**FAN7340 LED Backlight Driving Boost Switch** 

# **Features**

- Single-Channel Boost LED Switch
- Internal Power MOSFET for PWM Dimming:  $R_{DS(on)} = 3.4 \Omega$  at V<sub>GS</sub>=10 V, BV<sub>DSS</sub>=400 V
- Current Mode PWM Control
- Internal Programmable Slope Compensation
- Wide Supply Voltage Range: 10 V to 35 V
- LED Current Regulation: ±1%
- Programmable Switching Frequency
- Analog and PWM Dimming
- Wide Dimming Ratio: On Time=10 µs to DC
- **Cycle-by-Cycle Current Limiting**
- Thermal Shutdown: 150**°**C
- Open-LED Protection (OLP)
- Over-Voltage Protection (OVP)
- Over-Current Protection (OCP)
- Error Flag Generation (for External Load Switch)
- Internal Soft-Start
- 16-Lead SOIC Package

# **Applications**

- LED Backlight for LCD TV
- LED Backlight for LCD Monitor
- LED Lighting

# **Description**

The FAN7340 is a single-channel boost controller that integrates an N-channel power MOSFET for PWM dimming using Fairchild's proprietary planar Doublediffused MOS (DMOS) technology.

The IC operates as a constant-current source for driving high-current LEDs.

It uses Current Mode control with programmable slope compensation to prevent subharmonic oscillation. The IC provides protections including: open-LED protection, over-voltage protection, and direct-short protection for high system reliability.

The IC internally generates a FAULT signal with delay if an abnormal LED string condition occurs. PWM dimming and analog dimming functions can be implemented independently. Internal soft-start prevents inrush current flowing into output capacitor at startup.

# **Ordering Information**







July 2013



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**— LED Backlight Driving Boost Switch** 

TAN7340 - LED Backlight Driving Boost Switch



# <span id="page-2-0"></span>**Pin Definitions**



#### **Note:**

1. Pin 11 is a "No Connect" pin (not shown i[n Figure 2\)](#page-2-0).

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# **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.  $T_A = 25^\circ \text{C}$  unless otherwise specified.



**Notes:**<br>2. The

<span id="page-3-0"></span>2. Thermal resistance test board; size 76.2 mm x 114.3 mm x 1.6 mm (1S0P); JEDEC standard: JESD51-2, JESD51- 3.

<span id="page-3-1"></span>3. Assume no ambient airflow.

# **Pin Breakdown Voltage**





## **Electrical Characteristics**

For typical values, T<sub>A</sub> = 25°C and V<sub>CC</sub> = 15 V unless otherwise specified. Specifications to -40°C ~ 125°C are guaranteed by design based on final characterization results .



*Continued on the following page…*

## **Electrical Characteristics (Continued)**

For typical values, T<sub>A</sub> = 25°C and V<sub>CC</sub> = 15 V, unless otherwise specified. Specifications to -25°C  $\sim$  85°C are guaranteed by design based on final characterization results .



<span id="page-5-0"></span>4. These parameters, although guaranteed, are not tested in production.





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#### **Functional Description**

The FAN7340 operates as a constant-current source for driving high-current LEDs. It uses Current-Mode control with programmable slope compensation to prevent subharmonic oscillation.

The IC provides protections such as open-LED protection, over-voltage protection, and over-current protection for improved system reliability. The IC internally generates a FAULT OUT signal with a delay in case an abnormal LED string condition occurs. PWM dimming and analog dimming functions can be implemented independently. Internal soft-start prevents inrush current flowing into output capacitor at startup. Circuit operation is explained in the following sections.

#### **VCC Under-Voltage Lockout (UVLO)**

An internal regulator provides the regulated 5 V used to power the IC. The Under-Voltage Lockout (UVLO) turns off the IC in the event of the [voltage](http://en.wikipedia.org/wiki/Voltage) dropping below the specific threshold level. The UVLO circuit inhibits powering the IC until a voltage reference is established, up to predetermined threshold level.

#### **Enable**

Applying voltage higher than 1.22 V (typical) to the ENA pin enables the IC. Applying voltage lower than 1.15 V (typical) to the ENA pin disables the IC. If ENA pin voltage is higher than 1.22 V (typical) and  $V_{CC}$  is higher than 9.0 V (typical.), the IC starts to supply 5 V reference voltage from V<sub>cc</sub>.

#### **Oscillator (Boost Switching Frequency)**

Boost switching frequency is programmed by the value of the resistor connected from the RT pin to ground. RT pin voltage is set to 2 V. The current through the RT pin resistor determines boost switching frequency according to formula:

$$
f_{\rm OSC} = \frac{1}{(46.5 \times RT \text{ [k\Omega]} + 350) \times 10^{-6}} \text{ [kHz]} \tag{1}
$$

#### **Soft-Start Function at Startup**

During initial startup, the switching device can be damaged due to the over-current coming from the input line by the negative control. This can result in the initial overshoot of the LED current. Therefore, during initial startup, the soft-start control gradually increases the duty cycle so that the output voltage can rise smoothly to control inrush current and overshoot.

FAN7340 adapts the soft-start function in the boost converter stage. During soft-start period, boost switch turn-on duty is limited by clamped CMP voltage. The soft-start period is dependent on boost switching frequency, which is decided by the RT resistor (Equation [\(1\)\)](#page-10-0). Soft-start period is set to be cumulative time when the BDIM (PWM dimming) signal is HIGH:

$$
T_{SS} = 600 / f_{OSC} \text{[sec]}
$$
 (2)



**Figure 26. Soft-Start Waveforms** 

#### **LED Current Setting**

During the boost converter operating periods, the output LED current can be set by equation:

$$
I_{LED} = \frac{ADIM(V)}{R_{SENSE} + 60m\Omega}
$$
 (3)

where ADIM(V) is

ADIM pin applied voltage and, R<sub>SENSE</sub> is the sensing resistor value. An additional 60 mΩ comes from an internal wire bonding resistor. To calculate LED current precisely, consider the wire bonding resistor.

#### **Analog Dimming and PWM Dimming**

Analog dimming is achieved by varying the voltage level at the ADIM pin. This can be implemented either with a potentiometer from the VREF pin or from an external voltage source and a resistor divider circuit. The ADIM voltage level is adjusted to be the same as the feedback level  $(V_{\text{SENSE}})$ . A  $V_{\text{ADIM}}$  range from 0.3 V to 3 V is recommended.

<span id="page-10-0"></span>PWM dimming (BDIM) helps achieve a fast PWM dimming response in spite of the shortcomings of the boost converter. The PWM dimming signal controls three nodes in the IC; gate signal to the switching FET, gate signal to the dimming FET, and output connection of the trans-conductance amplifier. When the PWM dimming signal is HIGH, the gates of the switching FET and dimming FET are enabled. At the same time, the output of the transconductance ap-amp is connected to the compensation network. This allows the boost converter to operate normally.

#### **Dynamic Contrast Ratio**

The Dynamic Contrast Ratio (DCR) means the maximum contrast ratio achievable by adjusting the amount of light (dimming) of the screen instantaneously using the backlight during the extremely short period of time. FAN7340 can normally drive the LED backlight under 0.1% dimming duty cycle at 200 Hz dimming frequency. Even operating at 5 µs-dimming FET turn-on time and extremely low dimming duty, FAN7340 can operate LEDs with normal peak current level.

## **Internal Dimming MOSFET**

A dimming MOSFET (400 V N-channel MOSFET; such as FDD3N40) is incorporated in the FAN7340. The power transistor is produced using Fairchild's proprietary, planar stripe, DMOS technology. This advanced technology is tailored to minimize on-state resistance (R<sub>DS(on)</sub>=3.4  $\Omega$ ), to provide superior switching performance. This device is suited for high-efficiency SMPS and shows desirable thermal characteristic during operation. To prevent initial LED current overshoot at low V<sub>ADIM</sub> levels, gate resistance of the internal dimming FET is designed as  $5 \text{ k}\Omega$  experimentally.

## **Feedback Loop Compensation**

Stable closed-loop control can be accomplished by connecting a compensation network between COMP and GND. The compensation needed to stabilize the converter can be either a Type-I circuit (a simple integrator) or a Type-II circuit (and integrator with and additional pole-zero pair). The type of the compensation circuit required is dependent on the phase of the power stage at the crossover frequency.

FAN7340 adopts a Type-II compensator circuit.

## **Programmed Current Control**

FAN7340 uses a Current-Mode control method. Current-Mode control loops: an outer feedback loop that senses output voltage (current) and delivers a DC control voltage to an inner feedback loop, which senses the peak current of the inductor and keeps it constant on a pulse-by-pulse basis. One of the advantages of the Current-Mode control is line/load regulation, which is corrected instantaneously against line voltage changes without the delay of an error amplifier.

## **Programmable Slope Compensation**

When the power converter operates in Continuous Conduction Mode (CCM), the current programmed controller is inherently unstable when duty is larger than 50%, regardless of the converter topology. The FAN7340 uses a Peak-Current-Mode control scheme with programmable slope compensation and includes an internal transconductance amplifier to accurately control the output current over all line and load conditions.

An internal R<sub>slope</sub> resistor (5 kΩ) connected to sensing resistor  $R<sub>S</sub>$  and an external resistor  $R<sub>1</sub>$  can control the slope of  $V_{SC}$  for the slope compensation. Although the normal operating mode of the power converter is DCM, the boost converter operates in CCM in the case of rapid LED current increase. As a result, slope compensation circuit is an important feature.

The value of an external series resistor  $(R<sub>1</sub>)$  can be programmed by the user. In normal DCM operation, 5 k Ω is recommended.



**Figure 27. Slope Compensation Block Diagram** 

## **Cycle-by-Cycle Over-Current Protection**

In boost topology, the switch can be damaged in abnormal conditions (inductor short, diode short, output short). It is always necessary to sense the switch current to protect against over-current failures. Switch failures due to excessive current can be prevented by limiting  $I_d$ .



**Figure 28. Cycle-by-Cycle OCP Circuit** 

When the voltage drops at  $R_1$  and  $R_5$  exceed a threshold of approximately 0.5 V, the power MOSFET over-current function is triggered after minimum turn-on time or LEB time (300 ns).

The peak voltage level at CS terminal:

$$
V_{cs,peak} = 45\mu \times (R_1 + R_s) \times DT_s + i_d \times R_s \tag{4}
$$

Choose the boost switch current-sensing resistor  $(R_{CS})$ :

$$
R_{CS} \ge \frac{0.25}{i_{L,peak}}\tag{5}
$$

# **Open-LED Protection (OLP)**

After the first PWM dimming-HIGH signal, the feedback sensing resistor (RSENSE) starts sensing the LED current. If the feedback voltage of the SENSE pin drops below 0.2 V, the OLP triggers to generate an error flag signal. Because OLP can be detected only in PWM dimming-HIGH; if OLP detecting time is over 5 μs, PWM dimming signal is pulled HIGH internally regardless of external dimming signal. If OLP signal continues over blanking time, an error flag signal is triggered.

OLP blanking time is dependent on boost switch frequency per Equation [\(6\).](#page-11-0) FAULT OUT signal is made through the FO pin, which needs to be connected 5 V reference voltage through a pull-up resistor. In normal operation, FO pin voltage is pulled down to ground. In OLP condition, FO pin voltage is pulled HIGH.

<span id="page-11-0"></span>
$$
t_{\mathbf{d}.\mathbf{olp}} = 8192 / f_{\text{OSC}} \text{ [sec]}
$$
 (6)

In system operation, OLP is triggered in only direct-short condition. Direct short means that some point of the LED string is shorted to set ground. In direct-short condition, the boost controller cannot control the LED current and a large current flows into the LED string directly from input power. To prevent this abnormal condition, the FO signal is used to turn off input power or the total system. FO signal is only triggered in OLP condition.



In LED open load condition, OVP is triggered ahead of OLP.

## **Over-Voltage Protection (OVP)**

Over-voltage protection is triggered when the voltage of the external output voltage trip point meets 3 V. After triggering OVP, the dimming switch and boost switch are turned off. The protection signal is recovered when the output voltage divider is below 2.9 V.



# **LED Over-Current Protection (OCP)**

The primary purpose of the over-current protection function is to protect the internal dimming MOSFET from excessive current. The OCP is triggered when the feedback voltage meets the clamping level  $(1.4 V \sim 4 V)$ of the ADIM voltage x4. At 1 μs delay after the OCP is triggered, the IC turns off both the boost FET and dimming FET and restarts the gate signal every tan automatically.  $t_{AR}$  can be calculated as:

$$
\mathbf{t}_{\mathbf{AR}} = 128 / f_{\mathbf{OSC}} \,\mathrm{[sec]}
$$
 (7)

- 1. When  $V_{ADIM}=0.3$  V ( $V_{ADIM}x4=1.2$  V).
- 2. OCP threshold level is set to 1.4 V.
- 3. OCP is triggered at feedback voltage level = 1.4 V.



#### **Figure 32. OCP Waveforms at V<sub>ADIM</sub>=0.3 V**

- 1. When VADIM=0.8 V (VADIM x4=3.2 V).
- 2. OCP threshold level is set to 3.2 V.
- 3. OCP is triggered at  $V_{\text{SENSE}} = 3.2 \text{ V}$ .



#### **Figure 33. OCP Waveforms at VADIM=0.8 V**

- 1. When V<sub>ADIM</sub>=1.2 V (V<sub>ADIM</sub> x4=4.8 V).
- 2. OCP threshold level is set to 4.0 V.
- 3. OCP is triggered at  $V_{\text{SENSE}} = 4.0 \text{ V}$ .







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