

Compact Seven-Channel Regulator with Li+/Polymer Linear Battery Charger and I2C Interface

General Description

The AAT3608 is a member of Skyworks' Total Power Management IC (TPMIC™) product family. It contains a single-cell lithium ion/polymer battery charger, two 800mA switching regulators, and five low dropout (LDO) regulators in a small Pb-free 40-pin 5mmx5mm TQFN package, making it ideal for portable space-constrained systems. The single-input linear charger powers up from an adapter or a USB port. The adapter charge current is programmable with an external resistor or pin selectable between 100mA and 500mA when connected to a USB port. The device integrates a load switch for dynamic power path and features deep sleep mode operation. The step-down regulators are monolithic synchronous converters integrating the compensation network and soft start circuitry. The 1.5MHz operating frequency enables the use of tiny 2.2μH inductors and small 4.7μF output capacitors. External resistors set the output voltage for Buck 1 and Buck 2; the output voltage of Buck 2 is dynamically adjustable with I2C. The LDO regulators feature 3% output voltage accuracy over the full operating temperature range. The fast control loop of the LDO regulators also provide excellent transient response with a typical output voltage deviation of 1.5%. The AAT3608 provides protection features to safeguard from overtemperature operation, over-current operation, and a digital thermal loop to protect the battery during battery charging. The device is rated over an ambient temperature range of -40°C to 85°C.

Features

- 2.7V to 5.5V Operating Input Voltage Range
- Adapter or USB Single Input Linear Charger
- Battery Charger Digital Thermal Regulation
- Battery Temperature Monitoring
- Battery Charger Includes Programmable Timer
- Input Load Switch
- Dual 800mA Monolithic Switching Converters
	- **1.5MHz Switching Frequencies**
	- 95% Efficiency
	- **Example 1** Independent Input Power and Ground
	- **Buck1 Output Programmable With External** Resistors
	- **Buck 2 Feedback Voltage is Dynamically Adjustable** between 0.5V and 0.7V with I2C Interface
- Five Channel LDO Regulators
	- **300mA, Output Adjustable via Two Logic Inputs**
	- 80mA, Output Adjustable via I²C Interface
	- 50mA, 2.5V Output Voltage
	- 50mA, 3.3V Output Voltage
	- 80mA with 1.2V Fixed Output
	- 3% Accuracy and 1.5% Typical Transient Accuracy
- Very Low Shutdown Current
- Power-On Push Button
- Status Outputs
- **EXEDENT Interrupt, Reset and Status Pins, Low Battery Flag**
- Separate Enable Pin for LDO2, LDO4, LDO5, and Buck2 (when mask is removed)
- Over-Current and Over-Thermal Protection
- 5mmx5mm, 40-Pin TQFN Package

Applications

- GPS
- Handheld Devices
- Mobile Media Players
- MP3
- Portable Navigation

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Typical Application Circuit

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Pin Descriptions

Compact Seven-Channel Regulator with Li+/Polymer Linear Battery Charger and I2C Interface

Pin Configuration

Absolute Maximum Ratings¹

Thermal Information2, 3, 4

1. Stresses above those listed in Absolute Maximum Ratings may cause permanent damage to the device. Functional operation at conditions other than the operating conditions

specified is not implied. Only one Absolute Maximum Rating should be applied at any one time.

2. Thermal Resistance will be measured with the AAT3608 device on the 4-layer FR4 evaluation board in a thermal oven. The amount of power dissipation which will cause the thermal shutdown to activate will depend on the ambient temperature and the PC board layout ability to dissipate the heat.

3. Measured on the AAT3608 demo board.

4. Derate the maximum power dissipation by 40mW/°C above 25°C ambient temperature.

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Electrical Characteristics¹

 V_{PWR_IN} = 5V, V_{PWR_ID} = 5V, V_{BAT} = 3.6V, -40°C $\leq T_A \leq +85$ °C, unless noted otherwise. Typical values are T_A = 25°C.

1. Specification over the -40°C to +85°C operating temperature range is assured by design, characterization and correlation with statistical process controls.

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Electrical Characteristics (continued)¹

 $V_{PWR~IN}$ = 5V, $V_{PWR~ID}$ = 5V, V_{BAT} = 3.6V, -40°C $\leq T_A \leq +85$ °C, unless noted otherwise. Typical values are T_A = 25°C.

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Typical Characteristics−Charger

V(PWRIN-SYSOUT) (V)

Ideal Diode Load Switch between V_{BAT} and V_{SYSOUT}

Power-In to SYSOUT Switch Current Limit (100mA) 180 160 140 (pwRIN-SYSOUT) (MA) **I(PWRIN-SYSOUT) (mA)** 120 100 80 60 40 20 0 0 0 0.3 0.6 .9 1.2 1.5 1.8 2.1 2.4 2.7 3.0 3.3 3.6 3.9 4.2

V(PWRIN-SYSOUT) (V)

Constant Charging Current vs. RSET

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Typical Characteristics−Charger

Adapter Mode Supply Current vs. R_{SET} Resistor

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Typical Characteristics−Buck1

No Load Total Input Current vs. V_{BAT} Voltage (VEN = VBAT; Closed Loop)

Time (500ns/div)

Output Ripple $(V_{BAT} = 3.6V; V_{B1} = 2.5V; I_{OUTB1} = 1mA)$ LX Voltage (top) (V)
Inductor Current (bottom) (A) **Inductor Current (bottom) (A)** Output Voltage (middle) (V) **Output Voltage (middle) (V)** 3.6 **LX Voltage (top) (V)** $\overline{0}$ 2.55 2.50 2.45 0.2

Time (100µs/div)

0.0

System Line Transient Response $(V_{\text{IN}} = 3.5V \text{ to } 5V; V_{\text{BAT}} = 3.6V; V_{\text{OUTB1}} = 2.5V; I_{\text{OUTB1}} = 800 \text{mA}; \text{ falling})$

Time (200µs/div)

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Typical Characteristics−Buck1 (continued)

Time (200µs/div)

Time (100µs/div)

VBAT Voltage (V)

Output Voltage Error vs. Temperature $(V_{BAT} = 3.6V; V_{OUT1} = 2.5V)$

Switching Frequency vs. V_{BAT} Voltage $(\overrightarrow{V}_{\text{OUT1}} = 2.5V; I_{\text{OUT1}} = 800 \text{mA})$

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Typical Characteristics−Buck1 (continued)

Time (100µs/div)

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Typical Characteristics−Buck2

Output Ripple $(V_{BAT} = 3.6V; V_{OUTB2} = 1.2V; I_{OUTB2} = 1mA)$ Inductor Current (bottom) **Inductor Current (bottom) (A)** Output Voltage (middle) (V) **Output Voltage Voltage Voltage (V)** 3.6 LX Voltage (top) (V) **LX Voltage (top) (V)** 0 1.22 1.20 1.18 0.4 0.2 0.0 $\widehat{\mathcal{E}}$

Time (50µs/div)

Time (200µs/div)

Output Ripple $(V_{BAT} = 3.6V; V_{OUTB2} = 1.2V; I_{OUTB2} = 800mA)$

Time (500ns/div)

Time (200µs/div)

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Typical Characteristics−Buck2 (continued)

Time (100µs/div)

Soft Start $(V_{BAT} = 3.6V; V_{OUT1} = 1.2V; I_{OUT2} = 800mA; C_{FF} = 100pF)$ 4 **Output Current (bottom) (A)** EnableVoltage (top) (V)
Output Voltage (middle) (V) **Output Voltage Voltage Voltage Voltage Voltage (V)** 3 **EnableVoltage (top) (V)** 2 1 0 1.00.5 0.0

Time (100µs/div)

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Typical Characteristics−LDO1

Time (200µs/div)

Time (200µs/div)

System Line Transient Response $(V_{\text{IN}} = 3.5V \text{ to } 5V; V_{\text{BAT}} = 3.6V; V_{\text{LD01}} = 3V; I_{\text{LD01}} = 300 \text{mA}; \text{ falling})$ 6 Sysout Voltage (top) (V)
V_{ear} Voltage (middle) (V) **Sysout Voltage (top) (V) VBAT Voltage (middle) (V)** 5 **LDO1 Output Voltage** LDO1 Output Voltage 4 $\sum_{3.0}^{3.1}$ (A) (wo μ oq) **(bottom) (V)** 3 3.1 2.9 2.8

Time (200µs/div)

Line Regulation $(V_{\text{LDO1}} = 3.0V)$

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Typical Characteristics−LDO1 (continued)

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Typical Characteristics−LDO2

Time (200µs/div)

Load Transient Response $(I_{LDO2} = 8 \text{mA}$ to 80mA; $V_{BAT} = 3.6 V$; $V_{LDO2} = 1.2 V$; $C_{LDO2} = 4.7 \mu\text{F}$)

Time (200µs/div)

System Line Transient Response $(V_{\text{IN}} = 3.5V \text{ to } 5V; V_{\text{BAT}} = 3.6V; V_{\text{LDO2}} = 1.2V; I_{\text{LDO2}} = 80 \text{ mA}$; falling) 6 ϵ **Sysout Voltage (top) (V) VBAT Voltage (middle) (V)** 5 **LDO2 Output Voltage** LDO2 Output Voltage Sysout Voltage (top)
V_{BAT} Voltage (middle) 4 (V) (mottom) **(bottom) (V)** 3 1.3 1.2 1.1 1.0

Time (200µs/div)

Output Voltage Error vs. Temperature $(V_{BAT} = 3.6V; V_{LDO2} = 1.2V)$

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Typical Characteristics−LDO2 (continued)

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Typical Characteristics−LDO3

Time (200µs/div)

Load Transient Response $(I_{LDO3} = 8 \text{mA}$ to 80mA; $V_{BAT} = 3.6 \text{V}$; $C_{LDO3} = 4.7 \text{µF}$)

Time (200µs/div)

Time (200µs/div)

Line Regulation $(V_{LDO3} = 1.2V)$

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Typical Characteristics−LDO3 (continued)

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Typical Characteristics−LDO4

Time (200µs/div)

Load Transient Response $(I_{LDO4} = 5 \text{mA}$ to 50mA; $V_{BAT} = 3.6 V$; $V_{LDO4} = 2.5 V$; $C_{LDO4} = 4.7 \mu\text{F}$)

Time (200µs/div)

System Line Transient Response $(V_{\text{IN}} = 3.5V \text{ to } 5V; V_{\text{BAT}} = 3.6V; V_{\text{LD04}} = 2.5V; I_{\text{LD04}} = 50 \text{ mA}$; falling) 6 ϵ **Sysout Voltage (top) (V) VBAT Voltage (middle) (V)** 5 **LDO4 Output Voltage** LDO4 Output Voltage Sysout Voltage (top)
V_{BAT} Voltage (middle) 4 (V) (mottom) **(bottom) (V)** 3 2.7 2.6 2.5 2.4 2.3

Time (200µs/div)

Line Regulation $(V_{LDO4} = 2.5V)$

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Typical Characteristics−LDO4 (continued)

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Typical Characteristics−LDO5

Time (200µs/div)

Load Transient Response $(I_{LDOS} = 5mA$ to 50mA; $V_{BAT} = 3.9V$; $C_{LDOS} = 4.7\mu F$)

Time (200µs/div)

Time (200µs/div)

Line Regulation $(V_{LD05} = 3.3V)$

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Typical Characteristics−LDO5 (continued)

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Functional Block Diagram

Functional Description

The AAT3608 is a complete power management solution. It seamlessly integrates a battery charger with two stepdown converters and five low-dropout regulators to provide power from either an external power source or a single-cell Lithium Ion/Polymer battery. Internal load switches allow the converters to operate from the best available power source.

If only the battery is available, then the voltage converters are powered directly from the battery through a 100 mΩ load switch (BAT to SYSOUT). During this condition, the charger is put into sleep mode and draws less than 1µA quiescent current. If the system is connected to a wall adapter, then the voltage converters are powered directly from the adapter through a 200mΩ load-switch (PWR_IN to SYSOUT) and the battery is disconnected from the voltage converter inputs. This allows the system to operate regardless of the state of the battery. It can even operate with no battery.

System Output (SYSOUT)

Intelligent control of the integrated load switches is managed by the switch control circuitry. If the voltage across PWR_IN and GND pin is above the UVLO typical threshold voltage of 4.5, then the switch control will automatically short the load switch connecting PWR_IN to SYSOUT. Additionally, the charging switch will be enabled and switch connecting BAT and SYSOUT will be turned off. The location of the two switches and the battery charging switch allows the step-down converter and LDO to always have the best available source of power. Furthermore, AAT3806 control logic allows the voltage converters to operate with no battery, or with a battery voltage below the trickle charge threshold.

Compact Seven-Channel Regulator with Li+/Polymer Linear Battery Charger and I2C Interface

Battery Charging

Battery charging commences only after the AAT3608 battery charger checks several conditions in order to maintain a safe charging environment. When an adapter input is connected to PWR_IN and is greater than 4.5V, the EN_{CHG} bit is set (default) and the PWR_HOLD signal is high, the charger is enabled. The charger can be disabled by clearing the EN_{CHG} bit through the I²C interface.

Figure 1 illustrates the entire battery charging profile or operation, which consists of three phases:

- 1. Preconditioning (Trickle) Charge
- 2. Constant Current Charge
- 3. Constant Voltage Charge

During battery charging, the battery charger initially checks the condition of the battery and determines which charging mode to apply. If the battery voltage is below V_{MIN} , then the battery charger initiates trickle charge mode and charges the battery at 12% of the programmed constant-current magnitude. For example, if the programmed current (I_{SETA}) is 500mA, then the trickle charge current will be 60mA. Trickle charge is a safety precaution for a deeply discharged cell. It is intended to reduce stress on the battery, but also reduces the power dissipation in the internal series pass MOSFET when the inputoutput voltage differential is at its highest.

Trickle charge continues until the battery voltage reaches 2.8V. At this point the battery charger begins constant-current charging. The current level for this mode is programmed using a resistor from the ISETA pin to ground, or can be selected through the USBSEL pin with settings of 100mA or 500mA; refer to the logic settings in Table 2. Constant-current charging continues until the voltage reaches the charge voltage regulation point.

 $V_{BAT, REG}$ is factory programmed to 4.2V (nominal). Charging in constant-voltage mode will continue until the charge current has reduced to the charge termination current threshold. After the charge cycle is complete, the battery charger turns off the series pass device and automatically goes into a power saving sleep mode. During this time, the series pass device will block current in both directions to prevent the battery from discharging through the battery charger.

The battery charger will remain in sleep mode even if the charger source is disconnected. It will come out of sleep mode when either the battery terminal voltage drops below the V_{RCH} threshold, or the charging source is removed and reconnected. In all cases, the battery charger will monitor all parameters and resume charging in the most appropriate mode.

Battery Temperature Fault Monitoring

The TS pin is available to monitor the battery temperature. Connect a 10k NTC resistor from the TS pin to ground. The TS pin outputs a 75µA constant current into the resistor and monitors the voltage to ensure that the battery temperature does not fall outside the operating limits depending on the temperature coefficient of the resistor used. When the voltage goes above 2.39V or goes below 0.331V, the charging will be suspended. A Beta range of 3300 to 4000 will place the typical charging temperature between -4°C and 48°C.

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Battery Charging Flowchart

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Buck Regulators

The AAT3608 step-down converters are peak current mode PWM converters operating at 1.5MHz frequency. The input voltage range is 2.7V to 5.5V. The converters provide internal compensation. Power devices are sized for 800mA output current while maintaining over 85% efficiency at full load. Peak efficiency is above 90%. Light load efficiency is maintained at greater than 80% down to 85% of full load current. Soft start limits the current surge seen at the input and eliminates output voltage overshoot.

The input pin, INBUCK (Pin 24) must be connected to the SYSOUT output pin. The Buck1 output voltage is adjustable from 0.6V to 5.5V and is programmed through an external resistor divider. Buck2 output default value is set by external resistor feedback and then the feedback voltage can be dynamically adjusted via I2C in 12.5mV increments from 0.5V to 0.7V.

For overload conditions, the peak input current is limited. Also, thermal protection completely disables switching if internal dissipation becomes excessive, thus protecting the device from damage. The junction overtemperature threshold is 140°C with 15°C of hysteresis. Under-voltage lockout (UVLO) guarantees sufficient VIN bias and proper operation of all internal circuits prior to activation.

The current through the P-channel MOSFET (high side) is sensed for current loop control, as well as short circuit and overload protection. A fixed slope compensation signal is added to the sensed current to maintain stability for duty cycles greater than 50%. The peak current mode loop appears as a voltage-programmed current source in parallel with the output capacitor. The output of the voltage error amplifier programs the current mode loop for the necessary peak switch current to force a constant output voltage for all load and line conditions. Internal loop compensation terminates the transconductance voltage error amplifier output. The reference voltage is internally set to program the converter output voltage greater than or equal to 0.6V.

For conditions where the input voltage drops to the output voltage level, the converter duty cycle increases to 100%. As the converter approaches the 100% duty cycle, the minimum off-time initially forces the high side on-time to exceed the 1.5MHz clock cycle and reduces the effective switching frequency. Once the input drops

below the level where the converter can regulate the output, the high side P-channel MOSFET is enabled continuously for 100% duty cycle. At 100% duty cycle the output voltage tracks the input voltage minus the I*R drop of the high side P-channel MOSFET.

For overload conditions, the peak input current is limited. The bucks use a cycle-by-cycle current limit to protect itself and the load from an external fault condition. Thermal protection completely disables switching when internal dissipation becomes excessive. The junction over-temperature threshold is 140°C with 15°C of hysteresis. Once an over-temperature or over-current fault conditions is removed, the output voltage automatically recovers.

Low-Dropout Regulators

The advanced circuit design of the linear regulators has been specifically optimized for very fast start-up and shutdown timing. These proprietary LDOs are tailored for superior transient response characteristics. These traits are particularly important for applications which require fast power supply timing.

The high-speed turn-on capability is enabled through the implementation of a fast start control circuit, which accelerates the power up behavior of fundamental control and feedback circuits within the LDO regulator. For fast turn-off time response is achieved by an active output pull down circuit, which is enabled when the LDO regulator is placed in the shutdown mode. This active fast shutdown circuit has no adverse effect on normal device operation.

There are two LDO input pins, INLDO (pins 6 and 9), which must be connected to the SYSOUT output pin.The LDO1 output voltage is selectable using pins S1 and S2 as shown in Table 1. LDO2 is fixed at 1.2V, LDO4 is fixed at 2.5V and LDO5 is fixed at 3.3V. LDO3 output default value is 1.2V and then can be dynamically adjusted via I ²C in 25mV increments from 1.0V to 1.4V.

Table 1: LDO1 Output Voltages.

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Controlling the System Outputs

The AAT3608 has a specific startup and shutdown conditions depending on its mode of operation.

Shutdown Mode

"Shutdown Mode" is defined as the mode where the entire PMU (Power Management Unit) is shut down. This is a state that normally happens after all power has been disconnected from PWR_IN and BAT. Typically, after power has been applied and the part has been turned on, it will normally never need to be turned off. For GPS applications, the amount of time required for the SOC to start up from shutdown is prohibitively long, so the only time that it will go into Shutdown Mode (from any other mode) is when PWR_IN is disconnected and the BAT is below the Low-Battery comparator threshold.

Normal Mode

"Normal Mode" is defined as the mode where all regulators are active. Once the part is in Normal Mode, it will typically go into Sleep or Deep-Sleep Mode when trying to save current.

SOC Sleep Mode

"Sleep Mode" is an SOC-defined mode which simply means that all regulators are shut down except SYSOUT, Buck1, LDO1, and LDO3. To get into this mode from Normal, the SOC will pull the PWR_EN pin low to turn off LDO2, LDO4, and LDO5. Buck2 can also be controlled by PWR_EN only if the SOC masks PWR_EN through I²C. From a PMU point of view, it is no different from Normal Mode except for the regulators that have been switched off by pulling PWR_EN low.

Deep Sleep Mode

"Deep Sleep Mode" is both an SOC and PMU-defined mode where all regulators have been turned off except for SYSOUT and Buck1. Data is backed up by the SOC and Buck1 stays alive to maintain the memory. LDO4 and LDO5 would be turned off separately by I²C, but the DS_RDY and PWR_DS_I²C bits are used to get into and out of Deep Sleep Mode. See the flowchart diagrams for more detail.

PWR_ID Pin

The PWR_ID pin is an input logic pin which determines the current limits and fast charge currents that will be used by PMU. PWR_ID settings are listed in Table 2.

Timing Sequences

The AAT3608 has a specific startup sequence when the device is activated. See the timing diagrams in Figures 2 through 7.

RESET

The RESET pin is an open drain active low output signal for system reset. Connect a pull-up resistor from the RESET pin to SYSOUT pin with a recommended resistance value of 100kΩ. After Buck2 and LDO2 reach their target nominal output voltage, a delay of 200ms exists before RESET goes high; refer to the timing diagram in Figure 2.

Table 2: PWR_ID Settings.

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Notes 1: T1 at least 650µS for internal LVR setup time; T2 is about 2ms to wait until PLL is stable; other time interval is dependent on power stability.
Notes 2: After wake-up sequence from Deep-sleep Mode, the power on s

Figure 4: Normal \Leftrightarrow **Deep-Sleep Mode Sequence.**

Figure 5: Normal Mode Deep-Sleep Mode Normal Mode Flowchart.

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Figure 7: System Shutdown Normal Mode (Initial Start-Up) Flowchart.

Compact Seven-Channel Regulator with Li+/Polymer Linear Battery Charger and I2C Interface

I ²C Serial Interface and Programmability

Serial Interface

Many of the features of the AAT3608 can be controlled via the I2C serial interface. The I2C serial interface is a widely used interface where it requires a master to initiate all the communications with the slave devices. The I ²C protocol consists of 2 active wires, SDA (serial data line) and SCL (serial clock line). Both wires are open drain and require an external pull up resistor to V_{CC} (SYSOUT may be used as V_{cc}). The SDA pin serves I/O function, and the SCL pin controls and references the I2C bus. I2C protocol is a bidirectional bus which allows both read and write actions to take place. The timing diagram in Figure 8 depicts the transmission protocol.

START and STOP Conditions

START and STOP conditions are always generated by the master. Prior to initiating a START condition, both the SDA and SCL pin are idle mode (idle mode is when there is no activity on the bus and SDA and SCL are pulled to Vcc via external resistor). As depicted in Figure 9, a START condition is defined to be when the master pulls the SDA line low and after a short period pulls the SCL line low. A START condition acts as a signal to all ICs that something is about to be transmitted on the BUS. A STOP condition, also shown in Figure 9, is when the master releases the bus and SCL changes from low to high followed by SDA low to high transition. The master does not issue an ACKNOWLEDGE and releases the SCL and SDA pins.

Transferring Data

Every byte on the bus must be 8 bits long. A byte is always sent with the most significant bit first (see Figure 8).

Figure 8: Bit Order.

Acknowledge Bit

The acknowledge bit is the ninth bit of data. It is used to send back a confirmation to the master that the data has been received properly. For acknowledge to take place, the MASTER must first release the SDA line, then the SLAVE will pull the data line low as shown in Figure 9.

The address is embedded in the first seven bits of the byte. The eighth bit is reserved for the direction of the information flow for the next byte of information. For the AAT3608, this bit must be set to "0" when writing and "1" when reading. The full 8-bit address including the R/W bit is 0x9C (hex) or 10011100 in binary for writing and 0x9D(hex) or 10011101 in binary for reading.

I ²C Write Code

After sending the chip address, the master should send an 8-bit data stream ("2ND Word"). The "2ND Word" can consist of any one of the four sets of data listed in Table 3.

The "3RD Word" should be entered into the I²C only if $(Bit₇, Bit₆, Bit₅) = (0,0,0)$ in the "2ND Word". In this case, the bits (G2,G1,G0) are used to set the bit assignments as shown in Tables 4 and 5.

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Figure 9: I2C Protocol.

Table 3: I2C "2nd Word" Bit Assignments.

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Table 4: I2C "3rd Word" Bit Assignments for (G2,G1,G0) = (0,0,0)

Table 5: I²C "3rd Word" Bit Assignments for $(G2, G1, G0) = (0, 1, 0)$ **.**

 Table 7: LDO4 Output Voltage. Table 8: LDO5 Output Voltage.

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Table 9: Enable Settings.

Interrupt (Read from I2C)

A single byte is used when reading I^2C data from the AAT3608. The R/W address should be set to 1 so that complete address of the chip would be 0x9D or 10011101 in binary.

The INT (interrupt) pin is an open drain output which pulls low when there is an assertion in any one of the status bits (except the DS_RDY and PWR_DS bits). When a Read from the I2C is initiated AND completed by the SOC, the INT pin is released and the voltage will go high through the external pull-up resistor.

Table 10: I2C Read Table.

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Table 11: Status Bit Descriptions.

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Application Information

The two bucks are high performance 800mA 1.5MHz monolithic step-down converters. They have been designed with the goal of minimizing external component size and optimizing efficiency over the complete load range. Apart from the small bypass input capacitor, only a small L-C filter is required at the output.

Both bucks can be programmed with external feedback resistors to any voltage, ranging from 0.6V to the input voltage in default feedback voltage condition.

At dropout, the step down converters duty cycle increases to 100% and the output voltage tracks the input voltage minus the R_{DSON} drop of the P-channel high-side MOSFET.

Output Voltage Resistor Selection

Resistors R2 through R5 in Figure 10 program the output to regulate at a voltage higher than 0.6V in default mode. The feedback voltage of Buck2 can have a wider range and can be adjusted down to 0.5V through I²C. To limit the bias current required for the external feedback resistor string while maintaining good noise immunity, a suggested value for R3 and R5 is 59kΩ to provide a bias current of 10uA with a feedback voltage of 0.6V. Although a larger value will further reduce quiescent current, it will also increase the impedance of the feedback node, making it more sensitive to external noise and interference. Table 12 summarizes the resistor values for various output voltages with R3 and R5 set to either 59kΩ for good noise immunity or 100kΩ for reduced no load input current.

Table 12: Feedback Resistors (Feedback Voltage = 0.6V).

Input Capacitor (Bucks)

All input capacitors should be located as physically close to the power pin (INBUCK) and power ground pins (PGND1 and 2). Ceramic capacitors are recommended for their higher current operation and small profile. Also, ceramic capacitors are inherently capable to withstand input current surges from low impedance sources such as batteries in portable devices over tantalum capacitors. Typically, 10V or 16V rated capacitors are required.

The following are the typical recommended capacitance values:

Two 10μF capacitors for INBUCK One 10μF capacitor for INLDO One 10μF capacitor for SYSOUT One 10μF capacitor for PWR_IN One 10μF capacitor for BAT

Output Capacitor (Bucks)

For proper load voltage regulation and operational stability, a capacitor is required on the output of each buck. The output capacitor connection to the ground pin should be made as directly as practically possible for maximum device performance. Since the bucks have been designed to function with very low ESR capacitors, a 4.7μF ceramic capacitor is recommended for best performance.

Inductor Selection

The two bucks use peak current mode control with slope compensation to maintain stability for duty cycles greater than 50%. The output inductor value must be selected so the inductor current down slope meets the internal slope compensation requirements. The internal slope compensation is 1A/μs. The inductor should be set equal to the output voltage numeric value in micro henries (μH). This guarantees that there is sufficient internal slope compensation.

Inductor manufacturer's specifications list both the inductor DC current rating, which is a thermal limitation, and the peak current rating, which is determined by the saturation characteristics. The inductor should not show any appreciable saturation under normal load conditions. Some inductors may meet the peak and average current ratings yet result in excessive losses due to a high DCR. Always consider the losses associated with the DCR and its effect on the total converter efficiency when selecting an inductor.

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Input Capacitor (LDOs)

Typically, a 10μF or larger capacitor, C4 (see Figure 10), is recommended as close as possible to the device INLDO pin. The input capacitor value of 10μF will offer superior input line transient response and will assist in maximizing the highest possible power supply ripple rejection.

There is no specific capacitor ESR requirement; therefore ceramic, tantalum, or aluminum electrolytic capacitors may be selected for capacitor C4. However, ceramic capacitors are recommended due to their inherent capability over tantalum capacitors to withstand input current surges from low impedance sources such as batteries in portable devices.

Output Capacitor (LDOs)

For proper load voltage regulation and operational stability, a 4.7µF ceramic capacitor is required between the output of the LDOs and GND. If desired, the output capacitor may be increased without limit. The output capacitor connection to the LDO regulator ground pin should be made as direct as practically possible for maximum device performance.

Although the device is intended to operate with low ESR capacitors, it is stable over a very wide range of capacitor ESR, thus it will also work with higher ESR tantalum or aluminum electrolytic capacitors. However, for best performance, ceramic capacitors are recommended.

Layout Guidance

Figure 10 is the schematic for the evaluation board. The evaluation board has extra components for easy evaluation; the bill of materials for the system is shown in Table 12. When laying out the PC board, the following layout guidelines should be followed to ensure proper operation of the AAT3608:

- 1. The exposed pad (EP) must be reliably soldered to exposed copper pad on the board and electrically connected to GND/PGND pins.
- 2. The power traces, including GND traces, the LX traces and the VIN trace should be kept short, direct and wide to allow large current flow. Use several via pads when routing between layers.
- 3. The input capacitors should be connected as close as possible from SYSOUT and INBUCK to PGND1 and PGND2 to get good power filtering.
- 4. Keep the switching node LX away from the sensitive buck feedback nodes, FB1 and FB2.
- 5. The feedback trace for the bucks should be separate from any power trace and connected as closely as possible to the load point. Sensing along a high current load trace will degrade DC load regulation.
- 6. The output capacitors and inductors should be connected as close as possible and there should not be any signal lines under the inductor.
- 7. The resistance of the trace from the load return to PGND1 and PGND2 should be kept to a minimum. This will help to minimize any error in DC regulation due to differences in the potential of the internal signal ground and the power ground.

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Figure 10: AAT3608 Evaluation Board Schematic.

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Figure 11: AAT3608 Evaluation Board Silk Screen Layer.

 Figure 12: AAT3608 Evaluation Board Top Layer. Figure 13: AAT3608 Evaluation Board

 Mid Layer 1 (GND Plane).

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Figure 14: AAT3608 Evaluation Board **Figure 15: AAT3608 Evaluation Board**

Mid Layer 2 (SYSOUT). Bottom Layer.

Table 12: AAT3608 Evaluation Board Bill of Materials (BOM).

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Ordering Information

Skyworks Green™ products are compliant with all applicable legislation and are halogen-free. For additional information, refer to Skyworks Definition of Green™, document number SQ04-0074.

Package Information

All dimensions in millimeters.

1. XYY = assembly and date code.

3. Available exclusively outside of the United States and its territories.

4. The leadless package family, which includes QFN, TQFN, DFN, TDFN and STDFN, has exposed copper (unplated) at the end of the lead terminals due to the manufacturing process. A solder fillet at the exposed copper edge cannot be guaranteed and is not required to ensure a proper bottom solder connection.

^{2.} Sample stock is generally held on part numbers listed in **BOLD**.

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