

2-Phase Stepper-Motor Driver

TLE 4727

Bipolar IC

Overview

Features

- 2×0.7 amp. outputs
- Integrated driver, control logic and current control (chopper)
- Fast free-wheeling diodes
- Max. supply voltage 45 V
- Outputs free of crossover current
- Offset-phase turn-ON of output stages
- All outputs short-circuit proof
- 5 V output for logic supply
- Error-flag for overload, open load, overtemperature

Description

The TLE 4727 is a bipolar, monolithic IC for driving bipolar stepper motors, DC motors and other inductive loads that operate on constant current. The control logic and power output stages for two bipolar windings are integrated on a single chip which permits switched current control of motors with 0.7 A per phase at operating voltages up to 16 V.

The direction and value of current are programmable for each phase via separate control inputs. A common oscillator generates the timing for the current control and turn-on with phase offset of the two output stages. The two output stages in a full-bridge configuration include fast integrated free-wheeling diodes and are free of crossover current. The device can be driven directly by a microprocessor in several modes by programming phase direction and current control of each bridge independently.

A stabilized 5 V output allows the supply of external components up to 5 mA. With the error output the TLE 4727 signals malfunction of the device. Setting the control inputs high resets the error flag and by reactivating the bridges one by one the location of the error can be found.

Figure 1 Pin Configuration (top view)

Pin Definitions and Functions

Pin Definitions and Functions (cont'd)

Figure 2 Block Diagram

Absolute Maximum Ratings

Temperature $T_{\rm j}$ = $-$ 40 to 150 °C

Note: Stresses above those listed here may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Operating Range

Note: In the operating range, the functions given in the circuit description are fulfilled.

Characteristics

 $V_{\rm S}$ = 6 to 16 V; $T_{\rm j}$ = – 40 to 130 °C

Current Consumption

Oscillator

Characteristics (cont'd)

 $V_{\rm S}$ = 6 to 16 V; $T_{\rm j}$ = – 40 to 130 °C

P hase Current (V _S = 9 to 16 V)

Logic Inputs (IX1 ; IX0 ; phase X)

Error Output

Logic Supply Output

Thermal Protection

Characteristics (cont'd)

 $V_{\rm S}$ = 6 to 16 V; $T_{\rm j}$ = – 40 to 130 °C

Power Output Sink Diode Transistor Sink Pair (D13, T13; D14, T14; D23, T23; D24, T24)

Power Output Source Diode Transistor Source Pair (D11, T11; D12, T12; D21, T21; D22, T22)

Note: The listed characteristics are ensured over the operating range of the integrated circuit. Typical characteristics specify mean values expected over the production spread. If not otherwise specified, typical characteristics apply at $T_A = 25 \degree C$ and the given supply voltage.

Quiescent Current *I***^S versus Supply Voltage**

 $V_{\mathbf{S}}$; bridges not chopping; $T_{\mathbf{j}} = 25 \text{ }^{\circ}\text{C}$

Oscillator Frequency *f***OSC versus Junction Temperature** *T***^j**

Quiescent Current *I***^S versus Junction Temp.**

 T **j**; bridges not chopping; $V_s = 14$ V

Output Current I_{QX} **versus Junction Temperature** *T***^j**

Output Saturation Voltages V_{sat} **versus Output Current** I_{Ω}

Typical Power Dissipation P_{tot} **versus** Output Current I_{Ω} (non stepping)

Forward Current *I***_F of Free-Wheeling** Diodes versus Forward Voltages V_F

Input Characteristics of IXX , Phase X

Logic Supply Output Voltage versus Output Current *I***^L**

Output Leakage Current

Logic Supply Output Voltage versus Junction Temperature *T***^j**

Figure 3 Application Circuit

Figure 4 Test Circuit

Figure 5 Full-Step Operation

Figure 6 Half-Step Operation

Figure 7 Current Control in Chop-Mode

Calculation of Power Dissipation

The total power dissipation P_{tot} is made up of

The following equations give the power dissipation for chopper operation without phase reversal. This is the worst case, because full current flows for the entire time and switching losses occur in addition.

$$
P_{\text{tot}} = 2 \times P_{\text{sat}} + P_{\text{q}} + 2 \times P_{\text{s}}
$$

where

$$
P_{\text{sat}} \cong I_{\text{N}} \{ V_{\text{sat}} \times d + V_{\text{Fu}} (1 - d) + V_{\text{satUC}} \times d + V_{\text{satUD}} (1 - d) \}
$$

$$
P_{\text{q}} = I_{\text{q}} \times V_{\text{S}}
$$

$$
P_{\text{S}} \cong \frac{V_{\text{S}}}{T} \left\{ \frac{i_{\text{D}} \times t_{\text{DOM}}}{2} + \frac{(i_{\text{D}} + i_{\text{R}}) \times t_{\text{ON}}}{4} + \frac{I_{\text{N}}}{2} (t_{\text{DOFF}} + t_{\text{OFF}}) \right\}
$$

- I_N = nominal current (mean value)
- I_q = quiescent current
- i_D = reverse current during turn-ON delay
- $i_{\rm R}$ = peak reverse current
- t_p = conducting time of chopper transistor
- t_{ON} = turn-ON time
- t_{OFF} = turn-OFF time
- t_{DOM} = turn-ON delay
- t_{DOFF} = turn-OFF delay
 $T = \text{cycle duration}$
- = cycle duration
- $d =$ duty cycle t_p / T
- V_{sat} = saturation voltage of sink transistor (T_{X3}, T_{X4})
- V_{satuC} = saturation voltage of source transistor (T_{X1} , T_{X2}) during charge cycle
- V_{satuD} = saturation voltage of source transistor (T_{X1} , T_{X2}) during discharge cycle
- V_{Fu} = forward voltage of free-wheeling diode (D_{X1}, D_{X2})
 V_{S} = supply voltage
- = supply voltage

Figure 10 Voltage and Current at Chopper Transistor

Application Hints

The TLE 4727 is intended to drive both phases of a stepper motor. Special care has been taken to provide high efficiency, robustness and to minimize external components.

Power Supply

The TLE 4727 will work with supply voltages ranging from 5 V to 16 V at pin V_S . Surges exceeding 16 V at $V_{\rm S}$ won't harm the circuit up to 45 V, but whole function is not guaranteed. As soon as the voltage drops below approximately 16 V the TLE 4727 works promptly again.

As the circuit operates with chopper regulation of the current, interference generation problems can arise in some applications. Therefore the power supply should be decoupled by a 0.1μ F ceramic capacitor located near the package. Unstabilized supplies may even afford higher capacities.

Current Sensing

The current in the windings of the stepper motor is sensed by the voltage drop across R_{conger} . Depending on the selected current internal comparators will turn off the sink transistor as soon as the voltage drop reaches certain thresholds (typical 0 V, 0.07 V, 0.50 V and 0.70 V). These thresholds are not affected by variations of $V_{\rm S}$. Consequently unstabilized supplies will not affect the performance of the regulation. For precise current level it must be considered, that internal bonding wire (typ. 60 mΩ) is a part of R_{sense} .

Due to chopper control fast current rises (up to $10A/\mu s$) will occur at the sensing resistors. To prevent malfunction of the current sensing mechanism R_{sense} should be pure ohmic. The resistors should be wired to GND as directly as possible. Capacitive loads such as long cables (with high wire to wire capacity) to the motor should be avoided for the same reason.

Synchronizing Several Choppers

In some applications synchronous chopping of several stepper motor drivers may be desirable to reduce acoustic interference. This can be done by forcing the oscillator of the TLE 4727 by a pulse generator overdriving the oscillator loading currents (approximately \pm 120 μ A). In these applications low level should be between 0 V and 0.8 V while high level should be between 3 V and 5 V.

Optimizing Noise Immunity

Unused inputs should always be wired to proper voltage levels in order to obtain highest possible noise immunity.

To prevent crossconduction of the output stages the TLE 4727 uses a special break before make timing of the power transistors. This timing circuit can be triggered by short glitches (some hundred nanoseconds) at the Phase inputs causing the output stage to become high resistive during some microseconds. This will lead to a fast current decay during that time. To achieve maximum current accuracy such glitches at the Phase inputs should be avoided by proper control signals.

To lower EMI a ceramic capacitor of max. 3 nF is advisable from each output to GND.

Thermal Shut Down

To protect the circuit against thermal destruction, thermal shut down has been implemented.

Error Monitoring

The error output signals with low-potential one of the following errors:

error can be located in such way.

- **overtemperature** implemented as pre-alarm; appears approximately 20 K before thermal shut down. **short circuit** a connection of one output to GND for longer than 30 µs sets an internal error flipflop. A phase change-over of the affected bridge resets the flipflop. Being a separate flipflop for each bridge, the
- **underload** the recirculation of the inductive load is watched. If there is no recirculation after a phase change-over, the internal error flipflop is set. Additionally an error is signaled after a phase change-over during hold-mode.

Package Outlines

(Plastic Dual In-line Package)

Sorts of Packing Package outlines for tubes, trays etc. are contained in our Data Book "Package Information". Dimensions in mm