they differ for any reason, an FFn is set and the POE\_OK in SPI diagnostic register goes low.

## **Watchdog Timer**

The ARG82801-1 has two watchdog functions: window watchdog timer and Q&A watchdog timer. When the regulators (VUC and V5C) have been above their undervoltage thresholds for watchdog activation delay  $(t_{d(WD)})$ , WD is activated, WD state will be in the configuration state ("Config"), and the user can set the configuration within 220 ms (min,  $t_{WDTO(CONFIG)}$ ). If no configuration input until  $t_{WDTO(CONFIG)}$  is expired, WD moves into "RESET". Moving back to "Config" mode requires secure SPI command (0x0B).

#### **WINDOW WATCHDOG**

The ARG82801-1 window watchdog circuit monitors an external clock applied to the WDIN pin. This clock should be generated by the microcontroller or DSP. The time between rising edges of the clock must fall within a SPI-programmed "window" or a watchdog fault will be generated. A watchdog fault will set POE "low".

After startup, if no clock edges are detected at WDIN for watchdog activation delay  $t_{d(WD)}$  + max timeout (written in 0x09), the ARG82801-1 will generate watchdog fault and reset its counters. This process will repeat until the system recovers and clock edges are applied to WDIN.

![](_page_22_Picture_23.jpeg)

#### **Q&A WATCHDOG**

The Q&A watchdog circuit monitors an answer code from the microcontroller. The Q&A watchdog procedure is as follows:

- 1. Write 0x08 to set open window period and acceptable number of mis-refresh in "Config" mode.
- 2. Write 0x0B for watchdog restart. Then ARG82801-1 enters into "Normal" mode and generates 6-bit random code.
- 3. Microcontroller reads 0x0A to get 6-bit random code via SDO.
- 4. Write 0x0A with 6-bit inverted random code within open window period. In case the ARG82801-1 can't get the right inverted code, then the watchdog timer is refreshed and generates new 6-bit random code. ARG82801-1 can accept mis-refresh.
- 5. Repeat #2 to #4 within the programmed window.

#### **Analog Multiplexer Output**

The AMUXO terminal is an analog multiplexer output to monitor the voltage of the nodes detailed in Table 3. The output is selected through the serial interface (0x0C). The driving capability of this output is 1 mA and maximum voltage is 3.8 V. Reference response time from SPI register write to AMUX output change is  $\sim$ 20 µs.

![](_page_23_Picture_270.jpeg)

## **Table 3: Analog Multiplexer Output**

#### **Floating MOSFET Gate Drivers**

The ARG82801-1 has four independent floating gate drive outputs to drive external, low on-resistance, power N-channel MOS-FETs connected as a 3-phase solid state relay in phase-isolation applications and an input battery line isolator.

A charge pump regulator provides the above-battery supply voltage necessary to maintain the power MOSFETs in the on state continuously when the phase voltage is equal to the battery voltage.

An internal resistor,  $R_{GPD}$ , between the Gx and Sx pins plus an integrated hold-off circuit, will ensure that the gate-source voltage of the MOSFET is held close to 0 V even with the power disconnected. This can remove the need for additional gate-source resistors on the isolation MOSFETs. In any case, if gate-source resistors are mandatory for the application, then the pump regulator can provide sufficient current to maintain the MOSFET in the on state with a gate-source resistor as low as  $100 \text{ k}\Omega$ .

The four gate drives can be controlled independently through the serial interface by setting the appropriate bit in the control register.

The floating gate-drive outputs for external N-channel MOSFETs are provided on pins GVBB, GU, GV, and GW. Gx=1 (or "high") means that the upper half of the driver is turned on and current will be sourced to the gate of the MOSFET in the phase isolation circuit, turning it on. Gx=0 (or "low") means that the lower half of the driver is turned on and will sink current from the external MOSFET's gate to the respective Sx terminal, turning it off.

The reference points for the floating drives are the load phase connections, SVBB, SU, SV, and SW. The discharge current from the floating MOSFET gate capacitance flows through these connections.

In some applications, it may be necessary to provide a current recirculation path when the motor load is isolated. This will be necessary in situations where the motor driver does not reduce the load current to zero before the isolation MOSFETs are turned off.

The recirculation path can be provided by connecting a suitably rated power diode to the "motor" side of the isolation MOSFETs and GND. See the Functional Block Diagram for more details.

![](_page_23_Picture_22.jpeg)

#### **Table 4: Floating MOSFET Driver**

![](_page_24_Picture_307.jpeg)

![](_page_24_Picture_4.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

![](_page_25_Figure_2.jpeg)

**Figure 6: Watchdog State Diagram**

![](_page_25_Picture_4.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

### **SERIAL COMMUNICATION INTERFACE**

The ARG82801-1 provides the user with a three-wire synchronous serial interface that is compatible with SPI (Serial Peripheral Interface). A fourth wire can be used to provide diagnostic feedback and readback of the register content.

The serial interface timing requirements are specified in the Electrical Characteristics table and illustrated in the Serial Interface Timing diagram (Figure 1). Data is received on the SDI terminal and clocked through a shift register on the rising edge of the clock signal input on the SCK terminal. STRn is normally held high and is only brought low to initiate a serial transfer. No data is clocked through the shift register when STRn is high, allowing multiple SDI slave units to use common SDI, SCK, and SDO connections. Each slave then requires an independent STRn connection.

When 16 data bits have been clocked into the shift register, STRn must be taken high to latch the data into the selected register. When this occurs, the internal control circuits act on the new data and the Diagnostic register is reset.

If there are more than 16 rising edges on SCK or if STRn goes high and there are fewer than 16 rising edges on SCK, the write will be cancelled without writing data to the registers. In addition, the Diagnostic register will not be reset, and the SE (serial error) bit will be set to indicate a data transfer error.

Diagnostic information or the contents of the configuration and control registers is output on the SDO terminal MSB first while STRn is low, and changes to the next bit on each falling edge of SCK. The first bit, which is always the FF (fault flag) bit from the Diagnostic register, is output as soon as STRn goes low.

Each of the programmable (configuration and control) registers has a write bit, WR (bit 10), as the first bit after the register address. This bit must be set to 1 to write the subsequent bits into the selected register. If WR is set to 0, then the remaining data bits (bits 9 to 0) are ignored. The state of the WR bit also determines the data output on SDO. If WR is set to 1, then the Diagnostic register is output. If WR is set to 0, then the contents of the register selected by the first five bits is output. In all cases, the first bit output on SDO will always be the FF bit from the Diagnostic Register.

The ARG82801-1 has 15 register banks. Bit <15:11> represents the register address for read and write. Bit <10> detects the read and write operation. For write operation,  $Bit \le 10$  = 1, and for read operation, bit value is logic low. Bit <9> is an unused bit. Maximum data size is eight bits, so Bit  $\leq 8:1$  represents the data word. The last bit in the serial transfer,  $Bit < 0$  is parity bit that is set to ensure odd parity in the complete 16-bit word. Odd parity means that the total number of 1s in any transmission should always be an odd number. This ensures that there is always at

#### **Pattern at SDI Pin**

![](_page_26_Picture_263.jpeg)

#### **Pattern at SDO Pin after SDI Write**

![](_page_26_Picture_264.jpeg)

#### **Pattern at SDO Pin after SDI Read**

![](_page_26_Picture_265.jpeg)

![](_page_26_Picture_16.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

least one bit set to 1 and one bit set to 0 and allows detection of stuck-at faults on the serial input and output data connections. The parity bit is not stored but generated on each transfer.

Register data is output on the SDO terminal MSB first while STRn is low and changes to the next bit on each falling edge of the SCK. The first bit, which is always the FF bit from the status register, is output as soon as STRn goes low.

If there are more than 16 rising edges on SCL or if STRn goes high and there are fewer than 16 rising edges on SCK, the write will be cancelled without writing data to the registers. In addition, the diagnostic register will not be reset the SE bit will be set to indicate a data transfer error.

**SDI:** Serial data logic input with pull down. 16-bit serial word input MSB first.

**SCK:** Serial clock logic input with pull-down. Data is latched in from SDI on the rising edge of SCL. There must be 16 rising edges per write and SCK must be held high when STRn changes.

**STRn:** Serial data strobe and serial access enable logic input with pull-up. When STRn is high, any activity on SCK or SDI is ignored and SDO is high impedance, allowing multiple SDI slaves to have common SDI, SCK, and SDO connections.

**SDO:** Serial data output. High impedance when STRn is high. Output bit 15 of the status register, the fault flag (FF) as soon as STRn goes low.

## **Register Mapping**

#### **STATUS REGISTERS**

The ARG82801-1 provides three status registers. These registers are read only. They provide real-time status of various functions within the ARG82801-1.

These registers report on the status of all four system rails. They also report on internal rail status, including the charge pump, VREG, and VCC rails. The general fault flag and watchdog fault state are found in these status registers.

The logic that creates the power-on enable and power reset status are reported through these registers.

#### **CONFIGURATION REGISTERS**

The ARG82801-1 allows configuration of the watchdog validation parameters and disabling dithering function.

The watchdog can only be configured during "Config" state. This occurs when the ARG82801-1 is initially enabled or the watchdog is restarted through SPI.

The ARG82801-1 uses frequency dithering for pre-regulator to help reduce EMC noise. The user can disable this feature through the SPI. Default is enabled.

All WD Configuration must be entered before modifying the WD\_ SEL bits, meaning Config\_1 must be written before Config\_0.

#### **DIAGNOSTIC REGISTERS**

There are multiple diagnostic registers in the ARG82801-1. These registers can be read to evaluate the status of the ARG82801- 1. The high-level registers will indicate which area a fault has occurred. Logic high on a data bit in this register implies that no fault has occurred. The following are monitored by these registers:

- All four outputs
- ARG82801-1 bias voltage
- Charge pump voltage
- Pre-regulator voltage
- **Overtemperature**
- Watchdog output
- Shorts on LX pin or open diode on pre-regulator

Note some of these faults will cause the ARG82801-1 to shut down, which might shutdown the microprocessor monitoring the SPI. In this event, the only way to read the fault would be to have alternative power to the microprocessor so it can read the registers. If  $V_{CC}$  of the ARG82801-1 shuts down, all stored register information is lost and the registers revert back to default values.

Other diagnostic registers store more details on each fault, this includes:

- Overvoltage on a particular output or internal rail
- Undervoltage on a particular output or internal rail

The diagnostic registers are latch registers and will hold data if a fault has occurred but recovered. These registers are reset by writing a 1 to them.

#### **OUTPUT ENABLE/DISABLE REGISTER**

The output enable/disable register provides the user control of the LDO outputs and isolator drivers. For LDO control, two bits must be set high to enable an output. If only one bit is high, then the 5 V outputs remain off.

#### **WATCHDOG MODE KEY REGISTER**

At times, it may be necessary to re-flash or restart the processor. To do this, the user must put the watchdog into "Flash Mode" or "restart". This is done by writing a sequence of key words to the "watchdog\_mode\_key" register. If the correct word sequence is

![](_page_27_Picture_37.jpeg)

#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

not received, then the sequence must restart.

Once flash is complete, the processor must send the restart sequence of keywords for the watchdog to exit "Flash Mode". If  $V_{CC}$  has not been removed from the ARG82801-1, the watchdog will restart with the current configuration.

#### **VERIFY RESULT REGISTERS**

On every startup, the ARG82801-1 performs a self-test of the UV and OV detect circuits. This test should cause the diagnostic registers to toggle state. If the diagnostic register successfully changes state, the verify result register will latch high. Upon

#### **Table 5: Register Map**

![](_page_28_Picture_258.jpeg)

**Register Types:** RO = Read-Only

RW = Read or Write RW1C = Read or Write 1 to clear WO = Write-Only

![](_page_28_Picture_11.jpeg)

completion of startup, the system's microprocessor can check the verify result registers to see if the self-test passed.

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#### **0x00: STATUS REGISTER 0**

![](_page_29_Picture_243.jpeg)

![](_page_29_Picture_244.jpeg)

![](_page_29_Picture_245.jpeg)

![](_page_29_Picture_246.jpeg)

![](_page_29_Picture_247.jpeg)

**SERIA ERROR FLAGAZION FLAGAZION Reset Internal Logic Status** 0 No Fault Default 0 NPOR is Low Default 1 NPOR is High

![](_page_29_Picture_248.jpeg)

![](_page_29_Picture_249.jpeg)

![](_page_29_Picture_250.jpeg)

[1] SE Fault: If more than sixteen rising edges on SCK are detected while STRn is LOW or if STRn goes HIGH and there are fewer than sixteen rising edges on SCK.

#### **0x01: STATUS REGISTER 1**

![](_page_29_Picture_251.jpeg)

![](_page_29_Picture_252.jpeg)

![](_page_29_Picture_253.jpeg)

![](_page_29_Picture_254.jpeg)

![](_page_29_Picture_255.jpeg)

![](_page_29_Picture_256.jpeg)

![](_page_29_Picture_257.jpeg)

![](_page_29_Picture_258.jpeg)

![](_page_29_Picture_22.jpeg)

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#### **0x02: STATUS REGISTER 2**

![](_page_30_Picture_303.jpeg)

![](_page_30_Picture_304.jpeg)

![](_page_30_Picture_305.jpeg)

![](_page_30_Picture_306.jpeg)

![](_page_30_Picture_307.jpeg)

![](_page_30_Picture_308.jpeg)

![](_page_30_Picture_309.jpeg)

![](_page_30_Picture_310.jpeg)

![](_page_30_Picture_311.jpeg)

#### **0x03: STATUS REGISTER 3**

![](_page_30_Picture_312.jpeg)

![](_page_30_Picture_313.jpeg)

![](_page_30_Picture_314.jpeg)

![](_page_30_Picture_315.jpeg)

![](_page_30_Picture_316.jpeg)

![](_page_30_Picture_317.jpeg)

![](_page_30_Picture_318.jpeg)

![](_page_30_Picture_319.jpeg)

![](_page_30_Picture_320.jpeg)

[1] DBE Fault: it means that a dual bit error occurred loading the trim data from EEPROM.

![](_page_30_Picture_23.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

#### **0x04: DIAG REGISTER 0**

![](_page_31_Picture_220.jpeg)

![](_page_31_Picture_221.jpeg)

![](_page_31_Picture_222.jpeg)

![](_page_31_Picture_223.jpeg)

![](_page_31_Picture_224.jpeg)

![](_page_31_Picture_225.jpeg)

![](_page_31_Picture_226.jpeg)

#### **0x05: DIAG REGISTER 1**

![](_page_31_Picture_227.jpeg)

![](_page_31_Picture_228.jpeg)

![](_page_31_Picture_229.jpeg)

![](_page_31_Picture_230.jpeg)

![](_page_31_Picture_231.jpeg)

![](_page_31_Picture_232.jpeg)

![](_page_31_Picture_233.jpeg)

![](_page_31_Picture_234.jpeg)

![](_page_31_Picture_235.jpeg)

![](_page_31_Picture_20.jpeg)

![](_page_32_Picture_0.jpeg)

#### **0x06: OUTPUT ENABLE/DISABLE REGISTER 0**

![](_page_32_Picture_184.jpeg)

![](_page_32_Picture_185.jpeg)

![](_page_32_Picture_186.jpeg)

#### **0x07: OUTPUT ENABLE/ DISABLE REGISTER 1**

![](_page_32_Picture_187.jpeg)

![](_page_32_Picture_188.jpeg)

![](_page_32_Picture_189.jpeg)

![](_page_32_Picture_190.jpeg)

![](_page_32_Picture_191.jpeg)

![](_page_32_Picture_12.jpeg)

#### **0x08: CONFIGURATION REGISTER 0**

![](_page_33_Picture_178.jpeg)

![](_page_33_Picture_179.jpeg)

[1] Typical number at the internal clock is center value, need to keep enough margin for  $\pm 5\%$  tolerance of the clock.

1 | 1 | 1 | 1 | 144 ms | 288 ms

![](_page_33_Picture_6.jpeg)

#### **0x09: CONFIGURATION REGISTER 1**

![](_page_34_Picture_217.jpeg)

![](_page_34_Picture_218.jpeg)

![](_page_34_Picture_219.jpeg)

![](_page_34_Picture_220.jpeg)

![](_page_34_Picture_221.jpeg)

[1] Typical number at the internal clock is center value, need to keep enough margin for  $\pm$ 5% tolerance of the clock.

![](_page_34_Picture_222.jpeg)

#### **0x0A: Q&A WATCHDOG REGISTER**

![](_page_34_Picture_223.jpeg)

![](_page_34_Picture_12.jpeg)

![](_page_35_Picture_0.jpeg)

#### **0x0B: WATCHDOG SECURE KEY REGISTER**

![](_page_35_Picture_174.jpeg)

Three 8-bit words must be sent in the correct order to enable flash mode, config mode, Watchdog restart, or disable the watchdog for debugging purpose. If an incorrect word is received, then the register resets and the first word has to be resent.

![](_page_35_Picture_175.jpeg)

#### **0x0C: ANALOG MUX OUTPUT REGISTER**

![](_page_35_Picture_176.jpeg)

![](_page_35_Picture_177.jpeg)

![](_page_35_Picture_9.jpeg)

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#### **0x0D: VERIFY REGISTER 0**

![](_page_36_Picture_296.jpeg)

![](_page_36_Picture_297.jpeg)

![](_page_36_Picture_298.jpeg)

![](_page_36_Picture_299.jpeg)

![](_page_36_Picture_300.jpeg)

![](_page_36_Picture_301.jpeg)

![](_page_36_Picture_302.jpeg)

![](_page_36_Picture_303.jpeg)

![](_page_36_Picture_304.jpeg)

#### **0x0E: VERIFY REGISTER 1**

![](_page_36_Picture_305.jpeg)

![](_page_36_Picture_306.jpeg)

![](_page_36_Picture_307.jpeg)

![](_page_36_Picture_308.jpeg)

![](_page_36_Picture_309.jpeg)

![](_page_36_Picture_18.jpeg)

### **DESIGN AND COMPONENT SELECTION**

The following section briefly describes the component selection procedure for the ARG82801-1.

### **Setting up the Pre-Regulator**

This section discusses the component selection for the ARG82801-1 pre-regulator. It covers the charge pump circuit, inductor, diodes, boost MOSFET, and input and output capacitors. It will also cover loop compensation.

### **Charge Pump Capacitors**

The charge pump circuits require two capacitors: VCP1, a  $2.2 \mu F$ connected from pin VCP1 to VIN and 1 µF connected between pins CP1C1 and CP1C2; and VCP2, a 1 µF connected from pin VCP2 to VCP1 and 0.22 µF connected between pins CP2C1 and CP2C2. These capacitors should be high-quality ceramic capacitors, such as an X5R or X7R, with a voltage rating of at least 16 V.

### **PWM Switching Frequency**

The switching frequency of the ARG82801-1 is fixed at 2.2 MHz nominal. The ARG82801-1 includes a frequency foldback scheme that starts when  $V_{IN}$  is greater than 18 V. Between 18 V and 36 V, the switching frequency will foldback from 2.2 MHz typical to 1 MHz typical. The switching frequency for a given input voltage above 18 V and below 36 V is:

$$
f_{SW} = 3.4 - \frac{1.2}{18} \times V_{VIN} (MHz)
$$
 (1)

![](_page_37_Figure_11.jpeg)

**Figure 7: Typical Switching Frequency versus Input Voltage**

### **Pre-Regulator Output Inductor**

For peak current-mode control, it is well known that the system will become unstable when the duty cycle is above 50% without adequate Slope Compensation ( $S_E$ ). However, the slope compensation in the ARG82801-1 is a fixed value. Therefore, it is important to calculate an inductor value so the falling slope of the inductor current  $(S_F)$  will work well with the ARG82801-1's slope compensation.

Equation 2 can be used to calculate a range of values for the output inductor for the buck-boost. In equation 2, slope compensation can be found in the Electrical Characteristic table,  $V_F$  is the asynchronous diode's forward voltage,  $S_E$  is in A/ $\mu$ s, and L will be in  $\mu$ H:

$$
\frac{(V_{VREG} + V_F)}{S_E} \le L \le \frac{2 \times (V_{VREG} + V_F)}{S_E} \tag{2}
$$

If equation 2 yields an inductor value that is not a standard value, then the next closest available value should be used. The final inductor value should allow for 10%-20% of initial tolerance and 20%-30% for inductor saturation.

Due to topology and frequency switching of the ARG82801-1 pre-regulator, the inductor ripple current varies with input voltage per Figure 8 below:

![](_page_37_Figure_19.jpeg)

**Figure 8: Typical Peak Inductor Current versus Input Voltage for 0.8 A Output Current and 10 µH Inductor**

![](_page_37_Picture_21.jpeg)

The inductor should not saturate given the peak operating current during overload. Equation 3 calculates this current. In equation 3,  $V_{\text{VIN}(MAX)}$  is the maximum continuous input voltage, such as 16 V, and  $V_F$  is the asynchronous diode's forward voltage.

$$
I_{PEAK} = I_{LIM(ton,min)max} - \frac{S_E \times (V_{VREG} + V_F)}{0.9 \times f_{SW} \times (V_{VIN(MAX)} + V_F)}
$$
(3)

After an inductor is chosen, it should be tested during output overload and short-circuit conditions. The inductor current should be monitored using a current probe. A good design should ensure the inductor or the regulator are not damaged when the output is shorted to ground at maximum input voltage and the highest expected ambient temperature.

Inductor ripple current can be calculated using equation 4 for buck mode, and equation 5 for buck-boost mode.

$$
\Delta I_L = \frac{(V_{VIN} - V_{VREG}) \times V_{VREG}}{f_{SW} \times L \times V_{VIN}} \tag{4}
$$

$$
\Delta I_{L(B/B)} = \frac{V_{VIN} \times D_{BOOST}}{f_{SW} \times L}
$$
 (5)

#### **Pre-Regulator Output Capacitors**

The output capacitors filter the output voltage to provide an acceptable level of ripple voltage. They also store energy to help maintain voltage regulation during a load transient. The voltage rating of the output capacitors must support the output voltage with sufficient design margin.

The output voltage ripple  $(\Delta V_{VREG})$  is a function of the output capacitors parameters:  $C_O$ ,  $ESR_{CO}$ ,  $ESL_{CO}$ .

$$
\Delta V_{VREG} = \Delta I_L \times ESR_{CO} +
$$
  
\n
$$
\frac{V_{VIN} - V_{VREG}}{L} \times ESL_{CO} +
$$
  
\n
$$
\frac{\Delta I_L}{8 \times f_{SW} \times C_O}
$$
 (6)

The type of output capacitors will determine which terms of equation 6 are dominant. For ceramic output capacitors, the  $ESR_{CO}$  and  $ESL_{CO}$  are virtually zero, so the output voltage ripple will be dominated by the third term of equation 6.

$$
\Delta V_{VREG} = \frac{\Delta I_L}{8 \times f_{SW} \times C_O} \tag{7}
$$

To reduce the voltage ripple of a design using ceramic output capacitors, simply increase the total capacitance, reduce the inductor current ripple (i.e. increase the inductor value), or increase the switching frequency.

The transient response of the regulator depends on the number and type of output capacitors. In general, minimizing the ESR of the output capacitance will result in a better transient response. The ESR can be minimized by simply adding more capacitors in parallel or by using higher quality capacitors. At the instant of a fast load transient (di/dt), the output voltage will change by the amount:

$$
\Delta V_{VREG} = \Delta I_{LOAD} \times ESR_{CO} + \frac{di}{dt} \times ESL_{CO}
$$
 (8)

After the load transient occurs, the output voltage will deviate from its nominal value for a short time. This time will depend on the system bandwidth, the output inductor value, and output capacitance. Eventually, the error amplifier will bring the output voltage back to its nominal value.

The speed at which the error amplifier will bring the output voltage back to its setpoint will depend mainly on the closed-loop bandwidth of the system. A higher bandwidth usually results in a shorter time to return to the nominal voltage. However, a higher bandwidth system may be more difficult to obtain acceptable gain and phase margins. Selection of the compensation components  $(R_Z, C_Z, C_P)$  are discussed in more detail in the Compensation Components section of this datasheet.

#### **Ceramic Input Capacitors**

The ceramic input capacitor(s) must limit the voltage ripple at the VIN pin to a relatively low voltage during maximum load. Equation 8 can be used to calculate the minimum input capacitance,

$$
C_{\text{IN}} \ge \frac{I_{\text{VREG}(MAX)} \times 0.25}{0.90 \times f_{\text{SW}} \times 50 \text{ mV}} \tag{9}
$$

where  $I_{VREG(MAX)}$  is the maximum current from the pre-regulator,

$$
I_{VREG(MAX)} = I_{LINEAR} + I_{AUX} + 20 mA
$$
\n(10)

where  $I_{LINEAR}$  is the sum of all the internal linear regulators output currents,  $I_{AUX}$  is any extra current drawn from the VREG output to power other devices external to the ARG82801-1.

A good design should consider the DC bias effect on a ceramic capacitor—as the applied voltage approaches the rated value, the capacitance value decreases. The X5R and X7R type capacitors

![](_page_38_Picture_26.jpeg)

#### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

should be the primary choices due to their stability versus both DC bias and temperature. For all ceramic capacitors, the DC bias effect is even more pronounced on smaller case sizes, so a good design will use the largest affordable case size.

Also for improved noise performance, it is recommended to add smaller sized capacitors close to the input pin and the D1 anode. Use a 0.1 µF 0603 capacitor or less.

## **Buck-Boost Asynchronous Diode (D1)**

The highest peak current in the asynchronous diode (D1) occurs during overload and is limited by the ARG82801-1. Equation 3 can be used to calculate this current.

The highest average current in the asynchronous diode occurs when  $V_{VIN}$  is at its maximum,  $D_{BOOST} = 0\%$ , and  $D_{BUCK} = \text{mini}$ mum (10%),

$$
I_{AVG} = 0.9 \times I_{VREG(MAX)} \tag{11}
$$

where  $I_{VREG(MAX)}$  is calculated using equation 10.

### **Boost MOSFET (Q1)**

The RMS current in the boost MOSFET (Q1) occurs when  $V_{\text{VIN}}$ is at its minimum and both the buck and boost operate at their maximum duty cycles (approximately 64% and 58%, respectively),

$$
I_{QI(RMS)} = \sqrt{D_{BOOST} \times \left( \left( I_{PEAK} - \frac{\Delta I_{L(B/B)}}{2} \right)^2 + \frac{\Delta I_{L(B/B)}}{12} \right)^2} \tag{12}
$$

where  $\Delta I_{L(B/B)}$  and  $I_{PEAK}$  are derived using equations 3 and 5, respectively.

## **Boost Diode (D2)**

In buck mode, this diode will simply conduct the output current. However, in buck-boost mode, the peak currents in this diode may increase a lot. The ARG82801-1 limits the peak current to the value calculated using equation 3. The average current is simply the output current.

## **Pre-Regulator Compensation Components (R<sup>Z</sup> , C<sup>Z</sup> , CP)**

Although the ARG82801-1 can operate in buck-boost mode at low input voltages, it still can be considered a buck converter when looking at the control loop. The following equations can be used to calculate the compensation components.

First, select the target crossover frequency for the final system.

While switching at over 2 MHz, the crossover is governed by the required phase margin. Since a type II compensation scheme is used, the system is limited to the amount of phase that can be added. Hence, a crossover frequency,  $f_C$ , in the region of 55 kHz is selected. The total system phase will drop off at higher crossover frequencies. The  $R_Z$  selection is based on the gain required at the crossover frequency and can be calculated by the following simplified equation:

$$
R_Z = \frac{13.36 \times \pi \times f_C \times C_O}{gm_{POWE} \times gm_{EA}} \tag{13}
$$

where  $f_C$  is in kHz,  $C_O$  (actual capacitance at 5.35 V DC bias) is in μF, and R<sub>Z</sub> will be in kΩ. The  $gm_{\text{POWER}}$  (in A/V) and  $gm_{\text{EA}}$  (in µA/V) can be found in the Electrical Characteristic table.

The series capacitor,  $C_Z$ , along with the resistor,  $R_Z$ , set the location of the compensation zero. This zero should be placed no lower than ¼ the crossover frequency and should be kept to a minimum value. Equation 14 can be used to estimate this capacitor value.

$$
C_Z > \frac{4}{2\pi \times R_Z \times f_C} \tag{14}
$$

where  $f_C$  is in kHz,  $R_Z$  is in k $\Omega$ , and  $C_Z$  will be in  $\mu$ F.

Determine if the second compensation capacitor  $(C_P)$  is required. It is required if the ESR zero of the output capacitor is located at less than half of the switching frequency or the following relationship is valid:

$$
\frac{1}{2\pi \times C_O \times ESR_{CO}} < \frac{f_{SW}}{2} \tag{15}
$$

If this is the case, then add the second compensation capacitor  $(C<sub>P</sub>)$  to set the pole at the location of the ESR zero. Determine the  $C_P$  value by the equation:

$$
C_P = \frac{C_{OUT} \times ESR_{CO}}{R_Z} \tag{16}
$$

where  $C_O$  is in  $\mu$ F,  $ESR_{CO}$  is in m $\Omega$ ,  $R_Z$  is in k $\Omega$ , and  $C_Z$  will be in pF.

An Excel-based design tool is available from Allegro that accepts customer specifications and recommended values for both power and compensation components. The pre-regulator bode plot in Figure 9 was generated with this tool. The bandwidth of this system  $(f_C)$  is 56 kHz, the phase margin (PM) is 67 degrees, and the gain margin (GM) is 21 dB.

![](_page_39_Picture_30.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

![](_page_40_Figure_2.jpeg)

**Figure 9: Bode Plot for Pre-Regulator R**<sub>Z</sub> = 18.2 kΩ, C<sub>Z</sub> = 3.3 nF, C<sub>P</sub> = 47 pF  $L_0 = 4.7 \mu$ H, C<sub>O</sub> = 3 × 10 µF (16V/X7R/1206) MLCC

## **Linear Regulators**

The four linear regulators only require a single ceramic capacitor located near ARG82801-1 terminals to ensure stable operation. The range of acceptable values is shown in the Electrical Characteristics table. A 2.2 μF capacitor per regulator is recommended.

Also, since the V5P1 and V5P2 are used to power remote circuitry, their load may include external wiring. The inductance of this wiring may cause LC-type ringing and negative spikes on the V5P1 (V5P2) pin if a "fast" short-to-ground occurs. It is recommended a small Schottky diode be placed close to the V5P1 (V5P2) pin to clamp this negative spike. The MSS1P5 (or equivalent) is a good choice.

## **Internal Bias (VCC)**

The internal bias voltage should be decoupled at the VCC pin using a 1 μF ceramic capacitor. It is not recommended to use this pin as a source.

## **Signal Pins (NPOR, FFn, POE)**

The ARG82801-1 has many signal-level pins. The NPOR, FFn, and ENBAT are open-drain outputs and require external pull-up resistors. Allegro recommends sizing the external pull-up resistors so each pin will sink less than 2 mA when it is a logic low. The POE signal is push-pull output and does not require external pull-up resistor.

![](_page_40_Picture_11.jpeg)

### **Fully Integrated PMIC for Safety-Related Systems with Buck or Buck-Boost Pre-Regulator, 4× Linear Regulators, 4× Gate Drivers, and SPI**

### **PCB LAYOUT RECOMMENDATIONS**

The input ceramic capacitors must be located as close as possible to the VIN pins. In general, the smaller capacitors (0402, 0603) must be placed very close to the VIN pin. The larger capacitors should be placed within 0.5 inches of the VIN pin. There must not be any vias between the input capacitors and the VIN pins.

The pre-regulator asynchronous diode (D1), input ceramic capacitors, and RC snubber must be routed on one layer and "star" grounded at a single location with multiple vias.

The pre-regulator output inductor (L1) should be located close to the LX pins. The LX trace widths (to L1, D1) should be relatively wide and preferably on the same layer as the IC.

The pre-regulators output ceramic capacitors should be located near the VREG pin. There must be 1 or 2 smaller ceramic capacitors as close as possible to the VREG pin.

The four charge pump capacitors must be placed as close as pos-

sible to VCP1, CP1C1/CP1C2 and VCP2, CP2C1/ CP2C2.

The ceramic capacitors for the LDOs (VUC, V5C, V5P1, and V5P2) must be placed near their output pins. The V5P1 and V5P2 outputs must have a  $1 A/40 V$  Schottky diode located very close to their pins to limit negative voltages.

The VCC bypass capacitor must be placed very close to the VCC pin.

The COMP network of pre-regulators  $(R_Z, C_Z, and C_P)$  must be located very close to the COMP pin.

The thermal pad under the ARG82801-1 must connect to the ground plane(s) with multiple vias.

The boost MOSFET (Q1) and the boost diode (D2) must be placed very close to each other. Q1 should have thermal vias to a polygon on the bottom layer. Also, there should be "local" bypass capacitors from D2 cathode to Q1 source.

![](_page_41_Picture_14.jpeg)

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![](_page_42_Figure_2.jpeg)

**Figure 10: Package LV, 38-Pin eTSSOP**

![](_page_42_Picture_4.jpeg)

![](_page_43_Picture_0.jpeg)

#### **Revision History**

![](_page_43_Picture_90.jpeg)

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![](_page_43_Picture_11.jpeg)