

3A Dual Channel Synchronous Step-Down Switcher with Integrated FET

Check for Samples: [TPS54395](http://www.ti.com/product/tps54395 #samples)

- -
	- **No External Parts Required For Loop Digital TV Power Supply Compensation – Networking Home Terminal**
	- **Compatible with Ceramic Output Digital Set Top Box (STB) Capacitors – DVD Player/Recorder**
- **Wide Input Voltage Range : 4.5 V to 18 V Gaming Consoles and Other**
- **Output Voltage Range : 0.76V to 7.0V**
- **Highly Efficient Integrated FETs Optimized for DESCRIPTION**
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- **r**_{DS(on)} with 4000ppm/°C voltages from 4.5V to 18V.
-
-

¹FEATURES APPLICATIONS

- **² D-CAP2™ Control Mode Point-of-Load Regulation in Low Power – Fast Transient Response Systems for Wide Range of Applications**
	-
	-
	-
	-
	-

Low Duty Cycle Applications The TPS54395 is a dual, adaptive on-time D-CAP2™ **– 90 mΩ (High Side) and 60 mΩ (Low Side)** and **mode** synchronous buck converter. The TPS54395 enables system designers to complete the suite of enables system designers to complete the suite of enables system designers various end equipment's power bus regulators with a **• Supports Constant 3A at Both Channels** cost effective, low component count, and low standby
 Low-Side resessing Service Current Sensing current solution. The main control loops of the **Low-Side r_{DS(on)} Loss-Less Current Sensing example the Current Solution. The main control loops of the D-CAP2™ mode control which control which** TPS-339 use the D-CAP2™ mode control which

• Adjustabel Soft Start

• A external compensation components. The adaptive on-**100 kHz Switching Frequency • 11 time control supports seamless transition between • 700 kHz Switching Frequency • 700 kHz Switching Frequency • 70 PWM** mode at higher load conditions and Eco-**Puller at higher load conditions and Eco-**

• mode™ operation at light loads. Eco-mode™ allows

• mode™ operation at light loads. Eco-mode™ allows

• the TPS54395 to maintain high efficiency during the TPS54395 to maintain high efficiency during **Franceup Timer for Overload Protection** lighter load conditions. The TPS54395 is able to
Adoptive Cate Drivers with Integrated Boost adapt to both low equivalent series resistance (ESR) Adaptive Gate Drivers with Integrated Boost

• Adaptive Journ low equivalent series resistance (ESR)

• OUT CONS Switch

• OUT CONS Switch

• PMOS Switch
 PMOS Switch
 PMOS Switch
 PMOS Switch
 PMOS Switch
 PMOS S provides convenient and efficient operation with input

16-Pin HTSSOP, 16-Pin VQFN The TPS54395 is available in a 4.4 mm x 5 mm 16-**• Auto-Skip Eco-mode™ for High Efficiency at** pin TSSOP (PWP) and 4 mm x 4 mm 16-pin VQFN **Light Load** (RSA) package, and is specified for an ambient temperature range from –40°C to 85°C.

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of ÆΝ Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. D-CAP2, Eco-mode, Eco-Mode are trademarks of Texas Instruments.

[TPS54395](http://www.ti.com/product/tps54395 ?qgpn=tps54395)

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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com

(2) Package drawings, thermal data, and symbolization are available at www.ti.com/packaging.

(3) All packaging options have Cu NIPDAU lead/ball finish.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)⁽¹⁾⁽²⁾

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" are not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltages are with respect to IC GND terminal.

THERMAL INFORMATION

(1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, [SPRA953](http://www.ti.com/lit/pdf/spra953).

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RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

ELECTRICAL CHARACTERISTICS(1)

over recommended free-air temperature range, VIN = 12 V (unless otherwise noted)

(1) x means either 1 or 2, that is, VFBx means VFB1 or VFB2.

(2) Specified by design. Not production tested.

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ELECTRICAL CHARACTERISTICS[\(1\)](#page-3-0) (continued)

over recommended free-air temperature range, VIN = 12 V (unless otherwise noted)

(3) Specified by design. Not production tested.

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PIN FUNCTIONS(1)

(1) x means either 1 or 2, that is, VFBx means VFB1 or VFB2.

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FUNCTIONAL BLOCK DIAGRAM

OVERVIEW

The TPS54395 is a 3A/3A dual synchronous step-down (buck) converter with two integrated N-channel MOSFETs for each channel. It operates using D-CAP2™ control mode. The fast transient response of D-CAP2™ control reduces the required output capacitance to meet a specific level of performance. Proprietary internal circuitry allows the use of low ESR output capacitors including ceramic and special polymer types.

DETAILED DESCRIPTION

PWM Operation

The main control loop of the TPS54395 is an adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2™ control mode. D-CAP2™ control combines constant on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off when the internal timer expires. This timer is set by the converter's input voltage, VINx, and the output voltage, VOx, to maintain a pseudo-fixed frequency over the input voltage range hence it is called adaptive on-time control. The timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the nominal output voltage. An internal ramp is added to the reference voltage to simulate output voltage ripple, eliminating the need for ESR induced output ripple from D-CAP™ control.

PWM Frequency and Adaptive On-Time Control

TPS54395 uses an adaptive on-time control scheme and does not have a dedicated on board oscillator. The TPS54395 runs with a pseudo-fixed frequency of 700 kHz by using the input voltage and output voltage to set the on-time timer. The on-time is inversely proportional to the input voltage and proportional to the output voltage, therefore, when the duty ratio is VOx/VINx, the frequency is constant.

Auto-Skip Eco-Mode™ Control

The TPS54395 is designed with Auto-Skip Eco-mode™ to increase light load efficiency. As the output current decreases from heavy load condition, the inductor current also reduces and eventually comes to the point where its ripple valley touches the zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when zero inductor current is detected. As the load current further decreases the converter runs into discontinuous conduction mode. The on-time is kept almost the same as it was in the continuous conduction mode because it takes longer to discharge the output capacitor with smaller load current to the nominal output voltage. The transition point to the light load operation $I_{Ox(LL)}$ current can be estimated with [Equation 1](#page-6-0) with 700-kHz used as f_{SW} .

$$
I_{\text{Ox(LL)}} = \frac{1}{2 \times L1x \times f_{\text{SW}}} \times \frac{(V_{\text{INx}} - V_{\text{Ox}}) \times V_{\text{Ox}}}{V_{\text{INx}}} \tag{1}
$$

Soft Start and Pre-Biased Soft Start

The soft start time is adjustable. When the ENx pin becomes high, 8-µA current begins charging the capacitor which is connected from the SS_x pin to GND. Smooth control of the output voltage is maintained during start up. The equation for the slow start time is shown in [Equation 2.](#page-6-1) VFBx voltage is 0.765-V and SSx pin source current is 8-µA.

$$
T_{SS}(ms) = \frac{C4x(nF) \times VFBx(V)}{I_{SS}(\mu A)} = \frac{C4x(nF) \times 0.765 V}{8 \mu A}
$$
 (2)

The TPS54395 contains a unique circuit to prevent current from being pulled from the output during startup if the output is pre-biased. When the soft-start commands a voltage higher than the pre-bias level (internal soft start becomes greater than internal feedback voltage VFBx), the controller slowly activates synchronous rectification by starting the first low side FET gate driver pulses with a narrow on-time. It then increments that on-time on a cycle-by-cycle basis until it coincides with the time dictated by (1-D), where D is the duty cycle of the converter. This scheme prevents the initial sinking of the pre-biased output, and ensures that the output voltage (VOx) starts and ramps up smoothly into regulation from pre-biased startup to normal mode operation.

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Current Sensing and Over-Current Protection

The output over-current protection (OCP) is implemented using a cycle-by-cycle valley detection control circuit. The switch current is monitored by measuring the low-side FET switch voltage between the SWx and PGNDx pins. This voltage is proportional to the switch current and the on-resistance of the FET. To improve the measurement accuracy, the voltage sensing is temperature compensated.

During the on-time of the high-side FET switch, the switch current increases at a linear rate determined by VINx, VOx, the on-time and the output inductor value. During the on-time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current I_{Ox} . If the sensed voltage on the low-side FET is above the voltage proportional to the current limit, the converter keeps the low-side switch on until the measured voltage falls below the voltage corresponding to the current limit and a new switching cycle begins. In subsequent switching cycles, the on-time is set to the value determined for CCM and the current is monitored in the same manner.

Important considerations for this type of over-current protection: The load current is one half of the peak-to-peak inductor current higher than the over-current threshold. Also when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. When the over current condition is removed, the output voltage returns to the regulated value. This protection is nonlatching.

Undervoltage Protection and Hiccup Mode

Hiccup mode of operation protects the power supply from being damaged during an over-current fault condition. If the OCL comparator circuit detects an over-current event the output voltage falls. When the feedback voltage falls below 68% of the reference voltage, the UVP comparator output goes high and an internal UVP delay counter begins counting. After counting UVP delay time, the TPS54395 shuts off the power supply for a given time (7x UVP Enable Delay Time) and then tries to re-start the power supply. If the over-load condition has been removed, the power supply starts and operates normally; otherwise, the TPS54395 detects another over-current event and shuts off the power supply again, repeating the previous cycle. Excess heat due to overload lasts for only a short duration in the hiccup cycle, therefore the junction temperature of the power device is much lower.

UVLO Protection

Under-voltage lock out protection (UVLO) monitors the voltage of the V_{REG5} pin. When the V_{REG5} voltage is lower than the UVLO threshold, the TPS54395 shuts down. As soon as the voltage increases above the UVLO threshold, the converter starts again.

Thermal Shutdown

TPS54395 monitors its temperature. If the temperature exceeds the threshold value (typically 155°C), the device shuts down. When the temperature falls below the threshold, the IC starts again.

When VIN1 starts up and VREG5 output voltage is below its nominal value, the thermal shutdown threshold is lower than 155°C. As long as VIN1 rises, T_J must be kept below 110°C.

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TYPICAL CHARACTERISTICS

One output is enabled unless otherwise noted. $V_1 = VIN1$ or VIN2. VIN = 12 V, $T_A = 25^{\circ}C$ (unless otherwise noted).

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DESIGN GUIDE

Step By Step Design Procedure

To begin the design process, you must know a few application parameters:

- Input voltage range
- Output voltage
- Output current

In all formulas x is used to indicate that they are valid for both converters. For the calculations the estimated switching frequency of 700 kHz is used.

Figure 24. Schematic Diagram for the Design Example

Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the VFBx pin. It is recommended to use 1% tolerance or better divider resistors. Start by using [Equation 3](#page-12-0) to calculate V_{Ox} .

To improve the efficiency at very light loads consider using larger value resistors, but too high resistance values will be more susceptible to noise and voltage errors due to the VFBx input current will be more noticeable.

$$
V_{\text{Ox}} = 0.765 \text{ V} \times \left(1 + \frac{\text{R1x}}{\text{R2x}}\right) \tag{3}
$$

Output Filter Selection

The output filter used with the TPS54395 is an LC circuit. This LC filter has double pole at:

$$
F_{\rm P} = \frac{1}{2\pi\sqrt{L1x \times C1x}}\tag{4}
$$

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the TPS54395. The low frequency phase is 180 degrees. At the output filter pole frequency, the gain rolls off at a –40 dB per decade rate and the phase drops rapidly. D-CAP2™ introduces a high frequency zero that reduces the gain roll off to –20 dB per decade and increases the phase to 90 degrees one decade above the zero frequency. The inductor and capacitor selected for the output filter must be selected so that the double pole of [Equation 4](#page-12-1) is located below the high frequency zero but close enough that the phase boost provided by the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in [Table 1](#page-13-0).

Table 1. Recommended Component Values

(1) Optional

For higher output voltages at or above 1.8 V, additional phase boost can be achieved by adding a feed forward capacitor (Cffx) in parallel with R1x.

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 5,](#page-13-1) [Equation 6](#page-13-2) and [Equation 7.](#page-13-3) The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current.

For the calculations, use 700 kHz as the switching frequency, f_{SW} . Make sure the chosen inductor is rated for the peak current of [Equation 6](#page-13-2) and the RMS current of [Equation 7](#page-13-3).

$$
\Delta I_{L1x} = \frac{V_{Ox}}{V_{INx(MAX)}} \times \frac{V_{INx(MAX)} - V_{Ox}}{L1x \times f_{SW}}
$$
(5)

$$
I_{L1xpeak} = I_{Ox} + \frac{\Delta I_{L1x}}{2}
$$
\n
$$
I_{L1x(RMS)} = \sqrt{I_{Ox}^{2} + \frac{1}{40}\Delta I_{L1x}^{2}}
$$
\n(6)

L1x(RMS) $=$ \sqrt{Q} \sqrt{Q} $+$ $\frac{\sqrt{Q}}{4.2}$ \sqrt{Q} L1x 12 (7) For the above design example, the calculated peak current is 3.46 A and the calculated RMS current is 3.01 A

for VO2. The inductor used is a TDK CLF7045T-2R2N with a rated current of 5.5A based on the inductance change, and of 4.3A based on the temperature rise.

The capacitor value and ESR determines the amount of output voltage ripple. The TPS54395 is intended for use with ceramic or other low ESR capacitors. The recommended value range is from 20µF to 68µF. Use [Equation 8](#page-13-4) to determine the required RMS current rating for the output capacitor(s).

$$
I_{C2x(RMS)} = \frac{V_{Ox} \times (V_{INx} - V_{Ox})}{\sqrt{12} \times V_{INx} \times L1x \times f_{SW}}
$$
(8)

For this design two TDK C3216X5R0J226M 22µF output capacitors are used. The typical ESR is 2 mΩ each. The calculated RMS current is 0.19A and each output capacitor is rated for 4A.

Input Capacitor Selection

The TPS54395 requires an input decoupling capacitor and a bulk capacitor is needed depending on the application. A ceramic capacitor of or above 10µF is recommended for the decoupling capacitor. Additionally, 0.1 µF ceramic capacitors from pin 1 and Pin 16 to ground are recommended to improve the stability and reduce the SWx node overshoots. The capacitors voltage rating needs to be greater than the maximum input voltage.

Bootstrap Capacitor Selection

A 0.1 µF ceramic capacitors must be connected between the VBSTx and SWx pins for proper operation. It is recommended to use ceramic capacitors with a dielectric of X5R or better.

VREG5 Capacitor Selection

A 1 µF ceramic capacitor must be connected between the VREG5 and GND pins for proper operation. It is recommended to use a ceramic capacitor with a dielectric of X5R or better.

Thermal Information

This 16-pin PWP package incorporates an exposed thermal pad. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB is used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the exposed thermal pad and how to use the advantage of its heat dissipating abilities, refer to the Technical Brief, PowerPAD™ Thermally Enhanced Package, Texas Instruments Literature No. [SLMA002](http://www.ti.com/lit/pdf/SLMA002) and Application Brief, PowerPAD™ Made Easy, Texas Instruments Literature No. [SLMA004](http://www.ti.com/lit/pdf/SLMA004).

The exposed thermal pad dimensions for this package are shown in the following illustration.

Figure 25. Thermal Pad Dimensions

Layout Considerations

- 1. Keep the input current loop as small as possible. And avoid the input switching current through the thermal pad.
- 2. Keep the SW node as physically small and short as possible to minimize parasitic capacitance and inductance and to minimize radiated emissions.
- 3. Keep analog and non-switching components away from switching components.
- 4. Make a single point connection from the signal ground to power ground.
- 5. Do not allow switching currents to flow under the device.
- 6. Keep the pattern lines for VINx and PGNDx broad.

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- 7. Exposed pad of device must be soldered to PGND.
- 8. VREG5 capacitor should be placed near the device, and connected to GND.
- 9. Output capacitors should be connected with a broad pattern to the PGND.
- 10. Voltage feedback loops should be as short as possible, and preferably with ground shields.
- 11. Kelvin connections should be brought from the output to the feedback pin of the device.
- 12. Providing sufficient vias is preferable for VIN, SW and PGND connections.
- 13. PCB pattern for VIN, SW, and PGND should be as broad as possible.
- 14. VIN Capacitor should be placed as near as possible to the device.

Via to GND Plane

- **Blue parts can be placed on the bottom side**
- **Connect the SWx pins through another layer with the inductor (yellow line)**

Figure 26. TPS54395 Layout

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Figure 27. RSA Package Layout

REVISION HISTORY

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

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PACKAGE MATERIALS INFORMATION

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*All dimensions are nominal

TEXAS INSTRUMENTS

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TUBE

B - Alignment groove width

*All dimensions are nominal

GENERIC PACKAGE VIEW

PWP 16

PowerPAD[™] TSSOP - 1.2 mm max height
PLASTIC SMALL OUTLINE

Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

PWP0016A PowerPAD ™ HTSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. Reference JEDEC registration MO-153.
- 5. Features may not be present.

EXAMPLE BOARD LAYOUT

PWP0016A PowerPAD ™ HTSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.

EXAMPLE STENCIL DESIGN

PWP0016A PowerPAD ™ HTSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE

NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.

MECHANICAL DATA

NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- This drawing is subject to change without notice. Β.
- C. Quad Flatpack, No-leads (QFN) package configuration.
- The package thermal pad must be soldered to the board for thermal and mechanical performance. D.
- See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions. Ε.
- Falls within JEDEC MO-220. F.

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