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## 3 MHz, 1.6 A, PWM Synchronous Buck Converter

**High Efficiency, PWM Only, Low Ripple, Fixed Output Voltage**

# NCV6323F-xx

NCV6323F is a synchronous Buck converter optimized to supply different sub−systems from a pre−regulator supply rail in the 2.8 V to 5.5 V range. The device is able to deliver up to 1.6 A DC (85°C ambient temperature) on a fixed output voltage. Operation with 3 MHz switching frequency allows employing small size inductor and capacitors. Technology and internal structure allows the IC to operate from a wide input voltage range. Synchronous rectification offers improved system efficiency and integrated feedback network allows very simple and straightforward implementation to power supply designers with only a few components to select.

The NCV6323F is housed in in a space saving Wettable flank DFN8, 2x2 mm (0.8 mm thickness), 0.5 mm pitch package.

#### **Features**

- 2.8 V to 5.5 V Input Voltage Range
- Fixed Output Voltage
- Up to 1.6 A DC Output Current (85°C Ambient Temperature)
- Up to 1.2 A DC Output Current (105°C Ambient Temperature)
- 3 MHz Switching Frequency
- Synchronous Rectification
- Soft Start / Over Current Protection
- Thermal Shutdown Protection
- Output Active Discharge (Disabled)
- Enable Input / Power Good (PG) Option
- WDFNW8, 2x2 mm, 0.5 mm Pitch Package
- Maximum 0.8 mm Thickness
- AEC−Q100 Qualified and PPAP Capable
- These are Pb−Free Devices

## **Typical Applications**

- Automotive Advanced Driver−Assistance System (ADAS)
	- ♦ Front Camera Rear View Camera
	- Surround View
	- ♦ Blind Spot Monitoring
- Automotive Telematics Clusters − Camera
- Automotive Space−Optimized Systems
- Point Of Load



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**WDFNW8 2x2, 0.5P CASE 511CL**

#### **MARKING DIAGRAM**



XX = Specific Device Code

- $M =$  Date Code
- -= Pb−Free Package
- (Note: Microdot may be in either location)





#### **ORDERING INFORMATION**

See detailed ordering and shipping information on page [31](#page-31-0) of this data sheet.



**Figure 1. Application Schematic**







## **PIN OUT DESCRIPTION**



#### **PIN FUNCTION DESCRIPTION**



#### **MAXIMUM RATINGS**



Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

1. Refer to ELECTRICAL CHARACTERISTICS, RECOMMENDED OPERATING RANGES and/or APPLICATION INFORMATION for Safe Operating parameters.

3. Latch up Current per JEDEC standard: JESD78 class II.

4. Moisture Sensitivity Level (MSL): 1 per IPC/JEDEC standard: J−STD−020A.

#### **RECOMMENDED OPERATING CONDITIONS**



Functional operation above the stresses listed in the Recommended Operating Ranges is not implied. Extended exposure to stresses beyond the Recommended Operating Ranges limits may affect device reliability.

5. Including de−ratings (Refer to the Application Information section of this document for further details)

6. The thermal shutdown set to 150°C (typical) avoids potential irreversible damage on the device due to power dissipation.

7. NCV632F compensation network is integrated. Special care should be taken with the capacitive load (refer to the application information)

<sup>2.</sup> This device series contains ESD protection and passes the following ratings: Human Body Model (HBM) ±2.0 kV per JEDEC standard: JESD22−A114. Charged Device Model (CDM) ±500 V per JEDEC standard: JESD22−C101 Class IV.

#### <span id="page-5-0"></span>**THERMAL INFORMATION**



8. Calculated with infinite heatsink affixed to case top without any board present

9. Calculated with infinite heatsink affixed to case bottom without any board present.

10. Rθ<sub>JA</sub> is dependent on the PCB heat dissipation. Refer to AND8215/D (AND8215–D.PDF)

11. The thermal characterization parameters are measured on the Demo Board

12.The current capability (CC) is dependent on input voltage, PCB stack up and layout, as well as the external components selected. Filled with  $AV_{IN} = PV_{IN} = 5.0 V V_{OUT} = 1.8 V$ 

#### **ELECTRICAL CHARACTERISTICS** (Refer to the Application Information section of this data sheet for more details.

Min and Max Limits apply for T<sub>J</sub> = -40°C to +125°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> =  $C_{\text{OUT}}$  = 10  $\mu$ F and default configuration, unless otherwise specified.

Typical values are referenced to T<sub>J</sub> = + 25°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> = C<sub>OUT</sub> = 10  $\mu$ F and default configuration, unless otherwise specified.)



**OUTPUT VOLTAGE**



**ELECTRICAL CHARACTERISTICS** (Refer to the Application Information section of this data sheet for more details.

Min and Max Limits apply for T<sub>J</sub> = –40°C to +125°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> =  $C_{\text{OUT}}$  = 10  $\mu$ F and default configuration, unless otherwise specified.

Typical values are referenced to T<sub>J</sub> = + 25°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> = C<sub>OUT</sub> = 10 µF and default configuration, unless otherwise specified.) (continued)



60 95 150  $m\Omega$ 

 $\cdot$  V<sub>IN</sub> = 3.3 V (10, 11, 12, 18 Versions) (Note [19](#page-7-0))

RON\_LSN5 Low−Side MOSFET ON Resistance  $\cdot$  V<sub>IN</sub> = 5.0 V

<span id="page-7-0"></span>**ELECTRICAL CHARACTERISTICS** (Refer to the Application Information section of this data sheet for more details.

Min and Max Limits apply for T<sub>J</sub> = –40°C to +125°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> =  $C_{\text{OUT}}$  = 10  $\mu$ F and default configuration, unless otherwise specified.

Typical values are referenced to T<sub>J</sub> = + 25°C, A<sub>VIN</sub> = P<sub>VIN</sub> = 3.3 V (10, 11, 12, 18 Versions) or 5.0 V (33 Versions), L = 1 µH, C<sub>IN</sub> = C<sub>OUT</sub> = 10 µF and default configuration, unless otherwise specified.) (continued)



T<sub>SD\_HYST</sub> Thermal Shutdown Hysteresis − 25 − 25 <sup>o</sup>C Product parametric performance is indicated in the Electrical Characteristics for the listed test conditions, unless otherwise noted. Product performance may not be indicated by the Electrical Characteristics if operated under different conditions.

T<sub>SD</sub> Thermal Shutdown Threshold **For a struck of the struck of the struck** of the struck of th

13.Operation above 5.5 V input voltage for extended period of time may affect device reliability

14.  $V_{IN} \geq V_{OUT} + 0.5$  V or 2.8 V

15.Junction temperature must be maintained below 125°C. Output load current capability depends on the application thermal capability.

16.Characterized and not tested in Production

17.Limit for reverse current from SW to GND

18. The Output Peak Current Limit does not operate when  $V_{OUT}$  < 300 mA

19. Maximum values apply for  $T_J = 125^{\circ}C$ 

20.Covered by Scan

#### **TYPICAL OPERATING CHARACTERISTICS**











**(EN = High, VOUT = 1.8 V, No Load)**



**Figure 5. Quiescent Current vs. Input Voltage (EN = High, VOUT = 1.0 V, No Load)**





**Figure 7. Quiescent Current vs. Input Voltage (EN = High, VOUT = 1.2 V, No Load)**





Quiescent supply current vs VIN







#### **TYPICAL OPERATING CHARACTERISTICS** (continued)

**Figure 11. Efficiency vs. Output Current and Input Voltage (VOUT = 1.0 V, TA = 25**-**C, L = FDSD0420−H−1R0M) Figure 12. Efficiency vs. Output Current and Temperature at VIN = 3.3 V (VOUT = 1.0 V, L = FDSD0420−H−1R0M)**



**Figure 13. Efficiency vs. Output Current and Input Voltage (VOUT = 1.1 V, TA = 25**-**C, L = FDSD0420−H−1R0M)**



**Figure 15. Efficiency vs. Output Current and Input Voltage (VOUT = 1.2 V, TA = 25**-**C, L = FDSD0420−H−1R0M)**

lout (mA) **Figure 14. Efficiency vs. Output Current and Temperature** at V<sub>IN</sub> = 3.3 V (V<sub>OUT</sub> = 1.1 V, L = FDSD0420−H−1R0M)

800

DCDC Efficiency vs Output Current (Vout=1.2V) at VIN=3.3V

1200

1600



**Figure 16. Efficiency vs. Output Current and Input Voltage (VOUT = 1.2 V, TA = 25**-**C, L = FDSD0420−H−1R0M)**

DCDC Efficiency vs Output Current (Vout=1.1V) at **VIN=3.3V**  $40^{\circ}$ C  $-25^{\circ}$ C  $125^{\circ}$ C 100 90 80 70  $E_{FF}(%)$ 60 50 40

 $400$ 

 $\mathbf 0$ 



 $125^{\circ}$ C

1600

### **TYPICAL OPERATING CHARACTERISTICS** (continued)



**Figure 17. Efficiency vs. Output Current and Input Voltage (VOUT = 1.8 V, TA = 25**-**C, L = FDSD0420−H−1R0M)**



**Figure 19. Efficiency vs. Output Current and Input Voltage (VOUT = 3.3 V, TA = 25**-**C, L = FDSD0420−H−1R0M)**



**Figure 21. Load Regulation (V<sub>IN</sub> = 5.0 V, V<sub>OUT</sub> = 1.0 V) Figure 22. Load Regulation (V<sub>IN</sub> = 3.3 V, V<sub>OUT</sub> = 1.0 V)** 



**Figure 18. Efficiency vs. Output Current and Temperature** at V<sub>IN</sub> = 3.3 V (V<sub>OUT</sub> = 1.8 V, L = FDSD0420−H−1R0M)



lout (mA) **Figure 20. Efficiency vs. Output Current and Temperature**









#### **TYPICAL OPERATING CHARACTERISTICS** (continued)



















**12**









**Figure 31. Output Voltage DC Error vs Output Current (VOUT = 1.1 V, TA = 25**-**C)**

Output Voltage DC Error vs Output Current (Vout=1.8V)



**Figure 33. Output Voltage DC Error vs Output**  $Current (V_{OUT} = 1.8 V, T_A = 25°C)$ 



**Current (VOUT = 1.0 V, TA = 25**-**C)**

800<br>Iout (mA) 1000 1200 1400

1600

600

 $\pmb{0}$ 

200

400



**Current (VOUT = 1.2 V, TA = 25**-**C)**



**Figure 34. Output Voltage DC Error vs Output**  $Current (V_{OUT} = 3.3 V, T_A = 25°C)$ 

#### Output Voltage DC Error vs Output Current (Vout=1V)





## **TYPICAL OPERATING CHARACTERISTICS** (continued)

 $rac{1}{4}$ 



**Figure 36. Load Transient (VIN = 3.3 V, VOUT = 1.0 V, COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M) COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**  $500 \text{ mA} \rightarrow 1.2 \text{ A} \rightarrow 500 \text{ mA}$ 



**Figure 37. Load Transient (VIN = 3.3 V, VOUT = 1.0 V,**  $50 \text{ mA} \rightarrow 600 \text{ mA} \rightarrow 50 \text{ mA}$ 



**Figure 38. Load Transient (V<sub>IN</sub> = 3.3 V, V<sub>OUT</sub> = 1.1 V, COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M) COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**  $500 \text{ mA} \rightarrow 1.2 \text{ A} \rightarrow 500 \text{ mA}$ 





**Figure 39. Load Transient (V<sub>IN</sub> = 3.3 V, V<sub>OUT</sub> = 1.1 V,**  $50 \text{ mA} \rightarrow 600 \text{ mA} \rightarrow 50 \text{ mA}$ 







NCV6323F VOUT (AC COUPLING)

NCV6323

 $\tilde{E}$ 

## **TYPICAL OPERATING CHARACTERISTICS** (continued)









50  $\rightarrow$  600 mA

 $rac{1}{8}$ 

**Figure 44. Load Transient (V<sub>IN</sub> = 5.0 V, V<sub>OUT</sub> = 3.3 V, COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M) COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M) 500 mA 1.2 A 500 mA**





**Figure 45. Load Transient (V<sub>IN</sub> = 5.0 V, V<sub>OUT</sub> = 3.3 V, 50 mA 600 mA 50 mA**



**Figure 47. Line Transient (** $V_{OUT}$  **= 1.1 V,**  $C_{OUT}$  **= GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**

**Figure 43. Load Transient (V<sub>IN</sub> = 3.3 V, V<sub>OUT</sub> = 1.8 V, 50 mA 600 mA 50 mA**

NCV6323F VOUT (AC COUPLING)

NCV6323FLOAD





 $\frac{5}{9}$ 

**NOVERED VOIDT INDICATABLE** 

## **TYPICAL OPERATING CHARACTERISTICS** (continued)



**Figure 48. Line Transient (V<sub>OUT</sub> = 1.2 V, C<sub>OUT</sub> = GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**



Figure 50. Line Transient ( $V_{OUT}$  = 3.3 V,  $C_{OUT}$  = **GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**



**Figure 49. Line Transient (V<sub>OUT</sub> = 1.8 V, C<sub>OUT</sub> = GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**





**Figure 51. Output Voltage Ripple (V<sub>IN</sub> = 3.3 V, VOUT = 1.0 V, COUT = GCM21BR70J106KE22,**   $I_{OUT} = 500$  mA)



**Figure 53. Output Voltage Ripple (V<sub>IN</sub> = 3.3 V, VOUT = 1.2 V, COUT = GCM21BR70J106KE22,**   $I_{\text{OUT}} = 500 \text{ mA}$ 



**Figure 55. Output Voltage Ripple (V<sub>IN</sub> = 5.0 V, VOUT = 3.3 V, COUT = GCM21BR70J106KE22,**   $I_{\text{OUT}} = 500 \text{ mA}$ 



**Figure 52. Output Voltage Ripple (V<sub>IN</sub> = 3.3 V, VOUT = 1.1 V, COUT = GCM21BR70J106KE22,**   $I_{OUT} = 500$  mA)



**Figure 54. Output Voltage Ripple (V<sub>IN</sub> = 3.3 V, VOUT = 1.8 V, COUT = GCM21BR70J106KE22,**   $I_{\text{OUT}} = 500 \text{ mA}$ 

## **TYPICAL OPERATING CHARACTERISTICS** (continued)



**Figure 56. Inrush Current (V<sub>IN</sub> = 3.3 V, V<sub>OUT</sub> = 1.8 V,**  $I_{\text{OUT}}$  **= 800 mA,**  $C_{\text{OUT}}$  **= GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**



**Figure 58. Startup Time TSTART (NCV6323FCLMTW12, COUT = 10 -F)**



**Figure 57. PG Delay after Start Up – NCV6323F−E (VIN = 3.3 V, VOUT = 1.8 V, COUT = GCM21BR70J106KE22, L = FDSD0420−H−1R0M)**



**Figure 59. Soft Start Time Tss (NCV6323FCLMTW12, COUT = 10 -F)**



**Figure 61. Soft Start Time T<sub>SS</sub> (NCV6323FELMTW11, COUT = 10 -F)**



**Figure 60. Startup Time TSTART (NCV6323FELMTW11, COUT = 10 -F)**





**Figure 63. Soft Start Time Tss (NCV6323FELMTW10, COUT = 10 -F)**



**Figure 64. Startup Time TSTART (NCV6323FELMTW18, COUT = 10 -F)**



**Figure 66. Startup Time T<sub>START</sub> (NCV6323FELMTW33, COUT = 10 -F)**



**Figure 65. Soft Start Time Tss (NCV6323FELMTW18, COUT = 10 -F)**



**Figure 67. Soft Start Time Tss (NCV6323FELMTW33, COUT = 10 -F)**



**Figure 68. Bode Plot NCV6323FxLMTW18TBG**  $L = 1.0 \mu H - COUT = 10 \mu F$ 



**Figure 70. Bode Plot NCV6323FxLMTW33TBG L** = 1.0 μH – COUT = 10 μF



**Figure 72. Bode Plot NCV6323FxLMTW12TBG L** = 1.0 μH – COUT = 10 μF



**Figure 69. Bode Plot NCV6323FxLMTW18TBG L** = 1.0 μH – COUT = 100 μF



**Figure 71. Bode Plot NCV6323FxLMTW33TBG**  $L = 1.0 \mu H - COUT = 100 \mu F$ 



**Figure 73. Bode Plot NCV6323FxLMTW12TBG**  $L = 1.0 \mu H - COUT = 100 \mu F$ 



**Figure 74. Bode Plot NCV6323FxLMTW10TBG L** = 1.0 μH – COUT = 10 μF



**Figure 76. Bode Plot NCV6323FxLMTW11TBG L** = 1.0 μH – COUT = 10 μF



**Figure 75. Bode Plot NCV6323FxLMTW10TBG L** = 1.0 μH – COUT = 100 μF



**Figure 77. Bode Plot NCV6323FxLMTW11TBG**  $L = 1.0 \mu H - COUT = 100 \mu F$ 

#### **DETAILLED OPERATING DESCRIPTION**

#### **General**

The NCV6323F is a voltage mode standalone synchronous PWM DC−DC converter optimized to supply the different sub systems of automotive applications from a pre−regulator supply rail in the 2.8 V to 5.5 V range. It can deliver up to 1.6 A to an internally factory set voltage (please refer to the [ORDERING INFORMATION](#page-31-0) table). The 3 MHz switching frequency allows using small output filter components. A Power Good (PG) indicator is available. The synchronous rectification offers high system efficiency and integrated feedback network allows very simple and straightforward implementation to power supply designers with only a few components to select.

The NCV6323F is housed in a low profile 2.0 x 2.0 mm uDFN−8 package.

#### **DC−DC Converter Operation**

The converter integrates both high side and low side (synchronous) switches. Neither external transistors nor diodes are required for NCV6323F operation. The feedback and compensation networks are also fully integrated. It operates in PWM.

#### **PWM Operation**

The device operates in PWM mode with 3 MHz typical fixed switching frequency. In this operating scheme, the output voltage is regulated by on−time Pulse Width Modulation (PWM) of an integrated high side P−MOSFET. A low side N−MOSFET, also integrated in the IC, operates as synchronous rectifier and its turn−on signal is complimentary to that of the P−MOSFET (with built in dead time control to avoid cross conduction)

#### **Under Voltage Lockout**

The input voltage VIN must reach or exceed 2.8 V (maximum) before the NCV6323F enables the converter output to begin the startup sequence. The UVLO threshold hysteresis is typically 150 mV.

#### **Enable**

The NCV6323F has an enable logic input pin EN. A high level (above 1.1 V) on this pin enables the device to active mode. A low level (below 0.4 V) on this pin disables the device and makes the device in shutdown mode. There is an internal filter with  $5 \mu s$  time constant. The EN pin is pulled down by an internal 100 nA sink current source.



(1)  $T_{SS}$  timing depends on the IC version.

Please refer to the full part number of the considered version and to the electrical tables



#### **Power Good Output (PG)**

The device monitors the output voltage and provides a power good signal at the PG pin. This pin is an open−drain output. This signal indicates that the desired voltage is regulated properly and is valid as soon as the Enable (EN) pin enables the device. When EN is high, the power good pin is tied to low level when the output voltage is considered as out of regulation (less than 90% of the desired value).

During the startup sequence, this signal indicates that the output voltage is not yet established, while during normal operation, a High to Low transition of PG indicates that the output voltage sags under 90% of its target and is out of regulation. A low level at the power good signal indicates a power failure. An internal 5% hysteresis is implemented on the power good comparator.

When EN is low (NCV6323F disabled), the discharge path (refer to the "Discharge Path" section) drives the output voltage to ground. In that condition, the PG is maintained to low by a weak pull down.

#### **Soft−Start (SS)**

A soft start limits inrush current when the converter is enabled. After a minimum 80 us typical delay time following the enable signal, the output voltage ramp is controlled during the  $T_{SS}$  time. The  $T_{SS}$  time is factory programmed. Please refer to the ordering information to select the T<sub>SS</sub> that fit better with the application requirements or that is available. If not available, please contact your sales representative office.

 $T_{SS} = 440 \,\mu s \,(NCV6323F–xxE).$ 

#### **Active Output Discharge**

An output discharge operation is active in when EN is low. A discharge resistor (450  $\Omega$  typical) is enabled in 4  $\mu$ s after the High to Low transition of the EN signal to discharge the output capacitor through SW pin.

#### **Cycle−by−Cycle Current Limitation**

The NCV6323F protects the device from over current with a fixed−value cycle−by−cycle current limitation. The typical peak current limit ILMT is 2.6 A (10, 11, 12, 18 versions) and 2.45 A (33 version). If the inductor current exceeds the current limit threshold, the P−MOSFET will be turned off cycle−by−cycle. The maximum output current can be calculated by

$$
I_{MAX} = I_{LIMIT} - \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{2 \times V_{IN} \times f_{SW} \times L}
$$
 (eq. 1)

Where  $V_{IN}$  is input supply voltage,  $V_{OUT}$  is output voltage, L is inductance of the filter inductor, and  $f_{SW}$  is 3 MHz normal switching frequency.

In output short circuit condition, if the short impedance becomes low enough to maintain the NCV6323F  $V_{OUT}$ lower than 300 mA (max), because of the internal delays in the detection system, the Peak Current Limit can become non operative.

#### **Negative Current Protection**

The NCV6323F includes a cycle by cycle 0.8 A typical negative current protection in the N−MOSFET Low Side Switch (LSS). This current limitation protects the internal LSS when the output cap has to be discharged during regulation to allow fast recovery to the target output voltage. This can happen mainly when the capacitive load is pretty high and the IC recovers after a fast negative load transient (load release).

In output short circuit condition, if the short impedance becomes low enough to maintain the NCV6323F  $V<sub>OUT</sub>$ lower than 300 mA (max), because of the internal delays in the detection system, the Peak Current Limit can become non operative.

#### **Thermal Shutdown (TSD)**

The power dissipation of the output stage can lead the die temperature to exceed the maximum rating of the silicon. To avoid irreversible damage and hazard in its normal operation, the NCV6323F features a Thermal Shutdown to protect the device from overheating when the die temperature exceeds 150°C.

When activated, the TSD will immediately stop the power stage switching activity, turns it off and the output voltage is switched off. The PG indicator will transition to Low level, indicating a power fail.

During TSD activation, the die will cool down to a more acceptable temperature level and, when the temperature gets down below 125°C again , the switching activity will be released and the PG pin will transition to high again as soon as the output voltage has recovered.

#### **APPLICATION INFORMATION**

#### **Output Filter Design Considerations**

The output filter introduces a double pole in the system at a frequency of

$$
f_{LC} = \frac{1}{2 \times \pi \times \sqrt{L \times C}}
$$
 (eq. 2)

The internal compensation network design of the NCV6323F is optimized for a typical output filter comprised of a 1.0  $\mu$ H inductor and a 10  $\mu$ F ceramic output capacitor, which has a double pole frequency at about 50 kHz. Other possible output filter combinations may have a double pole around 50 kHz to have optimum operation with the typical feedback network. Normal selection range of the inductor is from 0.47  $\mu$ H to 4.7  $\mu$ H, and normal selection range of the output capacitor is from 4.7  $\mu$ F to 22  $\mu$ F.

#### **Inductor Selection**

The inductance of the inductor is determined by given peak−to−peak ripple current IL\_PP of approximately 20% to 50% of the maximum output current  $I<sub>OUT MAX</sub>$  for a trade−off between transient response and output ripple. The inductance corresponding to the given current ripple is

$$
L = \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN} \times f_{SW} \times I_{L\_PP}}
$$
 (eq. 3)

The selected inductor must have high enough saturation current rating to be higher than the maximum peak current that is

$$
I_{L\_MAX} = I_{OUT\_MAX} + \frac{I_{L\_PP}}{2}
$$
 (eq. 4)

The inductor also needs to have high enough current rating based on temperature rise concern. Low DCR is good for efficiency improvement and temperature rise reduction. Table xx shows some recommended inductors for high power applications and Table xx shows some recommended inductors for low power applications.





#### **Table 2. LIST OF RECOMMENDED INDUCTORS FOR LOW POWER APPLICATIONS**



#### **Output Capacitor Selection**

The output capacitor selection is determined by output voltage ripple and load transient response requirement. For a given peak−to−peak ripple current IL\_PP in the inductor of the output filter, the output voltage ripple across the output capacitor is the sum of three ripple components as below

$$
V_{\text{OUT\_PP}} \approx V_{\text{OUT\_PP(C)}} + V_{\text{OUT\_PP(ESR)}} + V_{\text{OUT\_PP(ESL)}} \quad (eq. 5)
$$

Where  $V_{\text{OUT PP(C)}}$  is a ripple component by an equivalent total capacitance of the output capacitors,  $V_{\text{OUT}}$   $PP(ESR)$  is a ripple component by an equivalent ESR of the output capacitors, and  $V_{\text{OUT}}$  pp(ESL) is a ripple component by an

equivalent ESL of the output capacitors. In PWM operation mode, the three ripple components can be obtained by

$$
V_{OUT\_PP(C)} = \frac{I_{L\_PP}}{8 \times C \times f_{SW}}
$$
 (eq. 6)

$$
V_{OUT\_PP(ESR)} = I_{L\_PP} \times ESR
$$
 (eq. 7)

$$
V_{OUT\_PP(ESL)} = \frac{ESL}{ESL + L} \times V_{IN}
$$
 (eq. 8)

And the peak−to−peak ripple current is

$$
I_{L\_PP} = \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN} \times f_{SW} \times L}
$$
 (eq. 9)

In applications with all ceramic output capacitors, the main ripple component of the output ripple is  $V_{\text{OUT}-PP(C)}$ . So that the minimum output capacitance  $C_{OUT\_MIN}$  can be calculated regarding to a given output ripple requirement V<sub>OUT</sub> pp in PWM operation mode.

$$
C_{OUT\_MIN} = \frac{I_{L\_PP}}{8 \times V_{OUT\_PP} \times f_{SW}}
$$
 (eq. 10)

#### **Input Capacitor Selection**

One of the input capacitor selection guides is the input voltage ripple requirement. To minimize the input voltage ripple and get better decoupling in the input power supply rail, ceramic capacitor is recommended due to low ESR and ESL. The minimum input capacitance  $C_{IN-MIN}$  regarding to the input ripple voltage  $V_{IN}$  pp is

$$
C_{IN\_MIN} = \frac{I_{OUT\_MAX} \times (D - D^{2})}{V_{IN\_PP} \times f_{SW}}
$$
 (eq. 11)

Where

$$
D = \frac{V_{OUT}}{V_{IN}} \tag{eq. 12}
$$

In addition, the input capacitor needs to be able to absorb the input current, which has an RMS value of

$$
I_{IN\_RMS} = I_{OUT\_MAX} \times \sqrt{D - D^2}
$$
 (eq. 13)

The input capacitor also needs to be sufficient to protect the device from over voltage spike, and normally at least a 4.7 µF capacitor is required. The input capacitor should be located as close as possible to the IC on PCB.



#### **Table 3. LIST OF RECOMMENDED INPUT AND OUTPUT CAPACITORS**

#### **Stability of the Regulation Loop**

The NCV6323F is a voltage mode DC to DC converter with a double pole at the  $f_{LC}$  frequency and a zero at the  $f_0$ frequency:

$$
f_{LC} = \frac{1}{2 \times \pi \times \sqrt{L \times C}}
$$
 (eq. 14)

$$
f_{ESR} = \frac{1}{2 \times \pi \times ESR \times C}
$$
 (eq. 15)

With  $L =$  the output inductor and C the total amount of capacitance connected to the NCV6323F output. This capacitance value should not only take into account the LC filter capacitor, but also all other capacitors connected between the rail NCV6323F supplies and the GND.

The loop is compensated by a type III network.

As, besides the external LC filter, all the other parameters that govern the loop response and stability are integrated in the NCV6323F, it is important to evaluate and consider, during the design stage, the real value of the output capacitor C and select the right NCV6323F option.

In order to accommodate a large range of applications, 2 options of the compensation loop are available (please refer to the [ORDERING INFORMATION](#page-31-0) table):

- NCV6323Fx*L* that address the application with output capacitor ranging from 10 to  $\sim$ 100  $\mu$ F
- NCV6323Fx*H* that address the application with output capacitor ranging from 50 to  $\sim$ 250 µF

If the output capacitor is comprised within the overlap range (50  $\sim$  100  $\mu$ F), it is suggested to select the L option if  $C \le 80 \mu$ F and the H option if  $C > 80 \mu$ F.

#### **Maximum Current and Thermal Considerations**

To avoid irreversible damage and overheating, the Thermal Shut Down (TSD) of the NCV6323F will stop the power stage switching activity as soon as the die temperature rises up to 150°C TSD threshold. Dissipation in the power stage mainly depends on the losses in the HSS (High Side Switch) and LSS (Low Side Switch) and is then directly function of the loading current.

The NCV6323F specification is guaranteed for a maximum Junction Temperature (T<sub>J\_MAX</sub>) of 125 $^{\circ}$ C. When the junction temperature ranges from 125°C to the TSD threshold, the IC will still operate and will not be damaged, but the specifications are not guaranteed and the parameters value may deviate significantly. It is then important to try to keep the  $T_J \leq 125$ °C.

The **[THERMAL INFORMATION](#page-5-0)** table provides the thermal parameters  $(R_{\Theta Jx})$  defined by the JEDEC JESD51−3 as well as some thermal characterization parameters  $(\Psi_{Jx})$ . The thermal characterization parameters are the result of measurements on the standard NCV6323F demo board, while the thermal parameters are the result of simulations in the JESD51 defined environment.

Based on those parameters and the efficiency, a Safe Operating Area, that keeps the junction temperature lower than 125°C, can be defined.

On the standard demo board, the maximum power ( $P_{\text{D MAX}}$ ) the package can dissipate with 105°C ambient temperature  $(T_A)$ , can be calculated as:

$$
P_{D\_MAX} = \frac{T_{J\_MAX} - T_{A\_MAX}}{R_{\Theta JA}}
$$
 (eq. 16)

With:  $T_{J\_MAX}$  = maximum junction temperature (125°C),  $T_A$ <sub>MAX</sub> = maximum ambient temperature (105°C) and  $R_{\Theta JA}$  = Junction to Ambient thermal resistance measured on our evaluation board (~40°C/W),  $P_{D_MAX} = 500$  mW.

Thus, for  $T_A = 105$ °C:

**Table 4. MAXIMUM OUTPUT CURRENT AT TA = 105**-**C**

$V_{IN} (V)$	$V_{OUT} (V)$	Max I <sub>OUT</sub> (A)
5.0	1.0	1.2
	1.1	1.2
	1.2	1.2
	1.8	1.2
	3.3	1.2
3.3	1.0	1.1
	1.1	1.1
	1.2	1.2
	1.8	1.2

The below figure is a simulation result showing the die temperature gradient when the NCV6323F dissipates 500 mW. As expected, the output stage is the hottest part of the die and gets to about 125°C.



**Figure 79. Die Temperature Simulation (500 mW Dissipated Power)**

#### **FeedBack (FB) Pin Leakage Current**

The FB pin is internally connected to the resistor ladder that divides the  $V_{\text{OUT}}$  voltage and feeds the error amplifier. This ladder has a typical impedance of 260 k $\Omega$ , thus, the FB pin input leakage current value is:

$$
I_{FB} = (V_{OUT} - 0.6) / 260.10^3
$$
 (eq. 17)

#### **LAYOUT CONSIDERATIONS**

#### **Switching Noise Consideration**



**Figure 80. AC Current Flowing Loops**

- The DC/DC buck converter has two main loops where high AC currents flow.
- When the High−Side Switch (HSS) is on, the current flows from VCC via HSS and L to the output capacitor and the load. The current flows back via ground to the input. The AC portion of the current will flow via the input and output capacitors. This current is shown in red  $color(II).$
- When HSS switches off, the inductor current will keep flowing in the same direction, and the Low−Side Switch (LSS) is switched on. The current flows via LSS, L, load and output capacitor and back via ground to LSS. This loop is shown in blue (I2).
- Both I1 and I2 are discontinuous currents, meaning that they have sharp rising and falling edges at the beginning

and end of the active time. These sharp edges have fast rise and fall times (high dI/dt). Therefore they have a lot of high frequency content.

- I1 and I2 share a common path from switch node to inductor to output capacitor to ground back to the source of LSS. The sum of I1 and I2 is a relatively smooth continuous saw−tooth waveform, which has less high frequency content due to the absence of high dI/dt edges.
- From noise point of view, the current loop with the high dI/dt current is the red shaded area. This loop will generate the most high frequencies and should be considered the most critical loop for noise in buck converters. The dI/dt of the current in the blue shaded area is not as high as it is in the other area and generally generates a lot less noise.

#### **Electrical Layout Considerations**

Good electrical layout is a key to make sure proper operation, high efficiency, and noise reduction. Electrical layout guidelines are:

- Since the red shaded area is the noisiest loop, it is critical to identify it and to place the input cap in such a way that this loop is minimized. It is also important to make sure that the path between the 2 terminals of the input cap and the PVIN & PGND pins is as short as possible and free of any vias to either the VIN or the GND PCB plane. It can also be a good practice to make a local PGND and VIN planes and to keep those planes as solid as possible below and in the input switching loop. Any trace or vias in this area reduces the plane effectiveness and increase the plane impedance. Vias from these planes to the other main planes of the PCB should be placed outside of the critical loop.
- Also, it is important to place the output capacitor ground in an area that does not overlap the input capacitor switching loop : this could generate extra high frequency noise in the output voltage
- Connecting the PGND plane to the main PCB GND plane (to whitch the AGND pin should be connected too) in one point (doing a kind of "star routing") is also important to isolate the AGND and keep them quiet.
- Use wide and short traces for power paths (such as P<sub>VIN</sub>, V<sub>OUT</sub>, SW, and PGND) to reduce parasitic inductance and high−frequency loop area. It is also good for efficiency improvement.
- The device should be well decoupled by input capacitor and input loop area should be as small as possible to reduce parasitic inductance, input voltage spike, and noise emission.
- SW node should be a large copper pour, but compact because it is also a noise source.
- It would be good to have separated local ground planes for PGND and AGND and connect the two planes at one

point. Directly connect AGND pin to the exposed pad and then connect to AGND ground plane through vias. Try best to avoid overlap of input ground loop and output ground loop to prevent noise impact on output regulation.

• Arrange a "quiet" path for output voltage sense, and make it surrounded by a ground plane.

#### **Component Placement**

- $\bullet$  C<sub>IN</sub> Input capacitor placed as close as possible to the IC.
- PVIN directly connected to  $C_{IN}$  input capacitor, and then connected to the VIN plane. Local mini planes used on the top layer and the layer just below the top layer with laser vias.
- AVIN connected to the VIN plane just after the capacitor.
- AGND directly connected to the GND plane.
- $\bullet$  PGND directly connected to  $C_{IN}$  input capacitor, and then connected to the GND plane: Local mini planes used on the top layer and the layer just below the top layer with laser vias.
- SW connected to the LOUT inductor with local mini planes on the top layer.

#### **Thermal Layout Considerations**

Good thermal layout helps high power dissipation from a small package with reduced temperature rise. Thermal layout guidelines are:

- The exposed pad must be well soldered on the board.
- A four or more layers PCB board with solid ground planes is preferred for better heat dissipation.
- More free vias are welcome to be around IC and/or underneath the exposed pad to connect the inner ground layers to reduce thermal impedance.
- Use large area copper especially in top layer to help thermal conduction and radiation.
- Do not put the inductor to be too close to the IC, thus the heat sources are distributed



**Figure 81. Recommended Minimal Size PCB Layout (Without Optional CAVIN)**



**Figure 82. Recommended Large Size PCB Layout (With Optional CAVIN)**

#### **ORDERING INFORMATION**

#### <span id="page-31-0"></span>**ORDERING INFORMATION**



†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.





(\*) Available upon request (Please contact your ON Semiconductor sales office)

(\*\*) For more detailed information, refer to the Enable section of the DETAILLED OPERATING DESCRIPTION

**Figure 83.** 

### **PACKAGE DIMENSIONS**

**WDFNW8 2x2, 0.5P** CASE 511CL ISSUE B



- 1. DIMENSIONING AND TOLERANCING PER ASME Y14 5M, 2009.
- 2. CONTROLLING DIMENSION: MILLIMETERS
- 3. DIMENSIONS b AND b1 APPLY TO PLATED TERMINALS AND ARE MEASURED BETWEEN 0.15 AND 0.30MM FROM THE TERMINAL TIP.
- 4. COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS THE TERMINALS.





#### RECOMMENDED MOUNTING FOOTPRINT

\* For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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