# RENESAS

# DATASHEET

#### ISL3150E, ISL3152E, ISL3153E, ISL3155E, ISL3156E, ISL3158E Large 3V Output Swing, 16.5kV ESD, Full Fail-Safe, 1/8 Unit Load, RS-485/RS-422 Transceivers

The ISL315xE ([ISL3150E,](https://www.renesas.com/isl3150e) [ISL3152E,](https://www.renesas.com/isl3152e) [ISL3153E,](https://www.renesas.com/isl3153e)

[ISL3155E,](https://www.renesas.com/isl3155e) [ISL3156E,](https://www.renesas.com/isl3156e) and [ISL3158E\)](https://www.renesas.com/isl3158e) family of 5V powered RS-485/RS-422 transceivers features high output drive and high ESD protection and high EFT immunity. The devices withstand  $\pm 16.5$ kV IEC61000-4-2 ESD strikes and are immune to ±4kV IEC6100-4-4 EFT transients without latch-up. The large output voltage of 3.1V typical into a 54 $\Omega$  load provides high noise immunity, and enables the drive of up to 8000ft long bus segments, or eight  $120\Omega$  terminations in a star topology.

These devices possess less than 125µA bus input currents, thus constituting a true 1/8 unit load. The high output drive combined with the low bus input currents allows for connecting up to 512 transceivers on the same bus.

The receiver inputs feature a full fail-safe design that turns the receiver outputs high when the bus inputs are open or shorted.

The ISL315xE family includes half and full-duplex transceivers with active-high driver-enable pins and active-low receiver enable pins. These transceivers support data rates of 115kbps, 1Mbps, and 20Mbps. Their performance is characterized from -40°C to +85°C.

#### **Features**

- High V<sub>OD</sub>: 3.1V (Typ) into  $R_D = 54\Omega$
- $\cdot$  Low bus currents: 125 $\mu$ A constitutes a true 1/8 unit load
- Allows for up to 512 transceivers on the bus
- $\cdot \pm 16.5$ kV ESD protection on bus I/O pins
- $\cdot$  ±4kV EFT immunity on bus I/O pins
- $\cdot$  High transient overvoltage tolerance of  $\pm 100V$
- ï Full fail-safe outputs for open or shorted inputs
- Hot plug capability driver and receiver outputs remain high-impedance during power-up and power-down
- ï Supported data rates: 115kbps, 1Mbps, 20Mbps
- Low supply current (driver disabled): 550µA
- Ultra-low shutdown current: 70nA

#### **Applications**

- Automated utility e-meter reading systems
- High node count systems
- PROFIBUS and Fieldbus systems in factory automation
- Security camera networks
- Lighting, elevator, and HVAC control systems in building automation
- Industrial process control networks
- Networks with star topology
- Long-haul networks in coal mines and oil rigs







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### <span id="page-3-1"></span>**1.1 Typical Operating Circuits**



**Figure 2. Typical Operating Circuits of Half-Duplex and Full-Duplex Transceivers**

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**Notes:**

<span id="page-4-2"></span>1. Refer to **TB347** for details about reel specifications.

<span id="page-4-0"></span>2. These Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb-free soldering operations). Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.

<span id="page-4-1"></span>3. For Moisture Sensitivity Level (MSL), see the product information pages for the [ISL3150E](https://www.renesas.com/isl3150e), [ISL3152E,](https://www.renesas.com/isl3152e) [ISL3153E](https://www.renesas.com/isl3153e), [ISL3155E](https://www.renesas.com/isl3155e), [ISL3156E,](https://www.renesas.com/isl3156e) and [ISL3158E.](https://www.renesas.com/isl3158e) For more information about MSL, see [TB363](https://www.renesas.com/document/oth/tb363-guidelines-handling-and-processing-moisture-sensitive-surface-mount-devices-smds).



#### **Table 1. Key Differences of Device Features**



### <span id="page-5-0"></span>**2. Pin Information**

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### <span id="page-6-0"></span>**3. Specifications**

#### <span id="page-6-1"></span>**3.1 Absolute Maximum Ratings**



**CAUTION:** Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions can adversely impact product reliability and result in failures not covered by warranty. **Notes:**

<span id="page-6-4"></span>4. Absolute Maximum ratings mean the device will not be damaged if operated under these conditions. It does not guarantee performance.

<span id="page-6-6"></span>5. Tested according to TIA/EIA-485-A, Section 4.2.6 (±100V for 15µs at a 1% duty cycle).

### <span id="page-6-2"></span>**3.2 Thermal Information**



**Note:**

<span id="page-6-5"></span>6.  $θ<sub>l</sub>A$  is measured with the component mounted on a high-effective thermal conductivity test board in free air. See [TB379](https://www.renesas.com/document/oth/tb379-thermal-characterization-packaged-semiconductor-devices) for details.



#### <span id="page-6-3"></span>**3.3 Recommended Operating Conditions**





### <span id="page-7-0"></span>**3.4 Electrical Specifications**

Test Conditions: V<sub>CC</sub> = 4.5V to 5.5V; unless otherwise specified. Typical values are at V<sub>CC</sub> = 5V, T<sub>A</sub> = +25°C (<u>Note 7</u>). **Boldface limits apply across the operating temperature range, -40°C to +85°C**.





Test Conditions: V<sub>CC</sub> = 4.5V to 5.5V; unless otherwise specified. Typical values are at V<sub>CC</sub> = 5V, T<sub>A</sub> = +25°C (<u>Note 7</u>). **Boldface limits apply across the operating temperature range, -40°C to +85°C**. **(Continued)**

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Test Conditions: V<sub>CC</sub> = 4.5V to 5.5V; unless otherwise specified. Typical values are at V<sub>CC</sub> = 5V, T<sub>A</sub> = +25°C (Note 7). **Boldface limits apply across the operating temperature range, -40°C to +85°C**. **(Continued)**

#### **Notes:**

- <span id="page-10-3"></span>7. All currents in to device pins are positive; all currents out of device pins are negative. All voltages are referenced to device ground unless otherwise specified.
- <span id="page-10-4"></span>8. Supply current specification is valid for loaded drivers when DE = 0V.
- <span id="page-10-2"></span>9. Applies to peak current. See "Performance Curves" beginning on [page 15](#page-14-0) for more information.
- <span id="page-10-6"></span>10. Keep  $\overline{RE}$  = 0 to prevent the device from entering SHDN.
- <span id="page-10-9"></span>11. The  $\overline{\text{RE}}$  signal high time must be short enough (typically <100ns) to prevent the device from entering SHDN.
- <span id="page-10-7"></span>12. Transceivers are put into shutdown by bringing RE high and DE low. If the inputs are in this state for less than 60ns, the parts are guaranteed not to enter shutdown. If the inputs are in this state for at least 600ns, the parts are guaranteed to have entered shutdown. See "Low Current Shutdown Mode" on page 21.
- <span id="page-10-8"></span>13. Keep  $\overline{RE}$  = V<sub>CC</sub>, and set the DE signal low time >600ns to ensure that the device enters SHDN.
- <span id="page-10-10"></span>14. Set the RE signal high time >600ns to ensure that the device enters SHDN.
- <span id="page-10-0"></span>15. Parameters with MIN and/or MAX limits are 100% tested at +25°C, unless otherwise specified. Temperature limits established by characterization and are not production tested.
- <span id="page-10-1"></span>16. See [Figure 11 on page 15](#page-14-1) for more information and for performance over temperature.
- <span id="page-10-5"></span>17. Limits established by characterization and are not production tested.



### <span id="page-11-0"></span>**4. Test Circuits and Waveforms**



**Figure 3. Measurement of Driver Differential Output Voltage with Differential Load**

<span id="page-11-1"></span>

**Figure 4. Measurement of Driver Differential Output Voltage with Common-Mode Load**

<span id="page-11-2"></span>

<span id="page-11-3"></span>**Figure 5. Measurement of Driver Propagation Delay and Differential Transition Times**









<span id="page-12-1"></span>



**Figure 7. Measurement of Driver Data Rate**

<span id="page-12-0"></span>

<span id="page-12-2"></span>**Figure 8. Measurement of Receiver Propagation Delay and Data Rate**





<span id="page-13-0"></span>**Figure 9. Measurement of Receiver Enable and Disable Times**



### <span id="page-14-0"></span>**5. Performance Curves**

 $V_{CC}$  = 5V, T<sub>A</sub> = +25°C; Unless otherwise specified



**Figure 10. Driver Output High and Low Voltages vs Output Current**



**Figure 12. Driver Output Voltages vs Common-Mode Voltage**





<span id="page-14-1"></span>**Figure 11. Driver Differential Output Voltage vs Output Current**



**Figure 13. Driver Differential Output Voltage vs Temperature**





V<sub>CC</sub> = 5V, T<sub>A</sub> = +25°C; Unless otherwise specified (Continued)







**Figure 17. Waveforms (ISL3150E, ISL3152E)**



**Figure 19. Waveforms (ISL3153E, ISL3155E)**



**Figure 21. Waveforms (ISL3156E, ISL3158E)**



V<sub>CC</sub> = 5V, T<sub>A</sub> = +25°C; Unless otherwise specified (Continued)



**Figure 22. Differential Rise/Fall Times vs Temperature (ISL3150E, ISL3152E)**



**Figure 24. Differential Rise/Fall Times vs Temperature (ISL3153E, ISL3155E)**



**Figure 26. Differential Rise/Fall Times vs Temperature (ISL3156E, ISL3158E)**



**Figure 23. Differential Propagation Delay vs Temperature (ISL3150E, ISL3152E)**



**Figure 25. Differential Propagation Delay vs Temperature (ISL3153E, ISL3155E)**





### <span id="page-17-0"></span>**6. Device Description**

#### <span id="page-17-1"></span>**6.1 Overview**

The ISL3150E, ISL3153E, and ISL3156E are full-duplex RS-485 transceivers, and the ISL3152E, ISL3155E, and ISL3158E are half-duplex RS-485 transceivers. All transceivers feature a large output signal swing that is 60% higher than standard compliant transceivers. The devices are available in three speed grades suitable for data transmission up to 115kbps, 1Mbps, and 20Mbps.

Each transceiver has an active-high driver enable and an active-low receiver enable function. A shutdown current as low as 70nA can be accomplished by disabling both the driver and receiver for more than 600ns.

#### <span id="page-17-2"></span>**6.2 Functional Block Diagram**



**Figure 28. Block Diagram ISL3150E, ISL3153E, ISL3156E**



**Figure 29. Block Diagram ISL3152E, ISL3155E, ISL3158E**

#### <span id="page-17-3"></span>**6.3 Operating Modes**

#### <span id="page-17-4"></span>**6.3.1 Driver Operation**

A logic high at the driver enable pin, DE, activates the driver and causes the differential driver outputs, Y and Z, to follow the logic states at the data input, DI.

A logic high at DI causes Y to turn high and Z to turn low. In this case, the differential output voltage, defined as  $V_{OD} = V_Y - V_Z$ , is positive. A logic low at DI reverses the output states reverse, turning Y low and Z high, thus making  $V_{OD}$  negative.

A logic low at DE disables the driver, making Y and Z high-impedance. In this condition the logic state at DI is irrelevant. To ensure the driver remains disabled after device power-up, it is recommended to connect DE through a 1kΩ to 10kΩ pull-down resistor to ground.





Note:\* See Shutdown mode explanation in "Low Current Shutdown Mode" on page 21.

#### <span id="page-18-0"></span>**6.3.2 Receiver Operation**

A logic low at the receiver enable pin,  $\overline{RE}$ , activates the receiver and causes its output, RO, to follow the bus voltage at the differential receiver inputs, A and B. Here, the bus voltage is defined as  $V_{AB} = V_A - V_B$ .

For  $V_{AB} \ge -0.05V$ , RO turns high, and for  $V_{AB} \le -0.2V$ , RO turns low. For input voltages between -50mV and -200mV, the state of RO is undetermined, and thus could be high or low.

A logic high at RE disables the receiver, making RO high-impedance. In this condition the polarity and magnitude of the input voltage is irrelevant. To ensure the receiver output remains high when the receiver is disabled, it is recommended to connect RO, using a 1kΩ to 10kΩ pull-up resistor to V<sub>CC</sub>.

To enable the receiver to immediately monitor the bus traffic after device power-up, connect  $\overline{RE}$  through a 1kΩ to  $10kΩ$  pull-down resistor to ground.





Note:\* See Shutdown mode explanation in "Low Current Shutdown Mode" on page 21.

#### <span id="page-18-1"></span>**6.4 Device Features**

#### <span id="page-18-2"></span>**6.4.1 Large Output Signal Swing**

The ISL315xE family has a 60% larger differential output voltage swing than standard RS-485 transceivers. It delivers a minimum V<sub>OD</sub> of 2.4V across a 54Ω differential load, or 1.65V across a 15Ω differential load. [Figure 30](#page-18-3) shows that the V<sub>OD</sub> at 54 $\Omega$  is more than 50% higher than that of a standard transceiver.



<span id="page-18-3"></span>



<span id="page-18-4"></span>**Figure 31. Unit Load and Transceiver Drive of ISL315xE vs Standard RS-485 Transceiver**



[Figure 31](#page-18-4) compares the maximum number of unit loads and bus transceivers when choosing an ISL315xE over a standard transceiver. The RS-485 standard specifies a minimum total common-mode load resistance of  $R_{CM}$  = 375Ω between each signal conductor and ground. Because one unit load (1UL) is equivalent to 12kΩ, the total common-mode resistance of 375Ω yields  $12kΩ/375Ω = 32 ULs$ .

For an ISL315xE transceiver however,  $R_{CM}$  can be as small as 188 $\Omega$ , resulting in a total common-mode load of  $12kΩ/188Ω = 64 ULs$ . This means the driver of an ISL315xE transceiver can drive up to 64 x 1UL transceivers or 512 x 1/8UL transceivers.

The advantages of such superior drive capability are:

- Up to 900mV higher noise immunity (2.4V vs 1.5V V<sub>OD</sub>)
- Up to twice the maximum cable length of standard transceivers (~8000ft vs 4000ft)
- The design of star configurations or other multi-terminated nonstandard network topologies

#### <span id="page-19-0"></span>**6.4.2 Driver Overload Protection**

The RS-485 specification requires drivers to survive worst case bus contentions undamaged. The ISL315xE transceivers meet this requirement through driver output short circuit current limits and on-chip thermal shutdown circuitry.

The driver output stages incorporate short-circuit current limiters that ensure that the output current never exceeds the RS-485 specification, even at the common-mode voltage range extremes.

In the event of a major short-circuit conditions, the devices also include a thermal shutdown feature that disables the drivers whenever the temperature becomes excessive. This eliminates the power dissipation, allowing the die to cool. The drivers automatically re-enable after the die temperature drops about 15°C. If the contention persists, the thermal shutdown/re-enable cycle repeats until the fault is cleared. The receivers stay operational during thermal shutdown.

#### <span id="page-19-1"></span>**6.4.3 Full-Failsafe Receiver**

The differential receivers of the ISL315xE family are full-failsafe, meaning their outputs turn logic high when:

- The receiver inputs are open (floating) due to a faulty bus node connector
- The receiver inputs are shorted due to an insulation break of the bus cable
- The receiver input voltage is close to 0V due to a terminated bus not being actively driven

Full-failsafe switching is accomplished by offsetting the maximum receiver input threshold to -50mV. [Figure 32](#page-19-2) shows that, in addition to the threshold offset, the receiver also has an input hysteresis,  $\Delta V_{TH}$ , of 20mV. The combination of offset and hysteresis allows the receiver to maintain its output high, even in the presence of  $140mV_{P-P}$  differential noise, without the need for external failsafe biasing resistors.



**Figure 32. Full-Failsafe Performance with High Noise Immunity**

<span id="page-19-2"></span>

#### <span id="page-20-0"></span>**6.4.4 Low Current Shutdown Mode**

The ISL315xE transceivers use a fraction of the power required by their bipolar counterparts, but also include a shutdown feature that reduces the already low quiescent  $I_{CC}$  to a 70nA trickle. These devices enter shutdown whenever the receiver and the driver are simultaneously disabled ( $\overline{RE} = V_{CC}$  and  $DE = GND$ ) for a period of at least 600ns. Disabling both the driver and the receiver for less than 60ns guarantees that the transceiver will not enter shutdown.

Note that driver and receiver enable times increase when the transceiver enables from shutdown. Refer to [Notes 9](#page-10-2) to  $\frac{13}{13}$  at the end of "Electrical Specifications" on [page 11](#page-10-8).

#### <span id="page-20-1"></span>**6.4.5 Hot Plug Function**

When the equipment powers up, there is a period of time where the controller driving the RS-485 enable lines is unable to ensure that the driver and receiver outputs are kept disabled. If the equipment is connected to the bus, a driver activating prematurely during power-up may crash the bus. To avoid this scenario, the ISL315xE devices incorporate a Hot Plug function. During power-up and power-down, the Hot Plug function disables the driver and receiver outputs regardless of the states of DE and  $\overline{RE}$ . When V<sub>CC</sub> reaches ~3.4V, the enable pins are released. This gives the controller the chance to stabilize and drive the RS-485 enable lines to the proper states.

#### <span id="page-20-2"></span>**6.4.6 High ESD Protection**

The bus pins of the ISL315xE transceivers have on-chip ESD protection against  $\pm 16.5$ kV HBM, and  $\pm 9$ kV contact and ±16.5kV air-discharge according to IEC61000-4-2. The difference between the HBM and IEC ESD ratings lies in the test severity, as both standards aim for different application environments.

HBM ESD ratings are component level ratings, used in semiconductor manufacturing in which component handling can cause ESD damage to a single device. Because component handling is performed in a controlled ESD environment, the ESD stress upon a component is drastically reduced. These factors make the HBM test the less severe ESD test.

IEC ESD ratings are system level ratings. These are required in the uncontrolled field environment, where for example, a charged end user can subject handheld equipment to ESD levels of more than 40kV by touching connector pins when plugging or unplugging cables.

The main differences between the HBM and the IEC 61000-4-2 standards are the number of strikes applied during testing and the generator models [\(Figure 33\)](#page-20-3), which create differences in the waveforms' rise times and peak currents (**Figure 34**).



<span id="page-20-3"></span>

<span id="page-20-4"></span>The IEC model has 50% higher charge capacitance  $(C_S)$  and 78% lower discharge resistance  $(R_D)$  than the HBM model, thus producing shorter transient rise times and higher discharge currents. The ESD ratings of the ISL315xE transceivers exceed test level 4 of the IEC61000-4-2 standard, which significantly increases equipment robustness.



#### <span id="page-21-0"></span>**6.4.7 High EFT Immunity**

The bus pins of the ISL315xE transceivers withstand  $\pm$ 4kV Electrical Fast Transient (EFT) immunity per IEC61000-4-4. During the EFT test, the EFT generator produces a burst of 75 fast transients capacitively coupled onto RS-485 data lines using a capacitive clamp [\(Figure 35\)](#page-21-1).



<span id="page-21-1"></span>**Figure 35. Test Setup with Capacitive Clamp Figure 36. EFT Test Timing**

<span id="page-21-2"></span>

A burst period is 300ms and begins with 75 EFT pulses ( $t_{\text{Burst}}$ ) followed by a break interval ( $\frac{Figure\ 36}{2}$ ). Across a test time of 60 seconds minimum, multiple bursts are applied at a predefined repetition frequency of either 5kHz or 100kHz, unleashing a minimum of 15000 EFT pulses onto the data link. The ISL315xE transceivers have been tested with both repetition frequencies (5kHz and 100kHz).

In the test setup, a complete RS-485 data link (driver, receiver, and unshielded twisted pair cable) was tested during data transmission. Afterward, the devices were tested on an automatic test system (ATE) for parametric performance. The ATE pass criterion requires that a device show no parametric shift.

All ISL315xE transceivers passed the EFT tests with ±4kV test voltage, which places this transceiver family into the highest special test level category of the IEC61000-4-4 standard ([Table 4](#page-21-3), Test Level X).

<span id="page-21-3"></span>

<b>Test Level</b>	Test Voltage (V)	<b>Repetition Frequency (kHz)</b>	<b>Components Passing</b>
	0.25	5 and 100	ISL3150E, ISL3152E, ISL3153E, ISL3155E, ISL3156E, ISL3158E
	0.5	5 and 100	
		5 and 100	
		5 and 100	
		5 and 100	

**Table 4. EFT Test Level Category for ISL315xE Transceivers**

### <span id="page-22-0"></span>**7. Application Information**

#### <span id="page-22-1"></span>**7.1 Network Design**

Designing a reliable RS-485 network requires the consideration of a variety of factors that ultimately determine the network performance. These include network topology, cable type, data rate and/or cable length, stub length, distance between network nodes, and line termination.

The main difference between network designs is dictated by their modes of data exchange between bus nodes, which can be half-duplex or full-duplex  $(Figures 37$  and  $38)$ .





<span id="page-22-4"></span>**Figure 37. Half-Duplex Bus Figure 38. Full-Duplex Bus** 

<span id="page-22-3"></span>**Half-duplex networks** use only a single signal-pair of cables between one master node and multiple slave nodes, which allows the nodes to either transmit or receive data, but never both at the same time. Its reduced cabling effort makes these networks well suited for covering long distances of up to several thousands of feet. To maintain high signal integrity, the applied data rates range from as low as 9.6kbps up to 115kbps. This requires transceivers with long driver output transition times, typically in the range of microseconds, to ensure low EMI in the presence of large cable inductances.

To prevent signal reflections of the bus lines, each cable end must be terminated with a resistor,  $R_T$ , whose value should match the characteristic cable impedance,  $Z_0$ .

**Full-duplex networks**, on the other hand, aim for high data throughput. These networks use two signal-pairs to support the simultaneous transmitting and receiving of data. The signal pair denoted as the transmit path connects the driver output of the master node to the receiver inputs of multiple slave nodes. The other pair connects the driver outputs of the slave nodes with the receiver input of the master node.

Because the data flow in the transmit path is unidirectional, the transmit path requires only one termination at the remote cable end, opposite the master node. Data flow in the receive path, however, is bidirectional, thus requiring line termination at both cable ends. Commonly, high data throughput also calls for higher data rates in the 1Mbps to 10Mbps range. As cable losses increase with frequency, most full-duplex networks are limited to shorter bus cable lengths of a few hundred feet to maintain signal integrity.

The following sections discuss the aforementioned parameters that impact network performance. This discussion applies to both half-and full-duplex network designs.

#### <span id="page-22-2"></span>**7.1.1 Cable Type**

RS-485 networks use differential signaling over Unshielded Twisted Pair (UTP) cable. The conductors of a twisted pair are equally exposed to external noise. They pick up noise and other electromagnetically induced voltages as common-mode signals, which are effectively rejected by the differential receivers.

For best performance use industrial RS-485 cables, which are of the sheathed, shielded, twisted pair type, (STP), with a characteristic impedance of  $120\Omega$  and conductor sizes of 22 to 24 AWG (equivalent to diameters of 0.65mm and 0.51mm, respectively). They are available in single, two, and four signal-pair versions to



accommodate the design of half- and full-duplex systems. [Figure 39](#page-23-2) shows the cross section and cable parameters of a typical UTP cable.



**Figure 39. Single Pair STP Cable for RS-485 Applications**

#### <span id="page-23-2"></span><span id="page-23-0"></span>**7.1.2 Cable Length vs Data Rate**

RS-485 and RS-422 are intended for network lengths up to 4000ft, but the maximum system data rate decreases as the transmission length increases. Devices operating at 20Mbps are limited to lengths less than 100ft, while the 115kbps versions can operate at full data rates with lengths of several 1000ft. Note that ISL315xE transceivers can cover almost twice the distance of standard compliant RS-485 transceivers.



**Figure 40. Data Rate vs Cable Length Guidelines in Feet and Meters**

#### <span id="page-23-1"></span>**7.1.3 Topologies and Stub Lengths**

RS-485 recommends its nodes to be networked in daisy-chain or backbone topology. In these topologies the participating drivers, receivers, and transceivers connect to a main cable trunk through "short" stubs. A stub being the actual electrical link between transceiver and cable trunk.





**Figure 41. Stub Lengths in Daisy Chain (left) and Backbone (right) Topologies**

Because daisy chaining brings the cable trunk much closer to the transceiver bus terminals than a backbone design, the stub lengths between the two topologies can differ significantly. To prevent the bus from being overloaded by line terminations, stubs are never terminated. A stub therefore, represents a piece of unterminated transmission line. To eliminate signal reflections on the stub line, a rule of thumb is to keep its propagation delay below 1/5 of the driver output rise time, which leads to the maximum stub length of:

<span id="page-24-1"></span>
$$
(EQ. 1) \qquad L_{Stub} = v \cdot c \cdot \frac{t_r}{5}
$$

where

- $\cdot$  c is the speed of light (m/s)
- v is the signal velocity in the cable, expressed as a factor of c
- $t_r$  is the rise time of the driver output (ns)

Applying [Equation 1](#page-24-1) to the ISL315xE transceivers assuming a velocity of 78%, results in the maximum stub lengths associated with the corresponding transceivers, as shown in **[Table 5](#page-24-2)**.

<span id="page-24-2"></span>

<b>Device</b>	Data Rate (Mbps)	Rise Time (ns)	<b>Maximum Stub Length</b>
<b>ISL3150E, ISL3152E</b>	0.115	1100	168ft (51m)
<b>ISL3153E, ISL3155E</b>		150	23ft (7m)
<b>ISL3156E, ISL3158E</b>	20		$1.2$ ft (0.36m)

**Table 5. Stub Length as Function of Driver Rise Time**

[Table 5](#page-24-2) proves that transceivers with long driver rise times are well suited for applications requiring long stub lengths and low radiated emission in the presence of increased stub inductance.

#### <span id="page-24-0"></span>**7.1.4 Minimum Distance between Nodes**

The electrical characteristics of the RS-485 bus are primarily defined by the distributed inductance and capacitance along the bus cable and printed circuit board traces. Adding capacitance to the bus in the form of transceivers and connectors lowers the line impedance and causes impedance mismatches at the loaded bus section.

Input signals arriving at these mismatches are partially reflected back to the signal source, distorting the driver output signal. Ensuring a valid receiver input voltage during the first signal transition from a driver output anywhere on the bus, requires the bus impedance at the mismatches to be  $Z_{load} \ge 0.4Z_{nom}$  or  $0.4$  x 120Ω = 48Ω. This can be achieved by maintaining a minimum distance between bus nodes of:



$$
(EQ. 2) \qquad D_{\text{min}} \ge \frac{C_L}{5.25 \cdot C_C}
$$

where

- $\cdot$  C<sub>L</sub> is the lumped load capacitance
- $\cdot C_{\text{C}}$  is the distributed cable or PCB trace capacitance per unit length.

[Figure 42](#page-25-1) shows the relationship for the minimum node spacing as a function of  $C_C$  and  $C_L$  graphically. Load capacitance includes contributions from the line circuit bus pins, connector contacts, printed circuit board traces, protection devices, and any other physical connections to the trunk line as long as the distance from the bus to the transceiver, known as the stub, is electrically short.

Putting some values to the individual capacitance contributions: 5V transceivers typically possess a capacitance of 7pF, while 3V transceivers have about twice that capacitance at 16pF. Board traces add about 1.3 to 2pF/in depending upon their construction.

Connector and suppression device capacitance can vary widely. Media distributed capacitance ranges from 11pF/ft for low capacitance, unshielded, twisted-pair cable up to 22pF/ft for backplanes.



**Figure 42. Minimum Distance between Bus Nodes as Function of Cable and Load Capacitance**

#### <span id="page-25-1"></span><span id="page-25-0"></span>**7.1.5 Failsafe Biasing Termination**

As mentioned in "Full-Failsafe Receiver" on page 20, the ISL315xE transceivers are full-failsafe and capable of tolerating up to  $140mV_{p-p}$  of differential noise on a passive bus without needing external failsafe biasing.

However, in harsh industrial environments, such as the factor floors in industrial automation, the differential noise can reach levels of more than  $1V_{P-P}$ . In this case external failsafe biasing at the network's line terminations is strongly recommended. Here the termination resistors  $R_T$  connect through the biasing resistors  $R_B$  to the supply rails  $V_{CC}$  and GND.

Short data links (<100m) only require a single failsafe termination at one cable end, while the other end is terminated with the cable characteristic impedance  $Z_0$  (**Figure 43**, left circuit).





**Figure 43. Failsafe Biasing of Short (<100m) and Long (>100m) Data Links**

<span id="page-26-0"></span>The corresponding resistor values are calculated with **Equations 3** to [5.](#page-26-2)

<span id="page-26-1"></span>(EQ. 3) 
$$
R_B = \frac{V_S/V_{AB} + 1}{0.036}
$$

$$
(EQ. 4) \t R_{T2} = \frac{R_B \cdot 120\Omega}{R_B - 60\Omega}
$$

<span id="page-26-2"></span>
$$
(EQ. 5) \t RT1 = 120\Omega
$$

Longer data links (>100m) require two identical failsafe basing networks, one at each cable end, to minimize the differential voltage drop along the bus [\(Figure 43,](#page-26-0) right circuit). Their resistor values are calculated using [Equations 6](#page-26-3) and [7:](#page-26-4)

<span id="page-26-3"></span>(EQ. 6) 
$$
R_B = \frac{2V_S/V_{AB} + 1}{0.036}
$$

<span id="page-26-4"></span>
$$
(EQ. 7) \t RT = \frac{RB \cdot 120 \Omega}{RB - 60 \Omega}
$$

Note that **Equations 3** to [7](#page-26-4) apply to the multi-driver applications of half- and full-duplex networks. For single driver applications, the values of  $R_B$  and  $R_T$  are calculated using [Equations 8](#page-26-5) and [9](#page-26-6).



**Figure 44. Failsafe Biasing of a Single-Driver Network**

<span id="page-26-5"></span>(EQ. 8)

$$
R_B = 60\Omega \cdot \frac{V_S}{V_{AB}}
$$
  
(EQ. 9)  

$$
R_T = \frac{R_B \cdot 120\Omega}{R_B - 60\Omega}
$$

<span id="page-26-6"></span>For more details on failsafe biasing refer to **TB509**.



#### <span id="page-27-0"></span>**7.2 Transient Protection**

Although the ISL315xE transceivers have on-chip transient protection circuitry against Electrostatic Discharge (ESD), they are vulnerable to bursts of Electrical Fast Transients (EFT) and surge transients. Surge transients can be caused by lightning strikes or the switching of power systems including load changes and short circuits. Their energy content is up to 8 million times higher than that of ESD transients and thus, requires the addition of external transient protection.

Because standard RS-485 transceivers have asymmetric stand-off voltages of -9V and +14V, external protection requires a bidirectional Transient Voltage Suppressor (TVS) with asymmetric breakdown voltages. The only device satisfying this requirement is the 400W TVS, SM712.

The SM712 operates across the asymmetrical common-mode voltage range from -7V to +12V. The device protects transceivers against ESD, EFT, and surge transients up to the following levels:

- $\cdot$  IEC61000-4-2 (ESD) +15kV (air), +8kV (contact)
- IEC61000-4-4 (EFT) 40A (5/50ns)
- IEC61000-4-5 (Lightning) 12A (8/20μs)

Because the transceiver's ESD cells and the SM712 have a similar switching characteristics, series resistors  $(R_S)$ are used to prevent the two protection schemes from interacting with one another.

These resistors can be carbon composite or pulse-proof thick-film resistors which should be inserted between the TVS and the transceiver bus terminals to limit the bus currents into the transceiver during a surge event. Their value should be less than 20 $\Omega$  to minimize the attenuation of the bus voltage during normal operation. [Figure 45](#page-27-2) shows the schematic of a 1kV surge protection example for the ISL3152E and its bill of materials.





#### **Figure 45. IEC61000-4-5 Level 2 (1kV) Surge Protection and Associated Bill of Materials**

<span id="page-27-2"></span>For more information on transient protection, refer to [AN1976,](https://www.renesas.com/us/en/document/apn/an1976-important-transient-immunity-tests-rs-485-networks) [AN1977](https://www.renesas.com/us/en/document/apn/an1977-transient-voltage-suppressors-operation-and-features), [AN1978](https://www.renesas.com/us/en/document/apn/an1978-surge-protection-renesas-standard-rs-485-transceivers), and [AN1979.](https://www.renesas.com/us/en/document/apn/an1979-surge-protection-simplified-renesas-overvoltage-protected-ovp-transceivers)

#### <span id="page-27-1"></span>**7.3 Layout Guidelines**

Because ESD and EFT transients have a wide frequency bandwidth from approximately 3MHz to 3GHz, high-frequency layout techniques must be applied during PCB design.

- ï For your PCB design to be successful, start with the design of the protection circuit in mind.
- ï Place the protection circuitry close to the bus connector to prevent noise transients from penetrating your board.
- Use  $V_{CC}$  and ground planes to provide low-inductance. Note that high-frequency currents follow the path of least inductance and not the path of least impedance.
- ï Design the protection components into the direction of the signal path. Do not force the transient currents to divert from the signal path to reach the protection device.



- Apply 100nF to 220nF bypass capacitors as close as possible to the  $V_{CC}$  pins of the transceiver, UART, and controller ICs on the board.
- $\cdot$  Use at least two vias for V<sub>CC</sub> and ground connections of bypass capacitors and protection devices to minimize the effective via-inductance.
- Use  $1k\Omega$  to 10k $\Omega$  pull-up/down resistors for the transceiver enable lines to limit noise currents into these lines during transient events.
- ï Insert pulse-proof resistors into the A and B bus lines if the TVS clamping voltage is higher than the specified maximum voltage of the transceiver bus terminals. These resistors limit the residual clamping current into the transceiver and prevent it from latching up.

#### <span id="page-28-0"></span>**7.3.1 Layout Example**



**Figure 46. ISL3152E Layout Example**



### <span id="page-29-0"></span>**8. Revision History**









### <span id="page-31-0"></span>**9. Package Outline Drawings**

For the most recent package outline drawing, see **M8.15**.

M8.15

8 Lead Narrow Body Small Outline Plastic Package Rev 5, 4/2021



**NOTES:** 

- 1 Dimensioning and tolerancing conform to AMSEY14.5m-1994.
- 2 Package length does not include mold flash, protrustion or gate burrs. r ackage religion does not include more mash, protrustion or gate burrs.<br>Mold flash, protrustion and gate burrs shall not exceed 0.15mm (0.006<br>inch) per side.
- 3. Package width does not include interlead flash or protrustions. Interlead flash and protrustions shallnot exceed 0.25mm (0.010 lnch) per side.
- 4. The chamfer on the body is optional. if it is not present, a visual index<br>feature must be located within the crosshatched area.
- 5 Terminal numbers are shown for reference only.
- The lead width as measured 0.36mm (0.014 inch) or greater above the<br>seating plane, shall not exceed a maximum value of 0.61mm (0.024 inch). 6
- 7 Controlling dimension: MILLIMETER. Converted inch dimension are not necessarily exact
- 8 This outline conforms to JEDEC publication MS-012-AA ISSUE C.



For the most recent package outline drawing, see **M8.118**.

M8.118 8 Lead Mini Small Outline Plastic Package Rev 5, 5/2021









**TYPICAL RECOMMENDED LAND PATTERN**

**NOTES:**

- **Dimensions are in millimeters. 1.**
- **Dimensioning and tolerancing conform to JEDEC MO-187-AA 2. and AMSEY14.5m-1994.**
- **Plastic or metal protrusions of 0.15mm max per side are not 3. included.**
- **Plastic interlead protrusions of 0.15mm max per side are not 4. included.**
- 5. Dimensions are measured at Datum Plane "H".
- **Dimensions in ( ) are for reference only. 6.**



For the most recent package outline drawing, see **M10.118**.

M10.118 10 Lead Mini Small Outline Plastic Package Rev 2, 5/2021





**TYPICAL RECOMMENDED LAND PATTERN**

**NOTES:**

- **Dimensions are in millimeters. 1.**
- **Dimensioning and tolerancing conform to JEDEC MO-187-BA 2. and AMSEY14.5m-1994.**
- **Plastic or metal protrusions of 0.15mm max per side are not 3. included.**
- **Plastic interlead protrusions of 0.15mm max per side are not 4. included.**
- 5. Dimensions are measured at Datum Plane "H".
- **Dimensions in ( ) are for reference only. 6.**



For the most recent package outline drawing, see [M14.15.](https://www.renesas.com/us/en/document/psc/package-drawing-soicn-14pin-m1415)

#### M14.15

14 Lead Narrow Body Small Outline Plastic Package Rev 2, 6/20





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