

2-Phase Stepper-Motor Driver

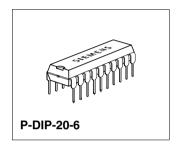
TLE 4727

Bipolar IC

Overview

Features

- 2 × 0.7 amp. outputs
- Integrated driver, control logic and current control (chopper)
- Fast free-wheeling diodes
- Max. supply voltage 45 V
- · Outputs free of crossover current
- Offset-phase turn-ON of output stages
- All outputs short-circuit proof
- 5 V output for logic supply
- Error-flag for overload, open load, overtemperature



Туре	Ordering Code	Package
TLE 4727	on request	P-DIP-20-6

Description

The TLE 4727 is a bipolar, monolithic IC for driving bipolar stepper motors, DC motors and other inductive loads that operate on constant current. The control logic and power output stages for two bipolar windings are integrated on a single chip which permits switched current control of motors with 0.7 A per phase at operating voltages up to 16 V.

The direction and value of current are programmable for each phase via separate control inputs. A common oscillator generates the timing for the current control and turn-on with phase offset of the two output stages. The two output stages in a full-bridge configuration include fast integrated free-wheeling diodes and are free of crossover current. The device can be driven directly by a microprocessor in several modes by programming phase direction and current control of each bridge independently.

A stabilized 5 V output allows the supply of external components up to 5 mA. With the error output the TLE 4727 signals malfunction of the device. Setting the control inputs high resets the error flag and by reactivating the bridges one by one the location of the error can be found.



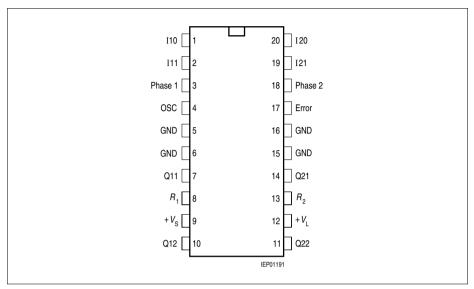


Figure 1 Pin Configuration (top view)



Pin Definitions and Functions

	Function								
1, 2, 19, 20	the particu	lar phase		gnitude of the current of					
	$I_{\rm set} = 500 \; {\rm n}$	nA with R	$_{\mathrm{Sense}}$ = 1 Ω						
	Current C IX1	ontrol IX0	Phase Current	Example of Motor Status					
	Н	Н	0	No current 1)					
	Н	L	0.14 × I _{set}	Hold					
	L	Н	I _{set}	Normal mode					
	L	L	$1.4 \times I_{\text{set}}$	Accelerate					
	1) "No currer below 3 m		ridges inhibits the circuit an	d current consumption will sink					
3		I the phas	e current flows from C	gh phase winding 1. On 11 to Q12, on L-potential					
4	Oscillator 2.2 nF.	; works at	typ. 25 kHz if this pin	is wired to ground across					
		Ground; all pins are connected at leadframe internally.							
5, 6, 15, 16	Ground; a	II pins are	e connected at leadfra	me internally.					
		outputs	e connected at leadfra Q11, Q12 for phase 1						
5, 6, 15, 16 7, 10 8	Push-pull wheeling d	outputs liodes.		with integrated free-					
7, 10	Push-pull wheeling d Resistor & Supply vo	outputs liodes. In for sense litage; blood le electro	Q11, Q12 for phase 1 sing the current in phace to ground, as closelytic capacitor of at least	with integrated free-					
7, 10	Push-pull wheeling d Resistor R Supply vo with a stab ceramic ca	outputs liodes. R ₁ for sens litage; blo le electro pacitor of outputs	Q11, Q12 for phase 1 sing the current in phace to ground, as closelytic capacitor of at least	with integrated free- use 1. e as possible to the IC, st 47 μF in parallel with a					
7, 10 8 9	Push-pull wheeling d Resistor K Supply vo with a stab ceramic ca Push-pull wheeling d Logic sup supply up to	outputs liodes. If for sense le electro epacitor of outputs liodes. ply volta to 5 mA; s	Q11, Q12 for phase 1 sing the current in phase cock to ground, as closelytic capacitor of at leaf 100 nF. Q22, Q21 for phase 2 ge; internally generate	with integrated free- use 1. e as possible to the IC, st 47 μF in parallel with a					



Pin Definitions and Functions (cont'd)

Pin No.	Function
17	Error output ; signals with "low" the errors: open load or short circuit to ground of one or more outputs or short circuits of the load or overtemperature.
18	Input phase 2; controls the current flow through phase winding 2. On H-potential the phase current flows from Q21 to Q22, on L-potential in the reverse direction.

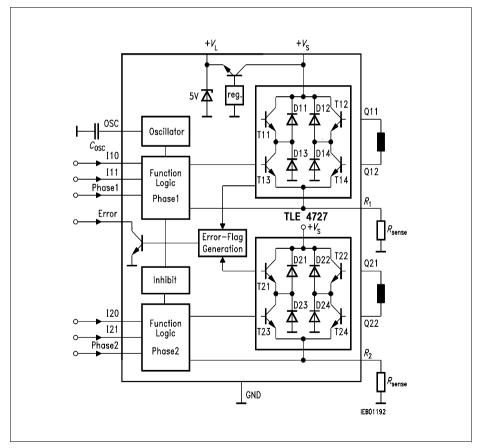


Figure 2 Block Diagram

Datasheet 4 2005-07-20



Absolute Maximum Ratings

Temperature $T_i = -40$ to 150 °C

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply voltage	V_{S}	- 0.3	45	٧	_
Error outputs	V_{Err}	- 0.3	45	٧	_
	I_{Err}	_	3	mA	_
Logic supply voltage	V_{L}	- 0.3	6.5	V	_
Output current of V _L	I_{L}	- 5	1)	mA	1) Int. limited
Output current	I_{Q}	– 1	1	Α	_
Ground current	I_{GND}	-2	_	Α	_
Logic inputs	V_{IXX}	– 15	15	٧	IXX; Phase X
Oscillator voltage	V_{Osc}	- 0.3	6	٧	_
R_1 , R_2 input voltage	V_{RX}	- 0.3	5	٧	_
Junction temperature	$T_{\rm j}$	_	125	°C	_
	$T_{\rm j}$	_	150	°C	Max. 10,000 h
Storage temperature	$T_{\rm stg}$	- 50	125	°C	_
Thermal resistance					
Junction ambient	R_{thja}	_	56	K/W	_
Junction ambient (soldered on a	R_{thja}	_	40	K/W	_
35 μm thick 20 cm ² PC board					
copper area)					
Junction case	$R_{th\ jc}$	_	18	K/W	Measured on pin 5

Note: Stresses above those listed here may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.



Operating Range

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply voltage	V_{S}	5	16	٧	_
Current from logic supply	I_{L}	_	5	mA	_
Case temperature	T_{C}	- 40	110	°C	Measured on pin 5 $P_{\text{diss}} = 2 \text{ W}$
Output current	I_{Q}	- 800	800	mA	_
Logic inputs	V_{IXX}	- 5	6	٧	IXX; Phase 1, 2
Error output	$V_{Err} \ I_{Err}$	_ 0	25 1	V mA	

Note: In the operating range, the functions given in the circuit description are fulfilled.

Characteristics

 $V_{\rm S}$ = 6 to 16 V; $T_{\rm i}$ = -40 to 130 °C

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		
Current Consumption						
from + $V_{\rm S}$	I_{S}	1	2	3	mA	IXX = H
from + V_S	I_{S}	20	30	50	mA	IXX = L;
						$I_{Q1, 2} = 0 A$
Oscillator						
Output charging current	I _{Osc}	90	120	135	μА	_
Charging threshold	$V_{\sf OscL}$	8.0	1.3	1.9	V	_
Discharging threshold	V_{OscH}	1.7	2.3	2.9	٧	_
Frequency	$f_{\rm Osc}$	18	24	30	kHz	$C_{\rm OSC} = 2.2 \rm nF$



Characteristics (cont'd)

 $V_{\rm S}$ = 6 to 16 V; $T_{\rm i}$ = -40 to 130 °C

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		
Phase Current ($V_S = 9$ to 16 V))					
Mode "no current"	I_{O}	-2	0	2	mΑ	IX0 = H;
Voltage threshold of current	•					IX1 = H
comparator at R_{sense} in mode:						
Hold	$V_{\sf ch}$	40	70	100	mV	IX0 = L; IX1 = H
Setpoint	V_{cs}	450	500	570	mV	IX0 = H; IX1 = L
Accelerate	V_{ca}	630	700	800	mV	IX0 = L; IX1 = L

Logic Inputs (IX1; IX0; phase X)

J 1 (/ /1	,					
Threshold	V_{I}	1.2	1.7	2.2	V	_
Hysteresis	V_{IHV}	_	50	_	mV	_
Low-input current	I_{IL}	– 10	– 1	1	μΑ	$V_{\rm I} = 1.2 \text{ V}$
Low-input current	I_{IL}	- 100	- 20	- 5	μΑ	$V_{\rm I} = 0 \text{ V}$
High-input current	I_{IH}	– 1	0	10	μΑ	$V_{\rm I} = 5 {\rm V}$

Error Output

Saturation voltage	V_{ErrSat}	50	200	500	mV	$I_{\rm Err} = 1 {\rm mA}$
Leakage current	I_{ErrL}	_	_	10	μΑ	$V_{Err} = 25 \; V$

Logic Supply Output

Output voltage	V_{L}	4.5	5	6	V	$T_{\rm j}$ < 150 °C 1 mA < $I_{\rm L}$ < 5 mA $V_{\rm S}$ = 6 to 45 V

Thermal Protection

Shutdown	T_{jsd}	140	150	160	°C	$I_{Q1, 2} = 0 \text{ A}$
Prealarm	$T_{\rm jpa}$	120	130	140	°C	$V_{Err} = L$
Delta	$\Delta T_{\rm j}$	10	20	30	K	$\Delta T_{\rm j} = T_{\rm jsd} - T_{\rm jpa}$



Characteristics (cont'd)

 $V_{\rm S} = 6$ to 16 V; $T_{\rm i} = -40$ to 130 °C

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		

Power Output Sink Diode Transistor Sink Pair

(D13, T13; D14, T14; D23, T23; D24, T24)

Saturation voltage	V_{satl}	0.1	0.4	0.6	٧	$I_{\rm O} = -0.5 \text{ A}$
Saturation voltage	V_{satl}	0.2	0.5	8.0	V	$I_{\rm O} = -0.7 \text{A}$
Reverse current	I_{RI}	500	1000	1500	μΑ	$V_{\rm S} = V_{\rm Q} = 40 \text{ V}$
Forward voltage	V_{FI}	0.6	0.95	1.25	V	$I_{\rm O} = 0.5 {\rm A}$
Forward voltage	V_{FI}	0.7	1	1.3	V	$I_{Q} = 0.7 \text{ A}$

Power Output Source Diode Transistor Source Pair

(D11, T11; D12, T12; D21, T21; D22, T22)

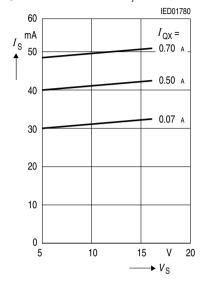
•		•				
Saturation voltage; charge	V_{satuC}	0.6	1.1	1.3	٧	$I_{\rm Q} = 0.5 {\rm A}$
Saturation voltage; discharge	V_{satuD}	0.1	0.4	0.7	V	$I_{\rm O} = 0.5 {\rm A}$
Saturation voltage; charge	$V_{\sf satuC}$	0.7	1.2	1.5	V	$I_{\rm O} = 0.7 {\rm A}$
Saturation voltage; discharge	V_{satuD}	0.2	0.5	8.0	V	$I_{\rm O} = 0.7 {\rm A}$
Reverse current	I_{Ru}	400	800	1200	μΑ	$V_{\rm S} = 40 \text{ V},$
						$V_{\rm O} = 0 \text{ V}$
Forward voltage	V_{Fu}	0.7	1.05	1.35	V	$I_{\rm O} = -0.5 {\rm A}$
Forward voltage	V_{Fu}	8.0	1.1	1.4	V	$I_{Q} = -0.7 \text{ A}$
Diode leakage current	I_{SL}	0	3	10	mΑ	$I_{\rm F} = -0.7 {\rm A}$

Note: The listed characteristics are ensured over the operating range of the integrated circuit. Typical characteristics specify mean values expected over the production spread. If not otherwise specified, typical characteristics apply at $T_A = 25\,^{\circ}\text{C}$ and the given supply voltage.



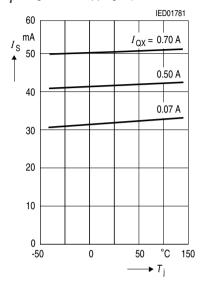
Quiescent Current $I_{\rm S}$ versus Supply Voltage

 $V_{\rm S}$; bridges not chopping; $T_{\rm i}$ = 25 °C

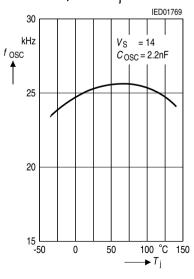


Quiescent Current $I_{\rm S}$ versus Junction Temp.

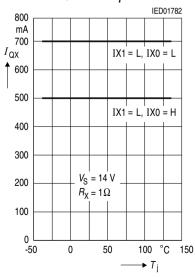
 T_i ; bridges not chopping; $V_s = 14 \text{ V}$



Oscillator Frequency $f_{\rm OSC}$ versus Junction Temperature $T_{\rm i}$

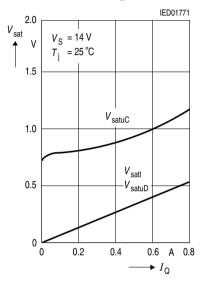


Output Current $I_{\rm QX}$ versus Junction Temperature $T_{\rm i}$

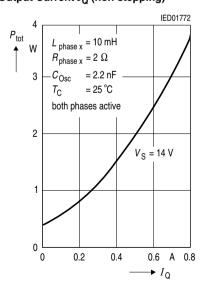




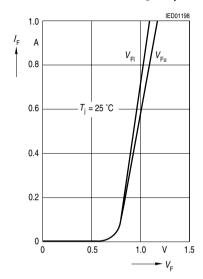
Output Saturation Voltages $V_{\rm sat}$ versus Output Current $I_{\rm Q}$



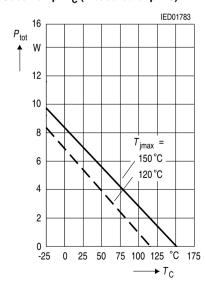
Typical Power Dissipation P_{tot} versus Output Current I_{Q} (non stepping)



Forward Current $I_{\rm F}$ of Free-Wheeling Diodes versus Forward Voltages $V_{\rm F}$

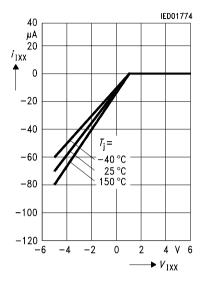


Permissible Power Dissipation $P_{\rm tot}$ versus Case Temp. $T_{\rm C}$ (measured at pin 5)

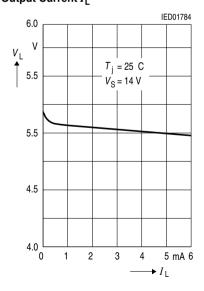




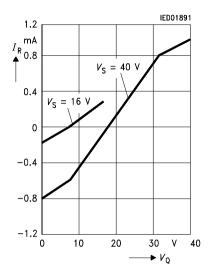
Input Characteristics of IXX , Phase X



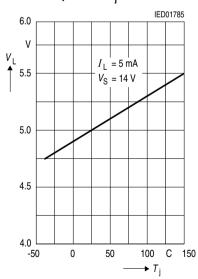
Logic Supply Output Voltage versus Output Current $I_{\rm L}$



Output Leakage Current



Logic Supply Output Voltage versus Junction Temperature $T_{\rm i}$





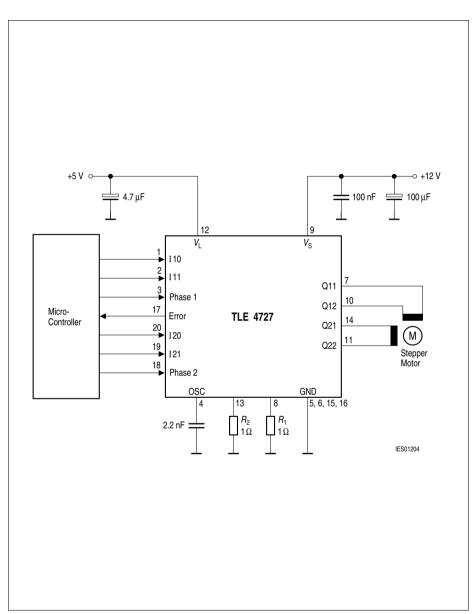


Figure 3 Application Circuit



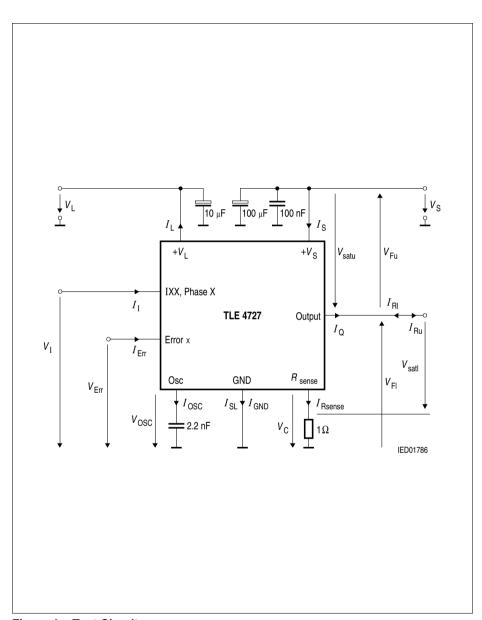


Figure 4 Test Circuit



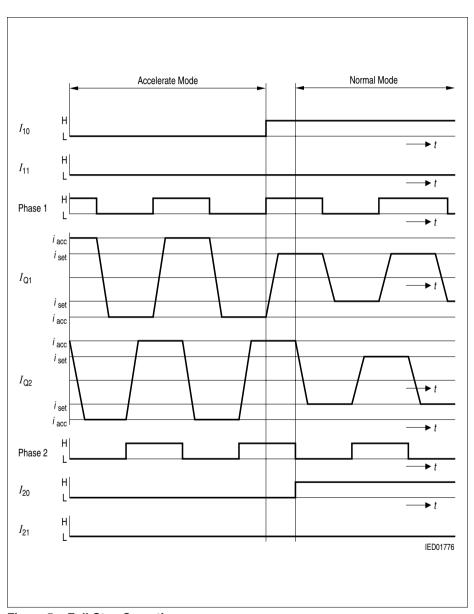


Figure 5 Full-Step Operation



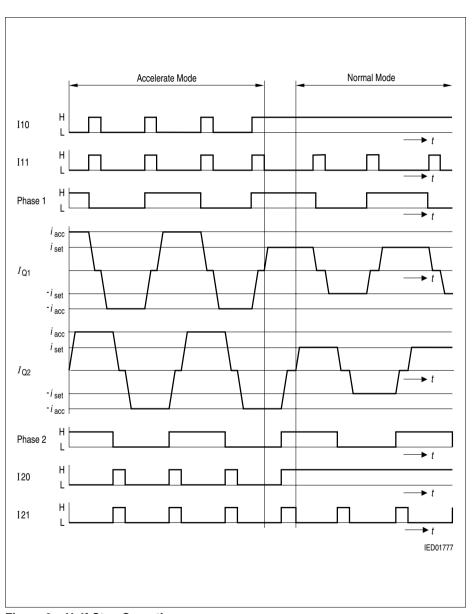


Figure 6 Half-Step Operation



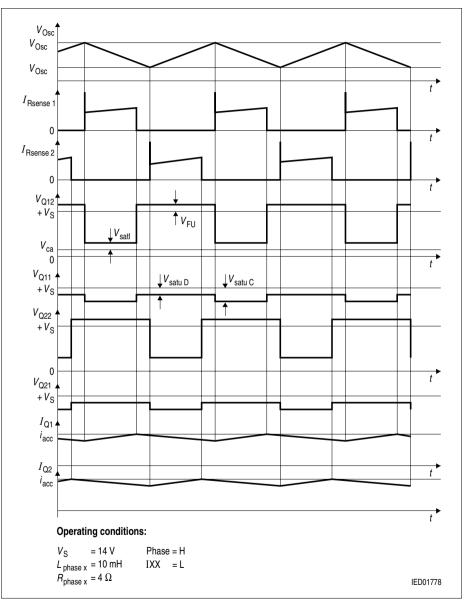


Figure 7 Current Control in Chop-Mode



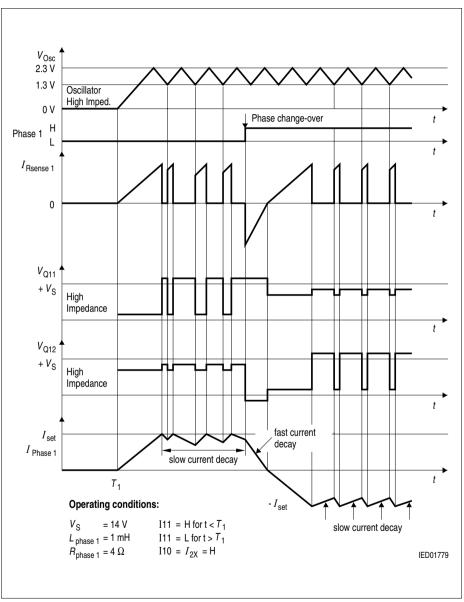


Figure 8 Phase Reversal and Inhibit



Calculation of Power Dissipation

The total power dissipation P_{tot} is made up of

 $\begin{array}{ll} \textbf{saturation losses } P_{\text{sat}} & \text{(transistor saturation voltage and diode forward voltages),} \\ \textbf{quiescent losses } P_{\text{q}} & \text{(quiescent current times supply voltage) and} \\ \textbf{switching losses } P_{\text{s}} & \text{(turn-ON / turn-OFF operations).} \\ \end{array}$

The following equations give the power dissipation for chopper operation without phase reversal. This is the worst case, because full current flows for the entire time and switching losses occur in addition.

$$\begin{split} P_{\text{tot}} &= 2 \times P_{\text{sat}} + P_{\text{q}} + 2 \times P_{\text{s}} \\ \text{where} \qquad \qquad P_{\text{sat}} &\cong I_{\text{N}} \left\{ V_{\text{satI}} \times d + V_{\text{Fu}} \left(1 - d \right) + V_{\text{satuC}} \times d + V_{\text{satuD}} \left(1 - d \right) \right\} \\ P_{\text{q}} &= I_{\text{q}} \times V_{\text{S}} \\ P_{\text{S}} &\cong \frac{V_{\text{S}}}{T} \left\{ \frac{i_{\text{D}} \times t_{\text{DON}}}{2} + \frac{(i_{\text{D}} + i_{\text{R}}) \times t_{\text{ON}}}{4} + \frac{I_{\text{N}}}{2} (t_{\text{DOFF}} + t_{\text{OFF}}) \right\} \end{split}$$

 I_N = nominal current (mean value)

 I_{q} = quiescent current

*i*_D = reverse current during turn-ON delay

 $i_{\rm R}$ = peak reverse current

 $t_{\rm p}$ = conducting time of chopper transistor

 $t_{
m ON}$ = turn-ON time $t_{
m OFF}$ = turn-OFF time $t_{
m DON}$ = turn-ON delay $t_{
m DOFF}$ = turn-OFF delay T = cycle duration d = duty cycle $t_{
m D}$ / T

 V_{satl} = saturation voltage of sink transistor (T_{X3} , T_{X4})

 $V_{\rm satuC}$ = saturation voltage of source transistor (T_{X1}, T_{X2}) during charge cycle $V_{\rm satuD}$ = saturation voltage of source transistor (T_{X1}, T_{X2}) during discharge cycle

 V_{Fu} = forward voltage of free-wheeling diode (D_{X1}, D_{X2})

 $V_{\rm S}$ = supply voltage



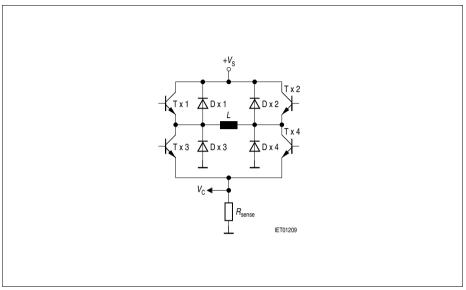


Figure 9

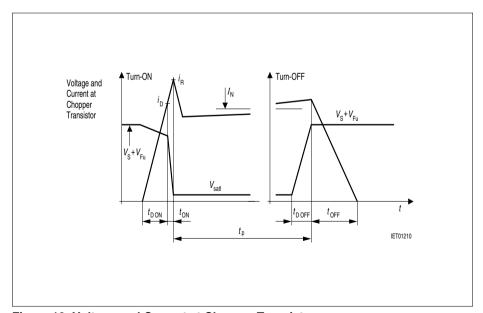


Figure 10 Voltage and Current at Chopper Transistor



Application Hints

The TLE 4727 is intended to drive both phases of a stepper motor. Special care has been taken to provide high efficiency, robustness and to minimize external components.

Power Supply

The TLE 4727 will work with supply voltages ranging from 5 V to 16 V at pin $V_{\rm S}$. Surges exceeding 16 V at $V_{\rm S}$ won't harm the circuit up to 45 V, but whole function is not guaranteed. As soon as the voltage drops below approximately 16 V the TLE 4727 works promptly again.

As the circuit operates with chopper regulation of the current, interference generation problems can arise in some applications. Therefore the power supply should be decoupled by a 0.1 μF ceramic capacitor located near the package. Unstabilized supplies may even afford higher capacities.

Current Sensing

The current in the windings of the stepper motor is sensed by the voltage drop across $R_{\rm sense}$. Depending on the selected current internal comparators will turn off the sink transistor as soon as the voltage drop reaches certain thresholds (typical 0 V, 0.07 V, 0.50 V and 0.70 V). These thresholds are not affected by variations of $V_{\rm S}$. Consequently unstabilized supplies will not affect the performance of the regulation. For precise current level it must be considered, that internal bonding wire (typ. 60 m Ω) is a part of $R_{\rm sense}$.

Due to chopper control fast current rises (up to $10A/\mu s$) will occur at the sensing resistors. To prevent malfunction of the current sensing mechanism $R_{\rm sense}$ should be pure ohmic. The resistors should be wired to GND as directly as possible. Capacitive loads such as long cables (with high wire to wire capacity) to the motor should be avoided for the same reason.

Synchronizing Several Choppers

In some applications synchronous chopping of several stepper motor drivers may be desirable to reduce acoustic interference. This can be done by forcing the oscillator of the TLE 4727 by a pulse generator overdriving the oscillator loading currents (approximately \pm 120 $\mu A). In these applications low level should be between 0 V and 0.8 V while high level should be between 3 V and 5 V.$



Optimizing Noise Immunity

Unused inputs should always be wired to proper voltage levels in order to obtain highest possible noise immunity.

To prevent crossconduction of the output stages the TLE 4727 uses a special break before make timing of the power transistors. This timing circuit can be triggered by short glitches (some hundred nanoseconds) at the Phase inputs causing the output stage to become high resistive during some microseconds. This will lead to a fast current decay during that time. To achieve maximum current accuracy such glitches at the Phase inputs should be avoided by proper control signals.

To lower EMI a ceramic capacitor of max. 3 nF is advisable from each output to GND.

Thermal Shut Down

To protect the circuit against thermal destruction, thermal shut down has been implemented.

Error Monitoring

The error output signals with low-potential one of the following errors:

overtemperature implemented as pre-alarm; appears approximately 20 K before

thermal shut down.

short circuit a connection of one output to GND for longer than 30 μs sets an

internal error flipflop. A phase change-over of the affected bridge resets the flipflop. Being a separate flipflop for each bridge, the

error can be located in such way.

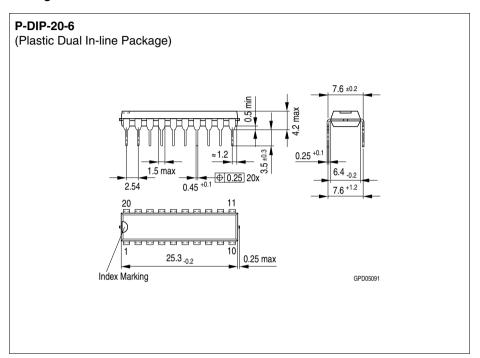
underload the recirculation of the inductive load is watched. If there is no

recirculation after a phase change-over, the internal error flipflop is set. Additionally an error is signaled after a phase change-over

during hold-mode.



Package Outlines



Sorts of Packing

Package outlines for tubes, trays etc. are contained in our Data Book "Package Information".

Dimensions in mm