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TPS549B22 1.5-V to 18-V VIN, 4.5-V to 22-V VDD, 25-A SWIFT™ Synchronous Step-Down Converter With Full Differential Sense and PMBus™

1 Features

- Input Voltage (PV_{IN}) : 1.5 V to 18 V
- Input Bias Voltage (V_{DD}) Range: 4.5 V to 22 V
- Output Voltage Range: 0.6 V to 5.5 V
- Integrated, 4.1-mΩ and 1.9-mΩ Power MOSFETs With 25-A Continuous Output Current
- Voltage Reference 0.6 V to 1.2 V in 50-mV Steps Using VSEL Pin
- ± 0.5 %, 0.9-V_{REF} Tolerance Range: -40 °C to +125°C Junction Temperature
- True Differential Remote Sense Amplifier
- D-CAP3™ Control Loop
- Adaptive On-Time Control with 8 PMBus™ Frequencies: 315 kHz, 425 kHz, 550 kHz, 650 kHz, 825 kHz, 900 kHz, 1.025 MHz, 1.125 MHz
- Temperature Compensated and Programmable Current Limit with R_{ILIM} and OC Clamp
- Choice of Hiccup or Latch-Off OVP or UVP
- V_{DD} UVLO External Adjustment by Precision EN
- Prebias Start-up Support
- Eco-mode™ and FCCM Selectable
- Full Suite of Fault Protection and PGOOD
- Standard VOUT_COMMAND and VOUT_MARGIN (HIGH and LOW)
- Pin-Strapping and On-the-Fly Programming
- Fault Reporting and Warning
- NVM Backup for Selected Commands
- 1-MHz PMBus with PEC and SMB_ALRT#
- • Create a Custom Design Using the TPS549B22 With the WEBENCH[®] [Power Designer](https://webench.ti.com/wb5/WBTablet/PartDesigner/quickview.jsp?base_pn=TPS549B22&origin=ODS&litsection=features)

2 Applications

- Enterprise Storage, SSD, NAS
- Wireless and Wired Communication Infrastructure
- Industrial PCs, Automation, ATE, PLC, Video **Surveillance**
- Enterprise Server, Switches, Routers
- ASIC, SoC, FPGA, DSP Core and I/O Rails

3 Description

The TPS549B22 device is a compact single buck converter with adaptive on-time, D-CAP3 mode control. It is designed for high accuracy, high efficiency, fast transient response, ease-of-use, low external component count and space-conscious power systems.

This device features full differential sense and TI integrated FETs with a high-side on-resistance of 4.1 m Ω and a low-side on-resistance of 1.9 m Ω . The device also features an accurate 0.5%, 0.9-V reference with an ambient temperature range between –40°C and +125°C. Competitive features include: very low external component count, accurate load regulation and line regulation, auto-skip or FCCM mode operation, and internal soft-start control.

The TPS549B22 device is available in 7 mm \times 5 mm, 40-pin, LQFN-CLIP (RVF) package (RoHs exempt).

Device Information[\(1\)](#page-0-0)

(1) For all available packages, see the orderable addendum at the end of the data sheet.

PVIN ADDR BP AGND DRGND g 2. E
R E
E Z
R Z
R E
E PGN VSEL MODE PGN PGN PGOOD PGOOD **PGN** ILIM TPS549B22 PGN RESV_TRK Load SMB_ALRT# PGN PMB_DATA RSN PMB_CLK EN_UVLO + ± PGN RSP BOOT w٨ $\tilde{\varepsilon}$ $\tilde{\mathbf{s}}$ $\tilde{\mathbb{S}}^ \tilde{\mathbb{S}}$ $\tilde{\mathbb{S}}$ VOSNS PGND ALERT# DA₁ CLO_C ENABLE Copyright © 2016, Texas Instruments Incorporated

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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

5 Pin Configuration and Functions

Pin Functions

(1) $I = input$, $O = output$, $G = GND$

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STRUMENTS

EXAS

Pin Functions (continued)

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)(2)

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to the network ground terminal unless otherwise noted.

6.2 ESD Ratings

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *[Semiconductor and IC Package Thermal Metrics](http://www.ti.com/lit/pdf/SPRA953)* application report.

6.5 Electrical Characteristics

over operating free-air temperature range, $V_{VDD} = 12 V$, $V_{EN_UVLO} = 5 V$ (unless otherwise noted)

Electrical Characteristics (continued)

over operating free-air temperature range, $V_{VDD} = 12 V$, $V_{ENUVLO} = 5 V$ (unless otherwise noted)

(1) Specified by design. Not production tested.
(2) Correlated with close-loop EVM measureme

Correlated with close-loop EVM measurement at load current of 30 A.

Electrical Characteristics (continued)

over operating free-air temperature range, $V_{VDD} = 12 V$, $V_{EN_UVLO} = 5 V$ (unless otherwise noted)

STRUMENTS

EXAS

Electrical Characteristics (continued)

over operating free-air temperature range, $V_{VDD} = 12 V$, $V_{EN_UVLO} = 5 V$ (unless otherwise noted)

(3) In order to use the 8-ms SS setting, follow the steps outlined in *[Application Workaround to Support 4-ms and 8-ms SS Settings](#page-20-0)*.

(4) In order to use the 4-ms SS setting, follow the steps outlined in *[Application Workaround to Support 4-ms and 8-ms SS Settings](#page-20-0)*.

(5) Calculated from 20-A test data. Not production tested.

Electrical Characteristics (continued)

over operating free-air temperature range, $V_{VDD} = 12 V$, $V_{EN_UVLO} = 5 V$ (unless otherwise noted)

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6.6 Typical Characteristics

Typical Characteristics (continued)

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Typical Characteristics (continued)

Typical Characteristics (continued)

7.1 Overview

TPS549B22 device is a high-efficiency, single-channel, FET-integrated, synchronous buck converter. It is suitable for point-of-load applications with 25 A or lower output current in storage, telecom and similar digital applications. The device features proprietary D-CAP3 mode control combined with adaptive on-time architecture. This combination is ideal for building modern high/low duty ratio, ultra-fast load step response DC-DC converters.

TPS549B22 device has integrated MOSFETs rated at 25-A TDC.

The converter input voltage range is from 1.5 V up to 18 V, and the V_{DD} input voltage range is from 4.5 V to 22 V. The output voltage ranges from 0.6 V to 5.5 V.

Stable operation with all ceramic output capacitors is supported as the D-CAP3 mode uses emulated current information to control the modulation. An advantage of this control scheme is that it does not require phase compensation network outside which makes it easy to use and also enables low external component count. . Adaptive on-time control tracks the preset switching frequency over a wide range of input and output voltage while increasing switching frequency as needed during load step transient.

The default preset switching frequency for this device is 650 kHz. Switching frequency is also programmable from 8 preset values via PMBus interface. supports digital communication via PMBus using standard interfacing pins, PMB_CLK, PMB_DATA and SMB_ALRT#. The detailed PMBus features, capabilities and command sets of the TPS549B22 can be found in *[PMBus Programming](#page-18-1)*.

7.2 Functional Block Diagram

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7.3 Feature Description

7.3.1 25-A FET

The TPS549B22 device is a high-performance, integrated FET converter supporting current rating up to 25 A thermally. It integrates two N-channel NexFET™ power MOSFETs, enabling high power density and small PCB layout area. The drain-to-source breakdown voltage for these FETs is 25-V DC and 27-V transient for 10 ns. Avalanche breakdown occurs if the absolute maximum voltage rating exceeds 27 V. In order to limit the switch node ringing of the device, TI recommends adding an R-C snubber from the SW node to the PGND pins. Refer to *[Layout Guidelines](#page-53-2)* for the detailed recommendations.

7.3.2 On-Resistance

The typical on-resistance ($R_{DS(on)}$) for the high-side MOSFET is 4.1 mΩ, and typical on-resistance for the lowside MOSFET is 1.9 mΩ with a nominal gate voltage (V_{GS}) of 5 V.

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Feature Description (continued)

7.3.3 Package Size, Efficiency and Thermal Performance

The TPS549B22 device is available in a 7 mm \times 5 mm QFN package with 40 power and I/O pins. The device employs TI proprietary MCM packaging technology with thermal pad. With a properly designed system layout, applications achieve optimized safe operating area (SOA) performance. The curves shown in [Figure 23](#page-15-0) and [Figure 24](#page-15-0) are based on the orderable evaluation module design. (See www.ti.com to order the EVM.)

7.3.4 Soft-Start Operation

In the TPS549B22 device the soft-start time controls the inrush current required to charge the output capacitor bank during start-up. The device offers selectable soft-start options of 1 ms, 2 ms, 4 ms and 8 ms. When the device is enabled (either by EN or V_{DD} UVLO), the reference voltage ramps from 0 V to the final level defined by VSEL pin-strap configuration, in a given soft-start time. The TPS549B22 device supports several soft-start times between 1 ms and 8 ms selected by MODE pin configuration. Refer to MODE definition table for details.

7.3.5 V_{DD} Supply Undervoltage Lockout (UVLO) Protection

The TPS549B22 device provides fixed V_{DD} undervoltage lockout threshold and hysteresis. The typical V_{DD} turnon threshold is 4.25 V, and hysteresis is 0.2 V. The V_{DD} UVLO can be used in conjunction with the EN_UVLO signal to provide proper power sequence to the converter design. UVLO is a non-latched protection.

7.3.6 EN_UVLO Pin Functionality

The EN UVLO pin drives an input buffer with accurate threshold and can be used to program the exact required turnon and turnoff thresholds for switcher enable, V_{DD} UVLO or VIN UVLO (if VIN and VDD are tied together). If desired, an external resistor divider can be used to set and program the turnon threshold for V_{DD} or VIN UVLO.

[Figure 25](#page-16-0) shows how to program the input voltage UVLO using the EN_UVLO pin.

Feature Description (continued)

Figure 25. Programming the UVLO Voltage

7.3.7 Fault Protections

This section describes positive and negative overcurrent limits, overvoltage protections, out-of-bounds limits, undervoltage protections, and overtemperature protections.

7.3.7.1 Current Limit (ILIM) Functionality

Figure 26. Current Limit Resistance vs OCP Valley Overcurrent Limit

The ILIM pin sets the OCP level. Connect the ILIM pin to GND through the voltage setting resistor, $R_{I L M}$. In order to provide both good accuracy and a cost-effective solution, the TPS549B22 device supports temperature compensated internal MOSFET $R_{DS(on)}$ sensing.

Feature Description (continued)

Also, the TPS549B22 device performs both positive and negative inductor current limiting with the same magnitudes. The positive current limit normally protects the inductor from saturation that causes damage to the high-side FET and low-side FET. The negative current limit protects the low-side FET during OVP discharge.

The voltage between GND pin and SW pin during the OFF time monitors the inductor current. The current limit has 1200 ppm/ \textdegree C temperature slope to compensate the temperature dependency of the on-resistance (R_{DS(on)}). The GND pin is used as the positive current sensing node.

The TPS549B22 device uses cycle-by-cycle over-current limiting control. The inductor current is monitored during the *OFF*-state and the controller maintains the OFF-state during the period that the inductor current is larger than the overcurrent I_{LIM} level. V_{ILIM} sets the valley level of the inductor current.

7.3.7.2 VDD Undervoltage Lockout (UVLO)

The TPS549B22 device has an UVLO protection function for the V_{DD} supply input. The on-threshold voltage is 4.25 V with 200 mV of hysteresis. During a UVLO condition, the device is disabled regardless of the EN_UVLO pin voltage. The supply voltage (V_{VDD}) must be above the on-threshold to begin the pin strap detection.

7.3.7.3 Overvoltage Protection (OVP) and Undervoltage Protection (UVP)

The device monitors a feedback voltage to detect overvoltage and undervoltage. When the feedback voltage becomes lower than 68% of the target voltage, the UVP comparator output goes high and an internal UVP delay counter begins counting. After 1 ms, the device latches OFF both high-side and low-side MOSFETs drivers. The UVP function enables after soft-start is complete.

When the feedback voltage becomes higher than 120% of the target voltage, the OVP comparator output goes high and the circuit latches OFF the high-side MOSFET driver and turns on the low-side MOSFET until reaching a negative current limit. Upon reaching the negative current limit, the low-side FET is turned off and the high-side FET is turned on again for a minimum on-time. The TPS549B22 device operates in this cycle until the output voltage is pulled down under the UVP threshold voltage for 1 ms. The fault is cleared with a reset of VDD or by retoggling the EN pin.

Table 1. Overvoltage Protection Details

7.3.7.4 Out-of-Bounds Operation

The device has an out-of-bounds (OOB) overvoltage protection that protects the output load at a much lower overvoltage threshold of 8% above the target voltage. OOB protection does not trigger an overvoltage fault, so the device is not latched off after an OOB event. OOB protection operates as an early no-fault overvoltageprotection mechanism. During the OOB operation, the controller operates in forced PWM mode only by turning on the low-side FET. Turning on the low-side FET beyond the zero inductor current quickly discharges the output capacitor thus causing the output voltage to fall quickly toward the setpoint. During the operation, the cycle-bycycle negative current limit is also activated to ensure the safe operation of the internal FETs.

7.3.7.5 Overtemperature Protection

TPS549B22 device has overtemperature protection (OTP) by monitoring the die temperature. If the temperature exceeds the threshold value (default value 165°C), TPS549B22 device is shut off. When the temperature falls about 25°C below the threshold value, the device turns on again. The OTP is a non-latch protection.

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ramp amplitude. The device uses an improved DCAP3 control loop architecture that incorporates a steady-state error integrator. The slow integrator improves the output voltage DC accuracy greatly and presents minimal impact to small signal transient response. To further enhance the small signal stability of the control loop, the device uses a modified ramp generator that supports a wider range of output LC stage.

7.4.2 DCAP Control Topology

For advanced users of this device, the internal DCAP3 ramp can be disabled using the MODE[4] pin-strap bit. This situation requires an external RCC network to ensure control loop stability. Place this RCC network across the output inductor. Use a range between 10 mV and 15 mV of injected RSP pin ripple. If no feedback resistor divider network is used, insert a 10-k Ω resistor between the VOUT pin and the RSP pin.

7.5 Programming

7.5.1 Programmable Pin-Strap Settings

ADDR, VSEL and MODE. Description: a 1% or better 100-kΩ resistor is needed from BP to each of the three pins. The bottom resistor from each pin to ground (see **MODE, VSEL, ADDR DETECTION** section of the *[Electrical Characteristics](#page-4-2)* table) in conjunction with the top resistor defines each pin strap selection. The pin detection checks for external resistor divider ratio during initial power up (VDD is brought down below approximately 3 V) when BP LDO output is at approximately 2.9 V.

7.5.1.1 Address Selection (ADDR) Pin

The TPS549B22 allows up to 16 different chip addresses for PMBus communication with the first 3 bits fixed as 001. The address selection process is defined by resistor divider ratio from BP pin to ADDR pin, and the address detection circuit starts to work only after the initial power up when V_{DD} has risen above its UVLO threshold. [Table 4](#page-24-0) lists all combinations of the address selections. The 1% or better tolerance resistors with typical temperature coefficient of ±100ppm/°C are recommended.

ADDR pin-strap configuration also programs the light load conduction mode.

7.5.1.2 VSEL Pin

VSEL pin strap configuration is used to program initial boot voltage value, hiccup mode and latch off mode. The initial boot voltage is used to program the main loop voltage reference point. VSEL voltage settings provide TI designated discrete internal reference voltages. [Table 2](#page-19-0) lists internal reference voltage selections.

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Table 2. Internal Reference Voltage Selections

(1) 1% or better and connect to ground

7.5.1.3 DCAP3 Control and Mode Selection

The MODE pinstrap configuration programs the control topology and internal soft-start timing selections. The TPS549B22 device supports both DCAP3 and DCAP operation

MODE[4] selection bit is used to set the control topology. If MODE[4] bit is 0, it selects DCAP operation. If MODE[4] bit is 1, it selects DCAP3 operation.

MODE[1] and MODE[0] selection bits are used to set the internal soft-start timing.

MODE[4]	MODE[3]	MODE[2]	MODE[1]	MODE[0]	R_{MODE} (kΩ) ⁽¹⁾	
1: DCAP3	0: Internal Reference	0: Internal SS	11: 8 ms ⁽²⁾		60.4	
			10: 4 ms ⁽²⁾		53.6	
			$01:2 \text{ ms}$		47.5	
			$00:1 \text{ ms}$		42.2	
0:DCAP	0: Internal Reference	0: Internal SS	11: 8 ms ⁽²⁾		4.64	
			10: 4 ms ⁽²⁾		3.16	
			$01:2 \text{ ms}$		1.78	
			$00:1 \text{ ms}$		0	

Table 3. Allowable MODE Pin Selections

(1) 1% or better and connect to ground

(2) See *[Application Workaround to Support 4-ms and 8-ms SS Settings](#page-20-0)*.

7.5.1.4 Application Workaround to Support 4-ms and 8-ms SS Settings

In order to properly design for 4-ms and 8-ms SS settings, additional application consideration is needed. The recommended application workaround to support the 4-ms and 8-ms soft-start settings is to ensure sufficient time delay between the V_{DD} and EN_UVLO signals. The minimum delay between the rising maximum V_{DD} UVLO level and the minimum turn on threshold of EN UVLO is at least T_{DELAY} _{MIN}.

 T_{DELAY} MIN $=$ K \times V_{REF}

where

- $K = 9$ ms/V for SS setting of 4 ms
- $K = 18$ ms/V for SS setting of 8 ms
- V_{REF} is the internal reference voltage programmed by VSEL pin strap (1) (1)

For example, if SS setting is 4 ms and V_{REF} = 1 V, program the minimum delay at least 9 ms; if SS setting is 8 ms, the minimum delay should be programmed at least 18 ms. See [Figure 27](#page-20-1) and [Figure 28](#page-21-0) for detailed timing requirement. Because TPS549B22 is a PMBus device, the end user has the option of programming power-on delay (POD) as another workaround. Be sure to follow the same calculation to determine the needed POD (see *[MFR_SPECIFIC_01 \(address = D1h\)](#page-35-0)* and [Table 25](#page-35-1) for detailed information).

Figure 27. Proper Sequencing of V_{DD} and EN_UVLO to Support the use of 4-ms SS Setting

Figure 28. Minimum Delay Between V_{DD} and EN_UVLO to Support the use of 4-ms and 8-ms SS settings

The workaround/consideration described previously is not required for SS settings of 1 ms and 2 ms.

7.5.2 Programmable Analog Configurations

7.5.2.1 RSP/RSN Remote Sensing Functionality

RSP and RSN pins are used for remote sensing purpose. In the case where feedback resistors are required for output voltage programming, connect the RSP pin to the mid-point of the resistor divider, and connect the RSN pin to the load return. In the case where feedback resistors are not required as when the VSEL programs the output-voltage setpoint, connect the RSP pin to the positive sensing point of the load, and the RSN pin must always be connected to the load return.

RSP and RSN pins are extremely high-impedance input terminals of the true differential remote sense amplifier. The feedback resistor divider must use resistor values much less than 100 k Ω .

7.5.2.1.1 Output Differential Remote Sensing Amplifier

The examples in this section show simplified remote sensing circuitry where each example uses an internal reference of 1 V. [Figure 29](#page-21-1) shows remote sensing without feedback resistors, with an output voltage setpoint of 1 V. [Figure 30](#page-21-1) shows remote sensing using feedback resistors, with an output voltage setpoint of 5 V.

Figure 29. Remote Sensing Without Feedback Resistors

Figure 30. Remote Sensing With Feedback Resistors

7.5.2.2 Power Good (PGOOD Pin) Functionality

The TPS549B22 device has power-good output that registers high when switcher output is within the target. The power-good function is activated after soft start has finished. When the soft-start ramp reaches 300 mV above the internal reference voltage, SS end signal goes high to enable the PGOOD detection function. If the output voltage becomes within ±8% of the target value, internal comparators detect power-good state and the powergood signal becomes high after a 1-ms programmable delay. If the output voltage goes outside of ±16% of the target value, the power-good signal becomes low after two microsecond (2-µs) internal delay. The open-drain power-good output must be pulled up externally. The internal N-channel MOSFET does not pull down until the V_{DD} supply is above 1.2 V.

7.5.3 PMBus Programming

TPS549B22 has seven internal custom user-accessible 8-bit registers. The PMBus interface has been designed for program flexibility, supporting direct format for write operation. Read operations are supported for both combined format and stop separated format. While there is no auto increment/decrement capability in the TPS549B22 PMBus logic, a tight software loop can be designed to randomly access the next register independent of which register was accessed first. The start and stop commands frame the data packet and the repeat start condition is allowed when necessary.

7.5.3.1 TPS549B22 Limitations to the PMBUS Specifications

TPS549B22 only recognizes seven bit addressing. This means TPS549B22 is not compatible with ten bit addressing and CBUS communication. The device can operate in standard mode (100 kbit/s), fast mode (400 kbit/s) or faster mode (1000 kbit/s).

7.5.3.2 Slave Address Assignment

The seven bit slave address is 001A₃A₂A₁A₀x, where A₃A₂A₁A₀ is set by the ADDR pin on the device. Bit 0 is the data direction bit, i.e. 001A₃A₂A₁A₀0 is used for write operation and 001A₃A₂A₁A₀1 is used for read operation.

7.5.3.3 PMBUS Address Selection

TPS549B22 allows up to 16 different chip addresses for PMBus communication, with the first three bits fixed as 001. The address selection process is defined by the resistor divider ratio from BP pin to ADDR pin, and the address detection circuit will start to work only after V_{DD} input supply has risen above its UVLO threshold. [Table 4](#page-24-0) lists the divider ratio and some example resistor values. The 1% tolerance resistors with typical temperature coefficient of ±100 ppm/ºC are recommended. Higher performance resistors can be used if tighter noise margin is required for more reliable address detection.

7.5.3.4 Supported Formats

The supported formats are described in the following subsections.

7.5.3.4.1 Direct Format — Write

The simplest format for a PMBus write is direct format. After the start condition [S], the slave chip address is sent, followed by an eighth bit indicating a write. TPS549B22 then acknowledges that it is being addressed, and the master responds with an 8 bit register address byte. The slave acknowledges and the master sends the appropriate 8-bit data byte. Once again the slave acknowledges and the master terminates the transfer with the stop condition [P].

7.5.3.4.2 Combined Format — Read

After the start condition [S], the slave chip address is sent, followed by an eighth bit indicating a write. TPS549B22 then acknowledges that it is being addressed, and the master responds with an 8-bit register address byte. The slave acknowledges and the master sends the repeated start condition [Sr]. Once again, the slave chip address is sent, followed by an eighth bit indicating a read. The slave responds with an acknowledge followed by previously addressed 8-bit data byte. The master then sends a non-acknowledge (NACK) and finally terminates the transfer with the stop condition [P].

7.5.3.5 Stop Separated Reads

Stop-separated reads can also be used. This format allows a master to set up the register address pointer for a read and return to that slave at a later time to read the data. In this format the slave chip address followed by a write bit are sent after a start [S] condition. TPS549B22 then acknowledges it is being addressed, and the master responds with the 8-bit register address byte. The master then sends a stop or restart condition and may then address another slave. After performing other tasks, the master can send a start or restart condition to the TPS549B22 with a read command. The device acknowledges this request and returns the data from the register location that had been set up previously.

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Table 4. ADDR Pin Selection Table

7.5.3.6 Supported PMBUS Commands and Registers

Only the following PMBus commands are supported by TPS549B22, and not all parts of each command are supported.

Table 5. PMBUS Command and Register Table

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CMD CODE COMMAND NAME DESCRIPTION NWM? TYPE **BIT PATTERN**
BYTES 7Eh STATUS_CML STATUS of communications, logic no Read Byte 1 XXX0 0000 0XX0 0000 = A valid or supported command has been received 1XX0 0000 = An invalid or unsupported command has been received X0X0 0000 = A valid or supported data has been received X1X0 0000 = An invalid or unsupported data has been received XX00 0000 = Packet error check has failed XX10 0000 = Packet error check has succeeded D0h | MFR_SPECIFIC_00 Customer programmable byte that does not affect chip functionality yes R/W Byte 1 Free format D1h MFR_SPECIFIC_01 Program PGOOD delay and Power-On delay delay and the set of the NW Byte 1 Provence 1 D2h MFR_SPECIFIC_02 Read SST, CM, HICLOFF, TRK and SEQ. Program Forced SKIP Soft Start. yes | R/W Byte | 1 D3h MFR_SPECIFIC_03 Program Fsw and control yes R/W Byte 1 D4h MFR_SPECIFIC_04 Program the DCAP3 offset yes R/W Byte 1 D6h MFR_SPECIFIC_06 Program the V_{DD} UVLO level yes R/W Byte 1 D7h | MFR_SPECIFIC_07 Program the final tracking set point and select .
pseudo/external tracking yes R/W Byte 1 FCh MFR_SPECIFIC_44 Read TI PMBUS GUI Devcie ID Head IT PMBUS GUI Device ID no Read Word 2
and IC revision code

Table 6. Status Word Summary Table

Table 7. Status V_{OUT} Summary Table

Table 8. Status IOUT Summary Table

EXAS ISTRUMENTS

7.6 Register Maps

7.6.1 OPERATION Register (address = 1h)

Figure 32. OPERATION

RLEGEND: $R/W = Read/Write$; $R = Read$ only; -n = value after reset

Table 9. OPERATION

7.6.2 ON_OFF_CONFIG Register (address = 2h)

Figure 33. ON_OFF_CONFIG

LEGEND: $R/W = Read/Write$; $R = Read$ only; $-n = value$ after reset

Table 10. ON_OFF_CONFIG

7.6.3 CLEAR FAULTS (address = 3h)

The CLEAR_FAULTS command is used to clear any fault bits that have been set. This command simultaneously clears all bits in all status registers. At the same time, the device clears its SMB_ALERT# signal output if the device is asserting the SMB_ALERT# signal.

The CLEAR_FAULTS command does not cause a unit that has latched off for a fault condition to restart. If the fault is still present when the bit is cleared, the fault bit shall immediately be set again and the host notified by the usual means.

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7.6.4 WRITE PROTECT (address = 10h)

Figure 34. WRITE PROTECT

LEGEND: $R/W = Read/Write$; $R = Read$ only; -n = value after reset

Table 11. WRITE PROTECT

7.6.5 STORE_DEFAULT_ALL (address = 11h)

Store all of the current storable register settings in the EEPROM memory as the new defaults on power up.

It is permitted to use the STORE_DEFAULT_ALL command while the device is operating. However, the device may be unresponsive during the write operation with unpredictable memory storage results. TI recommends to turn the device output off before issuing this command.

EEPROM programming faults will set the 'CML' bit in the STATUS_BYTE and the 'MEM' bit in the STATUS_CML registers.

7.6.6 RESTORE_DEFAULT_ALL (address = 12h)

Write EEPROM data to those CSRs that: (1) have EEPROM support, and; (2) are unprotected according to current setting of WRITE_PROTECT.

It is permitted to use the RESTORE_DEFAULT_ALL command while the device is operating. However, the device may be unresponsive during the copy operation with unpredictable, undesirable or even catastrophic results. TI recommends turning the device output off before issuing this command.

No data bytes are sent, just the command code is sent.

7.6.7 CAPABILITY (address = 19h)

This command provides a way for a host system to determine some key capabilities of this PMBus device.

Figure 35. CAPABILITY

LEGEND: $R/W = Read/Write$; $R = Read$ only; -n = value after reset

Table 12. CAPABILITY

7.6.8 VOUT_MODE (address = 20h)

Figure 36. VOUT_MODE

LEGEND: $R/W = Read/Write$; $R = Read$ only; -n = value after reset

Table 13. VOUT_MODE

7.6.9 VOUT_COMMAND (address = 21h)

The VOUT COMMAND command sets the output voltage in volts. The exponent is set be VOUT MODE at –9 (equivalent of 1.9531 mV/LSB). The programmed V_{OUT} is computed as:

 V_{OUT} = VOUT_COMMAND × VOUT_MODE volts = VOUT_COMMAND × 2^{-9} V (2)

The support range for TPS549B22 is: 0.5996 V to 1.1992 V. It is effectively 9 bits limited to 307 to 614 decimal. Slew-rate control is provided through MODE pin.

 V_{OUT} changes 1 step per t_{slew}, where t_{slew} is programmable by MODE pin: 4, 8, 16, or 32 µs.

Figure 37. VOUT_COMMAND

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 14. VOUT_COMMAND

7.6.10 VOUT_MARGIN_HIGH (address = 25h) ®

The VOUT_MARGIN_HIGH command loads the TPS549B22 with the voltage to which the output is to be changed when the OPERATION command is set to "Margin High".

The data bytes are two bytes formatted according to the setting of the VOUT_MODE command.

The support margin range for TPS549B22 is: 0.5996 V to 1.1992 V. It is effectively 9 bits limited to 307 to 614 decimal. Slew-rate control is provided through MODE pin.

Figure 38. VOUT_MARGIN_HIGH

LEGEND: $R/W = Read/Write$; $R = Read$ only; $-n = value$ after reset

Table 15. VOUT_MARGIN_HIGH

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7.6.11 VOUT_MARGIN_LOW (address = 26h)

The VOUT_MARGIN_LOW command loads the TPS549B22 with the voltage to which the output is to be changed when the OPERATION command is set to "Margin Low".

The data bytes are two bytes formatted according to the setting of the VOUT_MODE command.

The support margin range for TPS549B22 is: 0.5996 V to 1.1992 V. It is effectively 9-bits limited to 307 to 614 decimal. Slew-rate control is provided through MODE pin.

Figure 39. VOUT_MARGIN_LOW:

LEGEND: $R/W = Read/Write$; $R = Read$ only; -n = value after reset

Table 16. VOUT_MARGIN_LOW:

7.6.12 STATUS_BYTE (address = 78h)

Figure 40. STATUS_BYTE

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 17. STATUS_BYTE

7.6.13 STATUS_WORD (High Byte) (address = 79h)

Figure 41. STATUS_WORD (High Byte)

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 18. STATUS_WORD (High Byte)

7.6.14 STATUS_VOUT (address = 7Ah)

Figure 42. STATUS_VOUT

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 19. STATUS_VOUT

7.6.15 STATUS_IOUT (address = 7Bh)

Figure 43. STATUS_IOUT

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 20. STATUS_IOUT

7.6.16 STATUS_CML (address = 7Eh)

Figure 44. STATUS_CML

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 21. STATUS_CML

7.6.17 MFR_SPECIFIC_00 (address = D0h)

Figure 45. MFR_SPECIFIC_00

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 22. MFR_SPECIFIC_00

EXAS STRUMENTS

7.6.18 MFR_SPECIFIC_01 (address = D1h)

Figure 46. MFR_SPECIFIC_01

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 23. MFR_SPECIFIC_01

Table 24. PGD[2:0]

Table 25. POD[2:0]

7.6.19 MFR_SPECIFIC_02 (address = D2h)

The MFR_SPECIFIC_02 register allows the user to read the configuration of various pin-strap features and/or overwrite them. Note that any overwritten values here are only good until the next power-on-reset, when all parameters revert back to their pin-strap configurations.

Figure 47. MFR_SPECIFIC_02

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 26. MFR_SPECIFIC_02

Table 27. SST

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7.6.20 MFR_SPECIFIC_03 (address = D3h)

The MFR_SPECIFIC_03 register allows the user to read the configuration of the DCAP pin-strap feature (and/or overwrite it), as well configure the Ramp Generator and the PWM switching frequency.

Figure 48. MFR_SPECIFIC_03

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 28. MFR_SPECIFIC_03 Field Descriptions

Table 29. RCSP

Table 30. FS

7.6.21 MFR_SPECIFIC_04 (address = D4h)

The MFR_SPECIFIC_04 register allows the user to configure the D-CAP offset reduction and fixed offset correction.

Figure 49. MFR_SPECIFIC_04

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 31. MFR_SPECIFIC_04

Table 32. DCAP3OFFSET

FXAS ISTRUMENTS

7.6.22 MFR_SPECIFIC_06 (address = D6h)

The MFR_SPECIFIC_06 is a user-accessible register dedicated for configuring the V_{DD} UVLO threshold.

Figure 50. MFR_SPECIFIC_06

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 33. MFR_SPECIFIC_06

Table 34. VDDUVLO

7.6.23 MFR_SPECIFIC_07 (address = D7h)

The MFR_SPECIFIC_07 is a user-accessible register dedicated for configuring the device's PGOOD threshold and external tracking options.

Figure 51. MFR_SPECIFIC_07

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 35. MFR_SPECIFIC_07

Table 36. VTRKIN

EXAS ISTRUMENTS

7.6.24 MFR_SPECIFIC_44 (address = FCh)

The DEVICE_CODE command returns a 12-bit unique identifier code for the device and a 4 bit device revision code.

Figure 52. MFR_SPECIFIC_44

LEGEND: R/W = Read/Write; R = Read only; -n = value after reset

Table 37. MFR_SPECIFIC_44

Can

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The TPS549B22 device is a highly-integrated synchronous step-down DC-DC converter with PMBus features and capabilities. This devices is used to convert a higher DC input voltage to a lower DC output voltage, with a maximum output current of 25 A. Use the following design procedure to select key component values for this family of devices.

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8.2 Typical Applications

8.2.1 TPS549B22 1.5-V to 18-V Input, 1-V Output, 25-A Converter

Figure 53. Typical Application Schematic

8.2.2 Design Requirements

For this design example, use the input parameters shown in [Table 38.](#page-44-0)

Table 38. Design Example Specifications

8.2.3 Detailed Design Procedure

8.2.3.1 Custom Design With WEBENCH® Tools

[Click here](https://webench.ti.com/wb5/WBTablet/PartDesigner/quickview.jsp?base_pn=TPS549B22&origin=ODS&litsection=application) to create a custom design using the TPS549B22 device with the WEBENCH® Power Designer.

- 1. Start by entering the input voltage (V_{IN}) , output voltage (V_{OUT}) , and output current (I_{OUT}) requirements.
- 2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
- 3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at [www.ti.com/WEBENCH.](http://www.ti.com/lsds/ti/analog/webench/overview.page?DCMP=sva_web_webdesigncntr_en&HQS=sva-web-webdesigncntr-vanity-lp-en)

8.2.3.2 Switching Frequency Selection

The default switching frequency of the TPS549B22 device is 650 kHz. There are a total of 8 switching frequency settings that can be programmed via PMBus interface. For each switching frequency setting, there are 4 internal ramp compensations (DCAP3) to choose from, also via PMBus. When DCAP3 mode is selected (preferred), the internal ramp compensation is used for stabilizing the converter design. The ramp is a function of the switching frequency and duty cycle range (the output voltage to input voltage ratio). [Table 39](#page-45-0) summarizes the ramp choices using these functions.

Table 39. Switching Frequency Selection

8.2.3.3 Inductor Selection

To calculate the value of the output inductor, use [Equation 3](#page-45-1). The coefficient K_{IND} represents the amount of inductor ripple current relative to the maximum output current. The output capacitor filters the inductor ripple current. Therefore, choosing a high inductor ripple current impacts the selection of the output capacitor since the output capacitor must have a ripple current rating equal to or greater than the inductor ripple current. In general, maintain a K_{IND} coefficient between 0 and 40 for balanced performance. Using this target ripple current, the required inductor size can be calculated as shown in [Equation 3](#page-45-1)

$$
L1 = \frac{V_{OUT}}{\left(V_{IN(max)} \times f_{SW}\right)} \times \frac{V_{IN} - V_{OUT}}{\left(I_{OUT(max)} \times K_{IND}\right)} = \frac{1 \times (18 \text{ V} - 1 \text{ V})}{(18 \text{ V} \times 650 \text{ kHz} \times 25 \text{ A} \times 0.2)} = 0.29 \text{ }\mu\text{H}
$$
\n(3)

Selecting a K_{IND} of 0.2, the target inductance L₁ = 290 nH. Using the next standard value, the 330 nH is chosen in this application for its high current rating, low DCR, and small size. The inductor ripple current, RMS current, and peak current can be calculated using [Equation 4](#page-45-2), [Equation 5](#page-45-3) and [Equation 6.](#page-45-4) Use these values to select an inductor with approximately the target inductance value, and current ratings that allow normal operation with some margin.

$$
I_{RIPPLE} = \frac{V_{OUT}}{(V_{IN(max)} \times f_{SW})} \times \frac{V_{IN(max)} - V_{OUT}}{L1} = \frac{1 V \times (18 V - 1 V)}{18 V \times 650 kHz \times 330 nH} = 4.4 A
$$
\n
$$
I_{L(rms)} = \sqrt{(I_{OUT})^2 + \frac{1}{12} \times (I_{RIPPLE})^2} = 25 A
$$
\n(4)

$$
T(\text{rms}) = \sqrt{(2017)^{4} 12^{24} (RIPPEF)} = 25.1
$$
 (5)

$$
I_{L(peak)} = (I_{OUT}) + \frac{1}{2} \times (I_{RIPPLE}) = 27.2 \text{ A}
$$
 (6)

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8.2.3.4 Output Capacitor Selection

There are three primary considerations for selecting the value of the output capacitor. The output capacitor affects three criteria:

- **Stability**
- Regulator response to a change in load current or load transient
- Output voltage ripple

These three considerations are important when designing regulators that must operate where the electrical conditions are unpredictable. The output capacitance needs to be selected based on the most stringent of these three criteria.

8.2.3.4.1 Minimum Output Capacitance to Ensure Stability

To prevent sub-harmonic multiple pulsing behavior, TPS549B22 application designs must strictly follow the small signal stability considerations described in [Equation 7](#page-46-0).

$$
C_{OUT(min)} > \frac{t_{ON}}{2} \times \frac{8\tau}{L_{OUT}} \times \frac{V_{REF}}{V_{OUT}}
$$

where

- $C_{\text{OUT}(min)}$ is the minimum output capacitance needed to meet the stability requirement of the design
- t_{ON} is the on-time information based on the switching frequency and duty cycle (in this design, 128 ns)
- τ is the ramp compensation time constant of the design based on the switching frequency and duty cycle, (in this design, 25.9 µs, refer to [Table 39](#page-45-0))
- L_{OUT} is the output inductance (in the design, 0.33μ H)
- V_{REF} is the user-selected reference voltage level (in this design, 1 V)
- V_{OUT} is the output voltage (in this design, 1 V) (7) (7)

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The minimum output capacitance calculated from [Equation 7](#page-46-0) is 40 μ F. The stability is ensured when the amount of the output capacitance is 40 µF or greater. And when all MLCCs (multi-layer ceramic capacitors) are used, both DC- and AC-derating effects must be considered to ensure that the minimum output capacitance requirement is met with sufficient margin.

8.2.3.4.2 Response to a Load Transient

The output capacitance must supply the load with the required current when current is not immediately provided by the regulator. When the output capacitor supplies load current, the impedance of the capacitor greatly affects the magnitude of voltage deviation (such as undershoot and overshoot) during the transient.

Use [Equation 8](#page-46-1) and [Equation 9](#page-47-0) to estimate the amount of capacitance needed for a given dynamic load step and release.

NOTE

There are other factors that can impact the amount of output capacitance for a specific design, such as ripple and stability.

$$
C_{OUT(min_under)} = \frac{L_{OUT} \times (\Delta l_{LOAD(max)})^2 \times \left(\frac{V_{OUT} \times t_{SW}}{V_{IN(min)}} + t_{OFF(min)}\right)}{2 \times \Delta V_{LOAD(inset)}} \times \left(\left(\frac{V_{IN(min)} - V_{OUT}}{V_{IN(min)}}\right) \times t_{SW} - t_{OFF(min)}\right) \times V_{OUT}
$$
\n(8)

$$
C_{OUT(min_over)} = \frac{L_{OUT} \times \left(\Delta I_{LOAD(max)}\right)^2}{2 \times \Delta V_{LOAD(release)} \times V_{OUT}}
$$

where

- $C_{\text{OUT(min under)}}$ is the minimum output capacitance to meet the undershoot requirement
- $C_{\text{OUT/min}}$ _{oven} is the minimum output capacitance to meet the overshoot requirement
- L is the output inductance value $(0.33 \mu H)$
- $\Delta I_{\text{LOAD(max)}}$ is the maximum transient step (15 A)
- V_{OUT} is the output voltage value (1 V)
- t_{SW} is the switching period (1.54 μ s)
- $V_{IN(min)}$ is the minimum input voltage for the design (10.8 V)
- $t_{\text{OFF(min)}}$ is the minimum off time of the device (300 ns)
- ∆V_{LOAD(insert)} is the undershoot requirement (30 mV)
- $\Delta V_{\text{LOAD(release)}}$ is the overshoot requirement (30 mV) (9)

Most of the above parameters can be found in [Table 38.](#page-44-0)

The minimum output capacitance to meet the undershoot requirement is 516 μ F. The minimum output capacitance to meet the overshoot requirement is 1238 µF. This example uses a combination of POSCAP and MLCC capacitors to meet the overshoot requirement.

POSCAP bank 1: 2 x 470 μ F, 2.5 V, 6 m Ω per capacitor

I

MLCC bank 2: 7 \times 100 μF, 2.5 V, 1 mΩ per capacitor with DC+AC derating factor of 60%

Recalculating the worst case overshoot using the described capacitor bank design, the overshoot is 29.0 mV which meets the 30-mV overshoot specification requirement.

8.2.3.4.3 Output Voltage Ripple

The output voltage ripple is another important design consideration. [Equation 10](#page-47-1) calculates the minimum output capacitance required to meet the output voltage ripple specification. This criterion is the requirement when the impedance of the output capacitance is dominated by ESR.

$$
C_{OUT(min)RIPPLE} = \frac{I_{RIPPLE}}{8 \times f_{SW} \times V_{OUT(ripple)}} = 82 \,\mu\text{F}
$$
\n(10)

In this case, the maximum output voltage ripple is 10 mV. For this requirement, the minimum capacitance for ripple requirement yields 82 µF. Because this capacitance value is significantly lower compared to that of transient requirement, determine the capacitance bank from steps in the previous section *[Response to a Load](#page-46-2) [Transient](#page-46-2)*. Because the output capacitor bank consists of both POSCAP and MLCC type capacitors, it is important to consider the ripple effect at the switching frequency due to effective ESR. Use [Equation 11](#page-47-2) to determine the maximum ESR of the output capacitor bank for the switching frequency.

$$
ESR_{MAX} = \frac{V_{OUT(iapple)} - \frac{IRIPPLE}{8 \times f_{SW} \times C_{OUT}}}{I_{RIPPLE}} = 2.2 \text{ m}\Omega
$$
\n(11)

Estimate the effective ESR at the switching frequency by obtaining the impedance vs frequency characteristics of the output capacitors. The parallel impedance of capacitor bank 1 and capacitor bank 2 at the switching frequency of the design example is estimated to be 1.2 m Ω , which is less than that of the maximum ESR value. Therefore, the output voltage ripple requirement (10 mV) can be met. For detailed calculation on the effective ESR please contact the factory to obtain a user-friendly Excel based design tool.

8.2.3.5 Input Capacitor Selection

The TPS549B22 devices require a high-quality, ceramic, type X5R or X7R, input decoupling capacitor with a value of at least 1 μ F of effective capacitance on the VDD pin, relative to AGND. The power stage input decoupling capacitance (effective capacitance at the PVIN and PGND pins) must be sufficient to supply the high switching currents demanded when the high-side MOSFET switches on, while providing minimal input voltage ripple as a result. This effective capacitance includes any DC bias effects. The voltage rating of the input capacitor must be greater than the maximum input voltage. The capacitor must also have a ripple current rating greater than the maximum input current ripple to the device during full load. The input ripple current can be calculated using [Equation 12](#page-48-0).

$$
I_{CIN(rms)} = I_{OUT(max)} \times \sqrt{\frac{V_{OUT}}{V_{IN(min)}} \times \frac{\left(V_{IN(min)} - V_{OUT}\right)}{V_{IN(min)}}} = 10 \text{ arms}
$$
\n(12)

The minimum input capacitance and ESR values for a given input voltage ripple specification, $V_{IN(ripple)}$, are shown in [Equation 13](#page-48-1) and [Equation 14.](#page-48-2) The input ripple is composed of a capacitive portion, $V_{RIPPLE(cap)}$, and a resistive portion, $V_{RIPPLE(esr)}$.

$$
C_{IN(min)} = \frac{I_{OUT(max)} \times V_{OUT}}{V_{RIPPLE(cap)} \times V_{IN(max)} \times f_{SW}} = 21.4 \ \mu F
$$
\n
$$
ESR_{CIN(max)} = \frac{V_{RIPPLE(ESR)}}{I_{OUT(max)} + (\frac{I_{RIPPLE}}{2})} = 3.4 \ m\Omega
$$
\n(14)

The value of a ceramic capacitor varies significantly over temperature and the amount of DC bias applied to the capacitor. The capacitance variations due to temperature can be minimized by selecting a dielectric material that is stable over temperature. X5R and X7R ceramic dielectrics are usually selected for power regulator capacitors because they have a high capacitance to volume ratio and are fairly stable over temperature. The input capacitor must also be selected with the DC bias taken into account. For this example design, a ceramic capacitor with at least a 25-V voltage rating is required to support the maximum input voltage. For this design, allow 0.1-V input ripple for $V_{RIPPLE(cap)}$, and 0.1-V input ripple for $V_{RIPPLE(esr)}$. Using [Equation 13](#page-48-1) and [Equation 14,](#page-48-2) the minimum input capacitance for this design is 21.4 µF, and the maximum ESR is 3.4 mΩ. For this example, four 22-μF, 25- V ceramic capacitors and one additional 100-μF, 25-V low-ESR polymer capacitors in parallel were selected for the power stage.

8.2.3.6 Bootstrap Capacitor Selection

A ceramic capacitor with a value of 0.1 μ F must be connected between the BOOT and SW pins for proper operation. TI recommends using a ceramic capacitor with X5R or better grade dielectric. Use a capacitor with a voltage rating of 25 V or higher.

8.2.3.7 BP Pin

Bypass the BP pin to DRGND with 4.7 µF of capacitance. In order for the regulator to function properly, it is important that these capacitors be localized to the TPS549B22 , with low-impedance return paths. See *[Layout](#page-53-2) [Guidelines](#page-53-2)* for more information.

8.2.3.8 R-C Snubber and VIN Pin High-Frequency Bypass

Though it is possible to operate the TPS549B22 within absolute maximum ratings without ringing reduction techniques, some designs may require external components to further reduce ringing levels. This example uses two approaches: a high frequency power stage bypass capacitor on the VIN pins, and an R-C snubber between the SW area and GND.

The high-frequency VIN bypass capacitor is a lossless ringing reduction technique which helps minimizes the outboard parasitic inductances in the power stage, which store energy during the low-side MOSFET on-time, and discharge once the high-side MOSFET is turned on. For this example two 2.2-nF, 25-V, 0603-sized highfrequency capacitors are used. The placement of these capacitors is critical to its effectiveness. Their ideal placement is shown in [Figure 53](#page-43-1).

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Additionally, an R-C snubber circuit is added to this example. To balance efficiency and spike levels, a 1-nF capacitor and a 1- Ω resistor are chosen. In this example a 0805-sized resistor is chosen, which is rated for 0.125 W, nearly twice the estimated power dissipation. See *[Snubber Circuits: Theory, Design and Application](http://www.ti.com/lit/pdf/SLUP100)* for more information about snubber circuits.

8.2.3.9 Optimize Reference Voltage (VSEL)

Optimize the reference voltage by choosing a value for R_{VSEL} . The TPS549B22 device is designed with a wide range of precision reference voltage support from 0.6 V to 1.2 V with an available step change of 50 mV. Program these reference voltages using the VSEL pin-strap configurations. See [Table 2](#page-19-0) for internal reference voltage selections. In addition to providing initial boot voltage value, use the VSEL pin to program hiccup and latch-off mode.

There are two ways to program the output voltage set point. If the output voltage set point is one of the 16 available reference and boot voltage options, no feedback resistors are required for output voltage programming. In the case where feedback resistors are not needed, connect the RSP pin to the positive sensing point of the load. Always connect the RSN pin to the load return sensing point.

In this design example, since the output voltage set point is 1 V, select R_{VSEL(LS)} of either 75 kΩ (latch off) or 68.1 kΩ (hiccup) as shown in [Table 3](#page-20-2). If the output voltage set point is NOT one of the 16 available reference or boot voltage options, feedback resistors are required for output voltage programming. Connect the RSP pin to the mid-point of the resistor divider. Always connect the RSN pin to the load return sensing point as shown in Figure 23 and Figure 24.

The general guideline to select boot and internal reference voltage is to select the reference voltage closest to the output voltage set point. In addition, because the RSP and RSN pins are extremely high-impedance input terminals of the true differential remote sense amplifier, use a feedback resistor divider with values much less than 100 kΩ.

8.2.3.10 MODE Pin Selection

MODE pin strap configuration is used to program control topology and internal soft-start timing selections. TPS549B22 supports both DCAP3 and DCAP operation. For general POL applications, TI strongly recommends configuring the control topology to be DCAP3 due to its simple to use and no external compensation features. In the rare instance where DCAP is needed, an RCC network across the output inductor is needed to generate sufficient ripple voltage on the RSP pin. In this design example, $R_{MODE(LS)}$ of 42.2 kΩ is selected for DCAP3 and soft start time of 1 ms.

8.2.3.11 ADDR Pin Selection

ADDR pin strap configuration is used to program device address and light load conduction mode selection. The TPS549B22 allows up to 16 different chip addresses for PMBus communication with the first 3 bits fixed as 001. The address selection process is defined by resistor divider ratio from BP pin to ADDR pin, and the address detection circuit will start to work only after the initial power up when V_{DD} has risen above its UVLO threshold.

For this application example, a device address of 16d is desired. We select the low side RADDR to be 0 Ω considering the SKIP operation and device address of 16d. Table 4 lists all combinations of the address selections. The 1% or better tolerance resistors with typical temperature coefficient of ±100 ppm/°C are recommended

8.2.3.12 Overcurrent Limit Design

The TPS549B22 device uses the ILIM pin to set the OCP level. Connect the ILIM pin to GND through the voltage setting resistor, R_{ILIM}. In order to provide both good accuracy and cost effective solution, this device supports temperature compensated MOSFET on-resistance $(R_{DS(on)})$ sensing. Also, this device performs both positive and negative inductor current limiting with the same magnitudes. Positive current limit is normally used to protect the inductor from saturation therefore causing damage to the high-side and low-side FETs. Negative current limit is used to protect the low-side FET during OVP discharge.

The inductor current is monitored by the voltage between PGND pin and SW pin during the OFF time. The ILIM pin has 1200 ppm/°C temperature slope to compensate the temperature dependency of the on-resistance. The PGND pin is used as the positive current sensing node.

TPS549B22 has cycle-by-cycle over-current limiting control. The inductor current is monitored during the OFF state and the controller maintains the OFF state during the period that the inductor current is larger than the overcurrent ILIM level. The voltage on the ILIM pin $(V_{I\sqcup M})$ sets the valley level of the inductor current. The range of value of the R_{ILIM} resistor is between 9.53 kΩ and 105 kΩ. The range of valley OCL is between 5 A and 50 A (typical). If the R_{ILIM} resistance is outside of the recommended range, OCL accuracy and function cannot be ensured. (see [Table 40](#page-50-0))

Use [Equation 15](#page-50-1) to relate the valley OCL to the R_{ILIM} resistance.

 $R_{ILIM} = 2.0664 \times OCL_{VALLEY} - 0.6036$

where

- R_{ILIM} is in kΩ
- OCL_{VALLEY} is in A (15)

In this design example, the desired valley OCL is 43 A, the calculated R_{ILIM} is 61.9 kΩ. Use [Equation 16](#page-50-2) to calculate the DC OCL to be 32.1 A.

 $OCL_{DC} = OCL_{VALLEY} + 0.5 \times I_{RIPPLE}$

where

- R_{ILIM} is in kΩ
- OCL_{DC} is in A (16)

In an overcurrent condition, the current to the load exceeds the inductor current and the output voltage falls. When the output voltage crosses the under-voltage fault threshold for at least 1 ms, the behavior of the device depends on the VSEL pin strap setting. If hiccup mode is selected, the device restarts after a 16-ms delay (1-ms soft-start option). If the overcurrent condition persists, the OC hiccup behavior repeats. During latch-off mode operation the device shuts down until the EN pin is toggled or VDD pin is power cycled.

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	Fusion Digital Power Designer Version 7.0.11.3 [2017-05-18]							
		Scanning USB Adapter #1 for devices Found TPS549B22 at address 31d (1 device found)						
	(Fusion Digital Power Designer - TPS549C20 @ PHDes Address 26d (1Ah) - Texas Instruments							
File Device Tools Help								TP5549C20 @ 26d (1Ah) - Rel #1
	All Config							
/William Bardwick	Command		Code Value/Edit	Hex/Edit	Command	Cade	Value/Edit	Hex/Edit
Auto wite on rail or	Y Configuration				V Status			
	MFR 01 (PG000 DLY) MFR 02	0 ₂ 01	PGD:102. CM: T:u	0x12 0 ₀	STATUS BYTE STATUS CML	0x28	00000000 [54]	19400
State Config to NVM	MR.03	0:02 0:03	P5:625k	3x83	STATUS_IDUT	0x75 0x73	000000001 97 00000000 (v)	-10000 18/00
	MR 04				STATUS_VOUT			TWARD
Restore NVM Config	MFR_06	0 ² BIDS	OCAP3 V VDDJ/L	0x80 0x05	STATUS WORD	0:76 0.79	00000000 ~ Grtu. vi	Burnta
Chier Hestigot Noomi		0xD7	VTRKIN	DxSF	V HserParameters			
	MFR_07 MFR 33	0.51	Uxilit	0x00	MFR 00	0.00	exan	CxDO
	MFR 42		Uxil	0.00				
	MFR 44	0xFA 6.5C	0.0201 $ v $					
Group by Category		0<21		0x0201 0x0266				
	VOUT_COMMAND YOUT_MARGIN_HIGH	8:25	$1.199 \div v$ $1.199 - v$	0x0266				
	VOUT_MARGIN_LOW	$0 \leq 0$	1.199 C 0	3x0255				
	YOUT_MODE	02C	1974	H217				
	WRITE_PROTECT	0x10	$0x00 =$	0x00				
	V Manufacturer Info							
	LAPABLLIT	0 ₁₅	0x00 v	0<00				
	V On/Oli Configuration							
	OH OFF CONFIG	Config.	00/37 97	0x17				
	OPERATION	10x0	0x00	0x00				

Figure 54. VOUT Command Graphic User Interface

8.2.4 Application Curves

9 Power Supply Recommendations

This device is designed to operate from an input voltage supply between 1.5 V and 18 V. Ensure the supply is well regulated. Proper bypassing of input supplies and internal regulators is also critical for noise performance, as is the quality of the PCB layout and grounding scheme. See the recommendations in the *[Layout](#page-53-1)* section.

10 Layout

10.1 Layout Guidelines

Consider these layout guidelines before starting a layout work using TPS549B22.

- It is absolutely critical that all GND pins, including AGND (pin 30), DRGND (pin 29), and PGND (pins 13, 14, 15, 16, 17, 18, 19, and 20) are connected directly to the thermal pad underneath the device via traces or plane.
- Include as many thermal vias as possible to support a 25-A thermal operation. For example, a total of 35 thermal vias are used (outer diameter of 20 mil) in the TPS49B22EVM-847, which is available for purchase at www.ti.com.
- Placed the power components (including input/output capacitors, output inductor and TPS549B22 device) on one side of the PCB (solder side). Insert at least two inner layers (or planes) connected to the power ground, in order to shield and isolate the small signal traces from noisy power lines.
- Place the VIN pin decoupling capacitors as close as possible to the PVIN and PGND pins to minimize the input AC current loop. Place a high-frequency decoupling capacitor (with a value between 1 nF and 0.1 μ F) as close to the PVIN pin and PGND pin as the spacing rule allows. This placement helps suppress the switch node ringing.
- Place VDD and BP decoupling capacitors as close as possible to the device pins. Do not use PVIN plane connection for the VDD pin. Separate the VDD signal from the PVIN signal by using separate trace connections. Provide GND vias for each decoupling capacitor and make the loop as small as possible.
- Ensure that the PCB trace defined as switch node (which connects the SW pins and up-stream of the output inductor) are as short and wide as possible. In the TPS49B22EVM-847 design, the SW trace width is 200 mil. Use a separate via or trace to connect SW node to snubber and bootstrap capacitor. Do not combine these connections.
- Place all sensitive analog traces and components (including VOSNS, RSP, RSN, ILIM, MODE, VSEL and ADDR) far away from any high voltage switch node (itself and others), such as SW and BOOT to avoid noise coupling. In addition, place MODE, VSEL and ADDR programming resistors near the device pins.
- The RSP and RSN pins operate as inputs to a differential remote sense amplifier that operates with very high impedance. It is essential to route the RSP and RSN pins as a pair of diff-traces in Kelvin-sense fashion. Route them directly to either the load sense points $(+$ and $-)$ or the output bulk capacitors. The internal circuit uses the VOSNS pin for on-time adjustment. It is critical to tie the VOSNS pin directly tied to VOUT (load sense point) for accurate output voltage result.
- Pins 6, 7, and 26 are not connected in the 25-A TPS549B22 device, while pins 6, and 7 connect to SW and pins 26 connects to PVIN in the 40-A TPS549D22 device.

10.2 Layout Examples

Figure 63. EVM Inner Layer 1 Figure 64. EVM Inner Layer 2

[TPS549B22](http://www.ti.com/product/tps549b22?qgpn=tps549b22) SNVSAU8 –JUNE 2017 **www.ti.com**

Layout Examples (continued)

Figure 67. EVM Bottom Layer

10.3 Mounting and Thermal Profile Recommendation

Proper mounting technique adequately covers the exposed thermal tab with solder. Excessive heat during the reflow process can affect electrical performance. [Figure 68](#page-56-1) shows the recommended reflow oven thermal profile. Proper post-assembly cleaning is also critical to device performance. See

[QFN/SON PCB Attachment](http://www.ti.com/lit/pdf/SLUA271) for more information.

Time (s)

Figure 68. Recommended Reflow Oven Thermal Profile

	PARAMETER	MIN	TYP	MAX	UNIT			
RAMP UP AND RAMP DOWN								
$r_{\text{RAMP(up)}}$	Average ramp-up rate, $T_{S(max)}$ to T_P			3	$\mathrm{^{\circ}C/s}$			
$r_{\text{RAMP}(down)}$	Average ramp-down rate, T_P to $T_{S(max)}$			6	$\mathrm{^{\circ}C/s}$			
PRE-HEAT								
T_S	Pre-heat temperature	150		200	°C			
$t_{\rm S}$	Pre-heat time, $T_{S(min)}$ to $T_{S(max)}$	60		180	s			
REFLOW								
T_{L}	Liquids temperature		217		°C			
T_{P}	Peak temperature			260	°C			
' t _L	Time maintained above liquidus temperature, T ₁	60		150	s			
t _P	Time maintained within 5° C of peak temperature, T_P	20		40	s			
t_{25P}	Total time from 25° C to peak temperature, T_P			480	s			

11 Device and Documentation Support

11.1 Device Support

11.1.1 Development Support

11.1.1.1 Custom Design With WEBENCH® Tools

[Click here](https://webench.ti.com/wb5/WBTablet/PartDesigner/quickview.jsp?base_pn=TPS549B22&origin=ODS&litsection=device_support) to create a custom design using the TPS549B22 device with the WEBENCH® Power Designer.

- 1. Start by entering the input voltage (V_{IN}) , output voltage (V_{OUT}) , and output current (I_{OUT}) requirements.
- 2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
- 3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at [www.ti.com/WEBENCH.](http://www.ti.com/lsds/ti/analog/webench/overview.page?DCMP=sva_web_webdesigncntr_en&HQS=sva-web-webdesigncntr-vanity-lp-en)

11.2 Documentation Support

11.2.1 Related Documentation

For related documentation see the following: *[Snubber Circuits: Theory, Design and Application](http://www.ti.com/lit/pdf/SLUP100)*

11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.4 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of](http://www.ti.com/corp/docs/legal/termsofuse.shtml) [Use.](http://www.ti.com/corp/docs/legal/termsofuse.shtml)

[TI E2E™ Online Community](http://e2e.ti.com) *TI's Engineer-to-Engineer (E2E) Community.* Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

[Design Support](http://support.ti.com/) *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

11.5 Trademarks

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11.6 Electrostatic Discharge Caution

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

11.7 Glossary

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGE OUTLINE

DDA0008J PowerPAD™ SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
-
- 2. This drawing is subject to change without notice. 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side. 5. Reference JEDEC registration MS-012, variation BA.
-

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EXAMPLE BOARD LAYOUT

DDA0008J PowerPAD™ SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
-
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments liter
-
- 9. Size of metal pad may vary due to creepage requirement.

www.ti.com

EXAMPLE STENCIL DESIGN

DDA0008J PowerPAD™ SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE

NOTES: (continued)

10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

11. Board assembly site may have different recommendations for stencil design.

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www.ti.com 10-Dec-2020

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE OPTION ADDENDUM

TEXAS

TAPE AND REEL INFORMATION

STRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal **Device Package Type Package Drawing Pins SPQ Reel Diameter (mm) Reel Width W1 (mm) A0 (mm) B0 (mm) K0 (mm) P1 (mm) W (mm) Pin1 Quadrant** TPS549B22RVFR LQFN-CLIP RVF 40 2500 330.0 16.4 5.3 7.3 1.8 8.0 16.0 Q1 TPS549B22RVFT LQFN-CLIP RVF | 40 | 250 | 180.0 | 16.4 | 5.3 | 7.3 | 1.8 | 8.0 | 16.0 | Q1

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PACKAGE MATERIALS INFORMATION

www.ti.com 19-Jan-2023

*All dimensions are nominal

RVF 40

GENERIC PACKAGE VIEW

LQFN-CLIP - 1.52 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

RVF0040A LQFN-CLIP - 1.52 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.
- 4. Reference JEDEC registration MO-220.

EXAMPLE BOARD LAYOUT

RVF0040A LQFN-CLIP - 1.52 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

5. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

EXAMPLE STENCIL DESIGN

RVF0040A LQFN-CLIP - 1.52 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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