#### General Description

The MAX8588 power-management IC is optimized for devices using Intel X-Scale™ microprocessors, including smartphones, PDAs, internet appliances, and other portable devices requiring substantial computing and multimedia capability at low power.

The IC integrates seven high-performance, low-operatingcurrent power supplies along with supervisory and management functions. Included are three step-down DC-DC outputs, three linear regulators, and a seventh always-on output. DC-DC converters power I/O, memory, and the CPU core. The I/O supply can be preset to 3.3V or adjusted to other values. The DRAM supply is preset for 3.3V or 2.5V, or it can be adjusted with external resistors. The CPU core supply is serial programmed for dynamic voltage management and can supply up to 0.5A. Linear-regulated outputs are provided for SRAM, PLL, and USIM supplies.

To minimize quiescent current, critical power supplies have bypass "sleep" LDOs that can be activated when output current is very low. Other functions include separate on/off control for all DC-DC converters, low-battery and dead-battery detection, a reset and power-OK output, a backup-battery input, and a two-wire serial interface.

All DC-DC outputs use fast, 1MHz PWM switching and small external components. They operate with fixed-frequency PWM control and automatically switch from PWM to skip-mode operation at light loads to reduce operating current and extend battery life. The core output can be forced into PWM mode at all loads to minimize noise. A 2.6V to 5.5V input voltage range allows 1-cell lithium-ion (Li+), 3-cell NiMH, or a regulated 5V input. The MAX8588 is available in a tiny 6mm x 6mm, 48-pin thin QFN package.

#### **Applications**

PDA, Palmtop, and Wireless Handhelds Third-Generation Smart Cell Phones Internet Appliances and Web-Books

#### Features

♦ **Six Regulators in One Package Step-Down DC-DC for I/O at 1.3A Step-Down DC-DC for Memory at 0.9A Step-Down Serial-Programmed DC-DC for CORE Up to 0.5A Three LDO Outputs for SRAM, PLL, and USIM Always-On Output for VCC\_BATT**

**MAXM** 

- ♦ **Low Operating Current 60µA in Sleep Mode (Sleep LDOs On) 130µA with DC-DCs On (Core Off) 200µA All Regulators On, No Load 5µA Shutdown Current**
- ♦ **Optimized for X-Scale Processors**
- ♦ **Backup-Battery Input**
- ♦ **1MHz PWM Switching Allows Small External Components**
- ♦ **Tiny 6mm x 6mm, 48-Pin Thin QFN Package**

#### Ordering Information



**Pin Configuration appears at end of data sheet.**

#### Simplified Diagram



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#### **MAXIM**

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**For pricing, delivery, and ordering information, please contact Maxim/Dallas Direct! at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.**

#### **ABSOLUTE MAXIMUM RATINGS**

IN, IN45, IN6, MR, LBO, DBO, RSO, POK, SCL, SDA, BKBT, V7, SLP, SRAD, PWM3 to GND...............-0.3V to +6V



Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **ELECTRICAL CHARACTERISTICS**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .)



#### **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at  $T_A = +25$ °C.)



#### **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at TA = +25**°**C.)





#### **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at  $T_A = +25$ °C.)



# MAX8588

#### **ELECTRICAL CHARACTERISTICS**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = -40°C to +85°C**, unless otherwise noted.) (Note 5)



#### **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = -40°C to +85°C**, unless otherwise noted.) (Note 5)



#### **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = 3.6V, VBKBT = 3.0V, VLBI = 1.1V, VDBI = 1.35V, circuit of Figure 5, **TA = -40°C to +85°C**, unless otherwise noted.) (Note 5)



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#### **ELECTRICAL CHARACTERISTICS (continued)**

**Note 1:** Dropout voltage is guaranteed by the p-channel switch resistance and assumes a maximum inductor resistance of 45mΩ.

**Note 2:** The PWM-skip-mode transition has approximately 10mA of hysteresis.

**Note 3:** The maximum output current is guaranteed by the following equation:

$$
I_{\text{OUTmax}} = \frac{I_{\text{LIM}} - \frac{V_{\text{OUT}} (1 - D)}{2 \times f \times L}}{1 + (R_{\text{N}} + R_{\text{L}}) \frac{(1 - D)}{2 \times f \times L}}
$$

where:

$$
D = \frac{V_{OUT} + I_{OUT(MAX)} (R_N + R_L)}{V_{IN} + I_{OUT(MAX)} (R_N - R_P)}
$$

and  $R_N$  = n-channel synchronous rectifier  $R_{DS(ON)}$ 

 $Rp = p$ -channel power switch  $R_{DS(ON)}$ 

 $R_L$  = external inductor ESR

IOUT(MAX) = maximum required load current

 $f =$  operating frequency minimum

 $L =$  external inductor value

ILIM can be substituted for  $I_{\text{OUT}(MAX)}$  (desired) when solving for D. This assumes that the inductor ripple current is small relative to the absolute value.

**Note 4:** POK only indicates the status of supplies that are enabled (except V7). When a supply is turned off, POK does not trigger low. When a supply is turned on, POK immediately goes low until that supply reaches regulation. POK is forced low when all supplies (except V7) are disabled.

**Note 5:** Specifications to -40°C are guaranteed by design, not production tested.

Typical Operating Characteristics

(Circuit of Figure 6,  $V_{IN} = 3.6V$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.)

# MAX8588



/VI *A* XI /VI

#### Typical Operating Characteristics (continued)

(Circuit of Figure 6,  $V_{IN} = 3.6V$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.)



SWITCHING FREQUENCY vs. SUPPLY VOLTAGE







REFERENCE VOLTAGE vs. TEMPERATURE



#### REG1 SWITCHING WAVEFORMS WITH 10mA LOAD



**MAX8588** MAX8588

**/VI/IXI/VI** 

#### Typical Operating Characteristics (continued)

(Circuit of Figure 6,  $V_{IN} = 3.6V$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.)









V7 AND RSO STARTUP WAVEFORMS





MAX8588

#### Typical Operating Characteristics (continued)

(Circuit of Figure 6,  $V_{IN} = 3.6V$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.)



REG3 LOAD-TRANSIENT RESPONSE

200µs/div

MAX8588 toc22

0A

ILOAD3 200mA/div

V3 100mV/div AC-COUPLED



# **MAX8588** MAX8588

REG3 OUTPUT VOLTAGE CHANGING FROM 1.3V TO 1.0V WITH DIFFERENT VALUES OF CRAMP



200µs/div



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#### Pin Description



Dual Mode is a trademark of Maxim Integrated Products, Inc.



### Pin Description (continued)



#### Pin Description (continued)



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Figure 1. MAX8588 Functional Diagram



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MAX8588

#### Detailed Description

The MAX8588 power-management IC is optimized for devices using Intel X-Scale microprocessors, including third-generation smart cell phones, PDAs, internet appliances, and other portable devices requiring substantial computing and multimedia capability at low power. The MAX8588 complies with Intel Processor Power specifications.

The IC integrates seven high-performance, low-operating-current power supplies along with supervisory and management functions. Regulator outputs include three step-down DC-DC outputs (V1, V2, and V3), three linear regulators (V4, V5, and V6), and one always-on output, V7 (Intel VCC\_BATT). The V1 step-down DC-DC converter provides 3.3V or adjustable output voltage for I/O and peripherals. The V2 step-down DC-DC converter is preset for 3.3V or 2.5V. V2 can also be adjusted with external resistors on all parts. The V3 step-down DC-DC converter provides a serial-programmed output for powering microprocessor cores. The three linear regulators (V4, V5, and V6) provide power for PLL, SRAM, and USIM.

To minimize sleep-state quiescent current, V1 and V2 have bypass "sleep" LDOs that can be activated to minimize battery drain when output current is very low. Other functions include separate on/off control for all DC-DC converters, low-battery and dead-battery detection, a power-OK output, a backup-battery input, and a two-wire serial interface.

All DC-DC outputs use fast, 1MHz PWM switching and small external components. They operate with fixed-frequency PWM control and automatically switch from PWM to skip-mode operation at light loads to reduce operating current and extend battery life. The V3 core output is capable of forced-PWM operation at all loads. The 2.6V to 5.5V input voltage range allows 1-cell Li+, 3-cell NiMH, or a regulated 5V input.

The following power-supply descriptions include the Intel terms for the various voltages in parenthesis. For example, the V1 output is referred to as VCC\_IO in Intel documentation. See Figure 1.

#### V1 and V2 (VCC\_IO, VCC\_MEM) Step-Down DC-DC Converters

V1 is a 1MHz current-mode step-down converter. The V1 output voltage can be preset to 3.3V or adjusted using a resistor voltage-divider. V1 supplies loads up to 1300mA.

V2 is also a 1MHz current-mode step-down converter. The V2 step-down DC-DC converter is preset for 3.3V or 2.5V. V2 can also be adjusted with external resistors on all parts. V2 supplies loads up to 900mA.

Under moderate to heavy loading, the converters operate in a low-noise PWM mode with constant frequency and modulated pulse width. Switching harmonics generated by fixed-frequency operation are consistent and easily filtered. Efficiency is enhanced under light loading (<30mA typ), by assuming an Idle Mode<sup> $n$ </sup> during which the converter switches only as needed to service the load.

#### **Synchronous Rectification**

Internal n-channel synchronous rectifiers eliminate the need for external Schottky diodes and improve efficiency. The synchronous rectifier turns on during the second half of each cycle (off-time). During this time, the voltage across the inductor is reversed, and the inductor current falls. In normal operation (not forced PWM), the synchronous rectifier turns off at the end of the cycle (at which time another on-time begins) or when the inductor current approaches zero.

#### **100% Duty-Cycle Operation**

If the inductor current does not rise sufficiently to supply the load during the on-time, the switch remains on, allowing operation up to 100% duty cycle. This allows the output voltage to maintain regulation while the input voltage approaches the regulation voltage. Dropout voltage is approximately 180mV for an 800mA load on V1 and 220mV for an 800mA load on V2. During dropout, the high-side p-channel MOSFET turns on, and the controller enters a low-current-consumption mode. The device remains in this mode until the regulator channel is no longer in dropout.

#### **Sleep LDOs**

In addition to the high-efficiency step-down converters, V1 and V2 can also be supplied with low-quiescent current, low-dropout (LDO) linear regulators that can be used in sleep mode or at any time when the load current is very low. The sleep LDOs can source up to 35mA. To enable the sleep LDOs, drive SLP low. When SLP is high, the switching step-down converters are active. The output voltage of the sleep LDOs is set to be the same as the switching step-down converters as described in the Setting the Output Voltages section. SLPIN is the input to the V1 and V2 sleep LDOs and must connect to IN.

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#### V3 (VCC\_CORE) Step-Down DC-DC Converter

V3 is a 1MHz current-mode step-down converter. It supplies loads up to 500mA.

The V3 output is set by the I<sup>2</sup>C serial interface to between 0.7V and 1.475V in 25mV increments. The default output voltage on power-up, and after a reset, is 1.3V. See the Serial Interface section for programming details. See the Applications Information for instructions on how to increase the V3 output voltage.

#### **Forced PWM on REG3**

Under moderate to heavy loading, the V3 always operates in a low-noise PWM mode with constant frequency and modulated pulse width. Switching harmonics generated by fixed-frequency operation are consistent and easily filtered.

With light loads (<30mA) and PWM3 low, V3 operates in an enhanced-efficiency idle mode during which the converter switches only as needed to service the load. With PWM3 high, V3 operates in low-noise forced-PWM mode under all load conditions.

### Linear Regulators (V4, V5, and V6)

#### **V4 (VCC\_PLL)**

V4 is a linear regulator that provides a fixed 1.3V output and supplies loads up to 35mA. The power input for the V4 and V5 linear regulators is IN45, which is typically connected to V2. To enable V4, drive ON4 high, or drive ON4 low for shutdown. V4 is intended to connect to VCC\_PLL.

#### **V5 (VCC\_SRAM)**

V5 is a linear regulator that provides a fixed 1.1V output and supplies loads up to 35mA. The power input for the

V4 and V5 linear regulators is IN45, which is typically connected to V2. To enable V5, drive ON5 high, or drive ON5 low for shutdown. V5 is intended to connect to VCC\_SRAM.

#### **V6 (VCC\_USIM)**

V6 is a linear regulator that supplies loads up to 35mA. The V6 output voltage is programmed with the I2C serial interface to 0V, 1.8V, 2.5V, or 3.0V. The power-up default for V6 is 0V. See the Serial Interface section for details on changing the voltage. The power input for the V6 linear regulator is IN6, which is typically connected to V1. To enable V6, drive ON6 high, or drive ON6 low for shutdown. V6 is intended to connect to VCC\_USIM.

#### V7 Always-On Output (VCC\_BATT)

The V7 output is always active if V1 is enabled and in regulation or if backup power is present. When ON1 is high and V1 is in regulation, V7 is sourced from V1 by an internal MOSFET switch. When ON1 is low or V1 is out of regulation, V7 is sourced from BKBT by a second on-chip MOSFET. V7 can supply loads up to 30mA. V7 is intended to connect to VCC\_BATT on Intel CPUs.

Due to variations in system implementation, BKBT and V7 can be utilized in different ways. See the Backup-Battery Configurations section for information on how to use BKBT and V7.

#### Quiescent Operating Current in Various States

The MAX8588 is designed for optimum efficiency and minimum operating current for all typical operating modes, including sleep and deep sleep. These states are outlined in Table 1.

<b>OPERATING</b> <b>POWER MODE</b>	<b>DESCRIPTION</b>	<b>TYPICAL NO-LOAD</b> <b>OPERATING CURRENT</b>
<b>RUN</b>	All supplies on and running.	225 <sub>µ</sub> A
<b>IDLE</b>	All supplies on and running, peripherals on.	
<b>SENSE</b>	All supplies on, minimal loading, peripherals monitored.	
<b>STANDBY</b>	All supplies on, minimal loading, peripherals not monitored.	
SI FFP	PWR_EN controlled voltages (V3, V4, V5) are off. V1 and V2 on.	60µA if V1 and V2 SLEEP LDOs on: 130µA if V1, V2 step-down DC-DCs enabled
<b>DEEP SLEEP</b>	All supplies off except V7. V7 biased from backup battery.	$32\mu$ A if $IN > DBI$ threshold; $4\mu$ A if $IN <$ DBI threshold

**Table 1. Quiescent Operating Current in Various States**

#### Voltage Monitors, Reset, and Undervoltage-Lockout Functions

#### **Undervoltage Lockout**

When the input voltage is below 2.35V (typ), an undervoltage-lockout (UVLO) circuit disables the IC. The inputs remain high impedance while in UVLO, reducing battery load under this condition. All serial registers are maintained with the input voltage down to at least 2.35V.

#### **Reset Output** (RSO) **and** MR **Input**

The reset output  $(\overline{\text{RSO}})$  is low when the  $\overline{\text{MR}}$  input is low or when V7 is below 2.425V. V7 is powered from V1 (when enabled) or the backup-battery input (BKBT). RSO normally goes low:

- 1) When power is first applied in configurations with no separate backup battery (external diode from IN to BKBT).
- 2) When power is removed in configurations with no separate backup battery (external diode from IN to BKBT).
- 3) If the backup battery falls below 2.425V when V1 is off or out of regulation.
- 4) When the manual reset button is pressed (MR goes low).

If  $V_{IN}$  > 2.4V, an internal timer delays the release of  $\overline{RSO}$ for 65ms after V7 rises above 2.3V. However, if  $V_{IN} <$ 2.4V when V7 exceeds 2.3V, or if V<sub>IN</sub> and V7 rise at the same time,  $\overline{\text{RSO}}$  deasserts immediately with no 65ms delay. There is no delay in the second case because the timer circuitry is deactivated to minimize operating current during V<sub>IN</sub> undervoltage lockout.

If it is desired to have a 65ms RSO release delay for any sequence of  $V_{IN}$  and V7, the circuit in Figure 2 may be used. An RC connected from IN to MR delays the rise of  $\overline{\text{MR}}$  until after V<sub>IN</sub> powers up. The 65ms timer is valid for either sequence of V7 and V<sub>IN</sub> and does not release until 65ms after both are up. The only regulator output that affects RSO is V7. RSO will not respond to V1–V6, which are monitored by POK. Also, RSO is high impedance and does not function if BKBT is not powered.

MR is a manual reset input for hardware reset. A low input at MR causes the RSO output to go low for at least 65ms and also resets the V3 output to its default 1.3V setting and turns off the V6 output. MR impacts no other MAX8588 functions.

#### **Dead-Battery and Low-Battery Comparators—DBI, LBI**

The DBI and LBI inputs monitor input power (usually a battery) and trigger the DBO and LBO outputs. The dead-battery comparator triggers DBO when the battery



Figure 2. An RC delay connected from IN to MR ensures that the 65ms RSO release delay remains in effect for any sequence of IN and V7.



Figure 3. Setting the Low-Battery and Dead-Battery Thresholds with One Resistor Chain. The values shown set a DBI threshold of 3.3V and an LBI threshold of 3.5V (no resistors are needed for the factory preset thresholds).

(V<sub>IN</sub>) discharges to the dead-battery threshold. The factory-set 3.15V threshold is selected by connecting DBI to IN, or the threshold can be programmed with a resistor-divider at DBI. The low-battery comparator has a factory-set 3.6V threshold that is selected by connecting LBI to IN, or its threshold can be programmed with a resistor-divider at LBI.

One three-resistor-divider can set both DBI and LBI (R1, R2, and R3 in Figure 3) according to the following equations:

1) Choose R3 to be less than 250 $k\Omega$ 

- 2) R1 = R3  $V_{LB}$  (1 (1.232 /  $V_{DB}$ ))
- 3) R2 = R3 (1.232 x (V<sub>LB</sub> / V<sub>DB</sub>) 1)

where  $V_{LB}$  is the low-battery threshold and  $V_{DB}$  is the dead-battery threshold.



# MAX8588 **MAX8588**

# High-Efficiency, Low-IQ PMIC with Dynamic Core for PDAs and Smartphones



Figure 4. Setting the Low-Battery and Dead-Battery Thresholds with Separate Resistor-Dividers. The values shown set a DBI threshold of 3.3V and an LBI threshold of 3.5V (no resistors are needed for factory-preset thresholds).

Alternately, LBI and DBI can be set with separate tworesistor-dividers. Choose the lower resistor of the divider chain to be 250kΩ or less (R5 and R7 in Figure 4). The equations for upper divider-resistors as a function of each threshold are then:

$$
R4 = R5 (V_{DB} / 1.232) - 1)
$$

$$
R6 = R7 (V_{LB} - 1)
$$

When resistors are used to set  $V_{LB}$ , the threshold at LBI is 1.00V. When resistors are used to set  $V_{DB}$ , the threshold at DBI is 1.232V. A resistor-set threshold can also be used for only one of DBI or LBI. The other threshold can then be factory set by connecting the appropriate input to IN.

If BKBT is not powered, DBO does not function and is high impedance. DBO is expected to connect to nBATT\_FAULT on Intel CPUs. If BKBT is not powered, LBO does not function and is high impedance.

#### **Power-OK Output (POK)**

POK is an open-drain output that goes low when any activated regulator (V1–V6) is below its regulation threshold. POK does not monitor V7. When all active output voltages are within 10% of regulation, POK is high impedance. POK does not flag an out-of-regulation condition while V3 is transitioning between voltages set by serial programming or when any regulator channel has been turned off. POK momentarily goes low when any regulator is turned on, but returns high when that regulator reaches regulation. When all regulators (V1–V6) are off, POK is forced low. If the input voltage is below the UVLO threshold, POK is held low and maintains a valid low output with IN as low as 1V. If BKBT is not powered, POK does not function and is high impedance.

#### Connection to Processor and Power Sequencing

Typical processor connections have only power-control pins, typically labeled PWR\_EN and SYS\_EN. The MAX8588 provides numerous on/off control pins for maximum flexibility. In a typical application, many of these pins are connected together. ON1, ON2, and ON6 typically connect to SYS\_EN. ON3, ON4, and ON5 typically connect to PWR\_EN. V7 remains on as long as the main or backup power is connected. Sequencing is not performed internally on the MAX8588; however, all ON\_ inputs have hysteresis and can connect to RC networks to set sequencing. For typical connections to Intel CPUs, no external sequencing is required.

#### Backup-Battery Input

The backup-battery input (BKBT) provides backup power for V7 when V1 is disabled. Normally, a primary or rechargeable backup battery is connected to this pin. If a backup battery is not used, then BKBT should connect to IN through a diode or external regulator. See the Backup-Battery Configurations section for information on how to use BKBT and V7.

#### Serial Interface

An I2C-compatible, two-wire serial interface controls REG3 and REG6. The serial interface operates when IN exceeds the 2.40V UVLO threshold and at least one of ON1–ON6 is asserted. The serial interface is shut down to minimize off-current drain when no regulators are enabled.

The serial interface consists of a serial data line (SDA) and a serial clock line (SCL). Standard I2C-compatible write-byte commands are used. Figure 4 shows a timing diagram for the  $12C$  protocol. The MAX8588 is a slave-only device, relying upon a master to generate a clock signal. The master (typically a microprocessor) initiates data transfer on the bus and generates SCL to permit data transfer. A master device communicates to the MAX8588 by transmitting the proper address followed by the 8-bit data code (Table 2). Each transmit sequence is framed by a START (A) condition and a STOP (L) condition. Each word transmitted over the bus is 8 bits long and is always followed by an acknowledge clock pulse.

Table 2 shows the serial data codes used to program V3 and V6. The default power-up voltage for V3 is 1.3V and for V6 is 0V.



#### **Table 2. V3 and V6 Serial Programming Codes**



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Figure 5. I<sup>2</sup>C-Compatible Serial-Interface Timing Diagram

#### Bit Transfer

One data bit is transferred during each SCL clock cycle. The data on SDA must remain stable during the high period of the SCL clock pulse. Changes in SDA while SCL is high are control signals (see the START and STOP Conditions section). Both SDA and SCL idle high when the bus is not busy.

#### START and STOP Conditions

When the serial interface is inactive, SDA and SCL idle high. A master device initiates communication by issuing a START condition. A START condition is a high-tolow transition on SDA with SCL high. A STOP condition is a low-to-high transition on SDA while SCL is high (Figure 5). A START condition from the master signals the beginning of a transmission to the MAX8588. The master terminates transmission by issuing a not acknowledge followed by a STOP condition (see the Acknowledge Bit section). The STOP condition frees the bus.

When a STOP condition or incorrect address is detected, the MAX8588 internally disconnects SCL from the serial interface until the next START condition, minimizing digital noise and feedthrough.

#### **Acknowledge Bit (ACK)**

The acknowledge bit (ACK) is the ninth bit attached to every 8-bit data word. The receiving device always generates ACK. The MAX8588 generates an ACK when receiving an address or data by pulling SDA low during the ninth clock period. Monitoring ACK allows for detection of unsuccessful data transfers. An unsuccessful data transfer occurs if a receiving device is busy or if a system fault has occurred. In the event of an unsuccessful data transfer, the bus master should reattempt communication at a later time.

#### **Serial Address**

MAX8588

**MAX8588** 

A bus master initiates communication with a slave device by issuing a START condition followed by the 7-bit slave address (Table 3). When idle, the MAX8588 waits for a START condition followed by its slave address. The serial interface compares each address value bit by bit, allowing the interface to power down immediately if an incorrect address is detected.

The LSB of the address word is the read/write  $(R/\overline{W})$  bit. R/W indicates whether the master is writing or reading  $(RD/\overline{W}$  0 = write, RD $\overline{W}$  1 = read). The MAX8588 only supports the SEND BYTE format; therefore, RD/W is required to be 0.

After receiving the proper address, the MAX8588 issues an ACK by pulling SDA low for one clock cycle. The MAX8588 has two user-programmed addresses (Table 3). Address bits A6 through A1 are fixed, while A1 is controlled by SRAD. Connecting SRAD to GND sets  $A1 = 0$ . Connecting ADD to IN sets  $A1 = 1$ .

#### **V3 Output Ramp-Rate Control**

When V3 is dynamically changed with the serial interface, the output voltage changes at a rate controlled by a capacitor (CRAMP) connected from RAMP to ground. The voltage change is a conventional RC exponential described by:

 $Vo(t) = Vo(0) + dV(1 - exp(-t / (100kΩ CRAMP)))$ 

#### **Table 3. Serial Address**





A useful approximation is that it takes approximately 2.2 RC time constants for V3 to move from 10% to 90% of the voltage difference. For  $C_{\text{RAMP}} = 1500pF$ , this time is 330µs. For a 1V to 1.3V change, this equates to 1mV/µs. See the Typical Operating Characteristics for examples of different ramp-rate settings.

The maximum capacitor value that can be used at RAMP is 2200pF. If larger values are used, the V3 ramp rate is still controlled according to the above equation, but when V3 is first activated, POK indicates an "in regulation" condition before V3 reaches its final voltage.

The RAMP pin is effectively the reference for REG3. FB3 regulates to 1.28 times the voltage on RAMP.

#### Design Procedure

#### Setting the Output Voltages

The outputs V1 and V2 have preset output voltages, but can also be adjusted using a resistor voltage-divider. To set V1 to 3.3V, connect FB1 to GND. V2 can be preset to 3.3V or 2.5V. To set V2 to 3.3V, connect FB2 to IN. To set to 2.5V, connect FB2 to GND.

To set V1 or V2 to other than the preset output voltages, connect a resistor voltage-divider from the output voltage to the corresponding FB input. The FB\_ input bias current is less than 100nA, so choose the low-side (FB\_ to-GND) resistor (RL) to be 100kΩ or less. Then calculate the high-side (output-to-FB\_) resistor (RH) using:

 $R_H = R_L$  [( $V_{OUT}$  / 1.25) – 1]

The V3 (VCC\_CORE) output voltage is set from 0.7V to 1.475V in 25mV steps by the I2C serial interface. See the Serial Interface section for details.

Linear regulator V4 provides a fixed 1.3V output voltage. Linear regulator V5 provides a fixed 1.1V output voltage. V4 and V5 voltages are not adjustable.

The output voltage of linear regulator V6 (VCC\_USIM) is set to 0V, 1.8V, 2.5V, or 3.0V by the I<sup>2</sup>C serial interface. See the Serial Interface section for details.

Linear regulator V7 (VCC\_BATT) tracks the voltage at V1 as long as ON1 is high and V1 is in regulation. When ON1 is low or V1 is not in regulation, V7 switches to the backup battery (VBKBT).

#### Inductor Selection

The external components required for the step-down are an inductor, input-and-output filter capacitors, and a compensation RC network.

The MAX8588 step-down converter provides its best efficiency with continuous inductor current. A reasonable inductor value (LIDEAL) is derived from:

$$
LIDEAL = [2(V_{IN}) \times D(1 - D)] / (I_{OUT(MAX)} \times f_{OSC})
$$

This sets the peak-to-peak inductor current at 1/2 the DC inductor current. D is the duty cycle:

$$
D = V_{OUT} / V_{IN}
$$

Given LIDEAL, the peak-to-peak inductor ripple current is 0.5 x  $I_{\text{OUT}}$ . The peak inductor current is 1.25 x IOUT(MAX). Make sure the saturation current of the inductor exceeds the peak inductor current and the rated maximum DC inductor current exceeds the maximum output current (IOUT(MAX)). Inductance values larger than LIDEAL can be used to optimize efficiency or to obtain the maximum possible output current. Larger inductance values accomplish this by supplying a given load current with a lower inductor peak current. Typically, output current and efficiency are improved for inductor values up to about two times LIDEAL. If the inductance is raised too much, however, the inductor size may become too large, or the increased inductor resistance may reduce efficiency more than the gain derived from lower peak current.

Smaller inductance values allow smaller inductor sizes, but also result in larger peak inductor current for a given load. Larger output capacitance may then be needed to suppress the increase in output ripple caused by larger peak current.

#### Capacitor Selection

The input capacitor in a DC-DC converter reduces current peaks drawn from the battery or other input power source and reduces switching noise in the controller. The impedance of the input capacitor at the switching frequency should be less than that of the input source so high-frequency switching currents do not pass through the input source.

The output capacitor keeps output ripple small and ensures control-loop stability. The output capacitor must also have low impedance at the switching frequency. Ceramic, polymer, and tantalum capacitors are suitable, with ceramic exhibiting the lowest ESR and lowest high-frequency impedance.

Output ripple with a ceramic output capacitor is approximately:

 $V_{\text{RIPPLE}} = I_{\text{L(PEAK)}} [1 / (2\pi \times f_{\text{OSC}} \times C_{\text{OUT}})]$ 

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If the capacitor has significant ESR, the output ripple component due to capacitor ESR is:

 $V$ RIPPLE(ESR) =  $I_L$ (PEAK)  $\times$  ESR

Output capacitor specifics are also discussed in the Compensation and Stability section.

#### Compensation and Stability

The relevant characteristics for REG1, REG2, and REG3 compensation are:

- 1) Transconductance (from FB\_ to  $CC_$ ), gm $_{FA}$
- 2) Current-sense amplifier transresistance, R<sub>CS</sub>
- 3) Feedback regulation voltage, VFB (1.25V)
- 4) Step-down output voltage, VOUT, in V
- 5) Output load equivalent resistance,  $R_{LOAD} = V_{OUT} /$ ILOAD

The key steps for step-down compensation are:

- 1) Set the compensation RC zero to cancel the RLOAD COUT pole.
- 2) Set the loop crossover at or below approximately 1/10th the switching frequency.

For example, with  $V_{IN(MAX)} = 5V$ ,  $V_{OUT} = 2.5V$  for REG2, and  $I_{\text{OUT}}$  = 800mA, then R<sub>LOAD</sub> = 3.125Ω. For REG2,  $R_{CS} = 0.75V/A$  and  $g_{mEA} = 87\mu S$ .

Choose the crossover frequency,  $f_C \leq f_{\rm OSC}$  / 10. Choose 100kHz. Then calculate the value of the compensation capacitor, CC:

 $C_C = (VFB / VOUT) \times (RLOAD / RCS) \times (gm / (2\pi \times fc))$  $=$  (1.25 / 2.5) x (3.125 / 0.75) x (87 x 10<sup>-6</sup> / (6.28)  $x$  100,000)) = 289pF

Choose 330pF, the next highest standard value.

Now select the compensation resistor, R<sub>C</sub>, so transientdroop requirements are met. As an example, if 3% transient droop is allowed for the desired load step, the input to the error amplifier moves 0.03 x 1.25V, or 37.5mV. The error-amplifier output drives 37.5mV x gm $EA$ , or  $IEAO = 37.5$ mV x  $87\mu$ S = 3.26 $\mu$ A across R<sub>C</sub> to provide transient gain. Find the value of R<sub>C</sub> that allows the required load-step swing from:

 $RC = RCS \times I_{IND(PK)} / I_{EAO}$ 

where  $I_{IND(PK)}$  is the peak inductor current. In a stepdown DC-DC converter, if LIDEAL is used, output current relates to inductor current by:

$$
I_{IND(PK)} = 1.25 \times I_{OUT}
$$

So for an 800mA output load step with  $V_{IN} = 3.6V$  and  $V$ OUT = 2.5V:

#### **Table 4. Compensation Parameters**



#### **Table 5. Typical Compensation Values**



$$
RC = R_{CS} \times I_{IND(PK)} / I_{EAO} = (0.75 V/A) \times (1.25 \times 0.8A) / 3.26 \mu A = 230 k \Omega
$$

We choose 240kΩ. Note that the inductor does not limit the response in this case since it can ramp at  $(V_{1N} V_{\text{OUT}}$  / L, or (3.6 - 2.5) / 3.3 $\mu$ H = 242mA/ $\mu$ s.

The output-filter capacitor is then selected so that the COUT RLOAD pole cancels the RC CC zero:

$$
C_{OUT} \times R_{LOAD} = R_C \times C_C
$$

For the example:

$$
R_{LOAD} = V_{OUTX} I_{LOAD} = 2.5V / 0.8A = 3.125\Omega
$$

$$
C_{OUT} = RC \times CC / R_{LOAD} = 240k\Omega \times 330pF / 3.125\Omega = 25\mu F
$$

We choose 22µF.

Recalculate R<sub>C</sub> using the selected C<sub>OUT</sub>.

$$
RC = COUT \times RLOAD / CC = 208k\Omega
$$

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Figure 6. MAX8588 Typical Applications Circuit

*IVI A* XI*IV*I

MAX8588

Note that the pole cancellation does not have to be exact.  $R_C \times C_C$  need only be within 0.75 to 1.25 times RLOAD x COUT. This provides flexibility in component selection.

If the output-filter capacitor has significant ESR, a zero occurs at:

$$
Z_{ESR} = 1 / (2\pi \times C_{OUT} \times R_{ESR})
$$

If  $Z_{ESR}$  > f<sub>C</sub>, it can be ignored, as is typically the case with ceramic or polymer output capacitors. If ZESR is less than fc, it should be cancelled with a pole set by capacitor C<sub>P</sub> connected from CC\_ to GND:

 $C_P = C_{OUT}$  Resr / Rc

If  $C_P$  is calculated to be  $\lt$  10pF, it can be omitted.

#### **Optimizing Transient Response**

In applications that require load-transient response to be optimized in favor of minimum component values, increase the output-filter capacitor to increase the R in the compensation RC. From the equations in the previous section, doubling the output cap allows a doubling of the compensation R, which then doubles the transient gain.

#### Applications Information

#### Extending the Maximum Core Voltage Range

The V3 output can be serially programmed to supply from 0.7V to 1.475V in 25mV steps. In some cases, a higher CPU core voltage may be desired. The V3 voltage range can be increased by adding two resistors as shown in Figure 7.

R24 and R25 add a small amount of gain. They are set so that an internally programmed value of 1.475V results in a higher actual output at V3. The resistors shown in Figure 1 set a maximum output of 1.55V, 1.6V, or 1.65V. All output steps are shifted and the step size is also slightly increased.

The output voltage for each programmed step of V3 in Figure 7 is:

V3 = V3PROG + (R24[(V3PROG / R25) + (V3PROG / 185,500)])

where V3 is the actual output voltage, V3PROG is the original programmed voltage from the "OUTPUT (V)" column in Table 2, and 185,500 is the internal resistance of the FB3 pin.



Figure 7. Addition of R24 and R25 increases maximum core voltage. The values shown raise the maximum core from 1.475V to 1.55V.

#### Backup-Battery and V7 Configurations

The MAX8588 includes a backup-battery connection, BKBT, and an output, V7. These can be utilized in different ways for various system configurations.

#### **Primary Backup Battery**

A connection with a primary (nonrechargeable) lithium coin cell is shown in Figure 6. The lithium cell connects to BKBT directly. V7 powers the CPU VCC\_BATT from either V1 (if enabled) or the backup battery. It is assumed whenever the main battery is good, V1 is on (either with its DC-DC converter or sleep LDO) to supply V7.

#### **No Backup Battery (or Alternate Backup)**

If no backup battery is used, or if an alternate backup and VCC\_BATT scheme is used that does not use the MAX8588, then BKBT should be biased from IN with a small silicon diode (1N4148 or similar, as in Figure 8). BKBT must still be powered when no backup battery is used because  $\overline{DBO}$ ,  $\overline{RSO}$ , and POK require this supply to function. If BKBT is not powered, these outputs do not function and are high impedance.



Figure 8. BKBT connection when no backup battery is used, or if an alternate backup scheme, not involving the MAX8588, is used.



Figure 9. A 1-cell rechargeable Li+ battery provides more backup power when a primary cell is insufficient. The cell is charged to 3.3V when V1 is active. Alternately, the battery can be charged from IN if the voltages are appropriate for the cell type.



Figure 10. A 1-cell NiMH battery can provide backup by boosting with a low-power DC-DC converter. A series resistor-diode trickle charges the battery when the main power is on.

#### **Rechargeable Li+ Backup Battery**

If more backup power is needed and a primary cell has inadequate capacity, a rechargeable lithium cell can be accommodated as shown in Figure 9. A series resistor and diode charge the cell when the 3.3V V1 supply is active. In addition to biasing V7, the rechargeable battery may be required to also power other supplies.

#### **Rechargeable NiMH Backup Battery**

In some systems, a NiMH battery may be desired for backup. Usually this requires multiple cells because the typical NiMH cell voltage is only 1.2V. By adding a small DC-DC converter (MAX1724), the low-battery voltage is boosted to 3V to bias BKBT (Figure 10). The DC-DC converter's low operating current (1.5µA typ) allows it to remain on constantly so the 3V BKBT bias is always present. A resistor and diode trickle charge the NiMH cell when the main power is present.

#### PC Board Layout and Routing

Good PC board layout is important to achieve optimal performance. Conductors carrying discontinuous currents and any high-current path should be made as short and wide as possible. A separate low-noise ground plane containing the reference and signal grounds should connect to the power-ground plane at only one point to minimize the effects of power-ground currents. Typically, the ground planes are best joined right at the IC.

Keep the voltage feedback network very close to the IC, preferably within 0.2in (5mm) of the FB\_ pin. Nodes with high dV/dt (switching nodes) should be kept as small as possible and should be routed away from high-impedance nodes such as FB\_.



#### Pin Configuration Chip Information

TRANSISTOR COUNT: 13,958 PROCESS: BiCMOS

#### Package Information

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)



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#### Package Information (continued)

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)





NOTES:

1. DIMENSIONING & TOLERANCING CONFORM TO ASME Y14.5M-1994.

2. ALL DIMENSIONS ARE IN MILLIMETERS. ANGLES ARE IN DEGREES.

3. N IS THE TOTAL NUMBER OF TERMINALS.

A THE TERMINAL #1 IDENTIFIER AND TERMINAL NUMBERING CONVENTION SHALL CONFORM TO JESD 95-1 SPP-012. DETAILS OF TERMINAL #1 IDENTIFIER ARE OPTIONAL, BUT MUST BE LOCATED WITHIN THE ZONE INDICATED. THE TERMINAL #1 IDENTIFIER MAY BE EITHER A MOLD OR MARKED FEATURE.

6. DIMENSION b APPLIES TO METALLIZED TERMINAL AND IS MEASURED BETWEEN 0.25 mm AND 0.30 mm FROM TERMINAL TIP.

6. ND AND NE REFER TO THE NUMBER OF TERMINALS ON EACH D AND E SIDE RESPECTIVELY.

7. DEPOPULATION IS POSSIBLE IN A SYMMETRICAL FASHION.

- **8.** COPLANARITY APPLIES TO THE EXPOSED HEAT SINK SLUG AS WELL AS THE TERMINALS.
- 9. DRAWING CONFORMS TO JEDEC MO220, EXCEPT FOR 0.4mm LEAD PITCH PACKAGE T4866-1.
- 10. WARPAGE SHALL NOT EXCEED 0.10 mm.

**DALLAS // /XI//** ETARY INFORMATION PACKAGE OUTLINE 36, 40, 48L THIN QFN, 6x6x0.8mm OL NO. 21-0141 E  $\frac{2}{2}$ 

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