# **RICHTEK**

## **5A Step-Down Converter with I2C Interface**

### **General Description**

The RT5735 device is a full featured 5.5V, 5A, synchronous step down constant-on-time (COT) current mode converter with two integrated MOSFETs. The RT5735 enables small designs by integrating the MOSFETs, implementing current mode control to reduce external component count, reducing inductor size by enabling up to 2.4MHz switching frequency, and minimizing the IC footprint with a small WL-CSP-20B 1.6x2 (BSC) package. The RT5735 provides accurate regulation for a variety of loads with an accurate ±1% Voltage Reference (VREF) over temperature. Efficiency is maximized through the integrated  $34 \text{m}\Omega/18 \text{m}\Omega$  MOSFETs and 70 $\mu$ A typical quiescent current. Using the enable pin, shutdown supply current is less than  $2\mu A$  by entering a shutdown mode.

The output voltage startup ramp is controlled by the slow start pin. An open-drain power good signal indicates the output is within 90% to 95% of its nominal voltage.

### **Marking Information**

1ZW

1Z : Product Code W : Date Code

### **Features**

- **2.5V to 5.5V Input Supply Voltage**
- **Current Mode COT Control Loop Design**
- **Fast Transient Response**
- Internal 34mΩ and 18mΩ Synchronous Rectifier
- **Highly Accurate V<sub>OUT</sub> Regulation Over Load/Line Range**
- **Robust Loop Stability with Low-ESR COUT**
- **Over-Temperature Protection**

### **Applications**

- Distributed Power Systems
- Enterprise Servers, Ethernet Switches & Routers, and Global Storage Equipment
- Telecom & Industrial Equipment

### **Ordering Information**

 $RT5735D$ 

Package Type WSC : WL-CSP-20B 1.6x2 (BSC)

Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ► Suitable for use in SnPb or Pb-free soldering processes.

### **Simplified Application Circuit**







### **Pin Configurations**

#### (TOP VIEW)

A1	A2	A3	A4
<b>VSEL</b>	EN	SCL	<b>FB</b>
B1	<b>B2</b>	B3 :	B4
<b>SDA</b>	PGND	PG/PGND	PGND
$\left($ C1 $\right)$	$\left($ C2 $\right)$	: сз :	$\cdot$ C4
AGND	PGND	PGND	PGND
: D1 :	$\left( 02\right)$	D <sub>3</sub>	D <sub>4</sub>
<b>AVDD</b>	PVDD	LX	LX
E1	E2	E3	LX
<b>PVDD</b>	PVDD	LX	

WL-CSP-20B 1.6x2 (BSC)

### **Functional Pin Description**



### **Function Block Diagram**



### **Operation**

The RT5735 is a synchronous low voltage step-down converter that can support the input voltage range from 2.5V to 5.5Vand the output current can be up to 5A. The RT5735 uses a constant on-time, current mode architecture. In steady-state operation, the high-side N-MOSFET is turned on when the current feedback reaches COMP level which is the amplified difference between the reference voltage and the feedback voltage. The on time of high-side N-MOSFET is determined by on-time generator which is a function of input and output voltage. After on-time expires, high-side MOSFET is turned off and low-side MOSFET is turned on. Until the low-side current sensing signal reaches the COMP, the high-side MOSFET is turned on again. In this manner, the converter regulates the output voltage and keeps the frequency constant.

The switching frequency is 2.4MHz allows for efficiency and size optimization when selecting the output filter components.

The RT5735 reduces the external component count by integrating the boot recharge MOSFET.

The error amplifier EA adjusts COMP voltage by comparing the output voltage with the internal  $I^2C$  set reference voltage. When the load increases, it causes a drop in the output voltage relative to the reference, then the COMP voltage rises to allow higher inductor current to match the load current.

#### **PWM Frequency and Adaptive On Time Control**

The on-time can be roughly estimated by the equation :

$$
T_{on} = \frac{V_{OUT}}{V_{IN}} \times \frac{1}{F_{SW}}
$$
 where Fsw is nominal 2.4MHz

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#### **Auto-Zero Current Detector**

The auto-zero current detector circuit senses the LX waveform to adjust the zero current threshold voltage. When the current of low-side MOSFET decreases to the zero current threshold, the low-side MOSFET turns off to prevent negative inductor current. In this way, the zero current threshold can adjust for different condition to get better efficiency.

#### **Protection Features**

The RT5735 has many features to protect the device.

#### **Under-Voltage Protection (UVLO)**

The UVLO continuously monitors the voltage of AVDD to make sure the device works properly. When the AVDD is high enough to reach the high threshold voltage of UVLO, the step-down converter softly starts or pre-bias to its regulated output voltage. When the AVDD decreases to its low threshold (180mV hysteresis), the device will shut down.

#### **Power Good**

When the output voltage is higher than PG rising threshold, the PG flag is High.

#### **Output Under-Voltage Protection (UVP)**

When the output voltage is lower than 400mV after soft-start end is ok, the UVP is triggered. When UVP occurs, the device enters hiccup mode.

#### **Over-Current Protection (OCP)**

The RT5735 senses the current signal when low-side MOSFET turns on and uses a valley current limiting circuit. As a result, the OCP set point is the OCP DC limit minus half of the ripple current. The OCP is cycle-by-cycle limit. If the OCP occurs, the converter holds off the next on pulse until inductor current drops below the OCP limit. If the OCP keeps and the load current is larger than the current provided by the converter, the output voltage drops. When the output voltage triggers UVP, the converter enters hiccup mode.

#### **Soft-Start**

An internal current source charges an internal capacitor to build the soft-start ramp voltage. The typical soft-start time is  $130\mu s$ .

#### **Over-Temperature Protection (OTP)**

The RT5735 has over-temperature protection. When the device triggers the OTP, the device shuts down.



### **Absolute Maximum Ratings** (Note 1)



### **Recommended Operating Conditions** (Note 4)



### **Electrical Characteristics**

( $V_{IN}$  = 3.6V, T<sub>A</sub> = 25°C, unless otherwise specified)









**Note 1.** Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

- **Note 2.**  $\theta_{JA}$  is measured at  $T_A = 25^\circ C$  on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package.
- **Note 3.** Devices are ESD sensitive. Handling precaution recommended.
- **Note 4.** The device is not guaranteed to function outside its operating conditions.
- **Note 5.** Guaranteed by design and characterized.

### **Typical Application Circuit**



### **Typical Operating Characteristics**











**Output Voltage vs. Output Current**





2.64

**Current Limit vs. Input Voltage** 8.0 7.5 Inductor Valley Current (A) 1 Inductor Valley Current (A) 7.0 6.5 6.0 5.5 5.0 4.5  $IOC < 1:0> = 11$  $\text{IOC} < 1:0 > 10$ 4.0  $\text{IOC} < 1:0 > = 01$ 3.5  $\overline{OC}$  <1:0> = 00  $V_{OUT} = 1.1V$ 3.0 3 3.5 4 4.5 5 5.5 Input Voltage (V)















DS5735-00 August 2014 www.richtek.com







Time (50μs/Div)







### **Application Information**

The basic RT5735 application circuit is shown in Typical Application Circuit. External component selection is determined by the maximum load current and begins with the selection of the inductor value and operating frequency followed by  $C_{IN}$  and  $C_{OUT}$ .

#### **Inductor Selection**

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current,  $\Delta I_L$ , increases with higher V<sub>IN</sub> and decreases with higher inductance, as shown in equation below :

$$
\Delta I_L = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]
$$

where f is the operating frequency and L is the inductance. Having a lower ripple current reduces not only the ESR losses in the output capacitors, but also the output voltage ripple. Higher operating frequency combined with smaller ripple current is necessary to achieve high efficiency. Thus, a large inductor is required to attain this goal. The largest ripple current occurs at the highest V<sub>IN</sub>. A reasonable starting point for selecting the ripple current is  $\Delta I_L = 0.3 \times I_{MAX}$  to 0.4×IMAX. To guarantee that the ripple current stays below a specified maximum, the inductor value should be chosen according to the following equation :

$$
L = \left[\frac{V_{OUT}}{f \times \Delta I_{L(MAX)}}\right] \times \left[1 - \frac{V_{OUT}}{V_{IN(MAX)}}\right]
$$

The inductor's current rating (defined by a temperature rise from  $25^{\circ}$ C ambient to  $40^{\circ}$ C) should be greater than the maximum load current and its saturation current should be greater than the short-circuit peak current limit.

#### **Input and Output Capacitor Selection**

An input capacitor,  $C_{IN}$ , is needed to filter out the trapezoidal current at the source of the high-side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The RMS current is given by :

$$
I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}
$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I<sub>RMS</sub> = I<sub>OUT(MAX)</sub> / 2$ . This simple worst-case condition is commonly used for design. Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet the size or height requirements of the design. Ceramic capacitors have high ripple current, high voltage rating and low ESR, which makes them ideal for switching regulator applications. However, they can also have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can lead to significant ringing. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input. V<sub>IN</sub>. At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at V<sub>IN</sub> large enough to damage the part. Thus, care must be taken to select a suitable input capacitor.

The selection of COUT is determined by the required ESR to minimize output voltage ripple. Moreover, the amount of bulk capacitance is also a key for COUT selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response. The output voltage ripple,  $\triangle V$ OUT, is determined by :

$$
\Delta V_{OUT} \leq \Delta I_L \left[ ESR + \frac{1}{8f_{OSC} C_{OUT}} \right]
$$

where fosc is the switching frequency and  $\Delta I$  is the inductor ripple current. The output voltage ripple will be the highest at the maximum input voltage since ΔIL increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Ceramic capacitors have excellent low ESR characteristics, but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing. Nevertheless, high value, low cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications.

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#### **I <sup>2</sup>C Interface Function**

RT5735 can be used by  $I^2C$  interface to select VOUT voltage level, over current limit level, thermal warning temperature level, PWM control mode, and so on. The register of each function can be found from the following register map and it also explains how to use these function.

**VOUT Selection :** RT5735 has external VSEL pin to select PROGVSEL1(0X10) or PROGVSEL0(0X11) which can control  $V_{\text{OUT}}$  from 0.6V to 1393.75mV with 7bits resolution. Pull VSEL to high is for PROGVSEL1 and pull VSEL to low is for PROGVSEL0. If VSELGT bit in the COMMAND register is set to  $0$ ,  $V_{\text{OUT}}$  will only be controlled by PROGVSEL1.

**Discharge Function :** In the PGOOD register DISCHG bit is set to 1 can let  $V_{\text{OUT}}$  discharge by internal resistor when converter shuts down. If setting to 0  $V_{\text{OUT}}$  will decrease depending on the loading.

**Power Good Function :** In the PGOOD register PGDCDC bit can control if external PG pin is active. After PG function is active if PGDVS pin is 0, PG will not change state during VOUT changing. Once PGDVS pin is 1 PG will be low when  $V_{\text{OUT}}$  is much lower than  $V_{\text{REF}}$ during V<sub>OUT</sub> changing.

**Slew Rate Setting :** RT5735 can control slew rate as VOUT changing between two voltage levels for both up and down. In the time register DVS\_UP bits can control up-speed when in the LIMCONF register DVS\_DOWN can control down-speed. DVS\_DOWN is valid only when converter is at PWM mode or DVSMODE bit is 1.

**Force PWM Mode :** In the COMMAND register PWMSEL0 and PWMSEL1 can decide converter is always at PWM mode or enters power saving mode at light load condition. During output voltage is changed from high to low at light load, setting DVSMODE bit to 1 will make transition operate at PWM mode and output voltage will decrease quickly. If setting to 0, the output voltage will decrease depending on the loading.

**Over Current Level : RT5735 has four levels of over** current limit to be selected. Using IOC bits in the LIMCONF register can change different inductor valley current limit level.

**Thermal Shutdown Protection :** The default REARM bit in the LIMCONF register is 1. RT5735 will shut down switching operation when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 30°C the IC will resume normal operation with a complete soft-start. When REARM bit is set to 0, once the device triggers the OTP, the system will be latched and the output voltage will no longer be regulated during OTP latched state. Re-start input voltage or EN pin can unlatch the protection state. Using  $I^2C$  to shutdown the system and then re-enable it will also unlatch UVP function.

The RT5735 default  $1^2C$  slave address = 7'b0011100.  $1^2C$  interface support fast mode (bit rate up to 400kb/s). The write or read bit stream (N≥1) is shown below :



Figure 1. I<sup>2</sup>C Read and Write Stream and Timing Diagram

RT5735 can also support High-speed mode(bit rate up to 3.4Mb/s) with access code 08H. [Figure 2](#page-12-0) and [Figure](#page-13-0)  [3](#page-13-0) show detail transfer format. Hs-mode can only commence after the following conditions (all of which are in F/S-mode) :

- START condition (S)
- ▶ 8-bit master code (00001xxx)
- $\blacktriangleright$  not-acknowledge bit  $(\overline{A})$

<span id="page-12-0"></span>

Figure 2. Data Transfer Format in Hs-mode







<span id="page-13-0"></span>Figure 3. A Complete Hs-mode Transfer

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#### **Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

 $P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$ 

where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$ is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is  $125^{\circ}$ C. The junction to ambient thermal resistance,  $\theta_{\text{JA}}$ , is layout dependent. For WL-CSP-20B 1.6x2 (BSC) package, the thermal resistance,  $\theta_{JA}$ , is 55°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A = 25^{\circ}$ C can be calculated by the following formula :

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (55^{\circ}C/W) = 1.8W$  for WL-CSP-20B 1.6x2 (BSC) package

The maximum power dissipation depends on the operating ambient temperature for fixed TJ(MAX) and thermal resistance,  $\theta$ <sub>JA</sub>. The derating curve in Figure 4 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.



<span id="page-18-0"></span>Figure 4. Derating Curve of Maximum Power Dissipation

#### **Layout Considerations**

For best performance of the RT5735, the following layout guidelines must be strictly followed.

- Input capacitor must be placed as close to the IC as possible.
- ► SW should be connected to inductor by wide and short trace. Keep sensitive components away from this trace.
- $\triangleright$  Keep every trace connected to pin as wide as possible for improving thermal dissipation.



to the IC as possible. Suggest layout trace wider for thermal dissipation .

trace. Keep sensitive components away from this trace. Suggest layout trace wider for thermal dissipation .

Figure 5. PCB Layout Guide



### **Outline Dimension**





**20B WL-CSP 1.6x2 Package (BSC)** 

### **Richtek Technology Corporation**

14F, No. 8, Tai Yuen 1st Street, Chupei City Hsinchu, Taiwan, R.O.C. Tel: (8863)5526789

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