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SLVSDZ9 –MAY 2019

# **DRV8340-Q1 12-V / 24-V Automotive Gate Driver Unit (GDU) with Independent Half Bridge Control**

**Technical [Documents](http://www.ti.com/product/DRV8340-Q1?dcmp=dsproject&hqs=td&#doctype2)** 

# <span id="page-0-1"></span>**1 Features**

- AEC-Q100 qualified for automotive applications – Temperature grade 1:  $-40^{\circ}$ C ≤ T<sub>A</sub> ≤ 125°C
- Three independent half-bridge gate driver
	- Dedicated source (SHx) and drain (DLx) pins to support independent MOSFET control
	- Drives 3 high-side and 3 low-side N-channel MOSFETs (NMOS)
- Smart gate drive architecture
	- Adjustable slew rate control
	- 1.5-mA to 1-A peak source current
	- 3-mA to 2-A peak sink current
- Charge-pump of gate driver for 100% Duty Cycle
- SPI (S) and hardware (H) interface available
- 6x, 3x, 1x, and independent PWM modes
- Supports 3.3-V, and 5-V logic inputs
- Charge pump output can be used to drive the reverse supply protection MOSFET
- Linear voltage regulator, 3.3 V, 30 mA
- Integrated protection features
	- VM undervoltage lockout (UVLO)
	- Charge pump undervoltage (CPUV)
	- Short to battery (SHT\_BAT)
	- Short to ground (SHT\_GND)
	- MOSFET overcurrent protection (OCP)
	- Gate driver fault (GDF)
	- Thermal warning and shutdown (OTW/OTSD)
	- Fault condition indicator (nFAULT)

# <span id="page-0-2"></span><span id="page-0-0"></span>**2 Applications**

- 12-V and 24-V Automotive Motor-Control Applications
	- BLDC and BDC motor modules
	- Fans and blowers
	- Fuel and water pumps
	- Solenoid drive

# **3 Description**

Tools & [Software](http://www.ti.com/product/DRV8340-Q1?dcmp=dsproject&hqs=sw&#desKit)

The DRV8340-Q1 device is an integrated gate driver for three-phase applications. The device provides three half-bridge gate drivers, each capable of driving high-side and low-side N-channel power MOSFETs. The dedicated Source and Drain pins enable the independent MOSFET control for solenoid application. The DRV8340-Q1 generates the correct gate drive voltages using an integrated charge pump sufficient for the high-side MOSFETs and a linear regulator for the low-side MOSFETs. The Smart Gate Drive architecture supports peak gate drive currents up to 1-A source and 2-A. The DRV8340-Q1 can operate from a single power supply and supports a wide input supply range of 5.5 to 60 V for the gate driver.

Support & **[Community](http://www.ti.com/product/DRV8340-Q1?dcmp=dsproject&hqs=support&#community)** 

 $22$ 

The 6x, 3x, 1x, and independent input PWM modes allow for simple interfacing to controller circuits. The configuration settings for the gate driver and device are highly configurable through the SPI or hardware (H/W) interface.

A low-power sleep mode is provided to achieve low quiescent current. Internal protection functions are provided for undervoltage lockout, charge pump fault, MOSFET overcurrent, MOSFET short circuit, phasenode short to supply and ground, gate driver fault, and overtemperature. Fault conditions are indicated on the nFAULT pin with details through the device registers for the SPI device variant.

## **Device Information[\(1\)](#page-0-0)**



(1) For all available packages, see the orderable addendum at the end of the data sheet.

# **Simplified Schematic**





PP

<span id="page-1-0"></span>**4 Revision History**

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**DATE REVISION NOTES** May 2019 **May 2019 May 2019 May 2019 May 2019 May 2019** 



# **Table of Contents**



NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

**[DRV8340-Q1](http://www.ti.com/product/drv8340-q1?qgpn=drv8340-q1)**



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# <span id="page-2-0"></span>**5 Device Comparison Table**



(1) For more information on the device name and device options, see the *[Device Nomenclature](#page-67-6)* section.

**DRV8340H PHP PowerPAD™ Package 48-Pin HTQFP With Exposed Thermal Pad Top View**

# <span id="page-2-1"></span>**6 Pin Configuration and Functions**



### **Table 1. Pin Functions—DRV8340H**



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## **Table 1. Pin Functions—DRV8340H (continued)**



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#### **DRV8340S PHP PowerPAD™ Package 48-Pin HTQFP With Exposed Thermal Pad Top View**

## **Table 2. Pin Functions—DRV8340S**



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# **Table 2. Pin Functions—DRV8340S (continued)**



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# <span id="page-6-0"></span>**7 Specifications**

# <span id="page-6-1"></span>**7.1 Absolute Maximum Ratings**

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>



(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Continuous high-side gate pin (GHx) and phase node pin voltage (SHx) should be limited to  $-2$  V minimum for an absolute maximum of 65 V on VM. At 60 V and below, the full specification of –5 V continuous on GHx and SHx is allowable.

# <span id="page-6-2"></span>**7.2 ESD Ratings**



(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

**ISTRUMENTS** 

**EXAS** 

# **7.3 Recommended Operating Conditions**



(1) Operation at VM = 5.5V only when coming from higher VM. The minimum VM voltage for startup is greater than V<sub>UVLO</sub> (rising) voltage.<br>(2) VM recommended operating condition for electrical characteristic table. Product (2) VM recommended operating condition for electrical characteristic table. Product life time depends on VM voltage. The device is intended

(3) Power dissipation and thermal limits must be observed

# <span id="page-7-0"></span>**7.4 Thermal Information**



(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics application](http://www.ti.com/lit/pdf/spra953) [report.](http://www.ti.com/lit/pdf/spra953)

for 12–V and 24–V battery automotive system with life-time nominal voltage of 5.5 V - 50 V. The device can be operated during additional overvoltage events as specified in ISO16750-2:2012

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# <span id="page-8-0"></span>**7.5 Electrical Characteristics**

Over recommended operating conditions  $5.5 \le V_{VM} \le 60$  V (unless otherwise noted). Typical limits apply for  $V_{VM} = 24$  V



(1) Does not include OLP/Shorts diagnostic delay time in the H/W device

# **Electrical Characteristics (continued)**

Over recommended operating conditions  $5.5 \le V_{VM} \le 60$  V (unless otherwise noted). Typical limits apply for  $V_{VM} = 24$  V





# **Electrical Characteristics (continued)**

Over recommended operating conditions  $5.5 \le V_{VM} \le 60$  V (unless otherwise noted). Typical limits apply for  $V_{VM} = 24$  V



# **Electrical Characteristics (continued)**

Over recommended operating conditions  $5.5 \le V_{VM} \le 60$  V (unless otherwise noted). Typical limits apply for  $V_{VM} = 24$  V





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# **Electrical Characteristics (continued)**





# **Electrical Characteristics (continued)**



# Over recommended operating conditions  $5.5 \le V_{\text{OM}} \le 60$  V (unless otherwise noted). Typical limits apply for  $V_{\text{OM}} = 24$  V

# <span id="page-13-0"></span>**7.6 SPI Timing Requirements**

Over recommended operating conditions unless otherwise noted. Typical limits apply for  $V_{VM} = 24 V$ 





**Figure 1. SPI Slave Mode Timing Diagram**



## **7.7 Typical Characteristics**

<span id="page-14-0"></span>

# <span id="page-15-0"></span>**8 Detailed Description**

## <span id="page-15-1"></span>**8.1 Overview**

The DRV8340-Q1 device is an integrated gate driver for three-phase motor driver automotive applications. These devices decrease system complexity by integrating three independent half-bridge gate drivers, charge pump, and linear regulator for the supply voltages of the high-side and low-side gate drivers.. A standard serial peripheral interface (SPI) provides a simple method for configuring the various device settings and reading fault diagnostic information through an external controller. Alternatively, a hardware interface (H/W) option allows for configuring the most common settings through fixed external resistors.

The gate drivers support external N-channel high-side and low-side power MOSFETs and can drive up to 1-A source, 2-A sink peak currents. A doubler charge pump generates the supply voltage of the high-side gate drive. This charge pump architecture regulates the VCP output voltage for driving high-side power MOSFET. The supply voltage of the low-side gate driver is generated using a linear regulator from the VM power supply that regulates for driving low-side power MOSFET. A Smart Gate Drive architecture provides the ability to dynamically adjust the strength of the gate drive output current which lets the gate driver control the  $V_{DS}$ switching speed of the power MOSFET. This feature lets the user remove the external gate drive resistors and diodes, reducing the component count in the bill of materials (BOM), cost, and area of the printed circuit board (PCB). The architecture also uses an internal state machine to protect against short-circuit events in the gate driver, control the half-bridge dead time, and protect against dV/dt parasitic turnon of the external power MOSFET.

In addition to the high level of device integration, the DRV8340-Q1 device provides a wide range of integrated protection features. These features include power supply undervoltage lockout (UVLO), charge pump undervoltage lockout (CPUV),  $V_{DS}$  overcurrent monitoring (OCP), gate driver short-circuit detection (GDF), and overtemperature shutdown (OTW and OTSD). Fault events are indicated by the nFAULT pin with detailed information available in the SPI registers on the SPI device version.



## <span id="page-16-0"></span>**8.2 Functional Block Diagram**



**Figure 6. Block Diagram for DRV8340H**

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# **Functional Block Diagram (continued)**



**Figure 7. Block Diagram for DRV8340S**

# <span id="page-17-0"></span>**8.3 Feature Description**

## **8.3.1 Three Phase Smart Gate Drivers**

The DRV8340-Q1 device integrates three, half-bridge gate drivers, each capable of driving high-side and lowside N-channel power MOSFETs. A doubler charge pump provides the correct gate bias voltage to the high-side MOSFET across a wide operating voltage range in addition to providing 100% support of the duty cycle. An internal linear regulator provides the gate bias voltage for the low-side MOSFETs. The half-bridge gate drivers can be used in combination to drive a three-phase motor or separately to drive other types of loads.



#### **Feature Description (continued)**

The DRV8340-Q1 device implements a Smart Gate Drive architecture which allows the user to dynamically adjust the gate drive current without requiring external resistors to limit the gate current. Additionally, this architecture provides a variety of protection features for the external MOSFETs including automatic dead time insertion, prevent of parasitic dV/dt gate turnon, and gate fault detection.

### *8.3.1.1 PWM Control Modes*

The DRV8340-Q1 device provides eight different PWM control modes in the SPI device and seven different modes in the H/W device to support various commutation and control methods. Texas Instruments does not recommend changing the MODE pin or PWM\_MODE register during operation of the power MOSFETs. Set all INHx and INLx pins to logic low before making a MODE pin or PWM\_MODE register change. [Table 3](#page-18-0) shows the different mode settings for the SPI device. The MODE bit setting of 100b is not available in the H/W device.

<span id="page-18-0"></span>

#### **Table 3. 6x PWM Mode Truth Table**

#### **8.3.1.1.1 6x PWM Mode (PWM\_MODE = 000b or MODE Pin Tied to AGND)**

<span id="page-18-1"></span>In 6x PWM mode, each half-bridge supports three output states: low, high, or high-impedance (Hi-Z). The corresponding INHx and INLx signals control the output state as listed in [Table 4](#page-18-1).



#### **Table 4. 6x PWM Mode Truth Table**





**Figure 8. 6-PWM Mode**

### **8.3.1.1.2 3x PWM Mode (PWM\_MODE = 001b or MODE Pin = 18 kΩ to AGND)**

<span id="page-19-0"></span>In 3x PWM mode, the INHx pin controls each half-bridge and supports two output states: low or high. The INLx pin is used to put the half bridge in the Hi-Z state. If the Hi-Z state is not required, tie all INLx pins to logic high. The corresponding INHx and INLx signals control the output state as listed in [Table 5.](#page-19-0)











#### **8.3.1.1.3 1x PWM Mode (PWM\_MODE = 010b or MODE Pin = 75 kΩ to AGND)**

In 1x PWM mode, the DRV8340-Q1 device uses 6-step block commutation tables that are stored internally. This feature allows for a three-phase BLDC motor to be controlled using one PWM sourced from a simple controller. The PWM is applied on the INHA pin and determines the output frequency and duty cycle of the half-bridges.

The half-bridge output states are managed by the INLA, INHB, and INLB pins which are used as state logic inputs. The state inputs can be controlled by an external controller or connected directly to the digital outputs of the Hall effect sensor from the motor (INLA = HALL\_A, INHB = HALL\_B, INLB = HALL\_C). The 1x PWM mode usually operates with synchronous rectification (low-side MOSFET recirculation); however, the mode can be configured to use asynchronous rectification (MOSFET body diode freewheeling) on SPI devices. This configuration is set using the 1PWM\_COM bit in the SPI registers.

The INHC input controls the direction through the 6-step commutation table which is used to change the direction of the motor when Hall effect sensors are directly controlling the state of the INLA, INHB, and INLB inputs. Tie the INHC pin low if this feature is not required.

The INLC input brakes the motor by turning off all high-side MOSFETs and turning on all low-side MOSFETs when the INLC pin is pulled low. This brake is independent of the state of the other input pins. Tie the INLC pin high if this feature is not required. In the SPI device, the brake and coast mode can also be selected by the 1PWM\_BRAKE register (see [Table 22](#page-47-0)).



#### **Table 6. Synchronous 1x PWM Mode**

(1) *!PWM* is the inverse of the PWM signal.

### **Table 7. Asynchronous 1x PWM Mode 1PWM\_COM = 1 (SPI Only)**



[Figure 10](#page-21-0) and [Figure 11](#page-21-0) show the different possible configurations in 1x PWM mode.





### <span id="page-21-0"></span>**8.3.1.1.4 Independent Half-Bridge PWM Mode (PWM\_MODE = 011b or MODE Pin is > 1.5 MΩ to AGND or Hi-Z)**

In independent half-bridge PWM mode, the INHx pin controls each half-bridge independently and supports two output states: low or high. The corresponding INHx and INLx signals control the output state as listed in [Table 8](#page-21-1). The INLx pin is used to change the half-bridge to high impedance. If the high-impedance (Hi-Z) state is not required, tie all INLx pins logic high.



## **Table 8. Independent Half-Bridge Mode Truth Table**

### <span id="page-21-1"></span>**8.3.1.1.5 Phases A and B are Independent Half-Bridges, Phase C is Independent FET (MODE = 100b)**

In this mode, phases A and B are independent half-bridge control, with independent fault handling and dead time enforcement by the device. Phase C is independent FET mode where the dead time inserted by the device is bypassed and both MOSFETs can be turned-on at the same time. This mode is not available in the H/W version.

#### **8.3.1.1.6 Phases B and C are Independent Half-Bridges, Phase A is Independent FET (MODE = 101b or MODE Pin is 75 kΩ to DVDD)**

In this mode, phases B and C are independent half-bridge control, with independent fault handling and dead time enforcement by the device. Phase A is independent FET mode where the dead time inserted by the device is bypassed and both MOSFETs can be turned-on at the same time.

#### **8.3.1.1.7 Phases A is Independent Half-Bridge, Phases B and C are Independent FET (MODE = 110b or MODE Pin is 18 kΩ to DVDD)**

In this mode, phase A is independent half-bridge control, with dead time enforcement by the device. Phases B and C are independent FET mode where the dead time is bypassed and both MOSFETs in a given phase can be turned-on at the same time. Fault handling is also done independently for each FET in phases B and C.

### **8.3.1.1.8 Independent MOSFET Drive Mode (PWM\_MODE = 111b or MODE Pin = 0.47 kΩ to DVDD)**

In independent MOSFET drive mode, the INHx and INLx pins control the outputs, GHx and GLx, respectively. This control mode lets the DRV8340-Q1 device drive separate high-side and low-side loads with each halfbridge. These types of loads include unidirectional brushed DC motors, solenoids, and low-side and high-side switches. In this mode, turning on both the high-side and low-side MOSFETs at the same time in a given halfbridge gate driver is possible to use the device as a high-side or low-side driver. The dead time  $(t_{DFAD})$  is bypassed in the mode and must be inserted by the external MCU.



# **Table 9. Independent PWM Mode Truth Table**





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[Figure 12](#page-22-0) shows how the DRV8340-Q1 device can be used to connect a high-side load and a low-side load at the same time with one half-bridge and drive the loads independently. In this mode, the VDS monitors are active for both the MOSFETs to protect from an overcurrent condition.



**Figure 12. Independent PWM High-Side and Low-Side Drivers**

<span id="page-22-0"></span>If the half-bridge is used to implement only a high-side or low-side driver, using the VDS monitors to help protect from an overcurrent condition is possible as shown in [Figure 13](#page-22-1) or [Figure 14](#page-22-1). The unused gate driver can stay disconnected.



<span id="page-22-1"></span>**Figure 13. One High-Side Driver Community Community Figure 14. One Low-Side Driver** 



[Figure 15](#page-23-0) shows how the DRV8340-Q1 device can be used to connect a solenoid load where both the high-side and low-side MOSFETs can be turned on at the same time to drive the load without causing shoot-through. TI recommends having the external diodes for current recirculation. If a half-bridge is not used, the gate pins (GHx and GLx) can stay unconnected and the sense pins (SHx and DLx) can be tied directly or with a resistor to GND.



**Figure 15. Solenoid Drive Configuration**

### <span id="page-23-0"></span>*8.3.1.2 Device Interface Modes*

The DRV8340-Q1 device supports two different interface modes (SPI and hardware) to let the end application design for either flexibility or simplicity. The two interface modes share the same four pins, allowing the different versions to be pin-to-pin compatible. This compatibility lets application designers evaluate with one interface version and potentially switch to another with minimal modifications to their circuit design and layout.

### **8.3.1.2.1 Serial Peripheral Interface (SPI)**

The SPI devices support a serial communication bus that lets an external controller send and receive data with the DRV8340-Q1 device. This support lets the external controller configure device settings and read detailed fault information. The interface is a four wire interface using the SCLK, SDI, SDO, and nSCS pins which are described as follows:

- The SCLK pin is an input that accepts a clock signal to determine when data is captured and propagated on the SDI and SDO pins.
- The SDI pin is the data input.
- The SDO pin is the data output. The SDO pin has a push-pull output structure.
- The nSCS pin is the chip select input. A logic low signal on this pin enables SPI communication with the DRV8340-Q1 device.

For more information on the SPI, see the *[SPI Communication](#page-42-2)* section.

### **8.3.1.2.2 Hardware Interface**

Hardware interface devices convert the four SPI pins into four resistor-configurable inputs which are IDRIVE, MODE, and VDS. This conversion lets the application designer configure the most common device settings by tying the pin logic high or logic low, or with a simple pullup or pulldown resistor. This removes the requirement for an SPI bus from the external controller. General fault information can still be obtained through the nFAULT pin.

- The IDRIVE pin configures the gate drive current strength.
- The MODE pin configures the PWM control mode.
- The VDS pin configures the voltage threshold of the  $V_{DS}$  overcurrent monitors.

For more information on the hardware interface, see the *[Pin Diagrams](#page-30-0)* section.





#### *8.3.1.3 Gate Driver Voltage Supplies*

The voltage supply for the high-side gate driver is created using a doubler charge pump that operates from the VM voltage supply input. The charge pump lets the gate driver correctly bias the high-side MOSFET gate with respect to the source across a wide input supply voltage range. The charge pump is regulated to keep a fixed output voltage  $V_{VCP}$  and supports an average output current  $I_{GATE_HS}$ . The charge pump is continuously monitored for undervoltage events to prevent under-driven MOSFET conditions. The charge pump requires a ceramic capacitor between the VM and VCP pins to act as the storage capacitor. Additionally, a flying capacitor is required between the CPH and CPL pins.



**Figure 18. Charge Pump Architecture**

The voltage supply of the low-side gate driver is created using a linear regulator that operates from the VM voltage supply input. The linear regulator lets the gate driver correctly bias the low-side MOSFET gate with respect to ground. The linear regulator output is  $V_{GSL}$  and supports an output current  $I_{GATE~LS}$ .

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### *8.3.1.4 Smart Gate Drive Architecture*

The DRV8340-Q1 gate drivers use an adjustable, complimentary, push-pull topology for both the high-side and low-side drivers. This topology allows for both a strong pullup and pulldown of the external MOSFET gates.



**Figure 19. Charge Pump Architecture**

Additionally, the gate drivers use a Smart Gate Drive architecture to provide additional control of the external power MOSFETs, additional steps to protect the MOSFETs, and optimal tradeoffs between efficiency and robustness. This architecture is implemented through two components called IDRIVE and TDRIVE which are described in the *[IDRIVE: MOSFET Slew-Rate Control](#page-26-0)* section and *[TDRIVE: MOSFET Gate Drive Control](#page-26-1)* section. [Figure 20](#page-26-2) shows the high-level functional block diagram of the gate driver.

The IDRIVE gate drive current and TDRIVE gate drive time should be initially selected based on the parameters of the external power MOSFET used in the system and the desired rise and fall times (see the *[Application and](#page-58-0) [Implementation](#page-58-0)* section).

The high-side gate driver also implements a Zener clamp diode to help protect the external MOSFET gate from overvoltage conditions in the case of external short-circuit events on the MOSFET.



**Figure 20. Gate Driver Block Diagram**

±

PGND

 $AGND \rightarrow T$  AGND

#### <span id="page-26-2"></span><span id="page-26-0"></span>**8.3.1.4.1 IDRIVE: MOSFET Slew-Rate Control**

The IDRIVE component implements adjustable gate drive current to control the MOSFET  $V_{DS}$  slew rates. The MOSFET  $V_{DS}$  slew rates are a critical factor for optimizing radiated emissions, energy, and duration of diode recovery spikes, dV/dt gate turnon resulting in shoot-through, and switching voltage transients related to parasitics in the external half-bridge. The IDRIVE component operates on the principal that the MOSFET  $V_{DS}$ slew rates are predominately determined by the rate of gate charge (or gate current) delivered during the MOSFET  $Q<sub>GD</sub>$  or Miller charging region. By letting the gate driver adjust the gate current, the gate driver can effectively control the slew rate of the external power MOSFETs.

The IDRIVE component lets the DRV8340-Q1 device dynamically switch between gate drive currents either through a register setting on SPI devices or the IDRIVE pin on hardware interface devices. The SPI devices provide 16  $I_{DRIVE}$  settings ranging from 1.5-mA to 1-A source and 3-mA to 2-A sink. Hardware interface devices provide 7  $I_{DRIVE}$  settings within the same ranges. The setting of the gate drive current is delivered to the gate during the turnon and turnoff of the external power MOSFET for the t<sub>DRIVE</sub> duration. After the MOSFET turnon or turnoff, the gate driver switches to a smaller hold current  $(I_{HOLD})$  to improve the gate driver efficiency. In the event of an overcurrent condition, the IDRIVE component is automatically decreased to help prevent device damage. For additional details on the IDRIVE settings, see the *[Register Maps](#page-44-0)* section for the SPI devices and the *[Pin](#page-30-0) [Diagrams](#page-30-0)* section for the hardware interface devices.

#### <span id="page-26-1"></span>**8.3.1.4.2 TDRIVE: MOSFET Gate Drive Control**

The TDRIVE component is an integrated gate drive state machine that provides automatic dead time insertion through handshaking between the high-side and low-side gate drivers, parasitic dV/dt gate turnon prevention, and MOSFET gate fault detection.

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The first component of the TDRIVE state machine is automatic dead time insertion. Dead time is period of time between the switching of the external high-side and low-side MOSFETs to make sure that they do not cross conduct and cause shoot-through. The DRV8340-Q1 device uses  $V_{GS}$  voltage monitors to measure the MOSFET gate-to-source voltage and determine the correct time to switch instead of relying on a fixed time value. This feature lets the dead time of the gate driver adjust for variation in the system such as temperature drift and variation in the MOSFET parameters. An additional digital dead time  $(t_{DEAD})$  can be inserted and is adjustable through the registers on SPI devices.

The second component of the TDRIVE state machine is parasitic dV/dt gate turnon prevention. To implement this component, the TDRIVE state machine enables a strong pulldown current (I<sub>STRONG</sub>) on the opposite MOSFET gate whenever a MOSFET is switching. The strong pulldown occurs for the TDRIVE duration. This feature helps remove parasitic charge that couples into the MOSFET gate when the voltage half-bridge switch node slews rapidly.

The third component implements a gate-fault detection scheme to detect pin-to-pin solder defects, a MOSFET gate failure, or a MOSFET gate stuck-high or stuck-low voltage condition. This implementation is done with a pair of  $V_{GS}$  gate-to-source voltage monitors for each half-bridge gate driver. When the gate driver receives a command to change the state of the half-bridge it starts to monitor the gate voltage of the external MOSFET. If, at the end of the t<sub>DRIVE</sub> period, the V<sub>GS</sub> voltage has not increased the correct threshold, the gate driver reports a fault. To make sure that a false gate drive fault (GDF) is not detected, a  $t_{DRIVE}$  time should be selected that is longer than the time required to charge or discharge the MOSFET gate. The  $t_{DRIVE}$  time does not increase the PWM time and will terminate if another PWM command is received while active. In the SPI device, for IDRIVE bit settings of 0000b, 0001b, 0010b, and 0011b, a longer  $t_{DRIVE}$  time of 20-µs is automatically selected by the TDRIVE\_MAX bit. If the 20-µs t<sub>DRVIE</sub> time is not required, write a 0 to the TDRIVE\_MAX bit to disable it and set the t<sub>DRIVE</sub> time by the TDRIVE bits. For all other IDRIVE settings, writing to the TDRIVE\_MAX bit is disabled. This option is not available in the H/W device.

For additional details on the TDRIVE settings, see the *[Register Maps](#page-44-0)* section for SPI devices and the *[Pin](#page-30-0) [Diagrams](#page-30-0)* section for hardware interface devices. [Figure 21](#page-27-0) shows an example of the TDRIVE state machine in operation.

<span id="page-27-0"></span>



#### **8.3.1.4.3 Propagation Delay**

The propagation delay time  $(t_{\text{od}})$  is measured as the time between an input logic edge to a detected output change. This time has three parts consisting of the digital input deglitcher delay, the digital propagation delay, and the delay through the analog gate drivers.

The input deglitcher prevents high-frequency noise on the input pins from affecting the output state of the gate drivers. To support multiple control modes and dead time insertion, a small digital delay is added as the input command propagates through the device. Lastly, the analog gate drivers have a small delay that contributes to the overall propagation delay of the device.

#### 8.3.1.4.4 MOSFET V<sub>DS</sub> Monitors

The gate drivers implement adjustable  $V_{DS}$  voltage monitors to detect overcurrent or short-circuit conditions on the external power MOSFETs. When the monitored voltage is greater than the V<sub>DS</sub> trip point (V<sub>VDS</sub> <sub>OCP</sub>) for longer than the deglitch time  $(t<sub>OCP</sub>)$ , an overcurrent condition is detected and action is taken according to the device  $V_{DS}$  fault mode.

The high-side  $V_{DS}$  monitors measure the voltage between the VDRAIN and SHx pins. The low-side  $V_{DS}$  monitor measures between the DLx and SLx pins.

The V<sub>VDS</sub> <sub>OCP</sub> threshold is programmable from 0.06 V to 1.88 V. For additional information on the V<sub>DS</sub> monitor levels, see the *[Register Maps](#page-44-0)* section for SPI devices and in the *[Pin Diagrams](#page-30-0)* section hardware interface device.



**Figure 22. DRV8340-Q1 V<sub>DS</sub> Monitors** 

## **8.3.1.4.5 VDRAIN Sense Pin**

The DRV8340-Q1 device provides a separate sense pin for the common point of the high-side MOSFET drain. This pin is called VDRAIN. This pin lets the sense line for the overcurrent monitors (VDRAIN) and the power supply (VM) stay separate and prevent noise on the VDRAIN sense line. This separation also lets implementation of a small filter on the gate driver supply (VM) or insertion of a boost converter to support lower voltage operation if desired. Care must still be used when designing the filter or separate supply because VM is still the reference point for the VCP charge pump that supplies the high-side gate drive voltage ( $V_{GSH}$ ). The VM supply must not drift too far from the VDRAIN supply to avoid violating the  $V_{GS}$  voltage specification of the external power MOSFETs.

## **8.3.1.4.6 nFAULT Pin**

The nFAULT pin has an open-drain output and should be pulled up to a 5 V or 3.3 V supply. When a fault is detected, the nFAULT line is logic low. For a 3.3-V pullup the nFAULT pin can be tied to the DVDD pin with a resistor (refer to the *[Application and Implementation](#page-58-0)* section). For a 5-V pullup an external 5-V supply must be used.



(1)

(2)



**Figure 23. nFAULT Pin**

During the power-up sequence, or when going from sleep mode, the digital core of the device is enabled to a VM voltage of approximately 3.3 V and the device is fully operational after VM exceeds 5.5 V. After the digital core is alive if the VM does not exceed 5.5 V within 100-us the device will flag a UVLO fault. In the H/W device, the nFAULT pin is driven low. In the SPI device, the FAULT and ULVO bits will be latched high

### **8.3.2 DVDD Linear Voltage Regulator**

A 3.3-V, 30-mA linear regulator is integrated into the DRV8340-Q1 device and is available for use by external circuitry. This regulator can provide the supply voltage for a low-power MCU or other circuitry supporting low current. The output of the DVDD regulator should be bypassed near the DVDD pin with a X5R or X7R, 1-µF, 6.3- V ceramic capacitor routed directly back to the adjacent AGND ground pin.

The DVDD nominal, no-load output voltage is 3.3 V. When the DVDD load current exceeds 30 mA, the regulator functions like a constant-current source. The output voltage drops significantly with a current load greater than 30 mA.



**Figure 24. DVDD Linear Regulator Block Diagram**

<span id="page-29-0"></span>Use [Equation 1](#page-29-0) to calculate the power dissipated in the device by the DVDD linear regulator.

 $P = (V_{VM} - V_{DVDD}) \times I_{DVDD}$ 

<span id="page-29-1"></span>For example, at a  $V_{VM}$  of 24 V, drawing 20 mA out of DVDD results in a power dissipation as shown in [Equation 2](#page-29-1).

 $P = (24 V - 3.3 V) \times 20 mA = 414 mW$ 



#### <span id="page-30-0"></span>**8.3.3 Pin Diagrams**

[Figure 25](#page-30-1) shows the input structure for the logic level pins, INHx, INLx, ENABLE, nSCS, SCLK, and SDI. The input can be driven with a voltage or external resistor.



**Figure 25. Logic-Level Input Pin Structure**

<span id="page-30-1"></span>[Figure 26](#page-30-2) shows the structure of the seven level input pins, MODE, IDRIVE and VDS, on hardware interface devices. The input can be set with an external resistor.



**Figure 26. Seven Level Input Pin Structure** (1)

<span id="page-30-2"></span>[Figure 27](#page-31-0) shows the structure of the open-drain output pin, nFAULT. The open-drain output requires an external pullup resistor to function correctly.

<sup>(1)</sup> V<sub>I7</sub> requires a 0.47 kΩ resistor to DVDD for MODE input pin. VDS and IDRIVE pins can be directly tied to DVDD.

**EXAS NSTRUMENTS** 



**Figure 27. Open-Drain Output Pin Structure**

### <span id="page-31-0"></span>**8.3.4 Gate Driver Protective Circuits**

The DRV8340-Q1 device is protected against VM undervoltage, charge pump undervoltage, MOSFET VDS overcurrent, gate driver shorts, and overtemperature events. The DRV8340-Q1 device also provides a detection mechanism for open-load, offline short-to-supply, and offline short-to-ground conditions. When a fault occurs, the individual fault bit is set high along with the global FAULT bit in the FAULT status register for the SPI device. The FAULT bit is OR'ed with all the other individual status bits. In the H/W device, only the nFAULT pin is driven low during a fault condition. Some of the protection and detection features can be disabled through SPI in the SPI device, or the nDIAG pin in the H/W device



# **Table 10. Fault Action and Response**



(1) The DRV8340-Q1 has a OTP (one time program) memory which stores TI internal data used for analog functional blocks. The memory has a check-sum feature, and nFAULT is pulled low if a fault is detected at power up.



### *8.3.4.1 VM Supply Undervoltage Lockout (UVLO)*

If at any time the input supply voltage on the VM pin falls lower than the  $V_{\text{UVLO}}$  threshold, all of the external MOSFETs are disabled, the charge pump is disabled, and the nFAULT pin is driven low. The FAULT and VM\_UVLO bits are also latched high in the registers on SPI devices. Normal operation starts again (gate driver operation and the nFAULT pin is released) when the VM undervoltage condition clears. The VM\_UVLO bit stays set until cleared through the CLR FLT bit or an ENABLE pin reset pulse ( $t_{RST}$ ).

## *8.3.4.2 VCP Charge Pump Undervoltage Lockout (CPUV)*

If at any time the voltage on the VCP pin (charge pump) falls lower than the CPUV threshold voltage of the charge pump, all of the external MOSFETs are disabled and the nFAULT pin is driven low. The FAULT and CPUV bits are also latched high in the registers in the SPI device. Normal operation starts again (gate driver operation and the nFAULT pin is released) when the VCP undervoltage condition is removed. The FAULT and CPUV bits stay set until cleared through the CLR\_FLT bit or an ENABLE pin reset pulse  $(t_{RST})$ . Setting the DIS\_CPUV bit high on the SPI devices disables this protection feature. If the DIS\_CPUV bit is set high and a charge pump undervoltage condition occurs, the device keeps operating but the CPUV fault bit is set high in the SPI register until cleared through the CLR\_FLT bit or an ENABLE pin reset pulse (t<sub>RST</sub>). CPUV protection cannot be disabled in the H/W device.

## *8.3.4.3 MOSFET VDS Overcurrent Protection (VDS\_OCP)*

A MOSFET overcurrent event is sensed by monitoring the VDS voltage drop across the external MOSFET  $R_{DS(on)}$ . If the voltage across an enabled MOSFET exceeds the V<sub>VDS OCP</sub> threshold for longer than the t<sub>OCP\_DEG</sub> deglitch time, a VDS\_OCP event is recognized and action is done according to the OCP\_MODE. On hardware interface devices, the V<sub>VDS OCP</sub> threshold is set with the VDS pin, the t<sub>OCP DEG</sub> is fixed at 4 μs, and the OCP\_MODE is configured for latched shutdown but can be disabled by tying the VDS pin to DVDD. In the SPI device, the V<sub>VDS OCP</sub> threshold is set through the VDS\_LVL SPI register, the t<sub>OCP DEG</sub> is set through the OCP\_DEG bits in the SPI register, and the OCP\_MODE bit can operate in four different modes:  $V_{DS}$  latched shutdown,  $V_{DS}$  automatic retry,  $V_{DS}$  report only, and  $V_{DS}$  disabled.

### 8.3.4.3.1 V<sub>DS</sub> Latched Shutdown (OCP\_MODE = 00b)

After a VDS\_OCP event in this mode, all external MOSFETs are disabled and the nFAULT pin is driven low. The FAULT, VDS\_OCP, and corresponding MOSFET OCP bits are latched high in the SPI registers. Normal operation starts again (gate driver operation and the nFAULT pin is released) when the VDS\_OCP condition clears and a clear faults command is issued either through the CLR FLT bit or an ENABLE reset pulse (t<sub>RST</sub>). This is the default mode in both the H/W and SPI device options.

### 8.3.4.3.2 V<sub>DS</sub> Automatic Retry (OCP\_MODE = 01b)

After a VDS OCP event in this mode, all the external MOSFETs are disabled and the nFAULT pin is driven low. The FAULT, VDS\_OCP, and corresponding MOSFET OCP bits are latched high in the SPI registers. Normal operation starts again automatically (gate driver operation and the nFAULT pin is released) after the tRETRY time elapses. The FAULT, VDS OCP, and MOSFET OCP bits stay latched until the  $t_{\text{RFTRY}}$  period expires.

### **8.3.4.3.3 VDS Report Only (OCP\_MODE = 10b)**

No protective action occurs after a VDS\_OCP event in this mode. The overcurrent event is reported by driving the nFAULT pin low and latching the FAULT, VDS\_OCP, and corresponding MOSFET OCP bits high in the SPI registers. The gate drivers continue to operate as usual. The external controller manages the overcurrent condition by acting appropriately. The reporting clears (nFAULT pin is released) when the VDS\_OCP condition clears and a clear faults command is issued either through the CLR FLT bit or an ENABLE reset pulse (t<sub>RST</sub>).

### 8.3.4.3.4 V<sub>DS</sub> Disabled (OCP\_MODE = 11b)

No action occurs after a VDS\_OCP event in this mode. The VDS overcurrent monitor is disabled for all three half-bridges at the same time and the DIS\_VDS\_x bits are locked. In the H/W device, VDS\_OCP is disabled for all three half-bridges at the same time through the VDS pin.



The GHx and GLx pins are monitored such that if the voltage on the external MOSFET gate does not increase or decrease after the t<sub>DRIVE</sub> time, a gate driver fault is detected. This fault may be encountered if the GHx or GLx pins are shorted to the PGND, SHx, SLx, or VM pins. Additionally, a gate driver fault may be encountered if the selected IDRIVE setting is not sufficient to turn on the external MOSFET within the  $t_{DRIVE}$  period. After a gate drive fault is detected, all external MOSFETs are disabled and the nFAULT pin driven low. In addition, the FAULT, GDF, and corresponding VGS bits are latched high in the SPI registers. Normal operation starts again (gate driver operation and the nFAULT pin is released) when the gate driver fault condition is removed and a clear faults command is issued either through the CLR FLT bit or an ENABLE reset pulse ( $t_{RST}$ ). In the SPI device, setting the DIS\_GDF bit high disables this protection feature. If DIS\_GDF bit is set high and a gate drive fault occurs, the device keeps operating but the appropriate VGS fault bit is set high in the SPI register until cleared through the CLR FLT bit or an ENABLE pin reset pulse ( $t_{RST}$ ). GDF cannot be disabled in the H/W device option.

Gate driver faults can indicate that the selected IDRIVE or  $t_{DRIVE}$  settings are too low to slew the external MOSFET in the desired time. Increasing either the IDRIVE or  $t_{DRIVF}$  setting can resolve gate driver faults in these cases. Alternatively, if a gate-to-source short occurs on the external MOSFET, a gate driver fault is reported because of the MOSFET gate not turning on. The  $t_{DRIVE}$  time also refers to the GDF fault blanking time.

Fault handling is done as follows based on the MODE setting:

- In 6x, 3x, and 1x PWM modes a GDF fault in one of the external MOSFETs turns off all the MOSFETs.
- In independent half-bridge mode (MODE = 011b or MODE pin is Hi-Z) a GDF fault in one half-bridge only disables both the MOSFETs in that half-bridge. The MOSFETs in the other half-bridges operate as commanded.
- In independent MOSFET mode (MODE = 111b or MODE pin tied to DVDD) a GDF fault in a MOSFET only disables that particular MOSFET. All the other MOSFETs operate as commanded. The same fault handling scheme applies for MODE =  $100b$ ,  $101b$ , and  $110b$ .
- A GDF fault in phases set as Independent half-bridge disables both MOSFETs in that particular phase.
- A GDF fault in phases set as Independent FET mode disables the MOSFET where the fault occurred.

## *8.3.4.5 Thermal Warning (OTW)*

If the die temperature exceeds the trip point of the thermal warning  $(T<sub>OTW</sub>)$ , the OTW bit is set in the registers of SPI devices. The device performs no additional action and continues to function. When the die temperature falls lower than the hysteresis point of the thermal warning, the OTW bit clears automatically. The OTW bit can also be configured to report on the nFAULT pin by setting the OTW\_REP bit to 1 through the SPI registers. OTW is not available in the H/W device.

### *8.3.4.6 Thermal Shutdown (OTSD)*

If the die temperature exceeds the trip point of the thermal shutdown limit  $(T<sub>OTSD</sub>)$ , all the external MOSFETs are disabled, the charge pump is shut down, and the nFAULT pin is driven low. In addition, the FAULT and OTSD bits are latched high. This protection feature cannot be disabled. The overtemperature protection can operate in two different modes.

#### **8.3.4.6.1 Latched Shutdown (OTSD\_MODE = 0b)**

In latched shutdown mode, after a OTSD event, normal operation starts again (motor driver operation and the nFAULT line released) when the OTSD condition is removed and a clear faults command has been issued either through the CLR\_FLT bit or an nSLEEP reset pulse. This is the default mode for a OTSD event in the SPI device.

When the DRV8340-Q1 device hits thermal shutdown, the OTSD and FAULT bits are latched in the SPI register. Clearing the fault through the CLR\_FLT bit or an nSLEEP reset pulse will clear the OSTD and FAULT bits. When the DRV8340-Q1 device hits thermal shutdown, the device will disable the charge pump without triggering CPUV. The charge pump will be enabled again when the OTSD and FAULT bits are cleared through the CLR FLT bit or an nSleep reset Pulse.



#### **8.3.4.6.2 Automatic Recovery (OTSD\_MODE = 1b)**

In automatic recovery mode, after a OTSD event, normal operation starts again (motor driver operation and the nFAULT line released) when the junction temperature falls to less than the overtemperature threshold limit minus the hysteresis ( $T<sub>OTSD</sub> - T<sub>HYS</sub>$ ). The OTSD bit stays latched high indicating that a thermal event occurred until a clear faults command is issued either through the CLR FLT bit or an nSLEEP reset pulse. This is the default mode for a OTSD event in the H/W device.

### *8.3.4.7 Open Load Detection (OLD)*

If the load is disconnected from the device, an open load is detected and the nFAULT pin is latched low. In the DRV8340-Q1 device, The FAULT, OL SHT, and the corresponding open load (OL\_PH\_x) bits in the SPI register are latched high. When the open-load condition is removed, and the MCU clears the fault through either the CLR FLT bit or an ENABLE-pin reset pulse ( $t_{RST}$ ), the device is ready to drive the motor based on the input commands.

#### **8.3.4.7.1 Open Load Detection in Passive Mode (OLP)**

In open load detection in passive mode, open load diagnosis is performed without the motor in motion. If the motor is disconnected from the device an open load is detected and the nFAULT pin will latch low until a clear faults command is issued by the MCU either through the CLR\_FLT bit or an ENABLE reset pulse. The fault also clears when the device is power cycled or comes out of sleep mode. OLP is designed for applications having capacitance less than the values listed in [Table 11](#page-35-0) between motor phase pins to ground.





<span id="page-35-0"></span>When the open load test is running, all external MOSFETs are disabled. For the H/W device option, at power-up or after going from sleep mode, the offline short-to-supply (SHT\_BAT) and short-to-ground (SHT\_GND) diagnostics run first followed by the OLP diagnostic if the nDIAG pin is left as no connect or tied to GND. If the nDIAG pin is tied to DVDD (or an external 3.3 V) the open load test is not performed. If a short condition is detected, the OLP diagnostic is not run (see [Offline Shorts Diagnostics](#page-38-0)). If a short condition and open load occurs on a given phase at device power-up, for example, only the short condition is reported on the nFAULT pin and through the SPI fault register. In the SPI device option the OLP test is performed when commanded through SPI. If both short and OLP diagnostics are enabled simultaneously and a short condition is detection, only the short condition is reported on the nFAULT pin and through the SPI fault register.

The sequence to perform open load diagnostics in passive mode is as follows:

- 1. Device powered up  $(ENABLE = 1)$ .
- 2. Mode is selected by SPI.
- 3. Hi-Z all three half-bridges by turning-off all the external MOSFETs.
- 4. Write a 1 to the EN\_OLP bit in the SPI register and OLP is performed.
	- If an open load is detected, the nFAULT pin is driven low, and the FAULT bit, the OLD bit, and the respective OL PH x bit are latched high. When the open load condition is removed, a clear faults command must be issued by the MCU either through the CLR\_FLT bit or an ENABLE reset pulse which resets the OL\_PH\_x register bit and causes the nFAULT pin to go high.
	- $-$  If open load is not detected, the EN\_OLP bits return to default setting (0b) after  $t_{OL}$  expires.

The EN OLP register keeps the written command until the diagnostic is complete. The half bridges must stay in Hi-Z state for the entire duration of the test. While open load diagnostic is running, if an input change occurs or the EN OLP bit is set low, the open load test is aborted to start normal operation again, and no fault is reported. OLP should not be performed if the motor is energized.


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The open load detection checks for a high impedance connection on the motor phase pins (SHx or DLx). The diagnostic has two major steps as listed in the *[OLP Steps](#page-36-0)* section. The sequencing of the pullup and pulldown current varies depending on the load connections. [Figure 28](#page-36-1) a simplified H-bridge configuration as an example for open load detection.



**Figure 28. Circuit for Open Load Detection in Passive Mode**

## <span id="page-36-1"></span><span id="page-36-0"></span>*8.3.4.7.1.1 OLP Steps*

The OLP algorithm list is as follows:

- The pullup current source is enabled. If a load is connected, current passes through the pullup resistor and the OLx PU comparator output stays low. If an open load condition occurs, the current through the pullup resistor goes 0 and the OLx\_PU comparator trips high.
- The pulldown current source is enabled. In the same way, the OLx\_PD comparator output either stays low to indicate load-connected, or trips high to indicate an open load condition.
- If both the OLx PU and OLx PD comparators report an open load, the OL PH  $x$  bit in the SPI register latches high, and the nFAULT line goes low, to indicate an OL fault.

When the OL condition is removed, a clear faults command must be issued by the micro-controller either through the CLR\_FLT bit or an ENABLE reset pulse which resets open load register bits. The charge pump stays active during this fault condition. The load connections shown in [Figure 29](#page-37-0) are not supported OLP.





**Figure 29. Load Configurations Not Supported**

#### <span id="page-37-0"></span>**8.3.4.7.2 Open Load Detection in Active Mode (OLA)**

An open load in active mode is disabled by default in the SPI device and can be enabled independently per halfbridge by writing a 1 to the EN\_OLA\_x bit. In the H/W device, OLA runs if the nDIAG pin is left as unconnected or tied to GND. OLA is detected when the motor gets disconnected from the driver when it is commutating. [Figure 30](#page-37-1) shows a simplified H-bridge configuration for OLA implementation during high-side current recirculation. When the voltage drop across the body diode of the MOSFET does not exhibit overshoot greater than the VOLA over VM between the time the low-side FET is switched off and the high side FET is switched on during an output PWM cycle. An open load is not detected if the energy stored in the inductor is high enough to cause an overshoot greater than the  $V_{\text{OIA}}$  over VM caused by the fly-back current flowing through the body diode of the high-side FET.



**Figure 30. Circuit for Open Load Detection in Active Mode**

#### **NOTE**

<span id="page-37-1"></span>Depending on the operating conditions and on external circuitry, such as the output capacitors, an open load could be reported even though the load is present. This case might occur during a direction change or for small load currents respectively small PWM duty cycles. Therefore, TI recommends evaluating the open load diagnosis only in known suitable operating conditions and to ignore it otherwise.



The device has a failure counter to avoid inadvertent triggering of the open load active diagnosis. Three consecutive occurrences of the internal open load signal must occur, essentially three consecutive PWM pulses without freewheeling detected, before an open load is reported through the nFAULT pin and in the respective SPI register.

In the SPI device, depending on the load configuration and the PWM sequence, OLA on one phase can latch all three OL\_PH\_x bits high. In that case, the OLP diagnostic can be initiated to determine which phase has the open load condition. The load connections shown in [Figure 29](#page-37-0) are not supported by OLA.

<span id="page-38-0"></span>For OLA to function correctly, place capacitors between the motor phase node and GND. This capacitor is required for BLDC, bi-directional BDC and unidirectional BDC motors at the phase node. If a solenoid load is connected, as shown in [Figure 15,](#page-23-0) the capacitor is not required. Size the capacitors according [Equation 3](#page-38-0). Make sure that the capacitor  $(C_{phase})$  is placed on the PCB.

$$
C_{phase} \geq \frac{V_{TH} \times C_{rss}}{V_{OLA(min)}} - C_{oss}
$$

where

- $\cdot$  V<sub>TH</sub> is the threshold voltage of the MOSFET.
- $V_{\text{OLA(min)}}$  is 150 mV. (3)

The values of C<sub>rss</sub> and C<sub>oss</sub> of the MOSFETs should be used for 0-V V<sub>DS</sub>. Derating of C<sub>phase</sub> must be considered when selecting the capacitance.

#### *8.3.4.8 Offline Shorts Diagnostics*

The device detects short-to-battery and short-to-ground conditions when the motor is not commutating. These offline diagnostics can be activated in the SPI device by setting the EN\_SHT\_TST bit high. Both the short-tobattery and short-to-ground diagnostics run when the EN\_SHT\_TST bit is set high. In the H/W device, these diagnostics run at power-up or when going from the sleep mode if the nDIAG pin is left unconnected or tied to GND. To disable the diagnostics in the H/W device, connect the nDIAG pin to the DVDD supply (or an external 3.3 V or 5 V rail). The short-to-supply diagnostic runs first (see [Offline Short-to-Supply Diagnostic \(SHT\\_BAT\)](#page-38-1)) followed by the short-to-ground diagnostic (see [Offline Short-to-Ground Diagnostic \(SHT\\_GND\)](#page-39-0)). In the SPI device, the duration for this diagnostics is selected through the OLP\_SHTS\_DLY register. In the H/W device, the duration is fixed to 2 ms.

#### <span id="page-38-1"></span>**8.3.4.8.1 Offline Short-to-Supply Diagnostic (SHT\_BAT)**

When the EN\_SHT\_TST bit is set high, all the pulldown current sources on the DLx pins are enabled. The voltage across each pulldown source is individually measured and compared to an internal threshold  $(V<sub>TH</sub>)$ . If the voltage across any of the current sources exceeds  $V_{TH}$ , the DRV8340-Q1 device flags that as a fault condition. The nFAULT pin is driven low, and in the SPI device the FAULT, OL SHT, and the corresponding SHT\_BAT\_x bit is set. [Figure 31](#page-39-1) shows the internal circuit for the short to battery detection.



**Figure 31. Offline Short-to-Supply Detection Circuit**

<span id="page-39-1"></span>In the SPI device, depending on the load configuration, SHT\_BAT on one phase can latch all three SHT\_BAT\_x bits high. To determine which phase has a short-to-supply fault condition, the external MOSFETs can be enabled and the appropriate VDS\_Lx fault bit is latched indicating the faulty phase node. SHT\_BAT is not supported for load configurations shown in [Figure 29](#page-37-0).

#### <span id="page-39-0"></span>**8.3.4.8.2 Offline Short-to-Ground Diagnostic (SHT\_GND)**

When the EN\_SHT\_TST bit is set high, all the pullup current sources on the SHx pins are enabled. The voltage across each pullup source is individually measured and compared to an internal threshold ( $V<sub>TH</sub>$ ). If the voltage across any of the current sources exceeds  $V<sub>TH</sub>$ , the DRV8340-Q1 device flags that as a fault condition. The nFAULT pin is driven low, and in the SPI device the FAULT, OL\_SHT, and the corresponding SHT\_GND\_x bit is set. [Figure 32](#page-40-0) shows the internal circuit for the short-to-ground detection.



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**Figure 32. Offline Short-to-Ground Detection Circuit**

<span id="page-40-0"></span>In the SPI device, depending on the load configuration, SHT\_GND on one phase can latch all three SHT\_GND\_x bits high. To determine which phase has a short-to-ground fault condition, the external MOSFETs can be enabled and the appropriate VDS Hx fault bit is latched indicating the faulty phase node. SHT\_GND is not supported for load configurations shown in [Figure 29](#page-37-0).

# *8.3.4.9 Reverse Supply Protection*

The circuit in [Figure 33](#page-41-0) can be implemented to help protect the system from reverse supply conditions. This circuit requires the following additional components:

- N-channel MOSFET
- NPN BJT
- Diode
- 10-kΩ and 43-kΩ resistors

The VCP voltage with respect to VM supplies the gate-source voltage of N-channel MOSFET, and the voltage  $V_{VCP}$  depends on VM voltage. The characteristics of N-Channel MOSFET (e.g. gate threshold voltage) and the VM voltage range of the system need to be reviewed by the system integrator.





<span id="page-41-0"></span>**Figure 33. Reverse Supply Protection**



#### **8.4 Device Functional Modes**

#### **8.4.1 Gate Driver Functional Modes**

#### *8.4.1.1 Sleep Mode*

The ENABLE pin manages the state of the DRV8340-Q1 device. When the ENABLE pin is low, the device goes to a low-power sleep mode. In sleep mode, all gate drivers are disabled, all external MOSFETs are disabled, the charge pump is disabled, the DVDD regulator is disabled, and the SPI bus is disabled. The  $t_{SLEEP}$  time must elapse after a falling edge on the ENABLE pin before the device goes to sleep mode. The device comes out of sleep mode automatically if the ENABLE pin is pulled high. The  $t_{\text{WAKE}}$  time must elapse before the device is ready for inputs.

In sleep mode and when  $V_{VM}$  <  $V_{UVLO}$ , all external MOSFETs are disabled. The high-side gate pins, GHx, are pulled to the SHx pin by an internal resistor and the low-side gate pins, GLx, are pulled to the PGND pin by an internal resistor.

#### *8.4.1.2 Operating Mode*

When the ENABLE pin is high and the  $V_{VM}$  voltage is greater than the  $V_{UVLO}$  voltage, the device goes to operating mode. The  $t_{\text{WAKE}}$  time must elapse before the device is ready for inputs. In this mode the charge pump, low-side gate regulator, DVDD regulator, and SPI bus are active.

## *8.4.1.3 Fault Reset (CLR\_FLT or ENABLE Reset Pulse)*

In the case of device latched faults, the DRV8340-Q1 device goes to a partial shutdown state to help protect the external power MOSFETs and system.

When the fault condition clears, the device can go to the operating state again by either setting the CLR\_FLT SPI bit on SPI devices or issuing a result pulse to the ENABLE pin on either interface variant. The ENABLE reset pulse  $(t_{RST})$  consists of a high-to-low-to-high transition on the ENABLE pin. The low period of the sequence should fall with the  $t_{RST}$  time window or else the device will start the complete shutdown sequence. The reset pulse has no effect on any of the regulators, device settings, or other functional blocks

# **8.5 Programming**

This section applies only to the DRV8340-Q1 SPI devices.

#### **8.5.1 SPI Communication**

#### *8.5.1.1 SPI*

On DRV8340-Q1 SPI devices, an SPI bus is used to set device configurations, operating parameters, and read out diagnostic information. The SPI operates in slave mode and connects to a master controller. The SPI input data (SDI) word consists of a 16-bit word, with an 8-bit command and 8 bits of data. The SPI output data (SDO) word consists of 8-bit register data. The first 8 bits are don't care bits.

A valid frame must meet the following conditions:

- The SCLK pin should be low when the nSCS pin transitions from high to low and from low to high.
- The nSCS pin should be pulled high for at least 400 ns between words.
- When the nSCS pin is pulled high, any signals at the SCLK and SDI pins are ignored and the SDO pin is placed in the Hi-Z state.
- Data is captured on the falling edge of the SCLK pin and data is propagated on the rising edge of the SCLK pin.
- The most significant bit (MSB) is shifted in and out first.
- A full 16 SCLK cycles must occur for transaction to be valid.
- If the data word sent to the SDI pin is less than or more than 16 bits, a frame error occurs and the data word is ignored.
- For a write command, the existing data in the register being written to is shifted out on the SDO pin following the 8-bit command data.

# **Programming (continued)**

# **8.5.1.1.1 SPI Format**

The SDI input data word is 16 bits long and consists of the following format:

- 1 read or write bit, W (bit B15)
- 7 address bits, A (bits B14 through B8)
- 8 data bits, D (bits B7 through B0)

The SDO output data word is 16 bits long and the first 5 bits are don't care bits. The data word is the content of the register being accessed.

For a write command (W0 = 0), the response word on the SDO pin is the data currently in the register being written to.

For a read command ( $W0 = 1$ ), the response word is the data currently in the register being read.







# **Figure 34. SPI Slave Timing Diagram**

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# **8.6 Register Maps**

This section applies only to the DRV8340-Q1 SPI devices.

#### **NOTE**

Do not modify reserved registers or addresses not listed in the register map (). Writing to these registers may have unintended effects. For all reserved bits, the default value is 0. To help prevent erroneous SPI writes from the master controller, set the LOCK bits to lock the SPI registers.





<span id="page-44-0"></span>Complex bit access types are encoded to fit into small table cells. [Table 15](#page-44-0) shows the codes that are used for access types in this section.





#### **8.6.1 Status Registers**

[Table 16](#page-45-0) lists the memory-mapped registers for the status registers. All register offset addresses not listed in [Table 16](#page-45-0) should be considered as reserved locations and the register contents should not be modified.

The status registers are used to reporting warning and fault conditions. Status registers are read-only registers.

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#### **Table 16. Status Registers Summary Table**

<span id="page-45-0"></span>

# *8.6.1.1 FAULT Status Register (Address = 0x00) [reset = 0x00]*

<span id="page-45-1"></span>FAULT Status is shown in [Figure 35](#page-45-1) and described in [Table 17](#page-45-3).

#### **Figure 35. FAULT Status Register**



# **Table 17. FAULT Status Register Field Descriptions**

<span id="page-45-3"></span>

# <span id="page-45-2"></span>*8.6.1.2 DIAG Status A Register (Address = 0x01) [reset = 0x00]*

<span id="page-45-4"></span>DIAG Status A is shown in [Figure 36](#page-45-4) and described in [Table 18.](#page-45-5)

# **Figure 36. DIAG Status A Register**



#### **Table 18. DIAG Status A Register Field Descriptions**

<span id="page-45-5"></span>



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# <span id="page-46-0"></span>*8.6.1.3 DIAG Status B Register (Address = 0x02) [reset = 0x00]*

<span id="page-46-2"></span>DIAG Status B is shown in [Figure 37](#page-46-2) and described in [Table 19.](#page-46-3)

## **Figure 37. DIAG Status B Register**



# **Table 19. DIAG Status B Register Field Descriptions**

<span id="page-46-3"></span>

# <span id="page-46-1"></span>*8.6.1.4 DIAG Status C Register (address = 0x03) [reset = 0x00]*

<span id="page-46-4"></span>DIAG Status C iss shown in [Figure 38](#page-46-4) and described in [Table 20](#page-46-5).

#### **Figure 38. DIAG Status C Register**



# **Table 20. DIAG Status C Register Field Descriptions**

<span id="page-46-5"></span>

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# **8.6.2 Control Registers**

[Table 21](#page-47-0) lists the memory-mapped registers for the control registers. All register offset addresses not listed in [Table 21](#page-47-0) should be considered as reserved locations and the register contents should not be modified.

The IC control registers are used to configure the device. Control registers are read and write capable.

#### **Table 21. Control Registers Summary Table**

<span id="page-47-0"></span>

#### <span id="page-47-1"></span>*8.6.2.1 IC1 Control Register (Address = 0x04) [reset = 0x00]*

<span id="page-47-2"></span>IC1 Control is shown in [Figure 39](#page-47-2) and described in [Table 22.](#page-47-3)

#### **Figure 39. IC1 Control Register**



#### **Table 22. IC1 Control Field Descriptions**

<span id="page-47-3"></span>



# **[DRV8340-Q1](http://www.ti.com/product/drv8340-q1?qgpn=drv8340-q1)**

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# <span id="page-48-0"></span>*8.6.2.2 IC2 Control Register (address = 0x05) [reset = 0x40]*

<span id="page-48-1"></span>IC2 Control is shown in [Figure 40](#page-48-1) and described in [Table 23.](#page-48-2)

# **Figure 40. IC2 Control Register**



# **Table 23. IC2 Control Field Descriptions**

<span id="page-48-2"></span>

# <span id="page-49-0"></span>*8.6.2.3 IC3 Control Register (Address = 0x06) [reset = 0xFF]*

<span id="page-49-1"></span>IC3 Control is shown in [Figure 41](#page-49-1) and described in [Table 24.](#page-49-2)

# **Figure 41. IC3 Control Register**



<span id="page-49-2"></span>

# **Table 24. IC3 Control Field Descriptions**



# <span id="page-50-0"></span>*8.6.2.4 IC4 Control Register (Address = 0x07) [reset = 0xFF]*

<span id="page-50-1"></span>IC4 Control is shown in [Figure 42](#page-50-1) and described in [Table 25.](#page-50-2)

# **Figure 42. IC4 Control Register**



<span id="page-50-2"></span>

# **Table 25. IC4 Control Field Descriptions**

# <span id="page-51-0"></span>*8.6.2.5 IC5 Control Register (Address = 0x08) [reset = 0xFF]*

<span id="page-51-1"></span>IC5 Control is shown in [Figure 43](#page-51-1) and described in [Table 26.](#page-51-2)

# **Figure 43. IC5 Control Register**



<span id="page-51-2"></span>

# **Table 26. IC5 Control Field Descriptions**



# <span id="page-52-0"></span>*8.6.2.6 IC6 Control Register (Address = 0x09) [reset = 0x99]*

<span id="page-52-1"></span>IC6 Control is shown in [Figure 44](#page-52-1) and described in [Table 27.](#page-52-2)

# **Figure 44. IC6 Control Register**



<span id="page-52-2"></span>

# **Table 27. IC6 Control Field Descriptions**

# <span id="page-53-0"></span>*8.6.2.7 IC7 Control Register (Address = 0x0A) [reset = 0x99]*

<span id="page-53-1"></span>IC7 Control is shown in [Figure 45](#page-53-1) and described in [Table 28.](#page-53-2)

# **Figure 45. IC7 Control Register**



<span id="page-53-2"></span>

# **Table 28. IC7 Control Field Descriptions**



# <span id="page-54-0"></span>*8.6.2.8 IC8 Control Register (Address = 0x0B) [reset = 0x99]*

<span id="page-54-1"></span>IC8 control is shown in [Figure 46](#page-54-1) and described in [Table 29.](#page-54-2)

# **Figure 46. IC8 Control Register**



<span id="page-54-2"></span>

#### **Table 29. IC8 Control Field Descriptions**

# <span id="page-55-0"></span>*8.6.2.9 IC9 Control Register (Address = 0x0C) [reset = 0x2F]*

<span id="page-55-2"></span>IC9 Control is shown in [Figure 47](#page-55-2) and described in [Table 30.](#page-55-3)

## **Figure 47. IC9 Control Register**



#### **Table 30. IC9 Control Field Descriptions**

<span id="page-55-3"></span>

# <span id="page-55-1"></span>*8.6.2.10 IC10 Control Register (Address = 0x0D) [reset = 0x61]*

<span id="page-55-4"></span>IC10 Control is shown in [Figure 48](#page-55-4) and described in [Table 31.](#page-55-5)

#### **Figure 48. IC10 Control Register**





<span id="page-55-5"></span>



# **[DRV8340-Q1](http://www.ti.com/product/drv8340-q1?qgpn=drv8340-q1)**



#### **Table 31. IC10 Control Field Descriptions (continued)**

# <span id="page-56-0"></span>*8.6.2.11 IC11 Control Register (Address = 0x0E) [reset = 0x00]*

<span id="page-56-2"></span>IC11 Control is shown in [Figure 49](#page-56-2) and described in [Table 32.](#page-56-3)

#### **Figure 49. IC11 Control Register**



# <span id="page-56-3"></span>**Bit** Field Type Default Description 7 RSVD RW 0b Reserved 6 OTW\_REP R/W 0b **0b = Overtemperature warning is not reported on nFAULT** 1b = Overtemperature warning is reported on nFAULT 5 CBC **R/W** 0b In retry OCP\_MODE, for both VDS\_OCP, the fault is automatically cleared when a PWM input is given 4 DIS\_VDS\_C R/W 0b Write a 1 to this bit to disable VDS\_OCP for MOSFETs in Phase C 3 DIS\_VDS\_B R/W 0b Write a 1 to this bit to disable VDS\_OCP for MOSFETs in Phase B 2 DIS\_VDS\_A R/W 0b Write a 1 to this bit to disable VDS\_OCP for MOSFETs in Phase A 1-0 OCP\_MODE R/W 00b **00b = Overcurrent causes a latched fault** 01b = Overcurrent causes an automatic retrying fault

# **Table 32. IC11 Control Field Descriptions**

# <span id="page-56-1"></span>*8.6.2.12 IC12 Control Register (Address = 0x0F) [reset = 0x2A]*

IC12 Control is shown in and described in .

# **Figure 50. IC12 Control Register**



#### **Table 33. IC12 Control Field Descriptions**



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10b = Overcurrent is report only but no action is taken 11b = Overcurrent is not reported and no action is taken

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#### **Table 33. IC12 Control Field Descriptions (continued)**



# <span id="page-57-0"></span>*8.6.2.13 IC13 Control Register (Address = 0x10) [reset = 0x7F]*

IC13 Control is shown in and described in .

## **Figure 51. IC13 Control Register**



## **Table 34. IC13 Control Field Descriptions**



# <span id="page-57-1"></span>*8.6.2.14 IC14 Control Register (Address = 0x10) [reset = 0x00]*

IC14 Control is shown in and described in .

# **Figure 52. IC14 Control Register**



#### **Table 35. IC14 Control Field Descriptions**





# **9 Application and Implementation**

# **NOTE**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

## **9.1 Application Information**

The DRV8340-Q1 device is primarily used in applications for three-phase brushless DC motor control. The design procedures in the *[Typical Application](#page-58-0)* section highlight how to use and configure the DRV8340-Q1 device.

# <span id="page-58-0"></span>**9.2 Typical Application**

#### **9.2.1 Primary Application**

The DRV8340-Q1 SPI device is used in this application example.



# **Typical Application (continued)**



**Figure 53. Primary Application Schematic**



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# **Typical Application (continued)**

# *9.2.1.1 Design Requirements*

lists the example input parameters for the system design.



**Table 36. Design Parameters**

## *9.2.1.2 Detailed Design Procedure*

#### **9.2.1.2.1 External MOSFET Support**

<span id="page-60-0"></span>The DRV8340-Q1 MOSFET support is based on the capacity of the charge pump and PWM switching frequency of the output. For a quick calculation of MOSFET driving capacity, use [Equation 4](#page-60-0) and [Equation 5](#page-60-1) for three phase BLDC motor applications.

**Trapezoidal 120° Commutation:**  $I_{VCP} > Q_q \times f_{PWM}$ 

where

- $f_{\text{PWM}}$  is the maximum desired PWM switching frequency.
- $I_{VCP}$  is the charge pump capacity, which depends on the VM pin voltage.
- The multiplier based on the commutation control method, may vary based on implementation. (4)

**Sinusoidal 180° Commutation:**  $I_{VCP} > 3 \times Q_g \times f_{PWM}$  (5)

#### <span id="page-60-1"></span>*9.2.1.2.1.1 Example*

If a system with a V<sub>VM</sub> voltage of 8 V ( $I_{VCP}$  = 15 mA) uses a maximum PWM switching frequency of 10 kHz, then the charge pump can support MOSFETs using trapezoidal commutation with a  $\mathsf{Q}_{\mathsf{g}}$  less than 750 nC, and MOSFETs using sinusoidal commutation with a  ${\sf Q}_{\sf g}$  less than 250 nC.

#### **9.2.1.2.2 IDRIVE Configuration**

The strength of the gate drive current,  $I_{DRIVE}$ , is selected based on the gate-to-drain charge of the external MOSFETs and the target rise and fall times at the outputs. If  $I_{DRIVE}$  is selected to be too low for a given MOSFET, then the MOSFET may not turn on completely within the  $t_{DRIVE}$  time and a gate drive fault may be asserted. Additionally, slow rise and fall times result in higher switching power losses. TI recommends adjusting these values in the system with the required external MOSFETs and motor to determine the best possible setting for any application.

The I<sub>DRIVEP</sub> and I<sub>DRIVEN</sub> current for both the low-side and high-side MOSFETs are independently adjustable on SPI devices through the SPI registers. On hardware interface devices, both source and sink settings are selected at the same time on the IDRIVE pin.

<span id="page-60-2"></span>For MOSFETs with a known gate-to-drain charge  $Q_{gd}$ , desired rise time (t<sub>r</sub>), and a desired fall time (t<sub>f</sub>), use [Equation 6](#page-60-2) and [Equation 7](#page-60-3) to calculate the value of  $I_{DRIVER}$  and  $I_{DRIVER}$  (respectively).

 $I_{DRIVER} > Q_{ad} \times t_r$ 

 $I_{DRIVEN} = 2 \times I_{DRIVEP}$ 

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(6) (7)

#### *9.2.1.2.2.1 Example*

<span id="page-61-0"></span>Use [Equation 8](#page-61-0) to calculate the value of  $I_{DRIVEP}$  for a gate-to-drain charge of 14 nC and a rise time from 100 to 300 ns.

$$
I_{DRIVER} = \frac{12 \text{ nC}}{1000 \text{ ns}} 14 \text{ mA}
$$

Select an I<sub>DRIVEP</sub> value that is close to 14 mA which will set the I<sub>DRIVEN</sub> value close to 28 mA. For this example, the value of  $I_{DRiVEP}$  was selected as 15 mA.

#### 9.2.1.2.3 V<sub>DS</sub> Overcurrent Monitor Configuration

<span id="page-61-1"></span>The V<sub>DS</sub> monitors are configured based on the worst-case motor current and the R<sub>DS(on)</sub> of the external MOSFETs as shown in [Equation 9.](#page-61-1)

 $V_{DS}$   $_{OCP}$  >  $I_{max}$   $\times$   $R_{DS(on)max}$ 

#### *9.2.1.2.3.1 Example*

The goal of this example is to set the  $V_{DS}$  monitor to trip at a current greater than 100 A. According to the CSD18536KCS 60 V N-Channel NexFET<sup>™</sup> Power MOSFET data sheet, the R<sub>DS(on)</sub> value is 1.8 times higher at 175°C, and the maximum R<sub>DS(on)</sub> value at a V<sub>GS</sub> of 10 V is 1.6 mΩ. From these values, the approximate worstcase value of R<sub>DS(on)</sub> is 1.8 × 1.6 m $\Omega$  = 2.88 m $\Omega$ .

<span id="page-61-2"></span>Using [Equation 9](#page-61-1) with a value of 2.88 mΩ for R<sub>DS(on)</sub> and a worst-case motor current of 100 A, [Equation 10](#page-61-2) shows the calculated the value of the  $V_{DS}$  monitors.

$$
V_{DS\_OCP} > 100 A \times 2.88 m\Omega
$$
  
\n
$$
V_{DS\_OCP} > 0.288 V
$$
 (10)

For this example, the value of  $V_{DS\_OCP}$  was selected as 0.31 V.

The SPI devices allow for adjustment of the deglitch time for the  $V_{DS}$  overcurrent monitor. The deglitch time can be set to 2 µs, 4 µs, 6 µs, 8 µs, 10 µs, 12 µs, 16 µs, or 20 µs.

#### **9.2.1.2.4 Design consideration of low-side gate drive (IDRIVE, GLx, SLx)**

The VGLS linear regulator of low-side gate driver is biased with respect to AGND. Since the external FET is referenced to bridge ground, any difference between the two grounds may cause the effective gate-source voltage on the low-side MOSFET to increase during high current switching events.

Steps can be taken during the design stage to reduce the severity of this effect

- Avoid excessively fast switching transients in the bridge ( <100ns slew rates on the phase node)
- Ensure low inductance between SLx pin to MOSFET ground
- <span id="page-61-3"></span>• Ensure low inductance in the path from GLx pin to MOSFET Gate . As a guidance, the below relationships [Equation 11](#page-61-3) may be used to estimate the highest  $V_{GSL}$  expected. The 1V term in the equation is required for additional margin.

$$
V_{GSL\_SWITCHING} = V_{GSL} + 1V + \frac{I_{DRIVER}^2}{Q_g} \times L_{gate}
$$

where

- $V_{\text{GSL}$  switching is the effective gate-source voltage on the low-side MOSFET
- $V_{GS}$  is the low-side gate drive voltage with no output load of GLx
- $I_{DRIVEP}$  is the peak source gate current
- $\quad$  Q<sub>g</sub> is the total gate charge of MOSFET
- $L_{\text{gate}}$  is the parasitic inductance in the path from GLx pin to MOSFET gate  $(11)$

(8)

(9)



#### **9.2.1.2.5 External Components**

lists the recommended external components.



#### **Table 37. External Components**

(1) The effective capacitance of ceramic capacitors varies with DC operating voltage and temperature. As a rule of thumb, expect the effective capacitance to decrease by as much as 50% at the extremes of the operating voltage. The system designer must review the capacitor characteristics and select the component accordingly.

(2) The VCC pin is not a pin on the DRV8340-Q1 device, but a VCC supply voltage pullup is required for the open-drain output, nFAULT. These pins can also be pulled up to DVDD.

# *9.2.1.3 Application Curves*



(1) SOC is available for DRV8343-Q1.



# **10 Power Supply Recommendations**

The DRV8340-Q1 device is designed to operate from an input voltage supply (VM) range from 6 V to 60 V.

# **10.1 Power Supply Consideration in Generator Mode**

When the motor shaft of BLDC or PMSM motor is turned by an external force, the motor windings will generate a voltage on the motor inputs. This condition is known as generator mode or motor back-drive. In the generator mode, a positive voltage can be observed on SHx pins of the device. If there is a switch between VDRAIN and VM (SW<sub>VDRAIN</sub> in [Figure 56](#page-63-0)) and the following conditions exist in the system, the absolute max voltage of VCP with respect to VM needs to be reviewed;

- Generator mode
- $SW<sub>VDRAIN</sub>$  is off
- VM and VCP are low voltage (e.g.  $VM = 0V$ )

If SHx voltage ( $V_{SHx}$ ) exceeds VCP voltage, the VCP voltage starts following  $V_{SHx}$  because of the device internal diodes D1 and D2 (or D3). If VCP - VM voltage exceeds the absolute max voltage of DRV8340-Q1, the ESD diode D4 starts conducting and results in a big current from SHx to VM through the diodes D2, D1 and D4. To avoid this condition, it is recommended to add an external diode  $D_{VDRAIN~VM}$  between VDRAIN and VM.



**Figure 56. Power Supply Consideration in Generator mode**

# <span id="page-63-0"></span>**10.2 Bulk Capacitance Sizing**

Having appropriate local bulk capacitance is an important factor in motor drive system design. It is generally beneficial to have more bulk capacitance, while the disadvantages are increased cost and physical size. The amount of local capacitance depends on a variety of factors including:

- The highest current required by the motor system
- The power supply's type, capacitance, and ability to source current



# **Bulk Capacitance Sizing (continued)**

- The amount of parasitic inductance between the power supply and motor system
- The acceptable supply voltage ripple
- Type of motor (brushed DC, brushless DC, stepper)
- The motor startup and braking methods

The inductance between the power supply and motor drive system will limit the rate current can change from the power supply. If the local bulk capacitance is too small, the system will respond to excessive current demands or dumps from the motor with a change in voltage. When adequate bulk capacitance is used, the motor voltage stays stable and high current can be quickly supplied.

The data sheet provides a recommended minimum value, but system level testing is required to determine the appropriate sized bulk capacitor.



**Figure 57. Motor Drive Supply Parasitics Example**



# **11 Layout**

#### **11.1 Layout Guidelines**

Bypass the VM pin to the PGND pin using a low-ESR ceramic bypass capacitor  $C<sub>VMI</sub>$ . Place this capacitor as close to the VM pin as possible with a thick trace or ground plane connected to the PGND pin. Additionally, bypass the VM pin using a bulk capacitor rated for VM. This component can be electrolytic. This capacitance must be at least 10 µF.

Additional bulk capacitance is required to bypass the high current path on the external MOSFETs. This bulk capacitance should be placed such that it minimizes the length of any high current paths through the external MOSFETs. The connecting metal traces should be as wide as possible, with numerous vias connecting PCB layers. These practices minimize inductance and let the bulk capacitor deliver high current.

Place a low-ESR ceramic capacitor  $C_{F1Y}$  between the CPL and CPH pins. Additionally, place a low-ESR ceramic capacitor  $C_{VCP}$  between the VCP and VM pins.

Bypass the DVDD pin to the AGND pin with C<sub>DVDD</sub>. Place this capacitor as close to the pin as possible and minimize the path from the capacitor to the AGND pin.

The VDRAIN pin can be shorted directly to the VM pin. However, if a significant distance is between the device and the external MOSFETs, use a dedicated trace to connect to the common point of the drains of the high-side external MOSFETs. Do not connect the SLx pins directly to PGND. Instead, use dedicated traces to connect these pins to the sources of the low-side external MOSFETs. These recommendations offer more accurate  $V_{DS}$ sensing of the external MOSFETs for overcurrent detection.

Minimize the loop length for the high-side and low-side gate drivers. The high-side loop is from the GHx pin of the device to the high-side power MOSFET gate, then follows the high-side MOSFET source back to the SHx pin. The low-side loop is from the GLx pin of the device to the low-side power MOSFET gate, then follows the low-side MOSFET source back to the PGND pin.



# **11.2 Layout Example**



# **Figure 58. Layout Example**



# **12 Device and Documentation Support**

#### **12.1 Device Support**

#### **12.1.1 Device Nomenclature**

The following figure shows a legend for interpreting the complete device name:



## **12.2 Documentation Support**

#### **12.2.1 Related Documentation**

- Texas Instruments, *[AN-1149 Layout Guidelines for Switching Power Supplies](http://www.ti.com/lit/pdf/SNVA021)* application report
- Texas Instruments, *[Enhanced Fault Diagnostics in DRV834x-Q1](http://www.ti.com/lit/pdf/SLVA973)* TI TechNote
- Texas Instruments, *[Hardware Design Considerations for an Electric Bicycle using BLDC Motor](http://www.ti.com/lit/pdf/SLVA642)*
- Texas Instruments, *[Layout Guidelines for Switching Power Supplies](http://www.ti.com/lit/pdf/SNVA021)*
- Texas Instruments, *[Sensored 3-Phase BLDC Motor Control Using MSP430™](http://www.ti.com/lit/pdf/SLAA503)* application report
- Texas Instruments, *[Understanding IDRIVE and TDRIVE In TI Motor Gate Drivers](http://www.ti.com/lit/pdf/SLVA714)* application report

# **12.3 Receiving Notification of Documentation Updates**

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

#### **12.4 Community Resources**

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of](http://www.ti.com/corp/docs/legal/termsofuse.shtml) [Use.](http://www.ti.com/corp/docs/legal/termsofuse.shtml)

**[TI E2E™ Online Community](http://e2e.ti.com)** *TI's Engineer-to-Engineer (E2E) Community.* Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**[Design Support](http://support.ti.com/)** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

#### **12.5 Trademarks**

PowerPAD, NexFET, MSP430, E2E are trademarks of Texas Instruments. All other trademarks are the property of their respective owners.



#### **12.6 Electrostatic Discharge Caution**



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

# **12.7 Glossary**

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

# **13 Mechanical, Packaging, and Orderable Information**

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



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# **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

**(6)** Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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# **PACKAGE OPTION ADDENDUM**



**TEXAS** 

# **TAPE AND REEL INFORMATION**

**ISTRUMENTS** 





#### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**






www.ti.com

### **PACKAGE MATERIALS INFORMATION**

www.ti.com 24-Feb-2023



\*All dimensions are nominal



**7 x 7, 0.5 mm pitch** QUAD FLATPACK

### **GENERIC PACKAGE VIEW**

**PHP 48 TQFP - 1.2 mm max height** 

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.





### **PACKAGE OUTLINE**

### **PHP0048C** PowerPAD™ TQFP - 1.2 mm max height

PLASTIC QUAD FLATPACK



NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. Reference JEDEC registration MS-026.
- 5. Feature may not be present.



### **EXAMPLE BOARD LAYOUT**

## **PHP0048C PowerPAD TQFP - 1.2 mm max height** TM

PLASTIC QUAD FLATPACK



NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. See technical brief, Powerpad thermally enhanced package, Texas Instruments Literature No. SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.
- 10. Size of metal pad may vary due to creepage requirement.



#### **EXAMPLE STENCIL DESIGN**

# **PHP0048C PowerPAD TQFP - 1.2 mm max height** TM

PLASTIC QUAD FLATPACK



NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.



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