19-3974; Rev 1; 4/07

**EVALUATION KIT AVAILABLE**



# High-Speed, Dual-Phase Driver with Integrated Boost Diodes

### General Description

The MAX8811 2-phase gate driver controls power MOSFETs in multiphase synchronous step-down converter applications, providing up to 30A output current per phase. The MAX8811 and MAX8810A (multiphase power-supply controller) combine to provide an efficient, low-cost solution for a wide range of multiphase powersupply applications. The MAX8811 handles system input voltages up to 26V. Each MOSFET driver is capable of driving 3000pF capacitive loads with 11ns typical rise and fall times.

Adaptive shoot-through protection circuitry is implemented to prevent shoot-through currents for the "highside off to low-side on" transition. A programmable delay is provided for the "low-side off to high-side on" transition. This maximizes overall converter efficiency while supporting operation with a variety of MOSFETs.

The MAX8811 provides an easy upgrade path from the MAX8523 dual driver. Integrated bootstrap diodes reduce external component count, while an enable input provides flexibility for power sequencing. The MAX8811 is available in a space-saving, 16-pin QSOP.

#### Applications

Processor Core Voltage Regulators Multiphase Buck Converters Voltage-Regulator Modules (VRMs) Switching Power Supplies DC-DC Converter Modules



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### Features

MAX8811

**MAX881** 

- ♦ **Dual-Phase Synchronous Buck Driver**
- ♦ **Integrated Bootstrap Diodes**
- ♦ **Up to 26V System Input Voltage**
- ♦ **6A Peak Gate Drive Current**
- ♦ **Capable of 30A per Phase**
- ♦ **0.4**Ω**/0.9**Ω **Low-Side, 0.7**Ω**/1.0**Ω **High-Side Drivers (typ)**
- ♦ **Typical 11ns Rise/Fall Times with 3000pF Load**
- ♦ **Adaptive Dead-Time Control**
- ♦ **User-Programmable Delay Time**
- ♦ **Enable Function with 0.04µA (typ) Quiescent Current in Shutdown**
- ♦ **Space-Saving, Lead-Free, 16-Pin QSOP**

### Ordering Information



+Denotes a lead-free package.

## Typical Operating Circuit



**For pricing, delivery, and ordering information, please contact Maxim/Dallas Direct! at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.**

### **ABSOLUTE MAXIMUM RATINGS**





Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### **ELECTRICAL CHARACTERISTICS**

(VDLY = VEN = VBST\_ = VVL\_ = 6.5V, VPGND\_ = VLX\_ = VPWM\_ = 0V, **TA = -40°C to +85°C**, unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 1)



### **ELECTRICAL CHARACTERISTICS (continued)**

(VDLY = VEN = VBST\_ = VVL\_ = 6.5V, VPGND\_ = VLX\_ = VPWM\_ = 0V, **TA = -40°C to +85°C**, unless otherwise noted. Typical values are at T<sub>A</sub> =  $+25^{\circ}$ C.) (Note 1)



**Note 1:** Specifications at -40°C guaranteed by design.

Typical Operating Characteristics  $(V_{VL1} = V_{VL2} = V_{EN} = V_{DLY} = 6.5V$ , 3000pF capacitive load,  $T_A = +25^{\circ}$ C, unless otherwise noted.)



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### Typical Operating Characteristics (continued)

 $(V_{VL1} = V_{VL2} = V_{EN} = V_{DLY} = 6.5V$ , 3000pF capacitive load,  $T_A = +25^{\circ}C$ , unless otherwise noted.)





## Pin Description









Figure 1. Functional Diagram



Figure 2. Driver Timing Diagram

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### Detailed Description

Principles of Operation

#### **MOSFET Gate Drivers (DH\_, DL\_)**

DH\_ is driven high when the PWM\_ is high; DL\_ is driven high when PWM\_ is low. PWM pulsewidths under 20ns (typ) are rejected, and no switching occurs.

The low-side drivers (DL\_) have typical  $0.9\Omega$  sourcing resistance and 0.4Ω sinking resistance, and are capable of driving 3000pF capacitive loads with 11ns typical rise and 8ns typical fall times. The high-side drivers (DH\_) have typical 1.0Ω sourcing resistance and 0.7Ω sinking resistance, and are capable of driving 3000pF capacitive loads with 14ns typical rise and 9ns typical fall times. This facilitates fast switching, reducing switching losses, and makes the MAX8811 ideal for both high-frequency and high-output current applications.

#### **Shoot-Through Protection**

Adaptive shoot-through protection is incorporated for the switching transition after the high-side MOSFET is turned off and before the low-side MOSFET is turned on. The low-side driver is turned on when the LX voltage falls below 2.5V, or after 135ns typical delay, whichever occurs first. Furthermore, the delay time between the low-side MOSFET turn-off and high-side MOSFET turn-on can be adjusted by selecting the value of R1 (see the Setting the Dead Time section).

#### Undervoltage Lockout (UVLO)

When the voltage at the VL1/VL2 connection is below the UVLO threshold, all driver outputs are held low. This prevents switching when the supply voltage is too low for proper operation.

#### Thermal Protection

Thermal-overload protection limits total power dissipation in the MAX8811. When the junction temperature exceeds +165°C, all driver outputs are held low. The IC resumes normal operation after the junction temperature cools by 15°C (typ).

#### Boost Capacitor Selection

The MAX8811 uses a bootstrap circuit to generate the supply voltages for the high-side drivers (DH). The selected high-side MOSFET determines the appropriate boost capacitance values, according to the following equation:

$$
C_{\text{BST}} = \frac{Q_{\text{GATE}}}{\Delta V_{\text{BST}}}
$$





where QGATE is the total gate charge of the high-side MOSFET and ∆VBST is the voltage variation allowed on the high-side MOSFET drive. Choose  $\Delta V_{\text{BST}} = 0.1V$  to 0.2V when determining C<sub>BST</sub>. Low-ESR ceramic capacitors should be used.

#### VL\_ Decoupling

VL1 and VL2 provide the supply voltage for the low-side drivers. The decoupling capacitors at VL\_ also charge the BST capacitors during the time period when DL\_ is high. Therefore, the decoupling capacitor C3 for VL\_ should be large enough to minimize the ripple voltage during switching transitions. Choose the VL capacitor approximately 10 times the value of the BST capacitor value.



#### **Table 2. Components for Figure 4, 300kHz, 30A/Phase Typical Application Circuit**

#### Setting the Dead Time

Connect DLY to VL\_ for the default delay time, typically 14ns. To increase the delay between the low-side MOSFET drive turn-off and the high-side MOSFET turnon, connect a resistor from DLY to PGND1. See the Typical Operating Characteristics section for a plot of the delay time vs. resistor value. The equation for this resistor is:

$$
t_{DLY} = 14 \mu s + (1pF) \times R_{DLY}
$$

#### Avoiding dV/dt-Induced Low-Side MOSFET Turn-On

At high input voltages, fast turn-on of the high-side MOSFET could momentarily turn on the low-side MOS-FET due to the high dV/dt appearing at the drain of the low-side MOSFET. The high dV/dt causes a current flow through the Miller capacitance (CRSS) and the input capacitance (CISS) of the low-side MOSFET. Improper selection of the low-side MOSFET that has a high ratio of CRSS/CISS makes the problem more severe. To avoid the problem, give special attention to the ratio of CRSS/CISS when selecting the low-side MOSFET. Adding a resistor between BST\_ and the BST\_ capacitor slows the high-side MOSFET turn-on. Adding a capacitor from the gate to the source of the high-side MOSFET has the same effect. However, both methods are at the expense of increasing the switching losses.

### Applications Information

#### Power Dissipation

Power dissipation in the IC package comes mainly from switching the MOSFETs. Therefore, it is a function of both switching frequency and the total gate charge of the selected MOSFETs. The total power dissipation when both drivers are switching is given by:

$$
P_{IC} = 2 \times f_S \times [N \times Q_{G\_TOTAL\_HS} \times
$$
  
\n
$$
\frac{R_{HS}}{R_{HS} + (R_{G\_HS} / N)} + M \times Q_{G\_TOTAL\_LS} \times
$$
  
\n
$$
\frac{R_{LS}}{R_{LS} + (R_{G\_LS} / N)} \times V_{PV\_} + V_{VCC} \times V_{VCC}
$$

where  $f_S$  is the switching frequency,  $Q_G$  TOTAL HS is the total gate charge of the selected high-side MOS-FET, QG TOTAL LS is the total gate charge of the selected low-side MOSFET, N is the total number of the high-side MOSFETs in parallel, M is the total number of the low-side MOSFETs in parallel, V<sub>VL</sub> is the voltage at VL, RHS is the on-resistance of the high-side MOSFET, and RG\_LS is the gate resistance of the selected lowside MOSFETs.

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#### PCB Layout

The MAX8811 sources and sinks large currents to drive MOSFETs at high switching speeds. The high di/dt can cause unacceptable ringing if the trace lengths and impedances are not well controlled. The following PCB layout guidelines are recommended when designing with the MAX8811:

- 1) Place all decoupling capacitors as close to their respective pins as possible.
- 2) Minimize the high-current loops from the input capacitor, upper switching MOSFET, and low-side MOSFET back to the input capacitor negative terminal.
- 3) Provide enough copper area at and around the switching MOSFETs and inductors to aid in thermal dissipation.
- 4) Connect PGND1 and PGND2 as close as possible to the source of the low-side MOSFETs.
- 5) Keep LX1 and LX2 away from sensitive analog components and nodes.
- 6) Gate drive traces should be at least 20 mils wide, kept as short as possible, and tightly coupled to reduce EMI and ringing induced by high-frequency gate noise. Adjacent DH\_ and LX\_ traces should be tightly coupled.

A sample evaluation layout is available in the MAX8811 Evaluation Kit.

Chip Information

PROCESS: BiCMOS

MAX8811



Figure 3. 800kHz, 20A/Phase Typical Application Circuit



Figure 4. 300kHz, 30A/Phase Typical Application Circuit

### Package Information

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)



### Revision History

Pages changed at Rev 1: 1, 2, 7, 8, 11

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