April 2012



# **FAN53523 — Digitally-Programmable 3MHz, USB-Compliant Power Management Subsystem**

## **Features**

- **Programmable USB-Compliant Input Current Limit**
- 1A Output System Buck Regulator
- System Regulator has Priority Over RF Power
- 7V V<sub>BUS</sub> Standoff
- 3MHz Fixed-Frequency Operation
- Voltage Limiting for Bulk Capacitors
- Reverse Blocking when  $V_{BUS}$  is Below Bulk Cap. Voltage
- PFM Mode for High Light-Load Efficiency
- Output Discharge Function when Disabled
- Low Ripple Light-Load PFM Mode
- 95µA Typical Quiescent Current in PFM Mode
- Internal Soft-Start
- Input Under-Voltage Lockout (UVLO)
- Thermal Shutdown and Overload Protection
- **Low-Power Suspend and Test Modes**
- Host Enable and Interrupt Functions
- 16-Bump, 0.4mm Pitch, WLCSP

## **Applications**

- USB Data Cards
- USB-to-Battery Power Replacement

## **Description**

The FAN53523 is a step-down switching voltage regulator that delivers an adjustable output from a 3.7V to 5.5V USB input voltage. The IC includes a programmable input current-limit circuit to prevent overloading the USB source ( $V_{\text{BUS}}$ ). The IC also features a voltage and current limiting input switch to charge bulk capacitors for an RF Power Amplifier (RFPA) power supply. The voltage limit is programmable in 140mV steps to allow optimal derating. The total input current is limited by an external sense resistor. The buck regulator is given priority when drawing power from  $V_{\text{BUS}}$ .

The buck regulator features a proprietary architecture with synchronous rectification and is capable of delivering 1A at over 90% efficiency, while maintaining a very high efficiency of over 80% at load currents as low as 2mA. The regulator is digitally programmable to conserve power, but still provides adequate power to the RFPA that may be attached through the current-limit switch at the buck regulator output. The regulator operates at a nominal fixed frequency of 3MHz, which reduces the value of the external components to as low as 1µH and as low as 10µF for the output capacitor. Additional output capacitance can be added to improve regulation during load transients without affecting stability. Inductance up to 1.2µH may be used with additional output capacitance.

At moderate and light loads, Pulse Frequency Modulation (PFM) is used to operate the device in Power-Save Mode with a typical quiescent current of 95µA. Even with such a low quiescent current, the IC exhibits excellent transient response during large load swings. At higher loads, the system automatically switches to fixed-frequency control, operating at 3MHz. In Shutdown Mode, supply current drops below 1µA, reducing power consumption. PFM Mode can be disabled if constant frequency is desired.

The VBUS input current limit  $(I_{\text{BUS}})$  is digitally programmable. Large capacitors can be used to store energy for high-current transient loads, such as GSM pulses at the output of the VBUS current limit switch.

The IC includes diagnostics that alert the host processor of changes in bulk capacitor charge condition and buck status.

The FAN53523 is available in 16-bump, 0.4mm pitch WLCSP.

## **Ordering Information**





**Figure 1. Typical Application using Bulk Capacitors at PMID to Provide RFPA Power (Bold Lines Indicate Power Path)** 







## **Pin Definitions**



## **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.



**Note:** 

1. Lesser of  $6.5V$  or  $V_{\text{PMID}} + 0.3V$ .

## **Recommended Operating Conditions**

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to absolute maximum ratings.



## **Thermal Properties**



**Note:** 

2. Junction-to-ambient thermal resistance is a function of application and board layout. This data is measured with two-layer 2s2p boards in accordance to JESD51- JEDEC standard. Special attention must be paid not to exceed junction temperature  $T_{J(max)}$  at a given ambient temperate  $T_{A}$ .

**FAN53523** 

## **Electrical Specifications**

Unless otherwise specified: circuit of Figure 1, recommended operating temperature range for  $T_J$  and  $T_A$ ,  $V_{BUS}$  = 5.0V, AUTO Mode, typical values are for  $T_J = 25^{\circ}C$ .



*Continued on the following page…* 

## **Electrical Specifications (Continued)**

Unless otherwise specified: circuit of Figure 1, recommended operating temperature range for  $T_J$  and  $T_A$ ,  $V_{BUS}$  = 5.0, typical values are for  $T_J = 25^{\circ}$ C.



## **I <sup>2</sup>C Timing Specifications**

Guaranteed by design.





# **Typical Characteristics**

Unless otherwise noted, circuit of Figure 1 with component values of Table 1 V<sub>BUS</sub>= 5.0V, AUTO Mode, V<sub>OUT</sub>=3.52V.



## **Typical Characteristics** (Continued) Unless otherwise noted, circuit of Figure 1 with component values of Table 1 V<sub>BUS</sub>= 5.0V, AUTO Mode, V<sub>OUT</sub>=3.52V. Tek Stop











![](_page_9_Figure_7.jpeg)

**(Ch1 HIGH=5.3V, Ch1 LOW=4.7V)** 

![](_page_9_Figure_9.jpeg)

![](_page_9_Figure_10.jpeg)

![](_page_9_Figure_11.jpeg)

![](_page_9_Figure_12.jpeg)

**FAN53523 FAN53523 ó Digitally-Programmable 3MHz, 1A USB-Compliant Power Management Subsystem**  Digitally-Programmable 3MHz, 1A USB-Compliant Power Management Subsystem

-40C +25C +85C

#### **Typical Characteristics** (Continued) Unless otherwise noted, circuit of Figure 1 with component values of Table 1 V<sub>BUS</sub>= 5.0V, AUTO Mode, V<sub>OUT</sub>=3.52V. 200 140 180 120 Input Current (LA) **Input Current (A)** Input Current (µA) **Input Current (A)** 160 100 80 140  $-40c$  $+25C$  $+85C$  $120 +$ <br>4.0  $60 +$ <br>4.0 4.0 4.5 5.0 5.5 6.0 4.0 4.5 5.0 5.5 6.0 **Input Voltage VBUS (V) Input Voltage VBUS (V) Figure 17. Quiescent Current, Not Suspend R1[6]=0, Figure 18. Quiescent Current, Suspend R1[6]=1, No Load V<sub>OUT</sub> or PMID No Load V<sub>OUT</sub> or PMID** The following scope shots were taken with 1.5m length USB cable, C<sub>BULK</sub> (on PMID)=3x470μF, 100mΩ Tantalum. Tek Prevu Tek Stop Trig? **I** BUS **LBUS**

Ch<sub>2</sub> High<br>4.97 V

Ch4 Mean<br>3.51 V

Ch1 High<br>4.80 V

![](_page_10_Figure_2.jpeg)

**Ghi** 2.00 V %Ch2 100mV %M 100ms A Ch1  $f$  1.16 V<br>Ch3 50.0mAΩ%Ch4 100mV Ω%

![](_page_10_Figure_3.jpeg)

**Figure 20. 2A GSM Pulse on PMID (577µs on, 217Hz, 5µs Edge) 500mA IBUSLIM, VLIM=4.68V, 3.52VOUT, 50Ω Load** 

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**VBUS** 

**VOUT** 

**PMID** 

## **Operation Description**

The FAN53523 combines a buck regulator that delivers an adjustable output from an input voltage supply of 4V to 6V, with USB protection and a current-limit switch. The current for both the buck regulator and the current-limiting switch (Q3 in Figure 1) pass through a current-sense resistor  $(R_{\text{SENSE}})$ . The voltage across the current-sense resistor controls the currentlimiting switch, limiting  $C_{\text{BULK}}$  charge current. The system power, therefore, has priority when using a current limited input supply (USB).

Using a proprietary architecture with synchronous rectification, the buck is capable of delivering 1A at over 90% efficiency. The regulator operates at a nominal frequency of 3MHz when in PWM Mode, which reduces the value of the external components to  $1\mu$ H for the output inductor and  $10\mu$ F for the output capacitor. High efficiency is maintained at light load with single-pulse PFM Mode.

The USB switch (Q3) limits the input current from the USB bus  $(I_{\text{BUS}})$  to charge bulk storage capacitors  $(C_{\text{BULK}})$ , which provide the high power required for Global System for Mobile Communications (GSM) and Long-Term Evolution (LTE) data transmission in USB data cards. The USB switch limits the maximum voltage ( $V_{LIM}$ ) on  $C_{BULK}$ , which allows the use of a 6.3V capacitor with voltage derating.  $V_{LIM}$  can be programmed in 140mV steps from 3V to 4.96V.

To limit total input current, an external sense resistor, RSENSE, is used. The buck regulator's input supply and the input to the current-limit switch are both taken from the PVDD side of the sense resistor. This gives the buck regulator priority over the bulk capacitor charging, ensuring that system power is not interrupted due to high-current demand from the RFPA.

### **Buck Control Scheme**

The FAN53523 uses a proprietary non-linear, fixed-frequency PWM modulator to deliver a fast load transient response, while maintaining a constant switching frequency over a wide range of operating conditions. Regulator performance is independent of the output capacitor Equivalent Series Resistance (ESR), allowing for the use of ceramic output capacitors. Although this type of operation normally results in a switching frequency that varies with input voltage and load current, an internal frequency loop holds the switching frequency constant over a large range of input voltages and load currents.

For very light loads, the FAN53523 operates in Discontinuous Current Mode (DCM) with single-pulse Pulse Frequency Modulation (PFM), which produces low output ripple compared with other PFM architectures. Transition between PWM and PFM is seamless, with a glitch of less than 18mV at  $V<sub>OUT</sub>$  during the transition between DCM and CCM Modes.

### **Startup**

Initially, the INT pin is LOW. When  $V_{\text{BUS}}$  rises above 4.4V, the buck regulator begins a soft-start sequence. When  $V_{\text{OUT}}$  has risen to its default value (3.52V), INT rises to indicate that power to the system is valid. In this way, the INT pin functions as a PGOOD pin that can be used to drive the host processor's enable pin. The system processor initializes and can then program the IC.

## **Programmability**

Power-on defaults for all programmable values are listed in **bold** characters in Table 2.

### **IBUS: Input Current Limit**

These bits establish the input current limit. This current is the sum of the current through Q3 and the input current to the buck regulator.

![](_page_11_Picture_418.jpeg)

![](_page_11_Picture_419.jpeg)

## **VLIM: PMID Voltage Limit**

To accommodate voltage derating of the typically tantalum bulk capacitors  $(C_{\text{BULK}})$ , the IC limits the voltage on PMID to a programmable value between 3.0V and 4.96V. If the VLIM bits are set to 1111, voltage limiting is disabled, which allows C<sub>BULK</sub> to rise to PVDD under no load.

![](_page_11_Picture_420.jpeg)

![](_page_11_Picture_421.jpeg)

## V<sub>SEL</sub>: V<sub>OUT</sub> Buck Output Voltage

The buck output voltage is programmable in 60mV steps from 3.1V to 4.0V.  $V_{\text{OUT}}$  may be changed "on the fly" by writing to the VSEL bit.

![](_page_12_Picture_189.jpeg)

#### Table 4.  $V_{OUT}$  Programming

## **V<sub>SEL</sub> Transitions**

The slew rate of a positive  $V_{\text{SEL}}$  is 2.4V/ms.

For positive V<sub>SEL</sub> transitions, the PGOOD bit goes LOW when the  $V_{\text{SEL}}$  value changes. When  $V_{\text{OUT}}$  has settled to its new value, PGOOD is set and INT pulses.

Negative V<sub>SEL</sub> transitions are controlled by the load current. When the V<sub>SEL</sub> value is lowered by the host, the PGOOD bit goes LOW, the buck regulator reference is lowered, and synchronous rectification is disabled until  $V_{OUT}$  reaches the  $V_{\rm SFI}$  value. At that point, synchronous rectification is enabled, PGOOD is set, and INT pulses.

### **Suspend Mode**

When the SUSPEND bit is set, the buck regulator continues to operate. The CC/CV limiter is powered down to reduce input current draw; however, a low-current precharge regulator keeps PMID charged at the VLIM setting.

## **Test Mode**

The TEST bit enables a special test mode to facilitate system test and characterization. The intention of the test mode is to allow a power supply to control PMID directly by applying a power source at VBUS. When TEST = 1:

- 1. The buck regulator operates normally.
- 2. Q3 operates as a switch, with its gate at GND.
- 3.  $V_{UVLO}$  for  $V_{BUS}$  falling is set to 2.7V to allow PMID to be driven to a lower voltage without the IC disabling the buck.

## **Status and Monitoring**

The IC provides extensive monitoring for PMID and VOUT. The monitoring functions are provided in the STAT0 registers and are described below.

## **PMID Charging Status**

The status of the CC/CV limiter that controls Q3 is reported on the CC and CV bits during normal operation. The CV bit is set when the VLIM loop is controlling PMID and Q3 is not in a current-limit condition. Status of this bit is latched in to the I<sup>2</sup>C registers when a read commences. The CC bit is set when current limit condition is entered. Status of the CC bit stays latched until reset by an  $I^2C$  read. For CV flag to rise, the current-limit loop must be released for at least 256µs.

## **INT Pin**

The open-drain INT pin initially is LOW. When  $V_{OUT}$  is in regulation, INT goes HIGH. When the DIS INT bit is cleared, INT pulses LOW for 125µs whenever a status bit changes state, except as noted below.

INT pulses when the I<sub>BUS</sub> loop either begins limiting current (CC Mode entry) or stops limiting current (CV Mode entry) through Q3. Read transaction for STAT0 register causes a single INT pulse to be issued

INT pulsing is inhibited by default. The host processor must clear the DIS INT bit after system startup is complete to receive interrupts. This facilitates use of the INT pin for a PGOOD pin function (host enable) without the use of external low-pass filtering on the INT pin.

If INT pulsing is not inhibited and INT is used as both interrupt and enable functions, an external low-pass filter to the enable pin is needed, as shown in Figure 21.

![](_page_12_Figure_25.jpeg)

![](_page_12_Figure_26.jpeg)

### **Thermal Regulation**

A dedicated thermal regulation circuit monitors the die temperature at Q3 and limits the thermal dissipation of the device by turning off the PMID path when die temperature exceeds 120°C.

The die temperature is sampled every 4ms. If the detected temperature exceeds 120°C for two consequent sampling periods, the PMID path is turned off for 8ms and a fault is indicated by pulsing INT LOW (T120 interrupt). The T120 interrupt can be disabled by setting the DIS\_T120 bit.

The thermal state of the device can be read back from the OT bit in the STAT0 register (STAT0[0]). The OT bit can be used in conjunction with the T120 interrupt to allow the host to ensure that the buck regulator does not shutdown due to the die continuing to heat.

## **Buck Regulator Details**

#### **Soft-Start**

The buck regulator uses output slew rate limiting to limit inrush current. If  $V_{\text{OUT}}$  fails to increase within 1ms from the beginning of soft-start, the regulator shuts down and waits 3.3ms before attempting a restart. If the regulator is at its current limit for more than  $\sim$ 100 $\mu$ s, the regulator shuts down before restarting 3.3ms later. This limits the duty cycle of full output current into a soft-start to about 3%.

$$
COUNT_{MAX} \approx \left(1A - \overline{I_{LOAD}}\right) \bullet \frac{2000 \,\mu}{V_{OUT}} \tag{1}
$$

Synchronous rectification is inhibited during soft-start, allowing the IC to start into a pre-charged load.

### **Under-Voltage Lockout**

The under-voltage lockout keeps the buck from operating until  $V_{\text{BUS}}$  rises above the V<sub>UVLO</sub> threshold (3.7V). This ensures no misbehavior of the regulator during startup or shutdown.

## **VBUS Over-Voltage Protection (OVP)**

When  $V_{\text{BUS}}$  exceeds ~5.7V, the IC stops switching and Q3 is turned off.  $V_{BUS}$  must return below 5.5V for the IC to restart.

## **Current Limiting**

A heavy load or short circuit on the output causes the current in the inductor to increase until a maximum current threshold is reached in the high-side switch. Upon reaching this point, the high-side switch turns off, preventing high currents from causing damage. A series of 16 consecutive PWM cycles in current limit causes the regulator to shut down and stay off for about 3.3ms before attempting a restart.

In the event of a short circuit, the soft-start circuit attempts to restart at 60% of normal current limit and produces an overcurrent fault after  $\sim$ 300 $\mu$ s, which results in a duty cycle of less than 10% providing current into a short.

## **Thermal Shutdown**

When the die temperature increases, due to a high load condition and/or a high ambient temperature, output switching is disabled until the temperature on the die has fallen sufficiently. The junction temperature at which the thermal shutdown activates is nominally 150°C with a 20°C hysteresis.

#### **Minimum Off-Time Effect on Switching Frequency**

 $t_{ON(MIN)}$  and  $t_{OFF(MIN)}$  are both 45ns. This imposes constraints

on the maximum *IN OUT V*  $V_{OUT}$  that the FAN53523 can provide while

maintaining a fixed switching frequency in PWM Mode.

The switching frequency drops when the regulator cannot provide sufficient duty cycle at 3Mhz to maintain regulation.

 $-I_{OUT}$   $\bullet$   $R_{ON}$   $-$ 

 $U_N - I_{OUT} \bullet R_{ON} - V_{OUT}$ 

The calculation for switching frequency is:

$$
f_{SW} = \min\left(\frac{1}{t_{SW(MAX)}}, \frac{1}{333.3ns}\right)
$$

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 $=45ns \cdot \left(1+\frac{V_{OUT}+I_{OUT}}{I_{OUT}}\right)$ 

 $S_{SW(MAX)} = 45ns \bullet \left(1 + \frac{V_{OUT} + I_{OUT} \bullet K_{OFF}}{V_{IV} - I_{OUT} \bullet R_{ON} - V_{ON}}\right)$  $t_{SW(MAX)} = 45ns \cdot \left(1 + \frac{V_{OUT} + I_{OUT} \cdot R}{V_{UT} - I_{UT} \cdot R}\right)$ 

where:

$$
(2)
$$

J J J  $\backslash$ 

## **Register Descriptions**

FAN53523 has the following user-accessible registers:

#### **Table 5. I<sup>2</sup>C Register Address**

![](_page_14_Picture_238.jpeg)

#### **Register Bit Definitions**

The following table defines the operation of each register bit for all IC versions. Default values are in **bold** text.

![](_page_14_Picture_239.jpeg)

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# **I <sup>2</sup>C Interface**

The FAN53523 serial interface is compatible with standard, fast, Fast Plus, and High-Speed (HS) Modes per the I<sup>2</sup>C-Bus® specifications. The SCL line is an input and its SDA line is a bi-directional open-drain output; it can only pull down the bus when active. The SDA line only pulls LOW during data reads and when signaling ACK. All data is shifted in MSB (bit 7) first.

#### **Slave Address**

#### **Table 6. I<sup>2</sup>C Slave Address**

![](_page_15_Picture_327.jpeg)

In Hex notation, the slave address assumes a 0 LSB. The hex slave address is D6H.

### **Bus Timing**

As shown in Figure 22, data is normally transferred when SCL is LOW. Data is clocked in on the rising edge of SCL. Typically, data transitions shortly at or after the falling edge of SCL to allow ample time for the data to set up before the next SCL rising edge.

![](_page_15_Figure_9.jpeg)

**Figure 22. Data Transfer Timing** 

Each bus transaction begins and ends with SDA and SCL HIGH. A transaction begins with a "START" condition, which is defined as SDA transitioning from 1 to 0 with SCL HIGH, as shown in Figure 23.

![](_page_15_Figure_12.jpeg)

A transaction ends with a "STOP" condition, which is defined as SDA transitioning from 0 to 1 with SCL HIGH, as shown in Figure 24.

![](_page_15_Figure_14.jpeg)

During a read from the FAN53523 (Figure 27), the master issues a "REPEATED START" after sending the register address and before resending the slave address. The "REPEATED START" is a 1-to-0 transition on SDA while SCL is HIGH, as shown in Figure 25.

## **High-Speed (HS) Mode**

The protocols for High-Speed (HS), Low-Speed (LS), and Fast-Speed (FS) Modes are identical, except the bus speed for HS Mode is 3.4MHz. HS Mode is entered when the bus master sends the HS master code 00001XXX after a START condition. The master code is sent in Fast or Fast Plus Mode (less than 1MHz clock); slaves do not ACK this transmission.

The master then generates a REPEATED START condition (Figure 23) that causes all slaves on the bus to switch to HS Mode. The master then sends  $I^2C$  packets, as described above, using the HS Mode clock rate and timing.

The bus remains in HS Mode until a STOP bit (Figure 24) is sent by the master. While in HS Mode, packets are separated by REPEATED START conditions (Figure 25).

![](_page_15_Figure_20.jpeg)

### **Read and Write Transactions**

The following figures outline the sequences for data read and write. Bus control is signified by the shading of the packet,

![](_page_15_Picture_328.jpeg)

#### **Table 7. Bit Definitions for Figure 26 and Figure 27**

![](_page_15_Picture_329.jpeg)

![](_page_16_Figure_1.jpeg)

## **Selecting the Inductor**

The output inductor must meet both the required inductance and the energy handling capability of the application.

The inductor value affects the average current limit, the PWMto-PFM transition point, output voltage ripple, and efficiency.

The ripple current (∆I) of the regulator is:

$$
\Delta I \approx \frac{V_{OUT}}{V_{IN}} \bullet \left(\frac{V_{IN} - V_{OUT}}{L \bullet f_{SW}}\right)
$$
 (3)

The maximum average load current,  $I_{MAX(LOAD)}$  is related to the peak current limit,  $I_{LIM(PK)}$  by the ripple current:

$$
I_{MAX(LOAD)} = I_{LIM(PK)} - \frac{\Delta I}{2}
$$
 (4)

The FAN53523 is optimized for operation with L=1µH, but is stable with inductances up to  $1.2\mu$ H (nominal). The inductor should be rated to maintain at least 80% of its value at I<sub>LIM(PK)</sub>. Failure to do so lowers the amount of DC current that the IC can deliver.

Efficiency is affected by the inductor DCR and inductance value. Decreasing the inductor value for a given physical size typically decreases the DCR; but since ∆I increases, the RMS current increases, as do the core and skin effect losses:

$$
I_{RMS} = \sqrt{I_{OUT(DC)}^2 + \frac{\Delta I^2}{12}}
$$
 (5)

The increased RMS current produces higher losses through the  $R_{DS(ON)}$  of the IC MOSFETs as well as the inductor ESR.

Increasing the inductor value produces lower RMS currents, but degrades transient response. For a given physical inductor size, increased inductance usually results in an inductor with lower saturation current.

Table 8 shows the effects of inductance higher or lower than the recommended 1µH on regulator performance.

### **Table 8. Inductor Effect on Regulator Performance**

![](_page_16_Picture_504.jpeg)

#### **Inductor Current Rating**

The FAN53523 current-limit circuit can allow a peak current of 1.8A to flow through L1 under worst-case conditions. If it is possible for the load to draw that much continuous current, the inductor should be capable of sustaining that current or failing in a safe manner.

For space-constrained applications, a lower current rating for L1 can be used. The FAN53523 may still protect these inductors in the event of a short circuit, but may not be able to protect the inductor from failure if the load is able to draw higher currents than the DC rating of the inductor.

## **Output Capacitor**

Table 1 suggests 0805 capacitors. 0603 capacitors may used if space is at a premium. Due to voltage effects, the 0603 capacitors have a lower in-circuit capacitance than the 0805 package, which can degrade transient response and output ripple.

Increasing  $C_{\text{OUT}}$  has no effect on loop stability and can therefore be increased to reduce output voltage ripple or to improve transient response. Output voltage ripple, ΔV<sub>OUT</sub>, is:

$$
\Delta V_{\text{OUT}} = \Delta I_{L} \left[ \frac{f_{\text{SW}} \cdot C_{\text{OUT}} \cdot \text{ESR}^{2}}{2 \cdot D \cdot (1 - D)} + \frac{1}{8 \cdot f_{\text{SW}} \cdot C_{\text{OUT}}} \right]
$$
(6)

If values greater than 100 $\mu$ F of C<sub>OUT</sub> are used, the regulator may fail to start.

If an inductor value greater than 1.0 $\mu$ H is used, at least 30 $\mu$ F of  $C_{\text{OUT}}$  should be used to ensure stability.

#### **Equivalent Series Inductance (ESL) Effects**

The ESL of the output capacitor network should be kept low to minimize the square wave component of output ripple that results from the division ratio  $C<sub>OUT</sub>$ 's ESL and the output inductor  $(L<sub>OUT</sub>)$ . The square wave component due to the ESL can be estimated as:

$$
\Delta V_{\text{OUT(SQ)}} \approx V_{\text{IN}} \bullet \frac{\text{ESL}_{\text{COUT}}}{L1} \tag{7}
$$

A good practice to minimize this ripple is to use multiple output capacitors to achieve the desired  $C<sub>OUT</sub>$  value. For example, to obtain  $C_{\text{OUT}} = 10 \mu F$ , a single 10 $\mu$ F 0805 would produce twice the square wave ripple of  $2 \times 4.7 \mu$ F 0805.

To minimize ESL, try to use capacitors with the lowest ratio of length to width. 0805s have lower ESL than 1206s. If low output ripple is a chief concern, some vendors produce 0508 or 0612 capacitors that have ultra-low ESL. Placing additional, small-value capacitors near the load also reduces the highfrequency ripple components.

#### **Input Capacitor**

The  $1\mu$ F ceramic input capacitor should be placed as close as possible between the VIN pin and PGND to minimize the parasitic inductance. If a long wire is used to bring power to the IC, additional bulk capacitance (electrolytic or tantalum) should be placed between  $C_{\text{IN}}$  and the power source lead to reduce under-damped ringing that can occur between the inductance of the power source leads and C<sub>IN</sub>.

The effective  $C_{IN}$  capacitance value decreases as  $V_{IN}$ increases due to DC bias effects. This has no significant impact on regulator performance.

#### **Layout Recommendations**

The layout recommendations below highlight various top copper planes by using different colors.

Bulk capacitors are shown as 7343 capacitors. Bulk capacitors may be paralleled by extending the PGND and PMID planes indefinitely, depending on the number of bulk caps required.

The  $0603$  C<sub>IN</sub> capacitor on PMID carries high-frequency currents and must be connected as close to the IC's PMID and PGND pins as possible, as shown in Figure 28 below. VOUT current has less high-frequency content. Its bypass capacitor is shown with a short return to GND. The VOUT pin carries no high-frequency current and can therefore be returned to the IC through vias. Similarly, the VBUS input carries no significant AC current, so the return of CBUS is carried through vias to PGND.

To minimize RFI, SW trace should be as short as possible.

Extending the PGND and VBUS planes improves IC cooling.

Logic signals (EN, SDA, SCL, INT) can connect through vias to the system control logic.

![](_page_17_Figure_17.jpeg)

**Figure 28. Layout Recommendation** 

![](_page_18_Figure_0.jpeg)

![](_page_18_Figure_1.jpeg)

#### **Product-Specific Dimensions**

![](_page_18_Picture_104.jpeg)

Package drawings are provided as a service to customers considering Fairchild components. Drawings may change in any manner without notice. Please note the revision and/or date on the drawing and contact a Fairchild Semiconductor representative to verify or obtain the most recent revision. Package specifications do not expand the terms of Fairchild's worldwide terms and conditions, specifically the warranty therein, which covers Fairchild products.

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**Rev. 161** 

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